

# Appendix C

## The Representative Reaches

***Appendix C1: A4/1a+ Fair Stability Reach (Trail Creek)***

***Appendix C2: A4a+ Poor Stability Reach (Northfield Gulch)***

***Appendix C3: A4a+ Poor Stability South Reach (Trail Creek)***

***Appendix C4: A4a+ Poor Stability Downstream Reach (Trail Creek)***

***Appendix C5: B4 Fair Stability Reach (Trail Creek)***

***Appendix C6: C4 Fair Stability Reach (Trail Creek)***

***Appendix C7: C4 Poor Stability Reach (Trail Creek)***

***Appendix C8: D4a+ Poor Stability Reach (Trail Creek)***

***Appendix C9: E4 Good Stability HWD Reach (Trail Creek)***

***Appendix C10: F4 Fair Stability Reach (West Monument Creek)***

***Appendix C11: F4b Fair-Poor Stability Reach (Trail Creek)***

***Appendix C12: F4b Poor Stability Reach (Northfield Gulch)***

***Appendix C13: F4b Poor Stability Mainstem Reach (Trail Creek)***

***Appendix C14: F4b Poor Stability Trib. Reach (Trail Creek)***

***Appendix C15: G4 Poor Stability Reach (Trail Creek)***

## The Reference Reaches

***Appendix C16: A4a+ Reference Reach (Trail Creek)***

***Appendix C17: A4/2 Reference Reach (West Monument Ck)***

***Appendix C18: B4 Reference Reach (Trail Creek)***

***Appendix C19: B4/2c Reference Reach (West Monument Ck)***

***Appendix C20: C4 Reference Reach (Trout Creek)***

***Appendix C21: D4a Reference Reach (Northfield Gulch)***

***Appendix C22: E4 Reference Reach (Trail Creek)***



## The Representative Reaches

Representative reaches were delineated and studied as their morphology, hydraulics, stability and sediment supply typify conditions found in such reaches. Once basic relations were measured, predicted, quantified, and documented, the data was extrapolated to the same stream type and valley type in a similar condition as observed elsewhere. Detailed site investigations were performed on each representative reach that emulate the full range of the various stream types, valley types, and stability conditions that occur within the Waldo Canyon Fire burn area. Basic relations used in the characterization of each representative reach were then extrapolated and used to characterize the remainder of the burn area. Approximately 117 miles (about 50%) of the streams in the watersheds affected by Waldo Canyon Fire were traversed obtaining direct observations of stream types, streambank erosion rates, and associated stability. The remaining 50% of the reaches utilized extrapolated relations due to similar boundary conditions and controlling variables. Each reach and its attendant watershed were evaluated using the WRENSS water yield model to predict pre- and post-fire water yields. The FLOWSED and POWERSED models were applied to each representative reach to obtain both pre- and post-fire sediment yields due to changes in streamflow, sediment transport capacity, and bed stability. The sediment from streambank erosion, using the BANCS model, was also determined in addition to sediment transport competency using a revised Shields relation.

The data, analysis, and results of each representative reach are summarized in this Appendix and their individual locations are mapped in **Figure C-1** and **Figure C-2**. A summary for all representative reaches of their morphology, dimension, pattern, and profile can be observed in the main report in **Table 9**. The stability summary for all representative reaches is shown in **Table 10**, while the streambank erosion data from the BANCS model and the overall stability ratings and sediment supply potential are summarized in **Table 11**. The POWERSED model was run for each representative reach (other than A stream types) to determine sediment transport capacity and associated bed stability. The stability conversion using a numerical index obtained from **Worksheet 5-29** documents the category ratings assigned for each representative reach (**Table 8**). A review of each representative reach in the aforementioned tables gives insight into the various and disproportionate sediment yields and corresponding stability summaries. The following summaries provide the detailed documentation for each reach.

## The Reference Reaches

The following reference reach descriptions and summaries represent a range of stable stream types used for extrapolation to unstable reaches of the same potential stream type in the same valley type. Because these streams represent the stable morphology there is not a *departure* for these stream types as they are the stream type of choice for a given valley type. The locations of each reference reach are shown in **Figure C-1** and **Figure C-2**. For stream types that are bedrock-controlled, such as the A4/1a+ reference reach, stability ratings are not provided due to the obvious stable conditions for such stream types. Where the boundary conditions and controlling variables provide adjustment opportunities for the stream reach, stability ratings are documented using the worksheets from the WARSSS textbook (Rosgen, 2006/2009).

Also included with each reference reach is a photograph and description of the dimension, pattern, profile, and materials associated with the physical character of each reach. Typical surveyed cross-sections, longitudinal profiles, channel materials (pebble counts), stream classification data, hydraulics, and dimensionless relations of the reach morphology for extrapolation to other potential stable stream types are shown. Such detailed data associated with each reference reach is extrapolated by the use of scaling factors (normalization parameters for bankfull conditions) to establish dimensional relations for departure analysis and natural channel design.

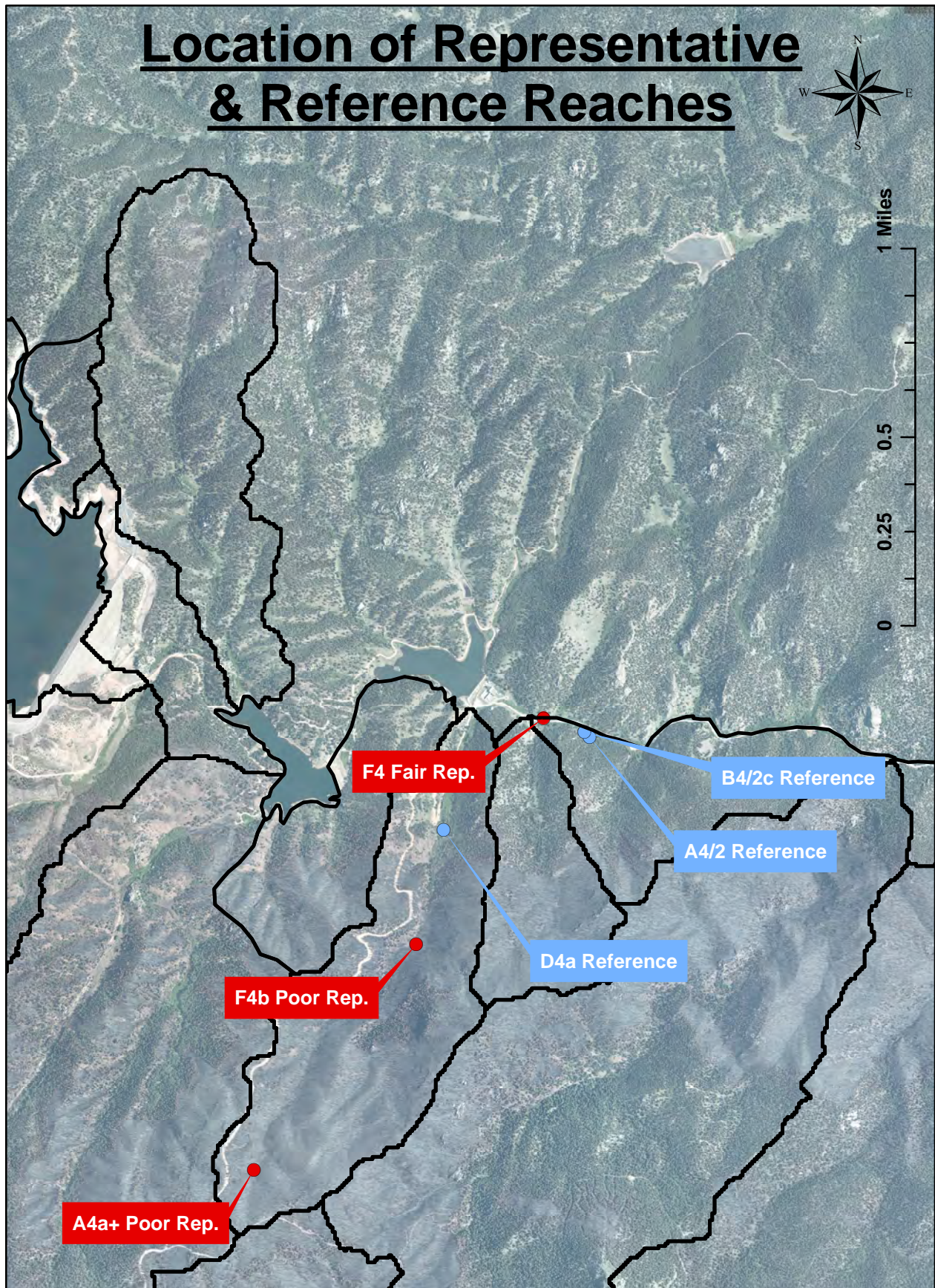


Figure C-1. Location of the Waldo Canyon Fire representative and reference reaches.

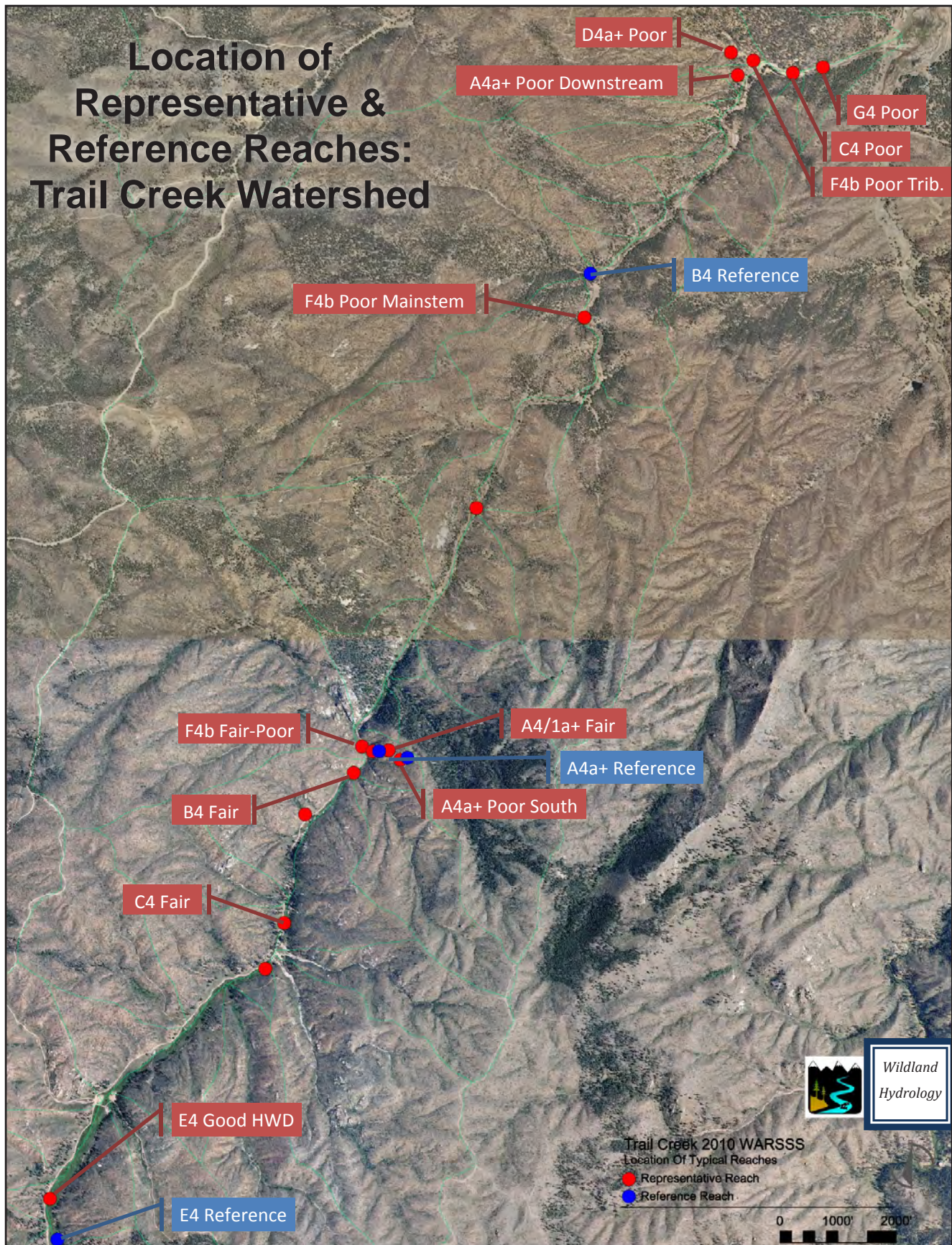


Figure C-2. Location of the reference and representative reaches within the Trail Creek Watershed.

# *Appendix C1*

## **A4/1a+ Stream Type** *Fair Stability Reach*





# Table of Contents

## *Appendix C1: A4/1a+ Fair Reach*

<b>Reach Location &amp; Overview.....</b>	<b>C1-2</b>
<b>Survey Summary.....</b>	<b>C1-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C1-6</b>
<b><i>Velocity, Classification &amp; Morphological Relations.....</i></b>	<b>C1-6</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b><i>Stability Indices.....</i></b>	<b>C1-10</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b><i>BANCS Model – Streambank Erosion.....</i></b>	<b>C1-20</b>
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b><i>FLOWSED Model – Total Annual Sediment Yield.....</i></b>	<b>C1-22</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b><i>Sediment Competence/Entrainment.....</i></b>	<b>C1-24</b>
Worksheet 5-22. Sediment competence calculations.	
<b><i>Channel Stability Ratings.....</i></b>	<b>C1-25</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b><i>Summary.....</i></b>	<b>C1-31</b>
Worksheet 5-32. Summary of stability condition categories.	

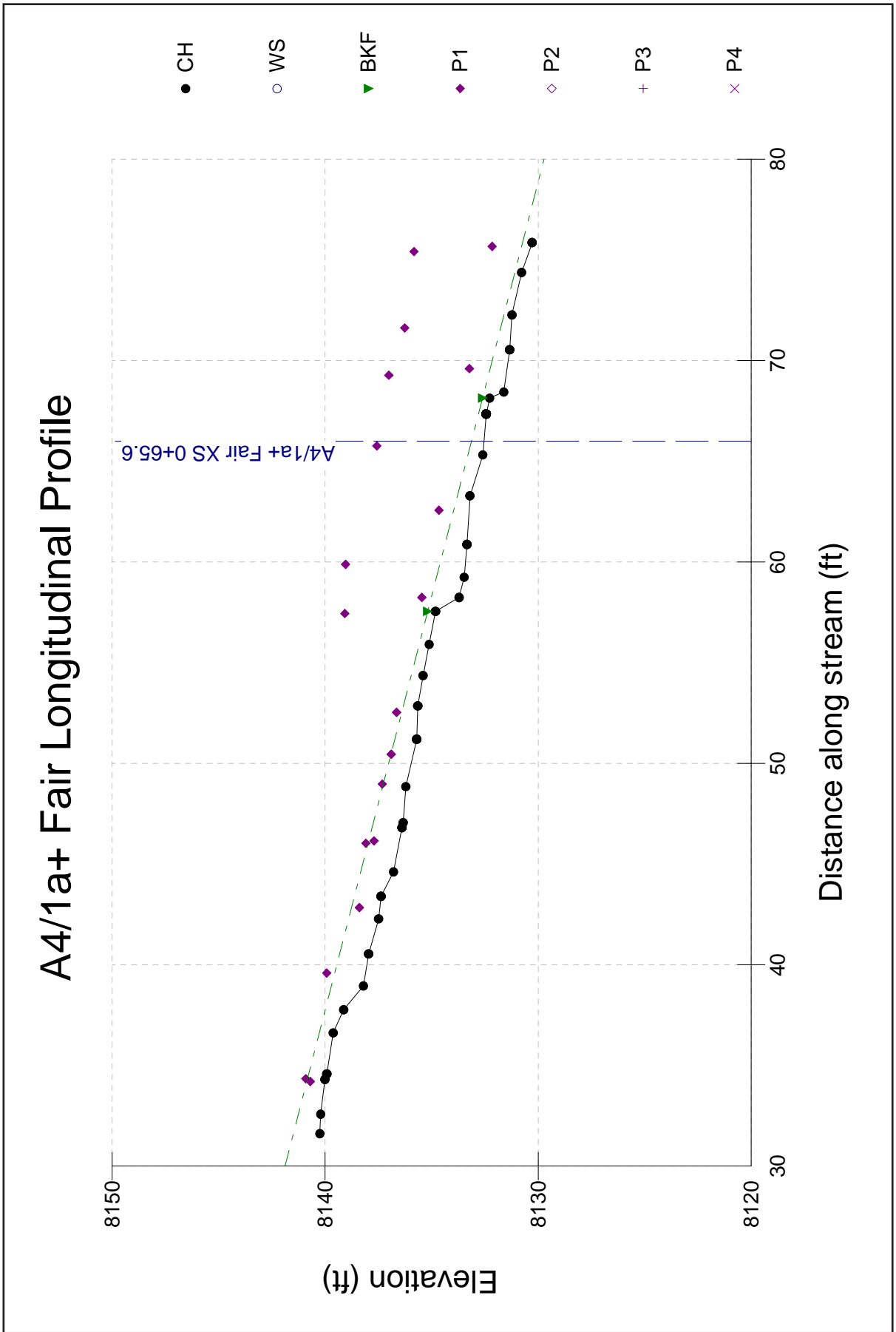
## A4/1a+ Fair Reach Location & Overview

The A4/1a+ Fair reach is located within the Trail Creek Watershed (**Figure C-2**). Although this is a bedrock-controlled, entrenched, gravel-bed channel, the stability rating is “Fair,” trending toward a higher sediment supply than the A4a+ reference reach. The streambank erosion rate is  $0.0055 \text{ tons/yr/ft}$  compared to  $0.0017 \text{ tons/yr/ft}$  for the reference condition. Although the streambank erosion rate of  $0.0055 \text{ tons/yr/ft}$  is not as high as other impaired reaches, this rate is larger than its reference condition and the overall condition is rated “Fair.” This rating indicates a potential increase in flow-related sediment based on increased post-fire streamflow peak flows. The stability indices document that the streambed is stable, typical of a bedrock-controlled channel, although the stream is moderately incised.

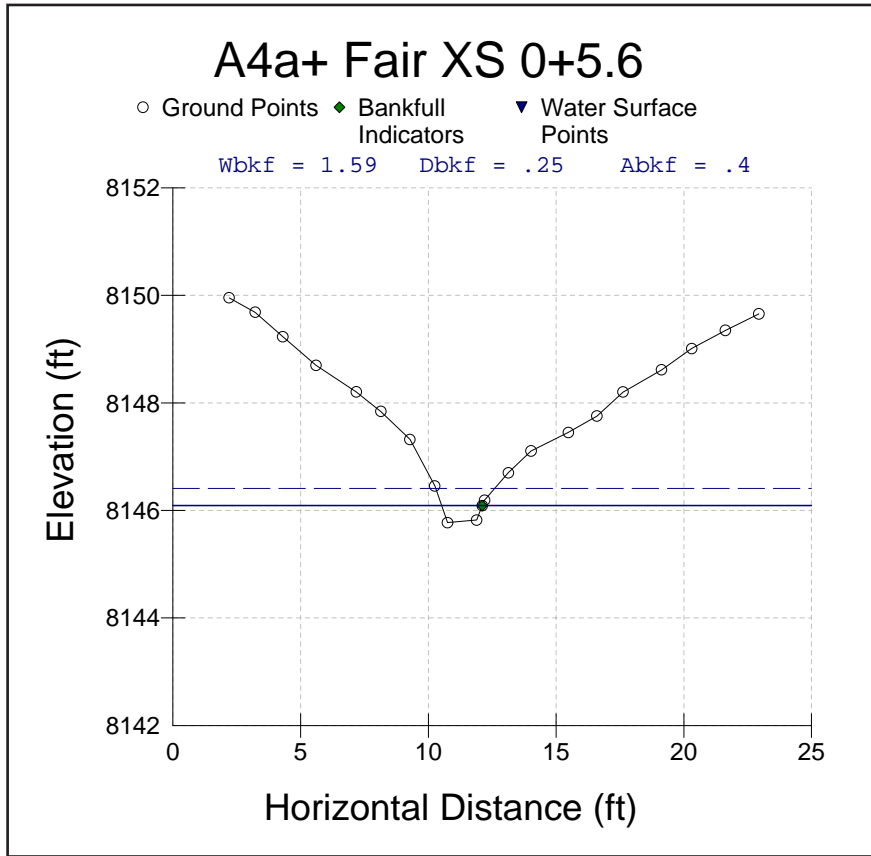
The photograph depicts the typical character of this ephemeral, 2<sup>nd</sup> order, representative A4/1a+ Fair stream type. The following graphs and summary worksheets provide the detail of the morphology, hydraulics, streambank erosion rates and stability condition.



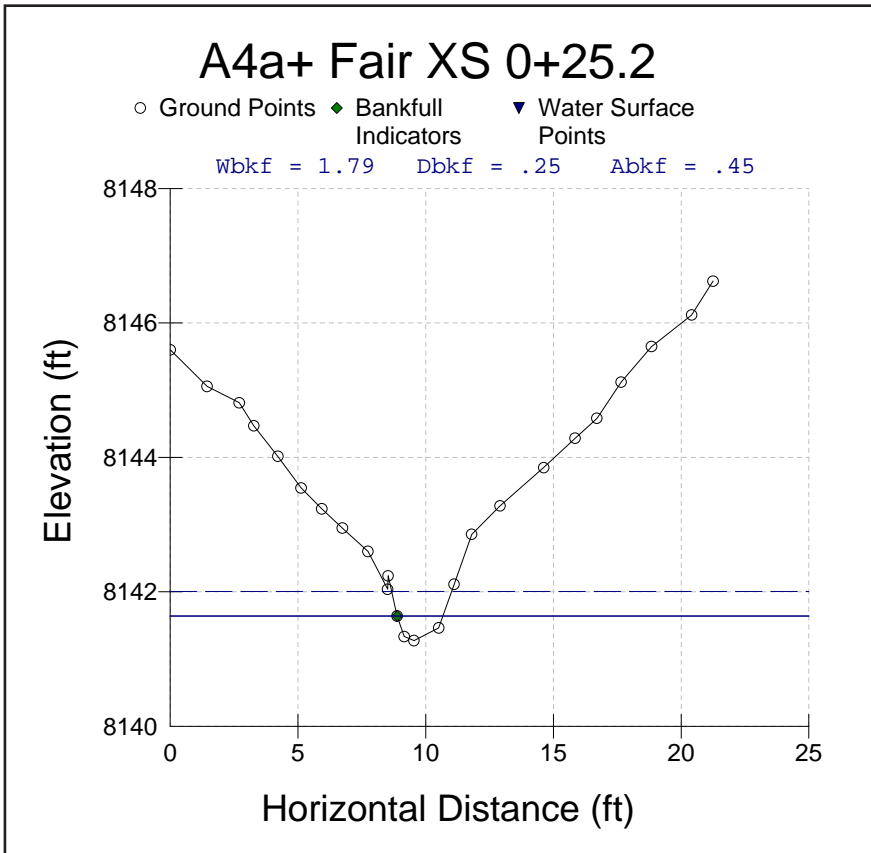
# Survey Summary



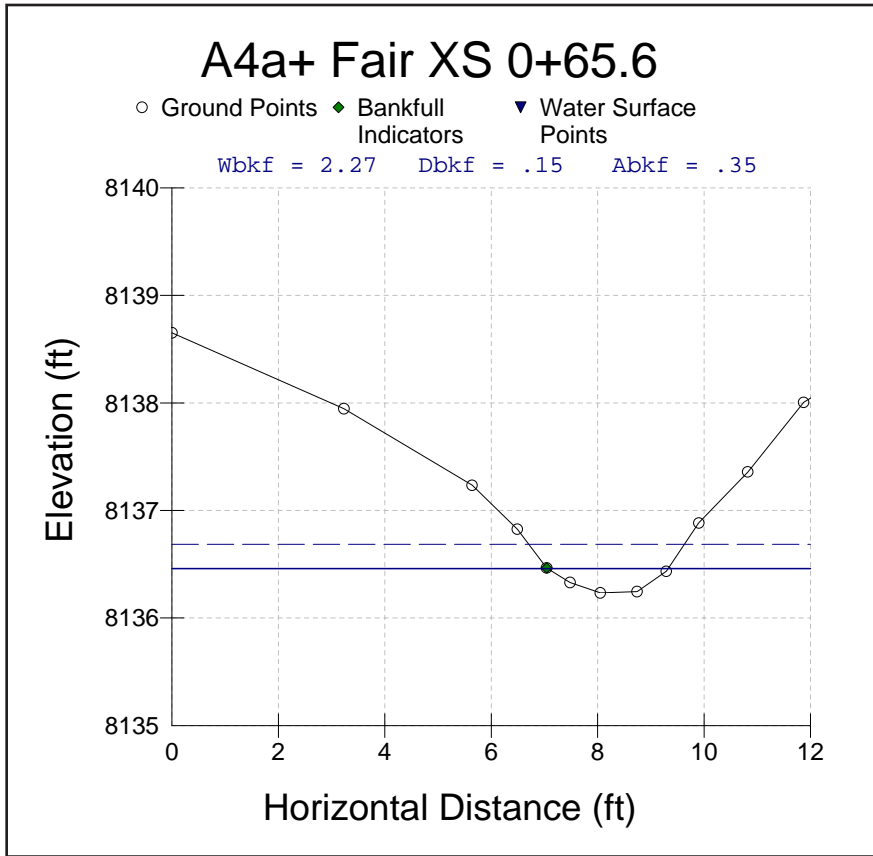
Longitudinal Profile (graph generated from RIVERMorph™)



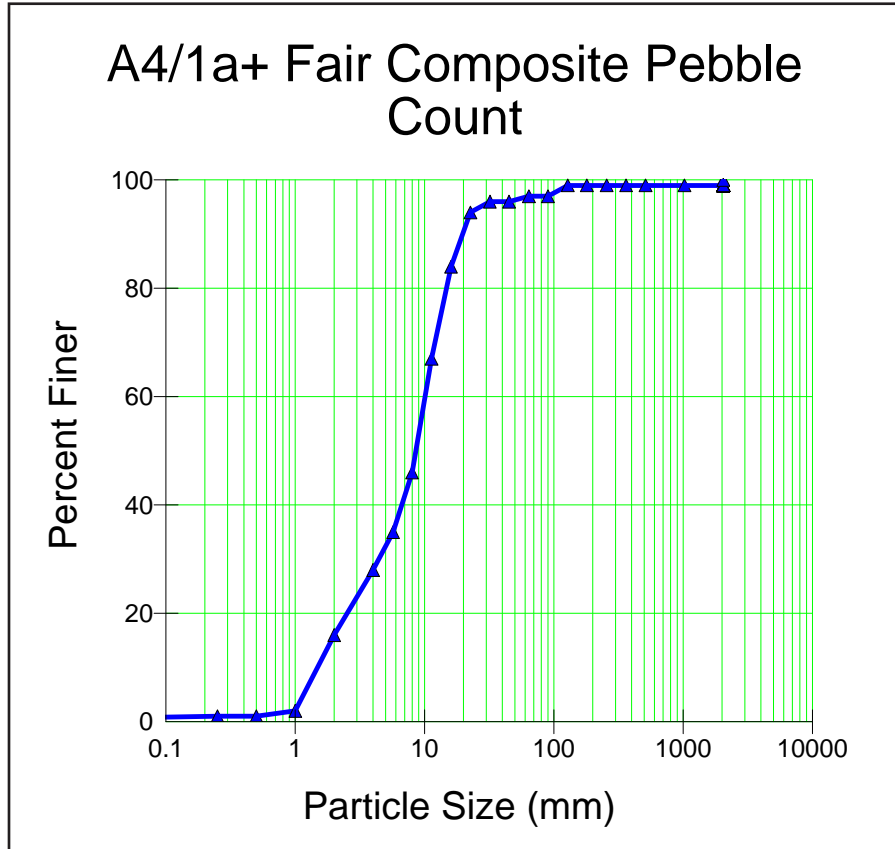
Cross-section 0+5.6 (graph generated from RIVERMorph™)



Representative Cross-section 0+25.2 (graph generated from RIVERMorph™)



Cross-section 0+65.6 (graph generated from RIVERMorph™)



Composite Pebble Count (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates						
Stream:	Trail Creek, A4/1a+ Fair Reach			Location:	XS 0+25.2, Pike N.F., Colorado	
Date:	9/2/2010	Stream Type:	A4/1a+	Valley Type:	I	
Observers:	Chavez, Kasun & Gallagher			HUC:	_ _ _ _ _	
INPUT VARIABLES			OUTPUT VARIABLES			
Bankfull Riffle Cross-Sectional AREA	0.45	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.25	$d_{bkf}$ (ft)	
Bankfull Riffle WIDTH	1.79	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim (2 * d_{bkf}) + W_{bkf}$	2.29	$W_p$ (ft)	
$D_{84}$ at Riffle	16.0	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.05	$D_{84}$ (ft)	
Bankfull SLOPE	0.2430	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	0.20	R (ft)	
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness $R(ft) / D_{84}(ft)$	3.74	$R / D_{84}$	
Drainage Area	0.0049	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	1.239	$u^*$ (ft/sec)	
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE	
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$			7.52	ft / sec	3.39	cfs
2. Roughness Coefficient: a) Manning's n from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.095$			2.61	ft / sec	1.18	cfs
2. Roughness Coefficient: b) Manning's n from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n =$ <input type="text"/>				ft / sec		cfs
2. Roughness Coefficient: c) Manning's n from Jarrett (USGS): $n = 0.39 * S^{0.38} * R^{-0.16}$ $n = 0.296$ <small>Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for Stream Types A1, A2, A3, B1, B2, B3, C2 &amp; E3</small>			0.84	ft / sec	0.38	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) <input type="text"/>				ft / sec		cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) <input type="text"/>				ft / sec		cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q =$ <input type="text"/> year $u = Q / A$				ft / sec		cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$				ft / sec		cfs
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation ( $R/D_{84}$ ) – Estimation Method 1						
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.						
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.						
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.						
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.						

**Worksheet 5-3.** Level II stream classification.

Stream: <b>Trail Creek, A4/1a+ Fair Reach</b>	
Basin:	Drainage Area: acres <b>0.0049</b> mi <sup>2</sup>
Location: <b>Pike National Forest, Colorado</b>	
Twp.&Rge:	Sec.&Qtr.:
Cross-Section Monuments (Lat./Long.): <b>XS 0+25.2</b> Date: <b>9/2/2010</b>	
Observers: <b>Chavez, Kasun &amp; Gallagher</b>	Valley Type: <b>I</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>1.79</b> ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A_{bkf} / W_{bkf}$ ).	<b>0.25</b> ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>0.45</b> ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>7.2</b> ft/ft
<b>Maximum DEPTH (<math>d_{max}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>0.37</b> ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkd}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>2.34</b> ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>1.31</b> ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the median or dominant diameter of channel materials, as sampled proportionately from the channel surface, between the bankfull stage and Thalweg elevations.	<b>8.63 mm over bedrock</b> mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.2430</b> ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope ( $S_{val} / S$ ).	<b>1.10</b>

<div style="border: 1px solid black; padding: 5px; display: inline-block;">Stream Type</div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: #e0f0ff;"><b>A4/1a+</b></div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;">See Classification Key (Figure 2-14)</div>
--	---	---

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, A4/1a+ Fair Reach</b>		Location: <b>Pike National Forest, Colorado</b>								
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/3/2010</b>		Valley Type: <b>I</b>		Stream Type: <b>A4/1a+</b>				
<b>River Reach Dimension Summary Data.....1</b>										
<b>Riffle Dimensions*</b> , **, ***	<b>Riffle Dimensions**</b> , ***, ***		<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Width ( $W_{bkt}$ )	<b>1.88</b>	<b>1.59</b>	<b>2.27</b>	ft	Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	<b>0.40</b>	<b>0.35</b>	<b>0.45</b>	
	Mean Riffle Depth ( $d_{bkt}$ )	<b>0.22</b>	<b>0.15</b>	<b>0.25</b>	ft	Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	<b>9.55</b>	<b>6.36</b>	<b>15.13</b>	
	Maximum Riffle Depth ( $d_{max}$ )	<b>0.31</b>	<b>0.23</b>	<b>0.37</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>1.43</b>	<b>1.28</b>	<b>1.53</b>	
	Width of Flood-Prone Area ( $W_{fpa}$ )	<b>2.53</b>	<b>2.31</b>	<b>2.93</b>	ft	Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )	<b>1.35</b>	<b>1.29</b>	<b>1.45</b>	
	Riffle Inner Berm Width ( $W_{ib}$ )				ft	Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )				
	Riffle Inner Berm Depth ( $d_{ib}$ )				ft	Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )				
	Riffle Inner Berm Area ( $A_{ib}$ )				ft <sup>2</sup>	Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )				
	Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )									
<b>Pool Dimensions*</b> , **, ***	<b>Pool Dimensions**</b> , ***, ***		<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Pool Dimensions &amp; Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Pool Width ( $W_{bkfp}$ )				ft	Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )				
	Mean Pool Depth ( $d_{bkfp}$ )				ft	Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )				
	Pool Cross-Sectional Area ( $A_{bkfp}$ )				ft	Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )				
	Maximum Pool Depth ( $d_{maxp}$ )				ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
	Pool Inner Berm Width ( $W_{ibp}$ )				ft	Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )				
	Pool Inner Berm Depth ( $d_{ibp}$ )				ft	Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )				
	Pool Inner Berm Area ( $A_{ibp}$ )				ft <sup>2</sup>	Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )				
	Point Bar Slope ( $S_{pb}$ )				ft/ft	Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )				
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Run Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Run Width ( $W_{bkfr}$ )				ft	Run Width to Riffle Width ( $W_{bkfr} / W_{bkt}$ )				
	Mean Run Depth ( $d_{bkfr}$ )				ft	Mean Run Depth to Mean Riffle Depth ( $d_{bkfr} / d_{bkt}$ )				
	Run Cross-Sectional Area ( $A_{bkfr}$ )				ft	Run Area to Riffle Area ( $A_{bkfr} / A_{bkt}$ )				
	Maximum Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )				
Run Width/Depth Ratio ( $W_{bkfr} / d_{bkfr}$ )				ft						
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Glide Dimensions &amp; Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Glide Width ( $W_{bkfg}$ )				ft	Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )				
	Mean Glide Depth ( $d_{bkfg}$ )				ft	Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )				
	Glide Cross-Sectional Area ( $A_{bkfg}$ )				ft	Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )				
	Maximum Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )				
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )				ft/ft	Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )				
	Glide Inner Berm Width ( $W_{ibg}$ )				ft	Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )				
	Glide Inner Berm Depth ( $d_{ibg}$ )				ft	Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )				
Glide Inner Berm Area ( $A_{ibg}$ )				ft <sup>2</sup>	Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )					
<b>Step**</b>	<b>Step Dimensions**</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Step Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Step Width ( $W_{bkfs}$ )				ft	Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )				
	Mean Step Depth ( $d_{bkfs}$ )				ft	Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )				
	Step Cross-Sectional Area ( $A_{bkfs}$ )				ft	Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )				
	Maximum Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )				
Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )										



**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, A4/1a+ Fair Reach</b>		Location: <b>Pike National Forest, Colorado</b>										
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/3/2010</b>		Valley Type: <b>I</b>		Stream Type: <b>A4/1a+</b>						
<b>River Reach Summary Data.....2</b>												
<b>Hydraulics</b>	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )		<b>0.84</b>		ft/sec		Estimation Method	<b>Manning's n from Jarrett</b>				
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )		<b>0.38</b>		cfs		Drainage Area	<b>0.0049</b> mi <sup>2</sup>				
<b>Channel Pattern</b>	<b>Geometry</b>			<b>Dimensionless Geometry Ratios</b>								
	Linear Wavelength ( $\lambda$ )	Mean	Min	Max	ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )	Mean	Min	Max			
	Stream Meander Length ( $L_m$ )				ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )						
	Radius of Curvature ( $R_c$ )				ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )						
	Belt Width ( $W_{bit}$ )	<b>2.8</b>			ft	Meander Width Ratio ( $W_{bit} / W_{bkt}$ )	<b>1.50</b>					
	Arc Length ( $L_a$ )				ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )						
	Riffle Length ( $L_r$ )				ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )						
	Individual Pool Length ( $L_p$ )				ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )						
Pool to Pool Spacing ( $P_s$ )				ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )							
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )	<b>0.2673</b>	ft/ft	Average Water Surface Slope (S)	<b>0.2430</b>	ft/ft	Sinuosity ( $S_{val} / S$ )	<b>1.10</b>				
	Stream Length (SL)		ft	Valley Length (VL)		ft	Sinuosity (SL / VL)					
	Low Bank Height (LBH)	start: <b>1.30</b>	ft	Max Bankfull Depth ( $d_{max}$ )	start: <b>0.84</b>	ft	Bank-Height Ratio (BHR) ( $LBH / d_{max}$ )	start: <b>1.5</b>				
		end:	ft		end:	ft		end:				
	<b>Facet Slopes</b>			<b>Dimensionless Facet Slope Ratios</b>								
	Riffle Slope ( $S_{rif}$ )	Mean	Min	Max	ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rif} / S$ )	Mean	Min	Max			
	Run Slope ( $S_{run}$ )				ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )						
	Pool Slope ( $S_p$ )				ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )						
	Glide Slope ( $S_g$ )				ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )						
	Step Slope ( $S_s$ )				ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )						
	<b>Max Depths<sup>a</sup></b>			<b>Dimensionless Depth Ratios</b>								
	Max Riffle Depth ( $d_{max}$ )	Mean	Min	Max	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	Mean	Min	Max			
	Max Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )						
	Max Pool Depth ( $d_{maxp}$ )				ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )						
	Max Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )						
Max Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )							
<b>Channel Materials</b>	<b>Reach<sup>b</sup></b>			<b>Riffle<sup>c</sup></b>			<b>Bar</b>			<b>Protrusion Height<sup>d</sup></b>		
	% Silt/Clay	<b>0</b>			$D_{16}$	<b>2</b>						mm
	% Sand	<b>16</b>			$D_{35}$	<b>6</b>						mm
	% Gravel	<b>81</b>			$D_{50}$	<b>9</b>						mm
	% Cobble	<b>2</b>			$D_{84}$	<b>16</b>						mm
	% Boulder	<b>0</b>			$D_{95}$	<b>27</b>						mm
	% Bedrock	<b>1</b>			$D_{100}$	<b>Bedrock</b>						mm

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.  
<sup>b</sup> Composite sample of riffles and pools within the designated reach.      <sup>c</sup> Active bed of a riffle.      <sup>d</sup> Height of roughness feature above bed.

## Stability Indices

**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation					
Stream: <b>Trail Creek, A4/1a+ Fair Reach</b>		Location: <b>Pike National Forest, Colorado</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>	Reference reach: <input type="checkbox"/>	Disturbed (impacted reach): <input checked="" type="checkbox"/>	Date: <b>9/2/2010</b>		
Existing species composition: <b>Aspen, Rose, Chokecherry, Ribes, Sedge, Grasses, Raspberries, Mullen</b>		Potential species composition: <b>More Mature Aspen, Chokecherry, Raspberry, Rose, Ponderosa Pine</b>			
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition
<b>1. Overstory</b>	Canopy layer	1%	1%	Aspen	100%
					100%
<b>2. Understory</b>	Shrub layer		39%	Rose Chokecherry Raspberry	20% 10% 70%
					100%
<b>3. Ground level</b>	Herbaceous		39%	Forbs Bunchgrass Toadflax Thistle	
	Leaf or needle litter		1%	<b>Remarks:</b> Condition, vigor and/or usage of existing reach: <b>Noxious weeds out of riparian but within potential</b>	100%
	Bare ground		20%		
			<b>Column total = 100%</b>		


\*Based on crown closure.

\*\*Based on basal area to surface area.

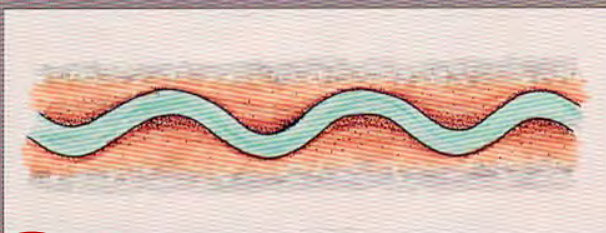




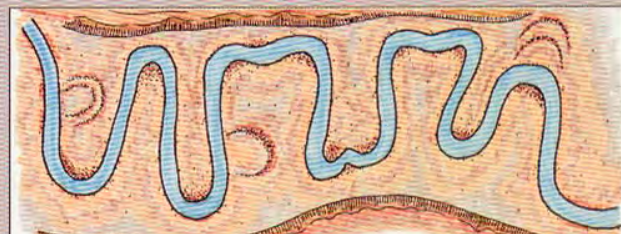
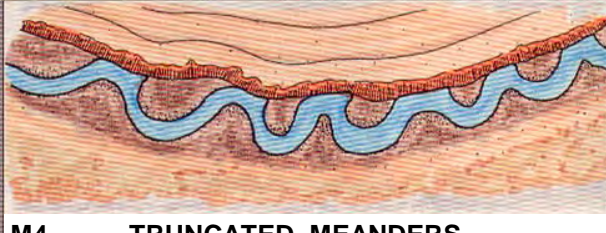
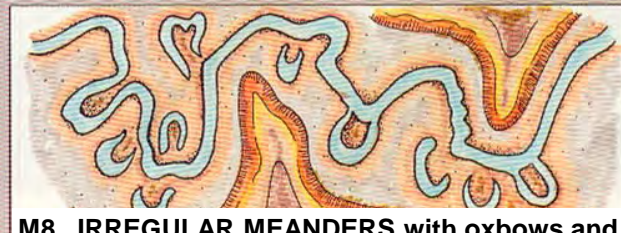
**Worksheet 5-7.** Flow regime.

<b>FLOW REGIME</b>								
Stream: <b>Trail Creek, A4/1a+ Fair Reach</b>			Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>Chavez, Kasun &amp; Gallagher</b>						Date: <b>9/2/2010</b>		
<b>List ALL COMBINATIONS that APPLY.....</b>	<b>E1</b>	<b>E2</b>	<b>E8</b>					
<b>General Category</b>								
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation							
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
<b>P</b>	Perennial stream channels: Surface water persists yearlong.							
<b>Specific Category</b>								
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
<b>4</b>	Streamflow regulated by glacial melt.							
<b>5</b>	Ice flows/ice torrents from ice dam breaches.							
<b>6</b>	Alternating flow/backwater due to tidal influence.							
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.							
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
<b>9</b>	Rain-on-snow generated runoff.							

**Worksheet 5-8.** Stream order & stream size.

<b>Stream Size and Order</b>			
Stream:	<b>Trail Creek, A4/1a+ Fair Reach</b>		
Location:	<b>Pike National Forest, Colorado</b>		
Observers:	<b>Chavez, Kasun &amp; Gallagher</b>		
Date:	<b>9/2/2010</b>		
<b>Stream Size Category and Order</b> 			<b>S-2(2)</b>
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0 - 305	<1	<input type="checkbox"/>
<b>S-2</b>	<b>0.3 - 1.5</b>	<b>1 - 5</b>	<input checked="" type="checkbox"/>
S-3	1.5 - 4.6	5 - 15	<input type="checkbox"/>
S-4	4.6 - 9	15 - 30	<input type="checkbox"/>
S-5	9 - 15	30 - 50	<input type="checkbox"/>
S-6	15 - 22.8	50 - 75	<input type="checkbox"/>
S-7	22.8 - 30.5	75 - 100	<input type="checkbox"/>
S-8	30.5 - 46	100 - 150	<input type="checkbox"/>
S-9	46 - 76	150 - 250	<input type="checkbox"/>
S-10	76 - 107	250 - 350	<input type="checkbox"/>
S-11	107 - 150	350 - 500	<input type="checkbox"/>
S-12	150 - 305	500 - 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
<b>Stream Order</b>			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			

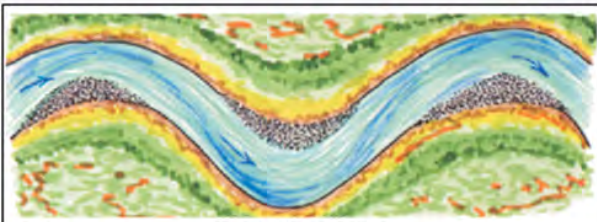

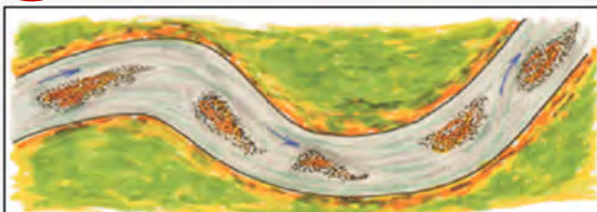

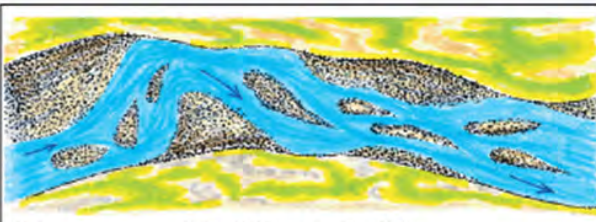
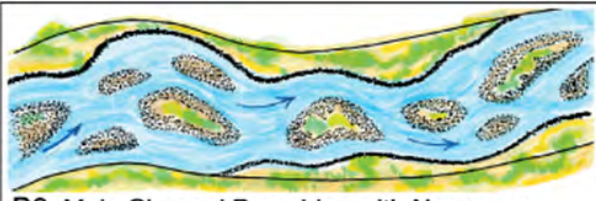
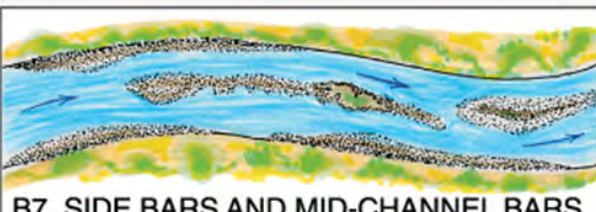

Worksheet 5-9. Meander patterns.

<b>Meander Patterns</b>					
Stream: <b>Trail Creek, A4/1a+ Fair Reach</b>	Location: <b>Pike National Forest, CO</b>				
Observers: <b>Chavez, Kasun &amp; Gallagher</b>	Date: <b>9/2/2010</b>				
List ALL CATEGORIES that APPLY	<b>M1</b>				
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>					
 <b>M1</b> <b>REGULAR MEANDERS</b>	 <b>M5</b> <b>UNCONFINED MEANDER SCROLLS</b>				
 <b>M2</b> <b>TORTUOUS MEANDERS</b>	 <b>M6</b> <b>CONFINED MEANDER SCROLLS</b>				
 <b>M3</b> <b>IRREGULAR MEANDERS</b>	 <b>M7</b> <b>DISTORTED MEANDER LOOPS</b>				
 <b>M4</b> <b>TRUNCATED MEANDERS</b>	 <b>M8</b> <b>IRREGULAR MEANDERS with oxbows and</b>				

**Worksheet 5-10.** Depositional patterns.

<b>Depositional Patterns</b>					
Stream:	Trail Creek, A4/1a+ Fair Reach	Location:	Pike National Forest, Colorado		
Observers:	Chavez, Kasun & Gallagher	Date:	9/2/2010		
List ALL CATEGORIES that APPLY	B2				

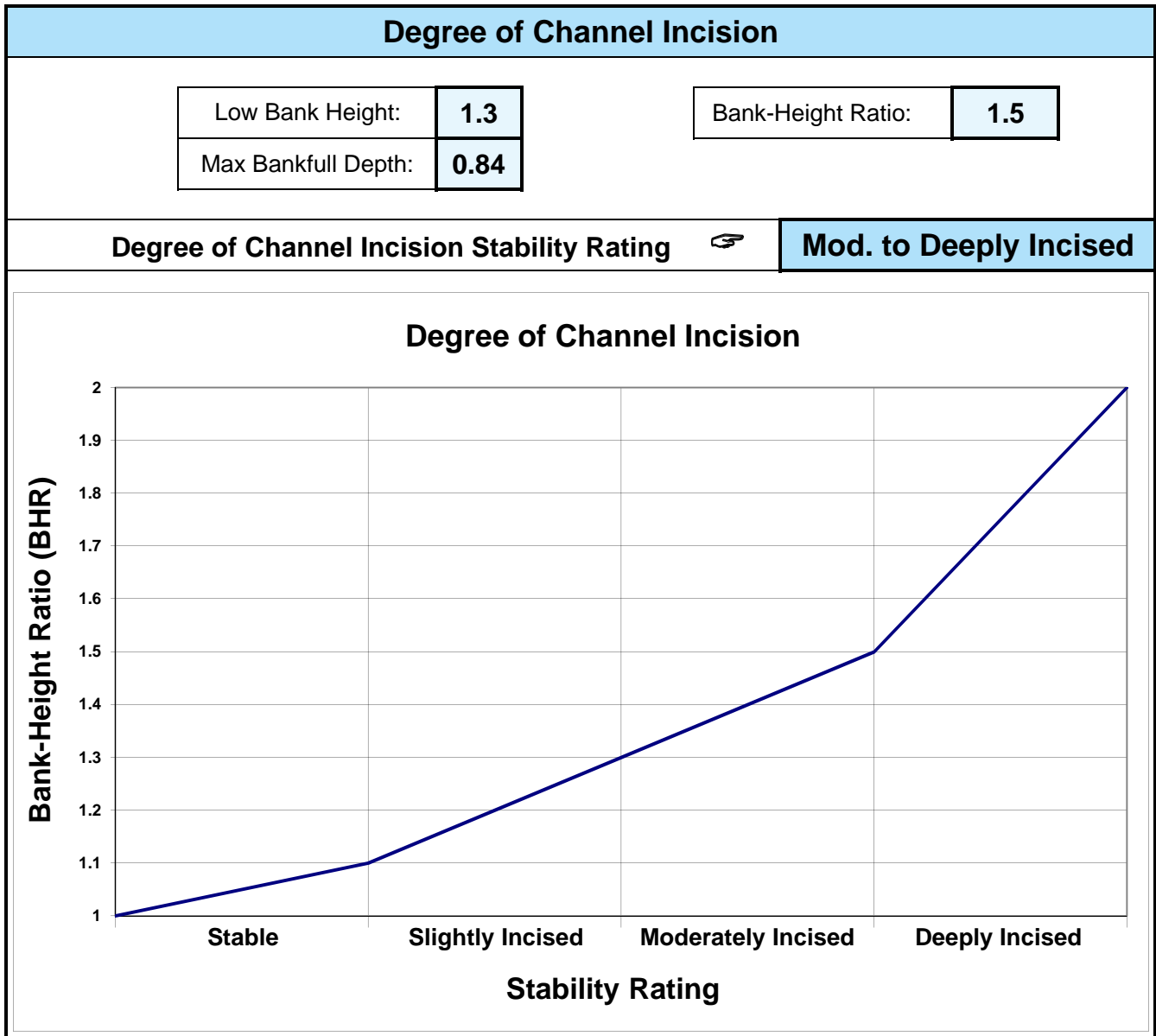
*Various Depositional Features modified from Galay et al. (1973)*

<div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B1</b> POINT BARS</p> </div> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B2</b> POINT BARS with Few MID-CHANNEL BARS</p> </div> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B3</b> NUMEROUS MID-CHANNEL BARS</p> </div> <div style="border: 1px solid black; padding: 5px;">  <p><b>B4</b> SIDE BARS</p> </div>	<div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B5</b> DIAGONAL BARS</p> </div> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B6</b> Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</p> </div> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B7</b> SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</p> </div> <div style="border: 1px solid black; padding: 5px;">  <p><b>B8</b> DELTA BARS</p> </div>
--	--

## Worksheet 5-11. Channel blockages.

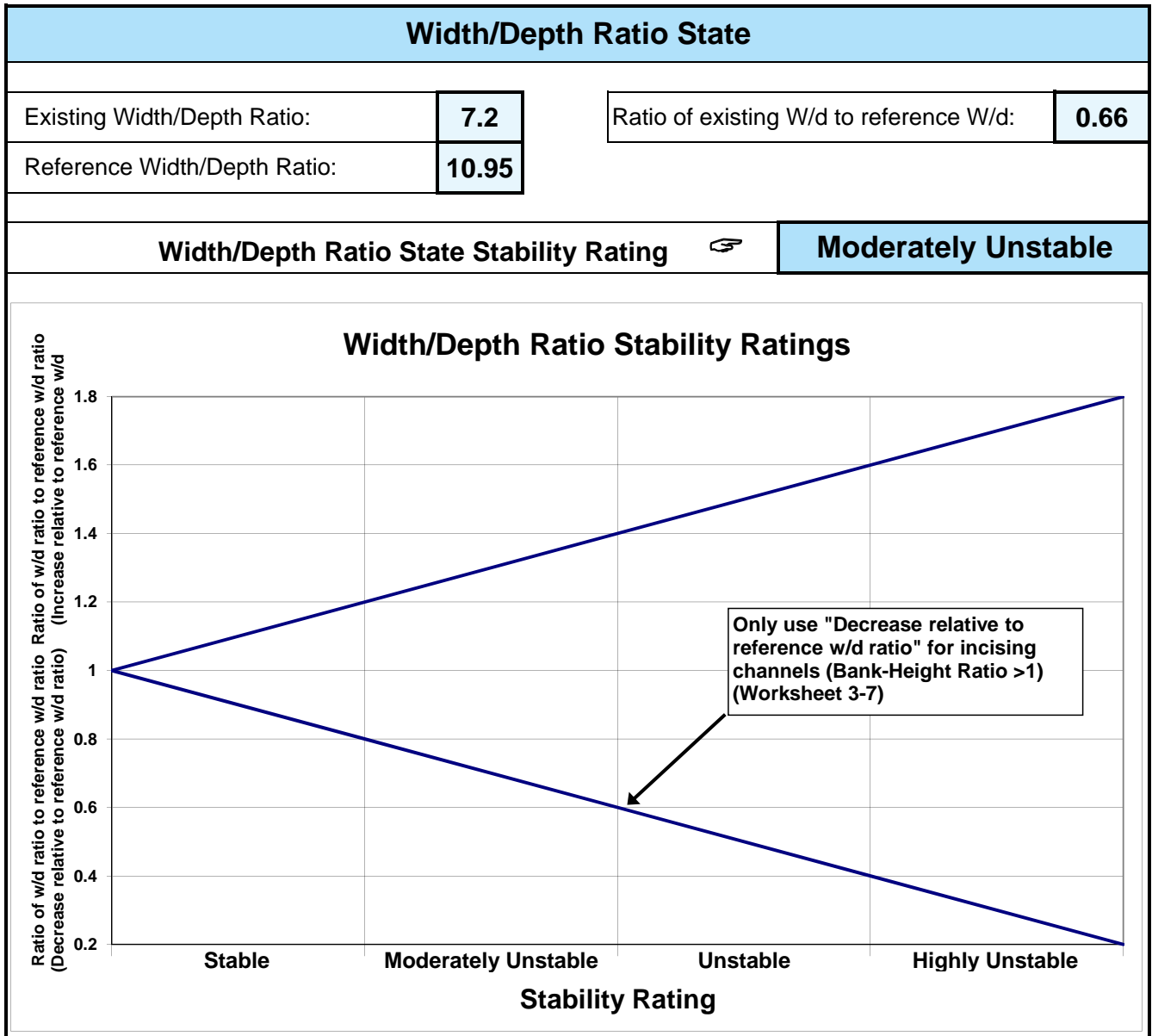
Channel Blockages		
Stream: <b>Trail Creek, A4/1a+ Fair Reach</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/2/2010</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input checked="" type="checkbox"/>
<b>D4</b> Numerous	<del>Significant build up of medium- to large sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.</del>	<input type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

**Worksheet 5-12.** Degree of channel incision.





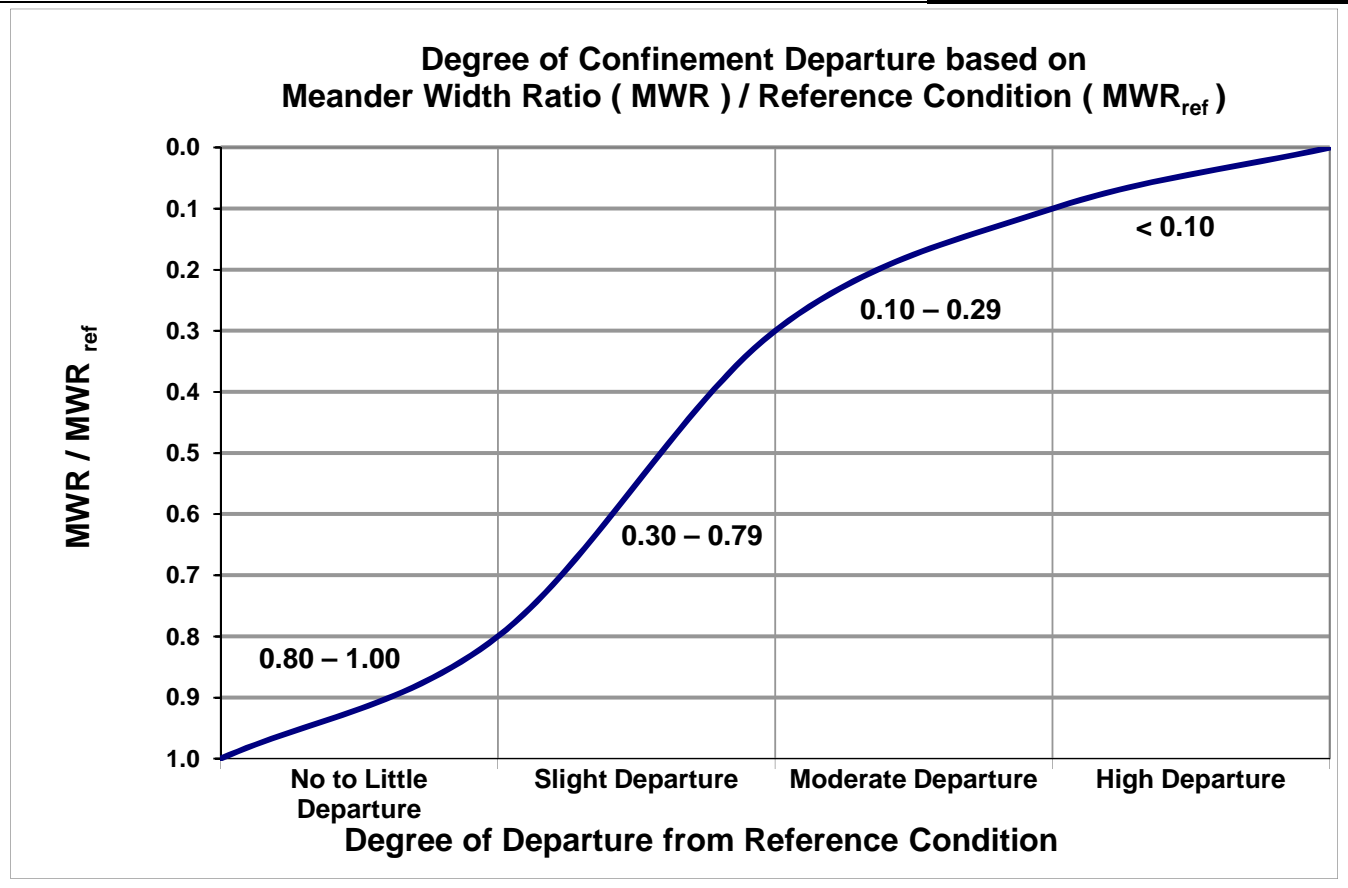
Worksheet 5-13. Width/depth ratio state.



**Worksheet 5-14.** Degree of channel confinement (lateral containment).

Degree of Confinement			
Existing Meander Width Ratio (MWR):	<b>1.5</b>	Ratio of MWR to $MWR_{ref}$ :	<b>0.99</b>
Reference Meander Width Ratio ( $MWR_{ref}$ ):	<b>1.52</b>		

Degree of Confinement Stability Rating	<b>No Departure</b>
--	---------------------



Worksheet 5-15. Pfankuch channel stability rating.

Stream: Trail Creek, A4/1a+ Fair Reach		Location: Pike National Forest		Valley Type: I		Observers: Chavez, Kasun & Gallagher		Date: 9/2/2010																
Loca- tion	Key	Excellent			Good			Fair			Poor													
		Description	Rating		Description	Rating		Description	Rating		Description	Rating												
Upper banks	1	Landform slope	Bank slope gradient <30%.	2	Bank slope gradient 30-40%.	4	Bank slope gradient 40-60%.	6	Bank slope gradient > 60%.	8														
	2	Mass erosion	No evidence of past or future mass erosion.	3	Infrequent. Mostly healed over. Low future potential.	7	Frequent or large, causing sediment nearly yearlong.	9	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.	12														
	3	Debris jam potential	Essentially absent from immediate channel area.	2	Present, but mostly small twigs and limbs.	4	Moderate to heavy amounts, mostly larger sizes.	6	Moderate to heavy amounts, predominantly larger sizes.	8														
	4	Vegetative bank protection	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	3	70-90% density. Fewer species or less vigor suggest less dense or deep root mass.	6	50-70% density. Lower vigor and fewer species from a shallow, discontinuous root mass.	9	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.	12														
Lower banks	5	Channel capacity	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0-1.1.	1	Width/depth ratio departure from reference width/depth ratio = 1.0-1.2. Bank-Height Ratio (BHR) = 1.0-1.1.	2	Width/depth ratio departure from reference width/depth ratio = 1.2-1.4. Bank-Height Ratio (BHR) = 1.1-1.3.	3	Bankfull stage is not contained: over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.	4														
	6	Bank rock content	> 65% with large angular boulders. 12'+ common.	2	40-65%. Mostly boulders and small cobbles 6-12".	4	20-40%. Most in the 3-6" diameter class.	6	<20% rock fragments of gravel sizes, 1-3" or less.	7														
	7	Obstructions to flow	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	2	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	3	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	6	Frequent obstructions and deflectors cause bank erosion yearlong. Sediment traps full, channel migration occurring.	8														
	8	Cutting	Little or none. Infrequent raw banks <6".	4	Some, intermittently at outcrops and constrictions. Raw banks may be up to 12".	5	Significant. Cuts 12-24" high. Root mat overhangs and sloughing evident.	12	Almost continuous cuts, some over 24" high. Failure of overhangs frequent.	16														
	9	Deposition	Little or no enlargement of channel or point bars.	4	Some new bar increase, mostly from coarse gravel.	6	Moderate deposition of new gravel and coarse sand on old and some new bars.	12	Extensive deposit of predominantly fine particles. Accelerated bar development.	16														
	10	Rock angularity	Sharp edges and corners. Plane surfaces rough.	1	Rounded corners and edges. Surfaces smooth and flat.	2	Corners and edges well rounded in 2 dimensions.	3	Well rounded in all dimensions, surfaces smooth.	4														
	11	Brightness	Surfaces dull, dark or stained. Generally not bright.	1	Mostly dull, but may have <35% bright surfaces.	2	Mixture dull and bright, i.e., 35-65% mixture range.	3	Predominantly bright, > 65% exposed or scored surfaces.	4														
	12	Consolidation of particles	Assorted sizes tightly packed or overlapping.	2	Moderately packed with some overlapping.	4	Mostly loose assortment with no apparent overlap.	6	No packing evident. Loose assortment, easily moved.	8														
	13	Bottom size distribution	No size change evident. Stable material 80-100%.	4	Distribution shift light. Stable material 50-80%.	8	Moderate change in sizes. Stable materials 20-50%.	12	Marked distribution change. Stable materials 0-20%.	14														
14	Scouring and deposition	<5% of bottom affected by scour or deposition.	6	5-30% affected. Scour at constrictions and where grades steepen. Some deposition in pools.	12	30-50% affected. Depositions and scour at obstructions, constrictions and bends. Some filling of pools.	18	More than 50% of the bottom in a state of flux or change nearly yearlong.	24															
15	Aquatic vegetation	Abundant growth moss-like, dark green perennial. In swift water too.	1	Common. Algae forms in low velocity and pool areas. Moss here too.	2	Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick.	3	Perennial types scarce or absent. Yellow-green, short-term bloom may be present.	4															
<b>Excellent total = 0</b>				<b>Good total = 31</b>				<b>Fair total = 33</b>				<b>Poor total = 33</b>												
<b>Stream type</b>	<b>A1</b>	<b>A2</b>	<b>A3</b>	<b>A4</b>	<b>A5</b>	<b>A6</b>	<b>B1</b>	<b>B2</b>	<b>B3</b>	<b>B4</b>	<b>B5</b>	<b>B6</b>	<b>C1</b>	<b>C2</b>	<b>C3</b>	<b>C4</b>	<b>C5</b>	<b>C6</b>	<b>D3</b>	<b>D4</b>	<b>D5</b>	<b>D6</b>	<b>Grand total = 97</b>	
Good (Stable)	38-43	38-43	54-90	60-95	50-80	38-45	38-45	38-45	40-60	40-64	48-68	40-60	38-50	38-50	60-85	70-90	70-90	60-85	85-107	85-107	85-107	85-107	85-107	67-98
Fair (Mod. unstable)	44-47	44-47	91-129	96-132	81-110	46-58	46-58	46-58	61-78	65-84	69-88	61-78	51-61	51-61	86-105	91-110	91-110	86-105	108-132	108-132	108-132	108-132	99-125	
Poor (Unstable)	48+	48+	130+	133+	143+	59+	59+	59+	79+	85+	89+	79+	62+	62+	106+	111+	111+	106+	133+	133+	133+	133+	126+	
<b>Stream type</b>	<b>DA3</b>	<b>DA4</b>	<b>DA5</b>	<b>DA6</b>	<b>E3</b>	<b>E4</b>	<b>E5</b>	<b>E6</b>	<b>F1</b>	<b>F2</b>	<b>F3</b>	<b>F4</b>	<b>F5</b>	<b>F6</b>	<b>G1</b>	<b>G2</b>	<b>G3</b>	<b>G4</b>	<b>G5</b>	<b>G6</b>	<b>G6</b>	<b>G6</b>	<b>G6</b>	<b>A4/1a+</b>
Good (Stable)	40-63	40-63	40-63	40-63	50-75	50-75	40-63	40-63	60-85	60-85	80-115	80-115	90-115	80-95	40-60	40-60	85-107	85-107	90-112	85-107	85-107	85-107	85-107	
Fair (Mod. unstable)	64-86	64-86	64-86	64-86	76-96	76-96	64-86	64-86	86-105	86-105	111-125	111-125	116-130	96-110	61-78	61-78	108-120	108-120	113-125	108-120	108-120	108-120	108-120	
Poor (Unstable)	87+	87+	87+	87+	97+	97+	87+	87+	106+	106+	126+	126+	131+	111+	79+	79+	121+	121+	126+	121+	121+	121+	121+	
<b>Modified channel stability rating = Fair</b>																								

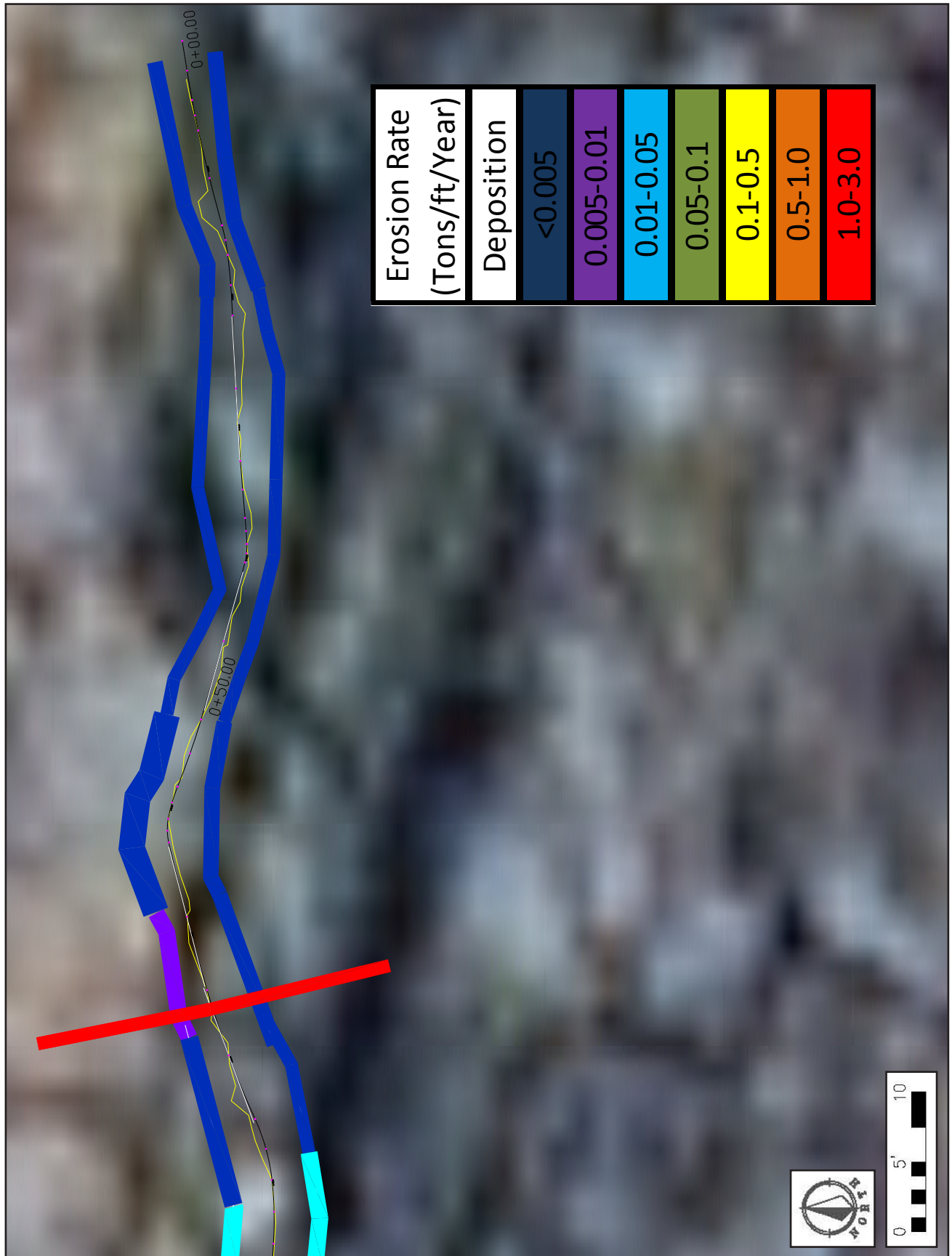
\*Rating is adjusted to potential stream type, not existing.

## BANCS Model – Streambank Erosion

**Worksheet 5-18.** Annual streambank erosion estimates.

Stream: <b>Trail Creek, A4/1a+ Fair Reach</b>				Location: <b>Pike National Forest, Colorado</b>			
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>77</b>			Date: <b>9/2/2010</b>		
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Valley Type: <b>I</b>		Stream Type: <b>A4/1a+</b>			
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 5-16) (adjective)	NBS rating (Worksheet 5-17) (adjective)	Bank erosion rate (Figure 5-34 or 5-35) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [[4]x(5)x(6)] (ft <sup>3</sup> /yr)	Erosion Rate {[(7)/27] × 1.3 / (5)}
1. 0+00 to 0+12 Left	Low	Low	0.03566	12.0	1.2	0.51	0.00206
2. 0+00 to 0+27 Right	Low	Low	0.03566	27.0	1.2	1.16	0.00206
3. 0+12 to 0+27 Left	Moderate	Low	0.15287	15.0	1.2	2.75	0.00883
4. 0+27 to 0+57 Right	Low	Low	0.03566	30.0	0.8	0.86	0.00137
5. 0+27 to 0+57 Left	Low	Low	0.03566	30.0	0.8	0.86	0.00137
6. 0+57 to 0+ 67 Right	Low	Low	0.03566	10.0	2.0	0.71	0.00343
7. 0+57 to 0+77 Left	Low	Low	0.03566	20.0	1.3	0.93	0.00223
8. 0+67 to 0+71 Right	Moderate	Low	0.15287	4.0	1.3	0.79	0.00957
9. 0+71 to 0+77 Right	Low	Low	0.03566	6.0	1.3	0.28	0.00223
10							
11							
12							
13							
14							
15							
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					Total Erosion (ft <sup>3</sup> /yr)	<b>8.85</b>	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					Total Erosion (yds <sup>3</sup> /yr)	<b>0.33</b>	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					Total Erosion (tons/yr)	<b>0.43</b>	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					Total Erosion (tons/yr/ft)	<b>0.0055</b>	

### Streambank Erosion Map



## FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Equation Type		Equation Source				Equation		Bankfull Discharge (cfs)			Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)		
1. Bedload Sediment		"Good/Fair" Pagosa				$y = -0.0113 + 1.0139x^{2.1929}$		0.38			0.001764		0.0304		
2. Suspended Sediment		"Good/Fair" Pagosa				$y = 0.0636 + 0.9326x^{2.4085}$									
		From Dimensional Flow-Duration Curve				From Sediment Rating Curves				Calculate		Calculate Sediment Yield			
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	
Percentage of Time	Daily Mean Discharge (cfs)	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimension-less Streamflow	Dimension-less Suspended Sediment Discharge ( $S/S_{bkt}$ )	Suspended Sediment Discharge (tons/day)	Dimension-less Bedload Discharge ( $b_b/b_{bkt}$ )	Bedload Sediment Discharge (tons/day)	Time Adjusted Streamflow $[(5) \times (6)]$	Suspended Sediment $[(5) \times (9)]$	Bedload Sediment $[(5) \times (11)]$	Suspended Sediment + Bedload Sediment $[(13) \times (14)]$	
(%)	(cfs)	(%)	(%)	(days)	(cfs)	( $Q/Q_{bkt}$ )	( $S/S_{bkt}$ )	(tons/day)	( $b_b/b_{bkt}$ )	(tons/day)	(cfs)	(tons)	(tons)	(tons)	
0%	1.0														
0.10%	0.8	0.05%	0.09%	0.34	0.9	2.363	7.461	0.00	6.670	1.12	0.3	0.00	0.38	0.38	
0.25%	0.7	0.08%	0.15%	0.55	0.8	2.036	5.232	0.00	4.809	0.81	0.4	0.00	0.44	0.44	
0.50%	0.6	0.13%	0.25%	0.91	0.7	1.761	3.706	0.00	3.494	0.59	0.6	0.00	0.54	0.54	
0.75%	0.5	0.13%	0.25%	0.91	0.6	1.513	2.592	0.00	2.502	0.42	0.5	0.00	0.38	0.38	
1%	0.5	0.13%	0.25%	0.91	0.5	1.300	1.817	0.00	1.790	0.30	0.5	0.00	0.27	0.27	
1.5%	0.4	0.25%	0.50%	1.83	0.4	1.120	1.289	0.00	1.289	0.22	0.8	0.00	0.40	0.40	
2%	0.3	0.25%	0.50%	1.83	0.4	0.949	0.886	0.00	0.893	0.15	0.7	0.00	0.27	0.27	
3%	0.3	0.50%	1.00%	3.65	0.3	0.795	0.600	0.00	0.602	0.10	1.1	0.00	0.37	0.37	
4%	0.2	0.50%	1.00%	3.65	0.3	0.674	0.424	0.00	0.415	0.07	0.9	0.00	0.25	0.25	
5%	0.2	0.50%	1.00%	3.65	0.2	0.587	0.322	0.00	0.304	0.05	0.8	0.00	0.19	0.19	
10%	0.1	2.50%	5.00%	18.25	0.2	0.450	0.200	0.00	0.165	0.03	3.1	0.00	0.51	0.51	
20%	0.1	5.00%	10.00%	36.50	0.1	0.269	0.103	0.00	0.045	0.01	3.7	0.00	0.28	0.28	
30%	0.0	5.00%	10.00%	36.50	0.1	0.158	0.075	0.00	0.006	0.00	2.2	0.00	0.04	0.04	
40%	0.0	5.00%	10.00%	36.50	0.0	0.108	0.068	0.00	0.000	0.00	1.5	0.00	0.00	0.00	
50%	0.0	5.00%	10.00%	36.50	0.0	0.079	0.066	0.00	0.000	0.00	1.1	0.00	0.00	0.00	
60%	0.0	5.00%	10.00%	36.50	0.0	0.061	0.065	0.00	0.000	0.00	0.8	0.00	0.00	0.00	
70%	0.0	5.00%	10.00%	36.50	0.0	0.047	0.064	0.00	0.000	0.00	0.7	0.00	0.00	0.00	
80%	0.0	5.00%	10.00%	36.50	0.0	0.039	0.064	0.00	0.000	0.00	0.5	0.00	0.00	0.00	
90%	0.0	5.00%	10.00%	36.50	0.0	0.032	0.064	0.00	0.000	0.00	0.4	0.00	0.00	0.00	
100%	0.0	5.00%	10.00%	36.50	0.0	0.016	0.064	0.00	0.000	0.00	0.2	0.00	0.00	0.00	
<b>Annual Totals:</b>										20.9 (cfs)		0.001 (tons/yr)		4.33 (tons/yr)	
										41.5 (acre-ft)					

Worksheet 19b. Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Equation Type		Equation Source		Equation		Bankfull Discharge (cfs)		Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)							
1. Bedload Sediment		"Good/Fair" Pagosa		$y = -0.0113 + 1.0139x^{2.1929}$		0.38		0.001775		31.00							
2. Suspended Sediment		"Good/Fair" Pagosa		$y = 0.0636 + 0.9326x^{2.4085}$													
From Dimensional Flow-Duration Curve						From Sediment Rating Curves											
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)			
Percentage of Time	Daily Mean Discharge	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Sediment Discharge	Suspended Sediment Discharge	Dimensionless Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow	Suspended Sediment	Bedload Sediment	Suspended + Bedload Sediment			
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>bed</sub> )	(S/S <sub>bed</sub> )	(tons/day)	(b <sub>y</sub> /b <sub>bed</sub> )	(tons/day)	(cfs)	(tons)	(tons)	(tons)			
0%	1.0																
0.10%	0.8	0.05%	0.09%	0.34	0.9	2.410	7.819	0.60	6.964	1.18	0.3	0.21	0.40	0.61			
0.25%	0.7	0.08%	0.15%	0.55	0.8	2.083	5.522	0.37	5.055	0.85	0.4	0.20	0.47	0.67			
0.50%	0.6	0.13%	0.25%	0.91	0.7	1.807	3.943	0.23	3.701	0.63	0.6	0.21	0.57	0.78			
0.75%	0.5	0.13%	0.25%	0.91	0.6	1.560	2.784	0.14	2.676	0.45	0.5	0.13	0.41	0.54			
1%	0.5	0.13%	0.25%	0.91	0.5	1.346	1.973	0.08	1.935	0.33	0.5	0.08	0.30	0.38			
1.5%	0.4	0.25%	0.50%	1.83	0.4	1.167	1.415	0.05	1.410	0.24	0.8	0.10	0.44	0.53			
2%	0.3	0.25%	0.50%	1.83	0.4	0.995	0.984	0.03	0.991	0.17	0.7	0.06	0.31	0.36			
3%	0.3	0.50%	1.00%	3.65	0.3	0.840	0.677	0.02	0.681	0.12	1.2	0.07	0.42	0.49			
4%	0.3	0.50%	1.00%	3.65	0.3	0.717	0.483	0.01	0.478	0.08	1.0	0.04	0.30	0.34			
5%	0.2	0.50%	1.00%	3.65	0.2	0.626	0.366	0.01	0.352	0.06	0.9	0.03	0.22	0.24			
10%	0.1	2.50%	5.00%	18.25	0.2	0.480	0.223	0.00	0.191	0.03	3.3	0.06	0.59	0.65			
20%	0.1	5.00%	10.00%	36.50	0.1	0.282	0.108	0.00	0.052	0.01	3.9	0.04	0.32	0.35			
30%	0.0	5.00%	10.00%	36.50	0.1	0.160	0.075	0.00	0.007	0.00	2.2	0.01	0.04	0.06			
40%	0.0	5.00%	10.00%	36.50	0.0	0.108	0.068	0.00	0.000	0.00	1.5	0.01	0.00	0.01			
50%	0.0	5.00%	10.00%	36.50	0.0	0.079	0.066	0.00	0.000	0.00	1.1	0.01	0.00	0.01			
60%	0.0	5.00%	10.00%	36.50	0.0	0.061	0.065	0.00	0.000	0.00	0.8	0.00	0.00	0.00			
70%	0.0	5.00%	10.00%	36.50	0.0	0.047	0.064	0.00	0.000	0.00	0.7	0.00	0.00	0.00			
80%	0.0	5.00%	10.00%	36.50	0.0	0.039	0.064	0.00	0.000	0.00	0.5	0.00	0.00	0.00			
90%	0.0	5.00%	10.00%	36.50	0.0	0.032	0.064	0.00	0.000	0.00	0.4	0.00	0.00	0.00			
100%	0.0	5.00%	10.00%	36.50	0.0	0.016	0.064	0.00	0.000	0.00	0.2	0.00	0.00	0.00			
						Annual Totals:						21.7		1.2		6.0	
												(cfs)		(tons/yr)		(tons/yr)	

## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>Trail Creek, A4/1a+ Fair Reach</b>		Stream Type: <b>A4/1a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/2/2010</b>			
<b>Enter Required Information for Existing Condition</b>					
9.0	$D_{50}$	Riffle bed material $D_{50}$ (mm)			
	$\hat{D}_{50}$	Bar sample $D_{50}$ (mm)			
0.42	$D_{max}$	Largest particle from <b>Bed Material</b> (ft)	128	(mm)	304.8 mm/ft
0.2430	$S$	Existing bankfull water surface slope (ft/ft)			
0.25	$d$	Existing bankfull mean depth (ft)			
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment			
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>					
N/A	$D_{50}/\hat{D}_{50}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 ( D_{50}/\hat{D}_{50} )^{-0.872}$		
N/A	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 ( D_{max}/D_{50} )^{-0.887}$		
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED:		
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	$d$	Required bankfull mean depth (ft)	$d = \frac{\tau^*(\gamma_s - 1)D_{max}}{S}$ (use $D_{max}$ in ft)		
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	$S$	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^*(\gamma_s - 1)D_{max}}{d}$ (use $D_{max}$ in ft)		
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					
<b>Sediment Competence Using Dimensional Shear Stress</b>					
3.79	Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d ) $\gamma = 62.4$ , $d =$ existing depth, $S =$ existing slope				
Shields <b>290</b>	CO <b>400</b>	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ ( <b>Figure 5-49</b> )			
Shields <b>2.0</b>	CO <b>0.9</b>	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) ( <b>Figure 5-49</b> )			
Shields <b>0.13</b>	CO <b>0.06</b>	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm)		$d = \frac{\tau}{\gamma S}$	
		$\tau =$ predicted shear stress, $\gamma = 62.4$ , $S =$ existing slope			
Shields <b>0.1282</b>	CO <b>0.0577</b>	Predicted slope required to initiate movement of measured $D_{max}$ (mm)		$S = \frac{\tau}{\gamma d}$	
		$\tau =$ predicted shear stress, $\gamma = 62.4$ , $d =$ existing depth			
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input checked="" type="checkbox"/> Degrading					



## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>Trail Creek, A4/1a+ Fair Reach</b>		Stream Type: <b>A4/1a+</b>
Location: <b>Pike National Forest, CO</b>		Valley Type: <b>I</b>
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/2/2010</b>
<b>Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)</b>		<b>Stability Rating (Check Appropriate Rating)</b>
<b>Stream Type at potential, (C→E),                  (F<sub>b</sub>→B), (G→B), (F→B<sub>c</sub>), (F→C), (D→C)</b>		<input checked="" type="checkbox"/> Stable
(E→C), (C→High W/d C)		<input type="checkbox"/> Moderately Unstable
(G→F), (F→D), (C→F)		<input type="checkbox"/> Unstable
(C→D), (B→G), (D→G), (C→G), (E→G)		<input type="checkbox"/> Highly Unstable

**Worksheet 5-25.** Lateral stability.

Stream: <b>Trail Creek, A4/1a+ Fair Reach</b>		Stream Type: <b>A4/1a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/2/2010</b>			
Lateral stability criteria (choose one stability category for each criterion 1-5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	2
	0.66 (2)	(4)	(6)	(8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	2
	B2 (1)	(2)	(3)	(4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		1
	M1 (1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	2
	L/L (2)	(4)	(6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	1
	0.99 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>8</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input checked="" type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input type="checkbox"/>	<i>Unstable</i> 13 – 21 <input type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	

**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>Trail Creek, A4/1a+ Fair Reach</b>		Stream Type: <b>A4/1a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/2/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
1 <b>Sediment Competence</b> (Worksheet 5-22)	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope—slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	2
	(2)	(4)	(6)	(8)	
2 <b>Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	2
	(2)	(4)	(6)	(8)	
3 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	2
	0.7 (2)	(4)	(6)	(8)	
4 <b>Stream Succession States</b> (Worksheet 5-24)	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	2
	at potential (2)	(4)	(6)	(8)	
5 <b>Depositional Patterns</b> (Worksheet 5-10)	B1	B2, B4	B3, B5	B6, B7, B8	2
	(1)	B2 (2)	(3)	(4)	
6 <b>Debris / Blockages</b> (Worksheet 5-11)	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	1
	D3 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>11</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
Vertical Stability for Excess Deposition / Aggradation (use total points and check stability rating)	<i>No Deposition</i> 10 – 14 <input checked="" type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input type="checkbox"/>	<i>Aggradation</i> > 30 <input type="checkbox"/>	

**Worksheet 5-27.** Vertical stability – degradation.

Stream: <b>Trail Creek, A4/1a+ Fair Reach</b>		Stream Type: <b>A4/1a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/2/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>1 Sediment Competence</b> (Worksheet 5-22)	Does not indicate excess competence	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed	$D_{100}$ of bed moved	Particles much larger than $D_{100}$ of bed moved	<b>4</b>
	(2)	(4)	(6)	(8)	
<b>2 Sediment Capacity</b> (POWERSED) (Worksheet 5-20)	Does not indicate excess capacity	Slight excess energy: up to 10% increase above reference	Excess energy sufficient to increase load up to 50% of annual load	Excess energy transporting more than 50% of annual load	<b>4</b>
	(2)	(4)	(6)	(8)	
<b>3 Degree of Channel Incision (BHR)</b> (Worksheet 5-12)	1.00 – 1.10	1.11 – 1.30	1.31 – 1.50	> 1.50	<b>7</b>
	(2)	(4)	(6)	1.5 (7) (8)	
<b>4 Stream Succession States</b> (Worksheets 5-12 and 5-24)	Does not indicate incision or degradation	If BHR > 1.1 and stream type has W/d between 5–10	If BHR > 1.1 and stream type has W/d less than 5	(B→G), (C→G), (E→G), (D→G)	<b>4</b>
	(2)	1.5 BHR, 7.2 W/d (4)	(6)	(8)	
<b>5 Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.80 – 1.00	0.30 – 0.79	0.10 – 0.29	< 0.10	<b>1</b>
	0.99 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>20</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation</b> (use total points and check stability rating)	<i>Not Incised</i> 9 – 11 <input type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input checked="" type="checkbox"/>	<i>Degradation</i> > 27 <input type="checkbox"/>	

Worksheet 5-28. Channel enlargement.

Stream: <b>Trail Creek, A4/1a+ Fair Reach</b>		Stream Type: <b>A4/1a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/2/2010</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1–4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	2
	at potential (2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	2
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	2
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	6
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>12</b>
<b>Category Point Range</b>					
Channel Enlargement Prediction (use total points and check stability rating)	<i>No Increase</i> 8 – 10 <input type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input checked="" type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input type="checkbox"/>	<i>Extensive</i> > 24 <input type="checkbox"/>	

Worksheet 5-29. Overall sediment supply.

Stream: <b>Trail Creek, A4/1a+ Fair Reach</b>		Stream Type: <b>A4/1a+</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>		
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/2/2010</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1-5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	1	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	1	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	3	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	2	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	2	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>9</b>	
<b>Category Point Range</b>				
Overall Sediment Supply Rating (use total points and check stability rating)	<i>Low</i> 5 <input type="checkbox"/>	<i>Moderate</i> 6 – 10 <input checked="" type="checkbox"/>	<i>High</i> 11 – 15 <input type="checkbox"/>	<i>Very High</i> 16 – 20 <input type="checkbox"/>

Worksheet 5-32. Summary of stability condition categories.

Stream: <b>Trail Creek, A4/1a+ Fair Reach</b>		Location: <b>Pike National Forest, Colorado</b>	
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Stream Type: <b>A4/1a+</b> Valley Type: <b>I</b>	
Date: <b>9/2/2010</b>		Cross-Sectional Area (ft <sup>2</sup> ): <b>0.45</b>	
Bankfull Width (ft): <b>1.79</b>		Width of Flood-Prone Area (ft): <b>2.34</b>	
Mean Bankfull Depth (ft): <b>0.25</b>		Entrenchment Ratio: <b>1.31</b>	
Channel Pattern		Sinuosity: <b>1.1</b>	
Mean: $\lambda/W_{bkf}$ : <b>N/A</b> Range: $L_m/W_{bkf}$ : <b>N/A</b> $R_c/W_{bkf}$ : <b>N/A</b> MWR: <b>1.5</b>		MWR: <b>1.5</b> Sinuosity: <b>1.1</b>	
River Profile & Bed Features		Check: <input type="checkbox"/> Riffle/Pool <input type="checkbox"/> Step/Pool <input checked="" type="checkbox"/> Plane Bed <input type="checkbox"/> Convergence/Divergence <input type="checkbox"/> Dunes/Antidunes/Smooth Bed Max Bankfull Depth (ft): Riffle Pool Depth Ratio (max to mean): Riffle Pool Pool-to-Pool Spacing: Valley: <b>0.2673</b> Water Surface: <b>0.243</b>	
Level III Stream Stability Indices		Riparian Vegetation: <b>Aspen/Shrubs/Mullen/Grass</b> Current Composition/Density: <b>Mature Aspen/P.Pine/Shrub</b> Remarks: Condition, Vigor & Usage of Existing Reach: Flow Regime: <b>E1, E2, E8 &amp; Order: S-2(2)</b> Meander Patterns: <b>M1</b> Depositional Patterns: <b>B2</b> Blockages: <b>D3</b> Degree of Incision Stability Rating: <b>Moderate To Deeply Incised</b> Modified Pfankuch Stability Rating: <b>97 (Fair)</b> Width/depth Ratio (W/d): <b>7.2</b> Reference W/d Ratio (W/d <sub>ref</sub> ): <b>11</b> Width/Depth Ratio State (W/d) / (W/d <sub>ref</sub> ): <b>0.66</b> W/d Ratio State Stability Rating: <b>Moderately Unstable</b> Meander Width Ratio (MWR): <b>1.5</b> Reference MWR <sub>ref</sub> : <b>1.52</b> Degree of confinement (MWR / MWR <sub>ref</sub> ): <b>0.99</b> MWR / MWR <sub>ref</sub> Stability Rating: <b>No Departure from Reference</b> Length of Reach Studied (ft): <b>77</b> Annual Streambank Erosion Rate: (tons/yr) <b>0.0055</b> (tons/yr/ft) <b>Colorado</b> Curve Used: <b>Colorado</b> Remarks:	
Bank Erosion Summary		Sediment Capacity <input type="checkbox"/> Insufficient Capacity <input checked="" type="checkbox"/> Excess Capacity Remarks:	
Sediment Capacity (POWERSED)		Largest Particle from Bed Material (mm): <b>128</b> $\tau =$ <b>3.79</b> $\tau^* =$ <b>N/A</b> Existing Depth: <b>0.25</b> Required Depth: <b>0.13</b> Existing Slope: <b>0.243</b> Required Slope: <b>0.128</b>	
Entrainment/Competence		Successional Stage Shift: <b>A4/1a+ → A4/1a+ →</b> Existing Stream State (Type): <b>A4/1a+</b> Potential Stream State (Type): <b>A4/1a+</b> Remarks/causes:	
Lateral Stability		Lateral Stability: <input checked="" type="checkbox"/> Stable <input type="checkbox"/> Mod. Unstable <input type="checkbox"/> Unstable <input type="checkbox"/> Highly Unstable Remarks/causes:	
Vertical Stability (Aggradation)		Vertical Stability (Aggradation): <input checked="" type="checkbox"/> No Deposition <input type="checkbox"/> Mod. Deposition <input type="checkbox"/> Ex. Deposition <input type="checkbox"/> Aggradation Remarks/causes:	
Vertical Stability (Degradation)		Vertical Stability (Degradation): <input type="checkbox"/> Not Incised <input type="checkbox"/> Slightly Incised <input checked="" type="checkbox"/> Mod. Incised <input type="checkbox"/> Degradation Remarks/causes:	
Channel Enlargement		Channel Enlargement: <input type="checkbox"/> No Increase <input checked="" type="checkbox"/> Slight Increase <input type="checkbox"/> Mod. Increase <input type="checkbox"/> Extensive Remarks/causes:	
Sediment Supply (Channel Source)		Sediment Supply (Channel Source): <input type="checkbox"/> Low <input checked="" type="checkbox"/> Moderate <input type="checkbox"/> High <input type="checkbox"/> Very High Remarks/causes:	





## *Appendix C2*

# **A4a+ Stream Type** *Poor Stability Reach*



# Table of Contents

## *Appendix C2: A4a+ Poor Stability Reach*

<b>Reach Location &amp; Overview.....</b>	<b>C2-2</b>
<b>Survey Summary.....</b>	<b>C2-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C2-8</b>
<b><i>Velocity, Classification &amp; Morphological Relations.....</i></b>	<b>C2-8</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b><i>Stability Indices.....</i></b>	<b>C2-12</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b><i>BANCS Model – Streambank Erosion.....</i></b>	<b>C2-22</b>
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b><i>FLOWSED Model – Total Annual Sediment Yield.....</i></b>	<b>C2-25</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b><i>Sediment Competence/Entrainment.....</i></b>	<b>C2-27</b>
Worksheet 5-22. Sediment competence calculations.	
<b><i>Channel Stability Ratings.....</i></b>	<b>C2-28</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b><i>Summary.....</i></b>	<b>C2-34</b>
Worksheet 5-32. Summary of stability condition categories.	

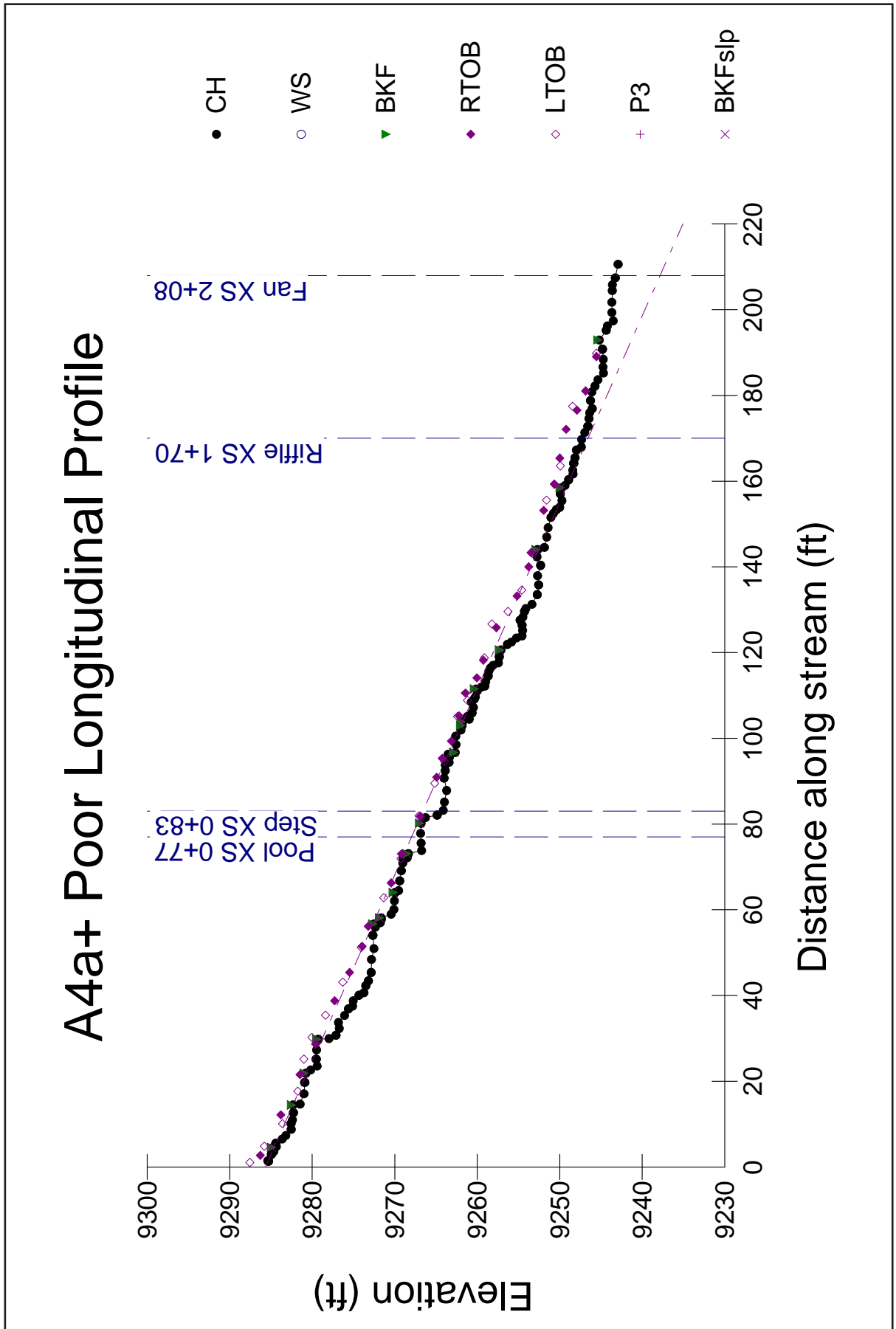
## A4a+ Poor Reach Location & Overview

The A4a+ Poor reach is a 1<sup>st</sup> order, ephemeral stream with a high sediment supply due to poor road drainage concentrating flow into the channel. This reach is located on Northfield Gulch shown in **Figure C-1**. The photograph depicts the advancing headcut documenting both bed instability and accelerated streambank erosion. The stability rating is “Poor” due to degradation, active incision, and lateral instability. The sediment supply also rates as *High* due to the same processes, including a *Moderate Increase* in channel enlargement. The streambank erosion rate is  $0.0617 \text{ tons/yr/ft}$ , more than one order of magnitude higher than its reference reach condition (**Worksheet 5-18**). The increase in water yield using the WRENSS model for this small, ephemeral channel of 0.22 cfs is  $5.4 \text{ acre-ft}$ . This increase corresponds with an increase in bedload using the FLOWSED model of  $0.5 \text{ tons/yr}$  and  $8.6 \text{ tons/yr}$  of suspended sediment. Post-fire increase in peak flow is likely to exacerbate the “Poor” condition in this reach. With the removal of vegetation post-fire, the reach is expected to continue on a downward trend without mitigation.

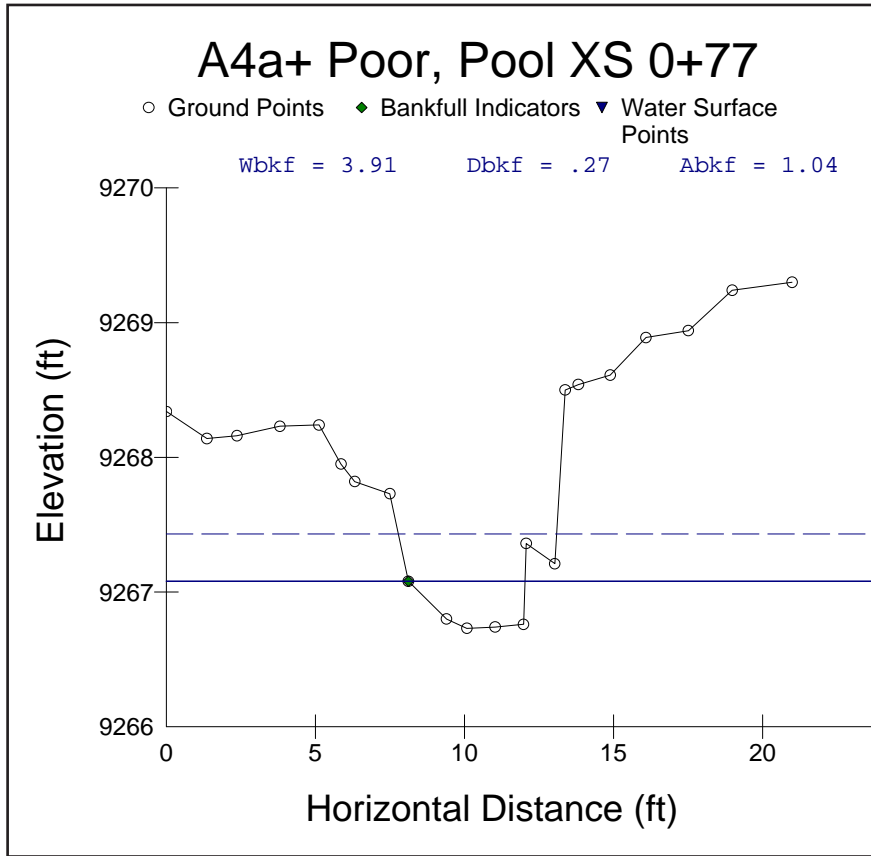
The following graphs and summary worksheets provide the detail of the morphology, hydraulics, streambank erosion rates, and stability conditions responsible for the overall “Poor” rating.



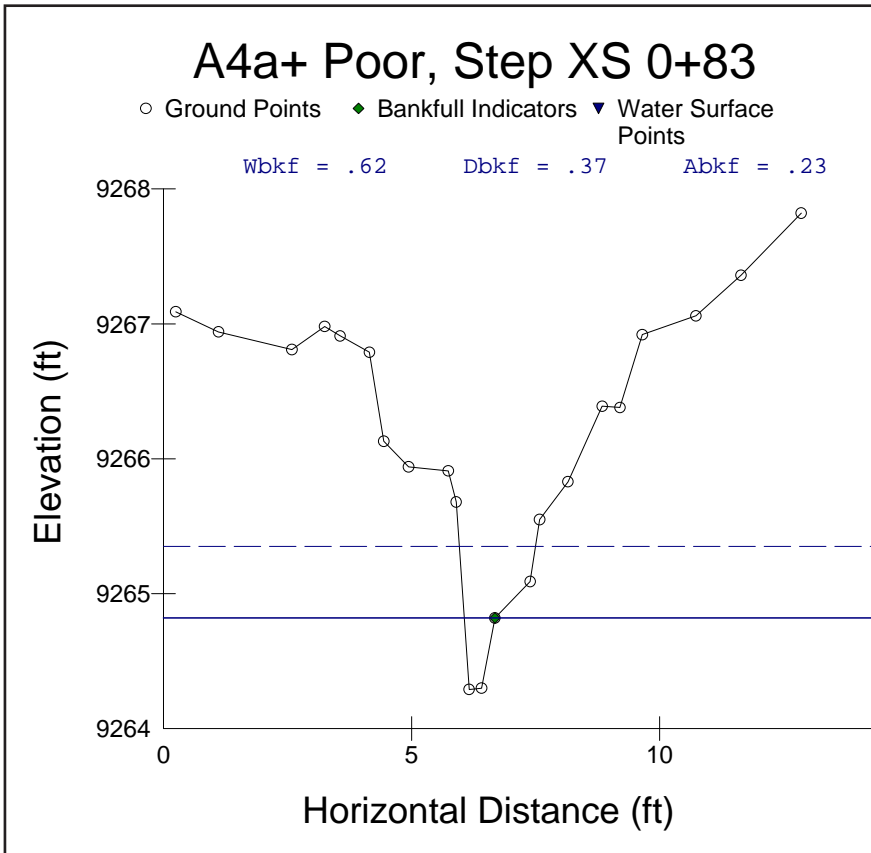
Survey Summary



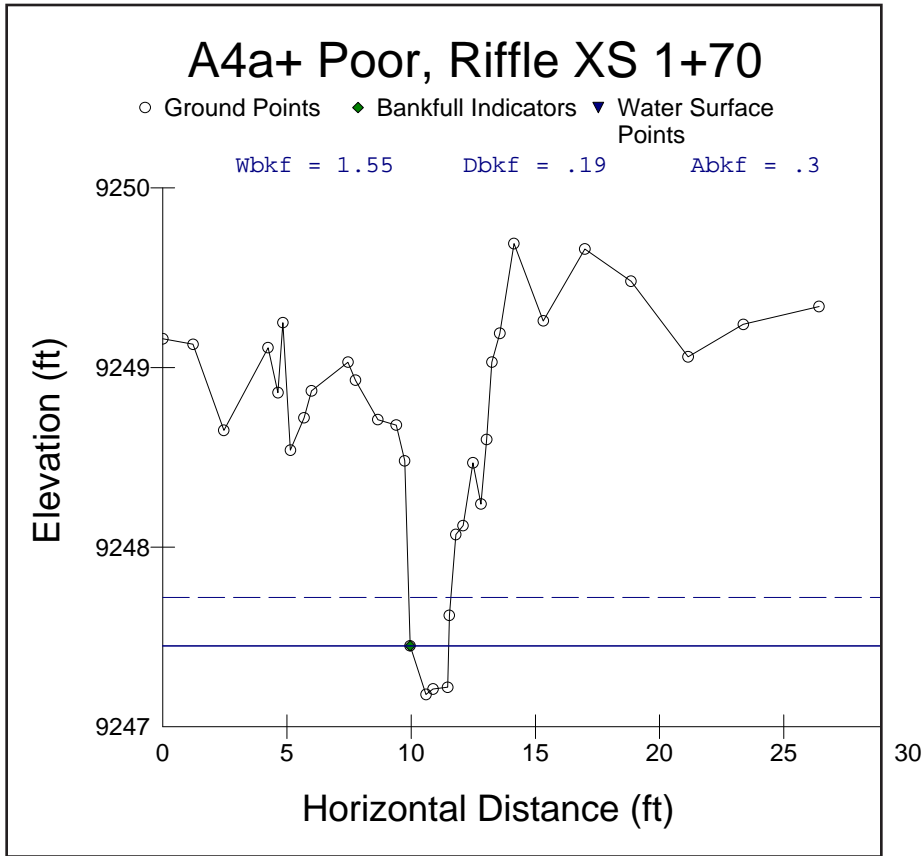
Longitudinal Profile (graph generated from RIVERMorph™)



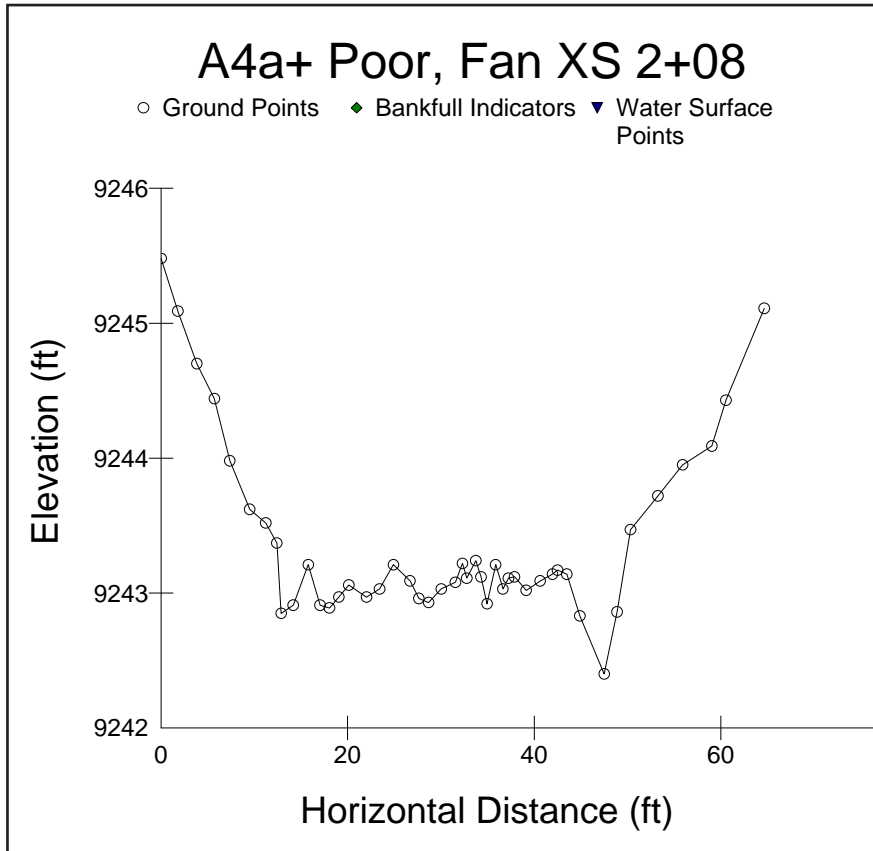
Cross-section 0+77 (graph generated from RIVERMorph™)



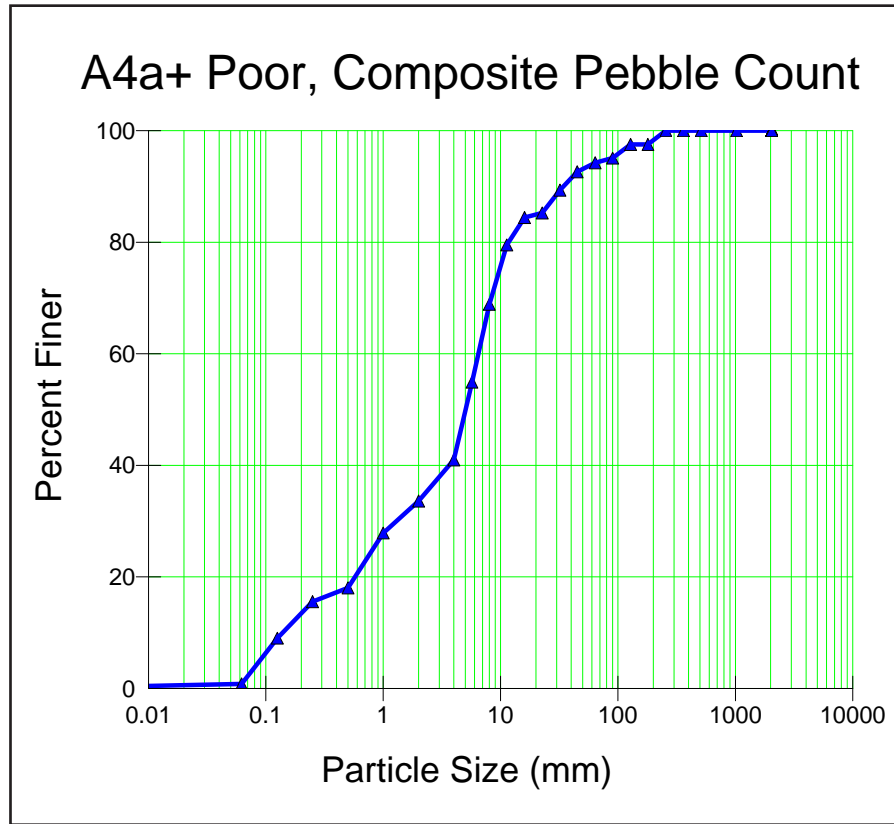
Cross-section 0+83 (graph generated from RIVERMorph™)



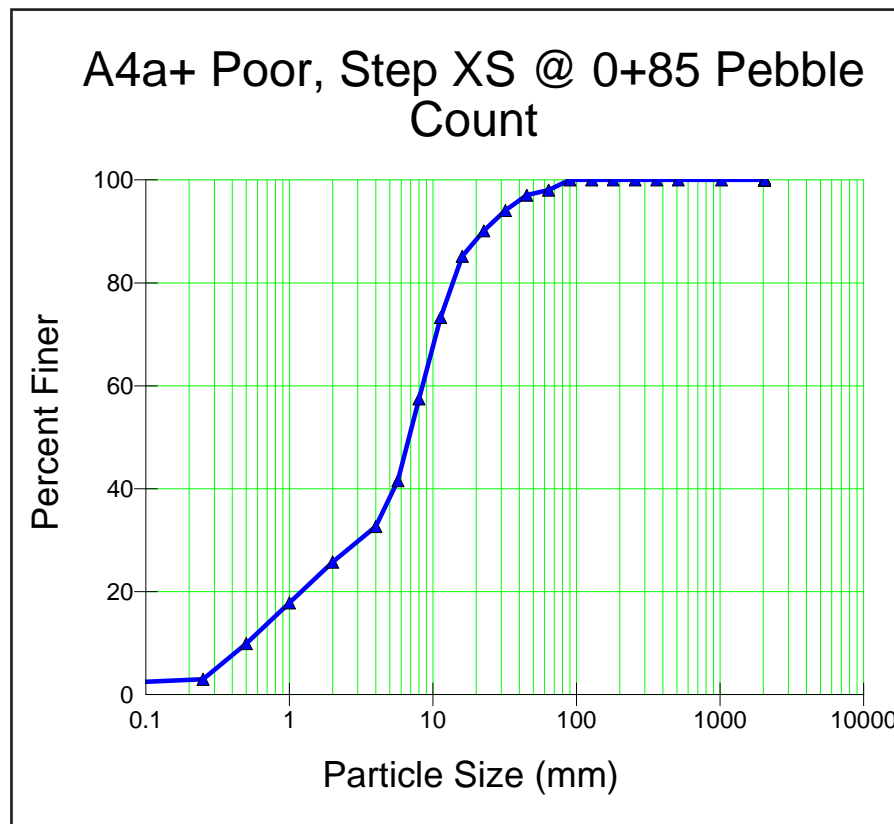
**Representative Cross-section 1+70** (graph generated from RIVERMorph™)



**Cross-section 2+08** (graph generated from RIVERMorph™)

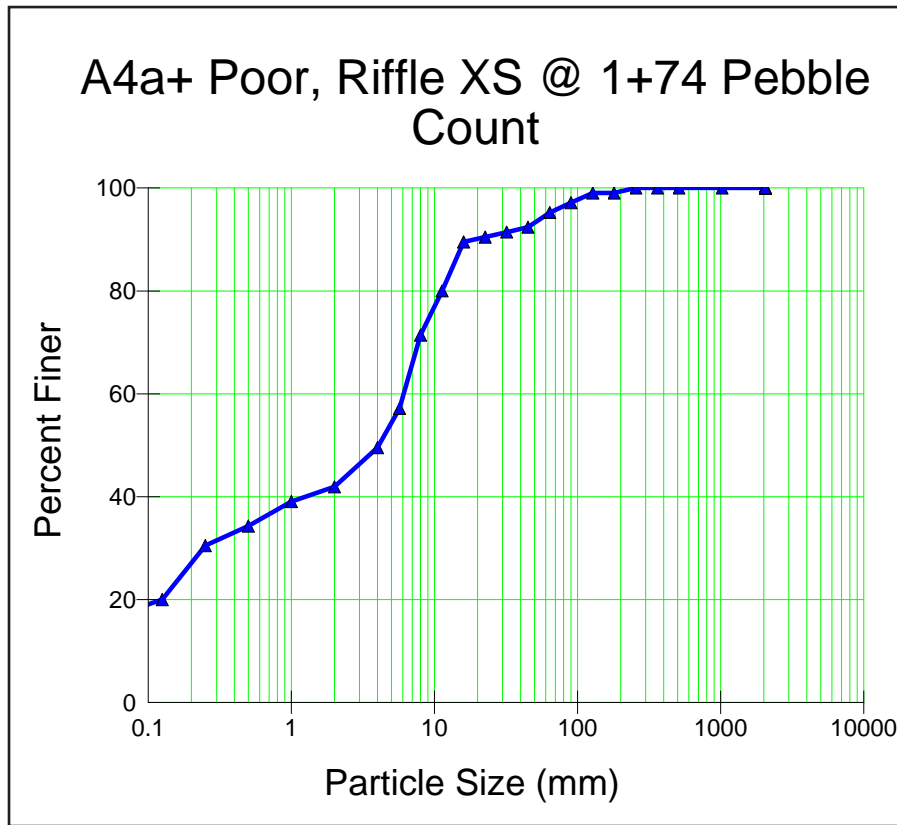


Composite Pebble Count (graph generated from RIVERMorph™)



Step Pebble Count (graph generated from RIVERMorph™)





Active Bed Riffle Pebble Count (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates						
Stream:	Northfield Gulch			Location:	A4a+ Poor XS 1+70	
Date:	11/8/2012	Stream Type:	A4a+	Valley Type:	I	
Observers:	Lee, Sumner, Jara, Leah			HUC:	__ __ __ __ __ __ __ __ __ __	
INPUT VARIABLES			OUTPUT VARIABLES			
Bankfull Riffle Cross-Sectional AREA	0.30	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.15	$d_{bkf}$ (ft)	
Bankfull Riffle WIDTH	1.6	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim (2 * d_{bkf}) + W_{bkf}$	1.85	$W_p$ (ft)	
$D_{84}$ at Riffle	13.3	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.04	$D_{84}$ (ft)	
Bankfull SLOPE	0.23	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	0.16	R (ft)	
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness $R(ft) / D_{84} (ft)$	3.72	$R / D_{84}$	
Drainage Area	0.02	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	1.095	$u^*$ (ft/sec)	
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE	
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$			6.81	ft / sec	2.04	cfs
2. Roughness Coefficient: a) Manning's n from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.2971$			0.73	ft / sec	0.22	cfs
2. Roughness Coefficient: b) Manning's n from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.15$			1.44	ft / sec	0.43	cfs
2. Roughness Coefficient: c) Manning's n from Jarrett (USGS): $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for Stream Types A1, A2, A3, B1, B2, B3, C2 & E3 $n = 0.298$			0.71	ft / sec	0.21	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Darcy-Weisbach (Leopold, Wolman and Miller)			7.71	ft / sec	2.3	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)				ft / sec		cfs
4. Continuity Equations: a) Regional Curves $u = Q / A$ Return Period for Bankfull Discharge $Q =$ <input type="text"/> year				ft / sec		cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$				ft / sec		cfs
<b>Protrusion Height Options for the <math>D_{84}</math> Term in the Relative Roughness Relation (<math>R/D_{84}</math>) – Estimation Method 1</b>						
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.						
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.						
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.						
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.						

**Worksheet 5-3.** Level II stream classification.

Stream: <b>NorthfieldGulch, Reach - A4a+ Poor</b>	
Basin:	Drainage Area: <b>14</b> acres <b>0.02</b> mi <sup>2</sup>
Location: <b>Pike National Forest, Colorado</b>	
Twp.&Rge:	Sec.&Qtr.:
Cross-Section Monuments (Lat./Long.): <b>XS 1+70</b> Date: <b>11/08/2012</b>	
Observers: <b>Lee, Sumner, Jara, Leah</b> Valley Type: <b>I</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>1.55</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A_{bkf} / W_{bkf}$ ).	<b>0.19</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>0.3</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>8.16</b>	ft/ft
<b>Maximum DEPTH (<math>d_{max}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>0.27</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>1.7</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>1.1</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the median or dominant diameter of channel materials, as sampled proportionately from the channel surface, between the bankfull stage and Thalweg elevations.	<b>5.1</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.22974</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope ( $S_{val} / S$ ).	<b>1.09</b>	

<b>Stream Type</b>	<b>A4a+</b>	<b>See Classification Key (Figure 2-14)</b>
--------------------	-------------	---

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Northfield Gulch A4a+ Poor</b>		Location: <b>Pike National Forest, Colorado</b>							
Observers: <b>Lee, Sumner, Jara, Leah</b>		Date: <b>11/08/12</b>		Valley Type: <b>I</b>		Stream Type: <b>A4a+</b>			
<b>River Reach Dimension Summary Data.....1</b>									
<b>Riffle Dimensions* ** ***</b>	<b>Riffle Dimensions* ** ***</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Width ( $W_{bkt}$ )	<b>1.6</b>	<b>1.6</b>	<b>1.6</b>	ft	Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	<b>0.3</b>	<b>0.3</b>	<b>0.3</b>
	Mean Riffle Depth ( $d_{bkt}$ )	<b>0.19</b>	<b>0.19</b>	<b>0.19</b>	ft	Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	<b>8.2</b>	<b>8.2</b>	<b>8.2</b>
	Maximum Riffle Depth ( $d_{max}$ )	<b>0.27</b>	<b>0.27</b>	<b>0.27</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>1.421</b>	<b>1.421</b>	<b>1.421</b>
	Width of Flood-Prone Area ( $W_{fpa}$ )				ft	Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )			
	Riffle Inner Berm Width ( $W_{ib}$ )				ft	Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )			
	Riffle Inner Berm Depth ( $d_{ib}$ )				ft	Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )			
	Riffle Inner Berm Area ( $A_{ib}$ )				ft <sup>2</sup>	Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )			
	Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )								
<b>Pool Dimensions* ** ***</b>	<b>Pool Dimensions* ** ***</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Pool Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Pool Width ( $W_{bkfp}$ )	<b>3.9</b>	<b>3.9</b>	<b>3.9</b>	ft	Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )	<b>2.523</b>	<b>2.523</b>	<b>2.523</b>
	Mean Pool Depth ( $d_{bkfp}$ )	<b>0.27</b>	<b>0.27</b>	<b>0.27</b>	ft	Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )	<b>1.421</b>	<b>1.421</b>	<b>1.421</b>
	Pool Cross-Sectional Area ( $A_{bkfp}$ )	<b>1.0</b>	<b>1.0</b>	<b>1.0</b>	ft	Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )	<b>3.467</b>	<b>3.467</b>	<b>3.467</b>
	Maximum Pool Depth ( $d_{maxp}$ )	<b>0.35</b>	<b>0.35</b>	<b>0.35</b>	ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	<b>1.842</b>	<b>1.842</b>	<b>1.842</b>
	Pool Inner Berm Width ( $W_{ibp}$ )				ft	Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )			
	Pool Inner Berm Depth ( $d_{ibp}$ )				ft	Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )			
	Pool Inner Berm Area ( $A_{ibp}$ )				ft <sup>2</sup>	Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )			
	Point Bar Slope ( $S_{pb}$ )				ft/ft	Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )			
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Run Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Run Width ( $W_{bkfr}$ )				ft	Run Width to Riffle Width ( $W_{bkfr} / W_{bkt}$ )			
	Mean Run Depth ( $d_{bkfr}$ )				ft	Mean Run Depth to Mean Riffle Depth ( $d_{bkfr} / d_{bkt}$ )			
	Run Cross-Sectional Area ( $A_{bkfr}$ )				ft	Run Area to Riffle Area ( $A_{bkfr} / A_{bkt}$ )			
	Maximum Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )			
Run Width/Depth Ratio ( $W_{bkfr} / d_{bkfr}$ )				ft					
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Glide Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Glide Width ( $W_{bkfg}$ )				ft	Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )			
	Mean Glide Depth ( $d_{bkfg}$ )				ft	Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )			
	Glide Cross-Sectional Area ( $A_{bkfg}$ )				ft	Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )			
	Maximum Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )			
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )				ft/ft	Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )			
	Glide Inner Berm Width ( $W_{ibg}$ )				ft	Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )			
	Glide Inner Berm Depth ( $d_{ibg}$ )				ft	Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )			
Glide Inner Berm Area ( $A_{ibg}$ )				ft <sup>2</sup>	Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )				
<b>Step**</b>	<b>Step Dimensions**</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Step Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Step Width ( $W_{bkfs}$ )	<b>0.6</b>	<b>0.6</b>	<b>0.6</b>	ft	Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )	<b>0.400</b>	<b>0.400</b>	<b>0.400</b>
	Mean Step Depth ( $d_{bkfs}$ )	<b>0.37</b>	<b>0.37</b>	<b>0.37</b>	ft	Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )	<b>1.947</b>	<b>1.947</b>	<b>1.947</b>
	Step Cross-Sectional Area ( $A_{bkfs}$ )	<b>0.2</b>	<b>0.2</b>	<b>0.2</b>	ft	Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )	<b>0.767</b>	<b>0.767</b>	<b>0.767</b>
	Maximum Step Depth ( $d_{maxs}$ )	<b>0.53</b>	<b>0.53</b>	<b>0.53</b>	ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )	<b>2.789</b>	<b>2.789</b>	<b>2.789</b>
Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )	<b>1.7</b>	<b>1.7</b>	<b>1.7</b>						

**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Northfield Gulch A4a+ Poor</b>		Location: <b>Pike National Forest, Colorado</b>						
Observers: <b>Lee, Sumner, Jara, Leah</b>		Date: <b>11/8/2012</b>		Valley Type: <b>I</b>		Stream Type: <b>A4a+</b>		
<b>River Reach Summary Data.....2</b>								
<b>Hydraulics</b>	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )		<b>0.73</b>	ft/sec	Estimation Method		<b>Friction Factor</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )		<b>0.22</b>	cfs	Drainage Area		<b>0.02</b> mi <sup>2</sup>	
<b>Channel Pattern</b>	<b>Geometry</b>			<b>Dimensionless Geometry Ratios</b>				
	Linear Wavelength ( $\lambda$ )	Mean	Min	Max	ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )	Mean Min Max	
	Stream Meander Length ( $L_m$ )				ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )		
	Radius of Curvature ( $R_c$ )				ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )		
	Belt Width ( $W_{bit}$ )	<b>16.2</b>	<b>9.2</b>	<b>28.7</b>	ft	Meander Width Ratio ( $W_{bit} / W_{bkt}$ )	<b>10.45 5.94 18.51</b>	
	Arc Length ( $L_a$ )				ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )		
	Riffle Length ( $L_r$ )				ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )		
	Individual Pool Length ( $L_p$ )				ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )		
Pool to Pool Spacing ( $P_s$ )				ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )			
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )	<b>0.2504</b>	ft/ft	Average Water Surface Slope ( $S$ )	<b>0.2297</b>	ft/ft	Sinuosity ( $S_{val} / S$ )	<b>1.09</b>
	Stream Length (SL)	<b>201.1</b>	ft	Valley Length (VL)	<b>184.3</b>	ft	Sinuosity (SL / VL)	<b>1.09</b>
	Low Bank Height (LBH)	start: <b>0.74</b> ft end: <b>1.85</b> ft		Max Bankfull Depth ( $d_{max}$ )	start: <b>0.20</b> ft end: <b>0.20</b> ft		Bank-Height Ratio (BHR) (LBH / $d_{max}$ )	start: <b>3.7</b> end: <b>9.3</b>
	<b>Facet Slopes</b>			<b>Dimensionless Facet Slope Ratios</b>				
	Riffle Slope ( $S_{rif}$ )	Mean	Min	Max	ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rif} / S$ )	Mean Min Max	
	Run Slope ( $S_{run}$ )				ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )		
	Pool Slope ( $S_p$ )				ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )		
	Glide Slope ( $S_g$ )				ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )		
	Step Slope ( $S_s$ )				ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )		
	<b>Max Depths<sup>a</sup></b>			<b>Dimensionless Depth Ratios</b>				
	Max Riffle Depth ( $d_{max}$ )	Mean	Min	Max	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	Mean Min Max	
	Max Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )		
	Max Pool Depth ( $d_{maxp}$ )				ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )		
	Max Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )		
Max Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
<b>Channel Materials</b>	<b>Reach<sup>b</sup></b>		<b>Riffle<sup>c</sup></b>		<b>Bar</b>		<b>Protrusion Height<sup>d</sup></b>	
	% Silt/Clay	<b>0.82</b>	<b>0.00</b>		$D_{16}$	<b>0.29</b>	<b>0.11</b>	mm
	% Sand	<b>32.79</b>	<b>41.90</b>		$D_{35}$	<b>2.38</b>	<b>0.57</b>	mm
	% Gravel	<b>60.65</b>	<b>53.34</b>		$D_{50}$	<b>5.10</b>	<b>4.11</b>	mm
	% Cobble	<b>5.74</b>	<b>4.76</b>		$D_{84}$	<b>15.59</b>	<b>13.27</b>	mm
	% Boulder	<b>0.00</b>	<b>0.00</b>		$D_{95}$	<b>87.46</b>	<b>62.41</b>	mm
	% Bedrock	<b>0.00</b>	<b>0.00</b>		$D_{100}$	<b>256.00</b>	<b>255.99</b>	mm

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.

## Stability Indices


**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation					
Stream: <b>Northfield Gulch, A4a+ Poor</b>			Location: <b>Pike National Forest, Colorado</b>		
Observers: <b>Lee, Sumner, Jara, Leah</b>		Reference reach <input type="checkbox"/>	Disturbed (impacted reach) <input checked="" type="checkbox"/>	Date: <b>11/08/2012</b>	
Existing species composition: <b>Burnt trees &amp; young aspen</b>			Potential species composition: <b>Aspen, Doug-fir, Ponderosa pine, Spruce</b>		
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition
<b>1. Overstory</b>	Canopy layer	<b>0%</b>	<b>30%</b>	<b>Spruce</b>	<b>30%</b>
				<b>Ponderosa Pine</b>	<b>30%</b>
				<b>Aspen</b>	<b>40%</b>
					<b>0%</b>
					<b>0%</b>
					<b>0%</b>
					<b>100%</b>
<b>2. Understory</b>	Shrub layer	<b>0%</b>	<b>1%</b>	<b>Young Aspen</b>	<b>100%</b>
					<b>0%</b>
					<b>0%</b>
					<b>0%</b>
					<b>0%</b>
					<b>0%</b>
					<b>100%</b>
<b>3. Ground level</b>	Herbaceous	<b>0%</b>	<b>0%</b>	<b>Remarks:</b> Condition, vigor and/or usage of existing reach: <b>Burnt tress dominate landscape, few young aspen repopulating.</b>	
	Leaf or needle litter	<b>0%</b>			
	Bare ground	<b>69%</b>			
*Based on crown closure. **Based on basal area to surface area.			<b>Column total = 100%</b>		

Worksheet 5-7. Flow regime.

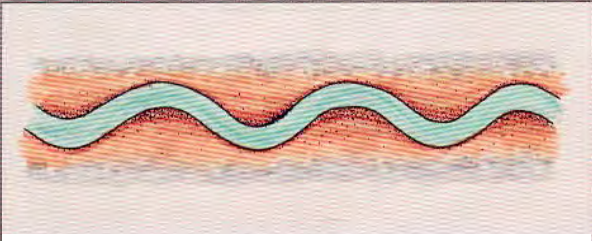
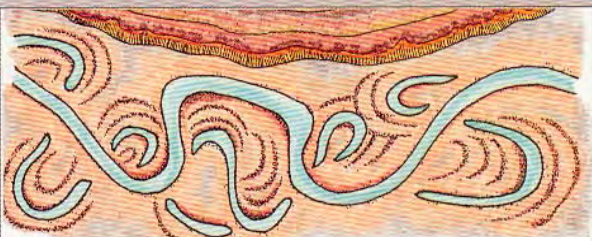

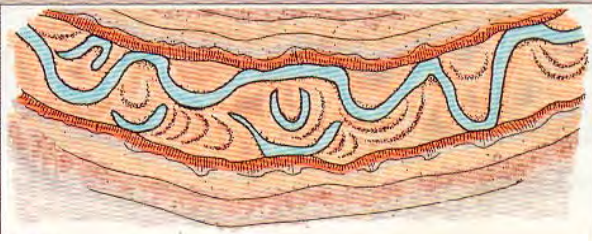


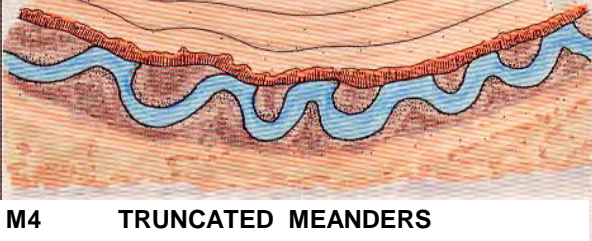
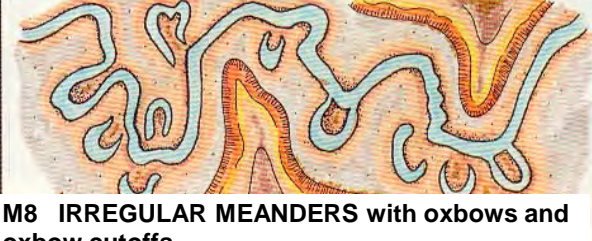
FLOW REGIME								
Stream: <b>Northfield Gulch A4a+ Poor</b>			Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>Lee, Sumner, Jara, Leah</b>						Date: <b>11/8/2012</b>		
List ALL COMBINATIONS that APPLY.....☞			E1	E2	E8			
General Category								
E	Ephemeral stream channels: Flows only in response to precipitation							
S	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
I	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
P	Perennial stream channels: Surface water persists yearlong.							
Specific Category								
1	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
2	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
3	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
4	Streamflow regulated by glacial melt.							
5	Ice flows/ice torrents from ice dam breaches.							
6	Alternating flow/backwater due to tidal influence.							
7	Regulated streamflow due to diversions, dam release, dewatering, etc.							
8	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
9	Rain-on-snow generated runoff.							

**Worksheet 5-8.** Stream order & stream size.

Stream Size and Order			
Stream:	Northfield Gulch A4a+ Poor		
Location:	Pike National Forest, Colorado		
Observers:	Lee, Sumner, Jara, Leah		
Date:	11/8/2012		
Stream Size Category and Order 			S-2(1)
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0 - 305	<1	<input type="checkbox"/>
<b>S-2</b>	<b>0.3 - 1.5</b>	<b>1 - 5</b>	<input checked="" type="checkbox"/>
S-3	1.5 - 4.6	5 - 15	<input type="checkbox"/>
S-4	4.6 - 9	15 - 30	<input type="checkbox"/>
S-5	9 - 15	30 - 50	<input type="checkbox"/>
S-6	15 - 22.8	50 - 75	<input type="checkbox"/>
S-7	22.8 - 30.5	75 - 100	<input type="checkbox"/>
S-8	30.5 - 46	100 - 150	<input type="checkbox"/>
S-9	46 - 76	150 - 250	<input type="checkbox"/>
S-10	76 - 107	250 - 350	<input type="checkbox"/>
S-11	107 - 150	350 - 500	<input type="checkbox"/>
S-12	150 - 305	500 - 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
Stream Order			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			



Worksheet 5-9. Meander patterns.

Meander Patterns					
Stream: <b>Northfield Gulch A4a+ Poor</b>		Location: <b>Pike National Forest, CO</b>			
Observers: <b>Lee, Sumner, Jara, Leah</b>			Date: <b>11/8/2012</b>		
List ALL CATEGORIES that APPLY	<b>N/A</b>				
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>					
 <b>M1 REGULAR MEANDERS</b>	 <b>M5 UNCONFINED MEANDER SCROLLS</b>				
 <b>M2 TORTUOUS MEANDERS</b>	 <b>M6 CONFINED MEANDER SCROLLS</b>				
 <b>M3 IRREGULAR MEANDERS</b>	 <b>M7 DISTORTED MEANDER LOOPS</b>				
 <b>M4 TRUNCATED MEANDERS</b>	 <b>M8 IRREGULAR MEANDERS with oxbows and oxbow cutoffs</b>				

**Worksheet 5-10.** Depositional patterns.

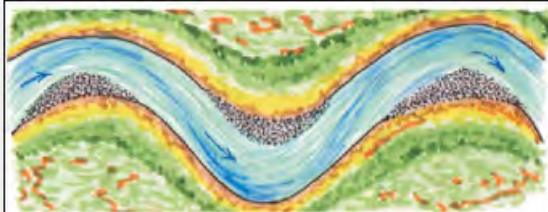
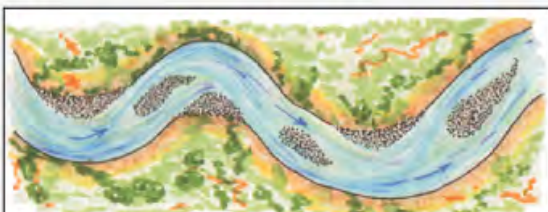
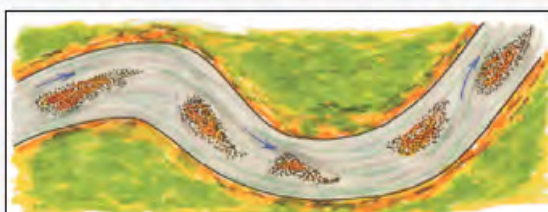

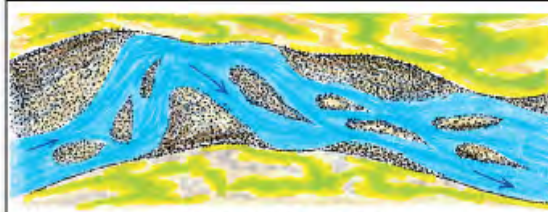
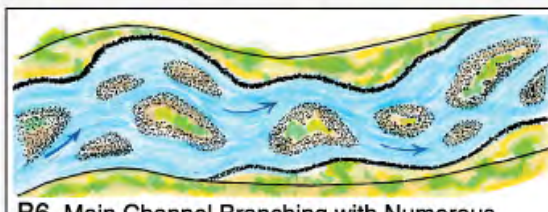
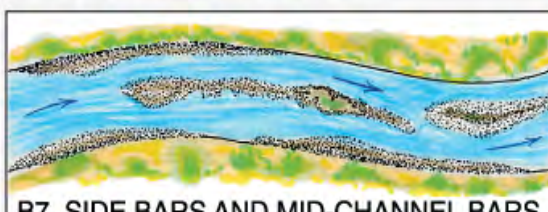

**Depositional Patterns**

Stream: **Northfield Gulch A4a+ Poor** Location: **Pike National Forest, Colorado**

Observers: **Lee, Sumner, Jara, Leah** Date: **11/8/2012**

List ALL CATEGORIES that APPLY	NA				
--------------------------------	----	--	--	--	--

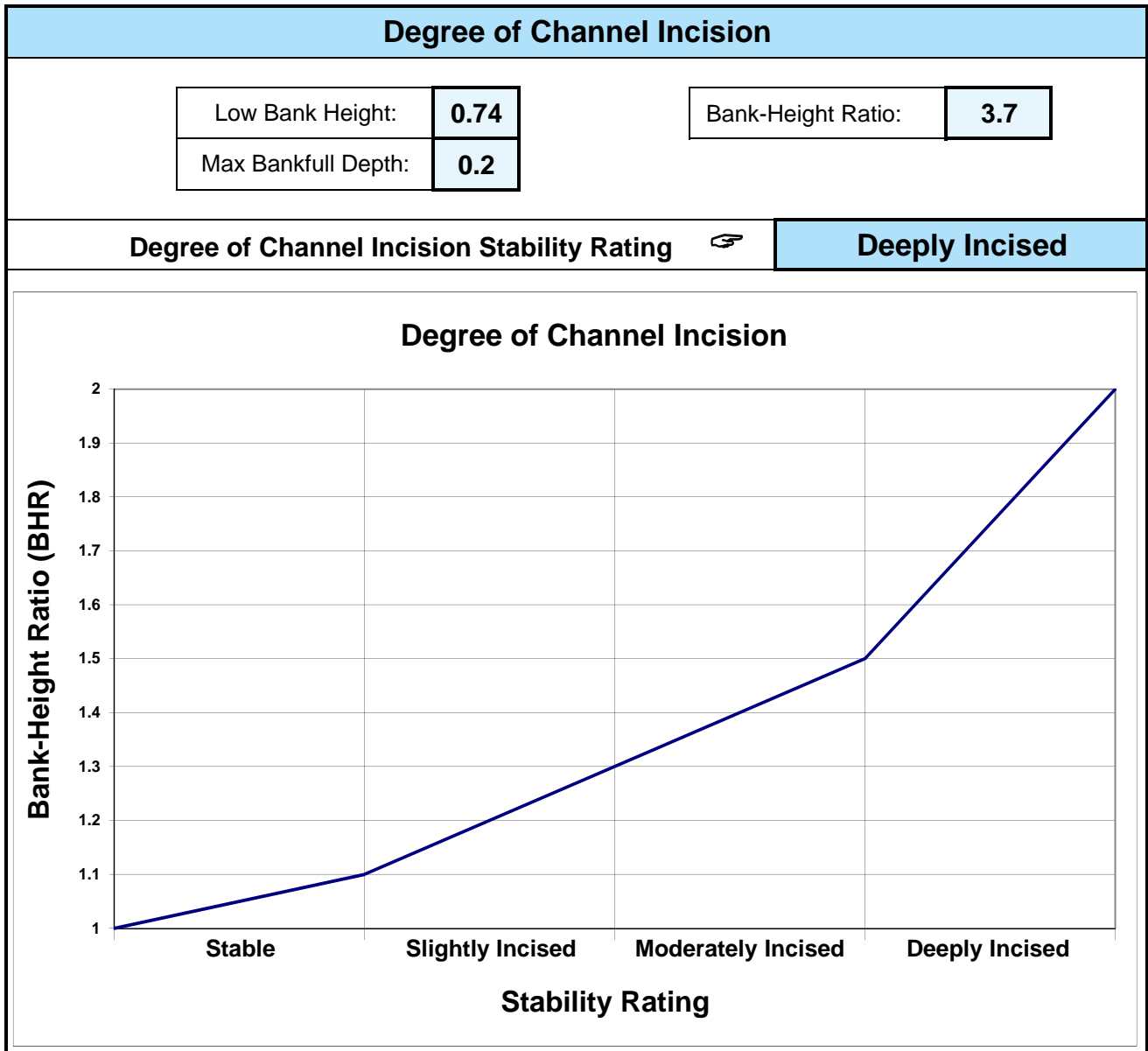
*Various Depositional Features modified from Galay et al. (1973)*

<div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B1</b> POINT BARS</p> </div> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B2</b> POINT BARS with Few MID-CHANNEL BARS</p> </div> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B3</b> NUMEROUS MID-CHANNEL BARS</p> </div> <div style="border: 1px solid black; padding: 5px;">  <p><b>B4</b> SIDE BARS</p> </div>	<div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B5</b> DIAGONAL BARS</p> </div> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B6</b> Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</p> </div> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B7</b> SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</p> </div> <div style="border: 1px solid black; padding: 5px;">  <p><b>B8</b> DELTA BARS</p> </div>
--	--

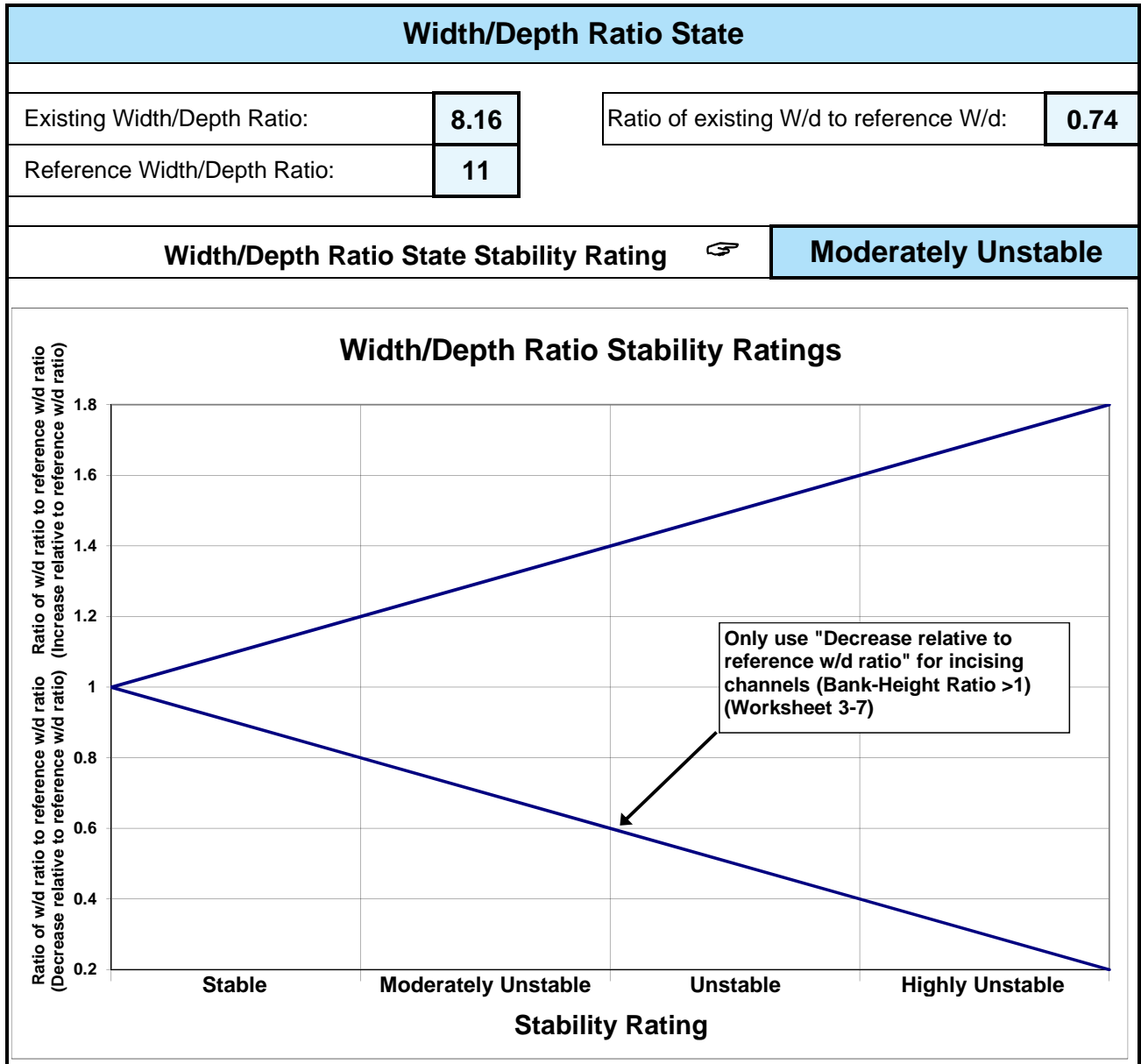
## Worksheet 5-11. Channel blockages.

Channel Blockages		
Stream: <b>Northfield Gulch A4a+ Poor</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>Lee, Sumner, Jara, Leah</b>		Date: <b>11/8/2012</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
D1 None	Minor amounts of small, floatable material.	<input type="checkbox"/>
D2 Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input checked="" type="checkbox"/>
D3 Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input type="checkbox"/>
D4 Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
D5 Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
D6 Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
D7 Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
D8 Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
D9 Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
D10 Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

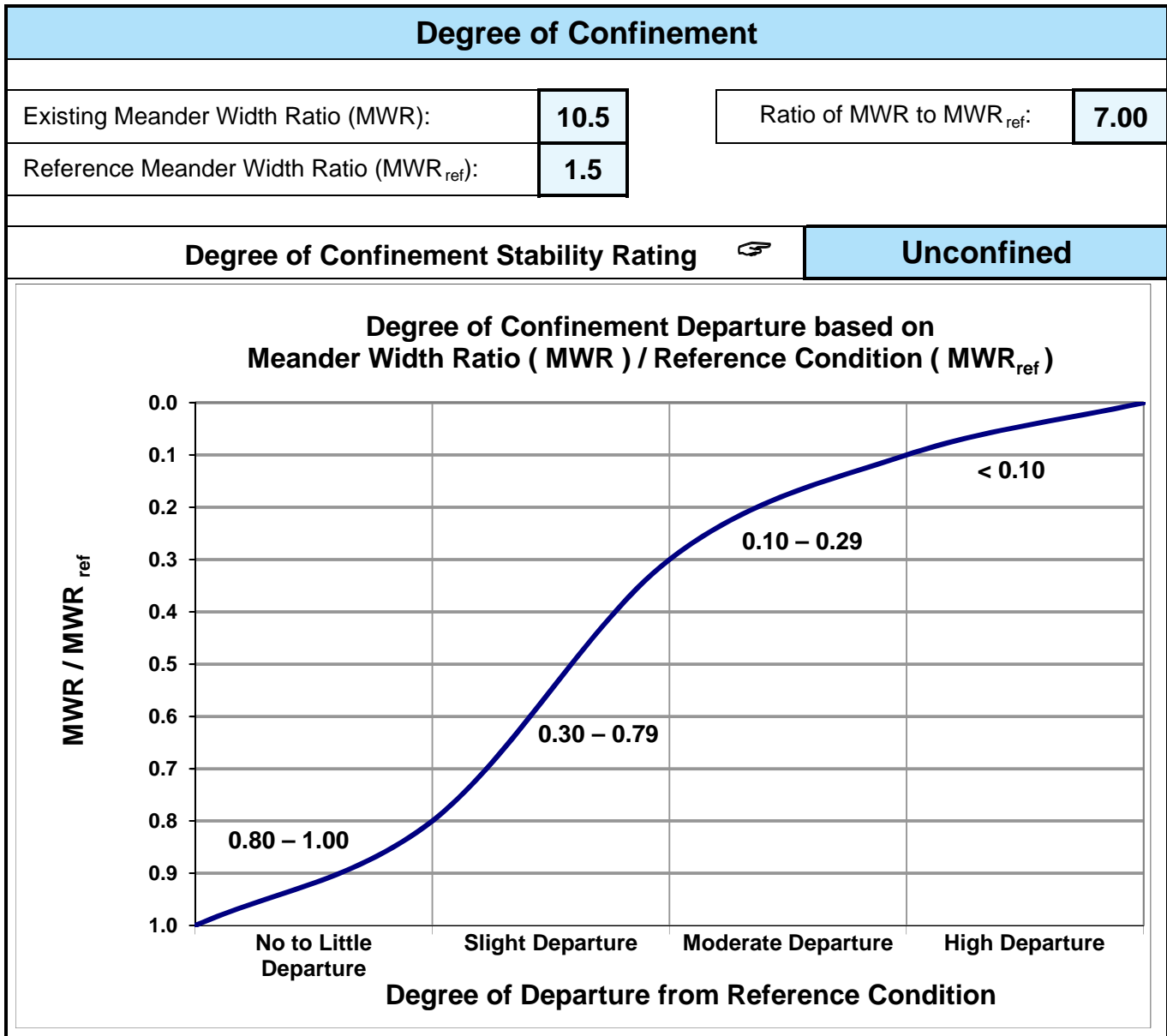
**Worksheet 5-12.** Degree of channel incision.



Worksheet 5-13. Width/depth ratio state.



**Worksheet 5-14.** Degree of channel confinement (lateral containment).



**Worksheet 5-15. Pfanckuch channel stability rating.**

Stream: Northfield Gulch A4+ Poor		Location: Pike National Forest, CO		Valley Type: I		Observers: Lee, Summer, Jara, Leah		Date: 11/8/2012															
Loca-tion	Key Category	Excellent		Good		Fair		Poor															
		Description	Rating	Description	Rating	Description	Rating	Description	Rating														
Upper banks	1	Landform slope	Bank slope gradient <30%.	2	Bank slope gradient 30–40%.	4	Bank slope gradient 40–60%.	6	Bank slope gradient > 60%.														
	2	Mass erosion	No evidence of past or future mass erosion.	3	Infrequent. Mostly healed over. Low future potential.	6	Frequent or large, causing sediment nearly yearlong.	9	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.														
	3	Debris jam potential	Essentially absent from immediate channel area.	2	Present, but mostly small twigs and limbs.	4	Moderate to heavy amounts, mostly larger sizes.	6	Moderate to heavy amounts, predominantly larger sizes.														
	4	Vegetative bank protection	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	3	70–90% density. Fewer species or less vigor suggest less dense or deep root mass.	6	50–70% density. Lower vigor and fewer species from a shallow, discontinuous root mass.	9	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.														
Lower banks	5	Channel capacity	Bankfull stage sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0.	1	Bankfull stage is contained within banks. Width/depth ratio departure from reference width/depth ratio = 1.0–1.2. Bank-Height Ratio (BHR) = 1.0–1.1.	2	Bankfull stage is not contained. Width/depth ratio departure from reference width/depth ratio = 1.2–1.4. Bank-Height Ratio (BHR) = 1.1–1.3.	3	Bankfull stage is not contained; over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.														
	6	Bank rock content	> 65% with large angular boulders. 12"+ common.	2	40–65%. Mostly boulders and small cobbles 6–12".	4	20–40%. Most in the 3–6" diameter class.	6	<20% rock fragments of gravel sizes, 1–3" or less.														
	7	Obstructions to flow	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	2	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	4	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	6	Frequent obstructions and deflectors cause bank erosion yearlong. Sediment traps full, channel migration occurring.														
	8	Cutting	Little or none. Infrequent raw banks	4	Some, intermittently at outcoves and constrictions. Raw banks may be up to 12".	9	Significant. Cuts 12–24" high. Root mat overhangs and sloughing frequent.	12	Almost continuous cuts, some over 24" high. Failure of overhangs frequent.														
	9	Deposition	Little or no enlargement of channel or point bars.	4	Some new bar increase, mostly from coarse gravel.	8	Moderate deposition of new gravel and coarse sand on old and some new bars.	13	Extensive deposit of predominantly fine particles. Accelerated bar development.														
Bottom	10	Rock angularity	Sharp edges and corners. Plane surfaces rough.	1	Rounded corners and edges. Surfaces smooth and flat.	2	Corners and edges well rounded in 2 dimensions.	3	Well rounded in all dimensions, surfaces smooth.														
	11	Brightness	Surfaces dull, dark or stained. Generally not bright.	1	Mostly dull, but may have <35% bright surfaces.	2	Mixture dull and bright, i.e., 35–65% mixture range.	3	Predominantly bright, > 65% exposed or scoured surfaces.														
	12	Consolidation of particles	Assorted sizes tightly packed or overlapping.	2	Moderately packed with some overlapping.	4	Mostly loose assortment with no apparent overlap.	6	No packing evident. Loose assortment, easily moved.														
	13	Bottom size distribution	No size change evident. Stable material 80–100%.	4	Distribution shift light. Stable material 50–80%.	8	Moderate change in sizes. Stable materials 20–50%.	12	Marked distribution change. Stable materials 0–20%.														
	14	Scouring and deposition	<5% of bottom affected by scour or deposition.	6	5–30% affected. Scour at constrictions and where grades steepen. Some deposition in pools.	12	30–50% affected. Deposits and scour at obstructions, constrictions and bends. Some filling of pools.	20	More than 50% of the bottom in a state of flux or change nearly yearlong.														
	15	Aquatic vegetation	Abundant growth moss-like, dark green perennial. In swift water too.	1	Common. Algae forms in low velocity and pool areas. Moss here too.	2	Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick.	3	Perennial types scarce or absent. Yellow-green, short-term bloom may be present.														
		<b>Excellent total = 2</b>		<b>Good total = 8</b>		<b>Fair total = 19</b>		<b>Poor total = 104</b>															
Stream type	A1	A2	A3	A4	A5	A6	B1	B2	B3	B4	B5	B6	C1	C2	C3	C4	C5	C6	D3	D4	D5	D6	
Good (Stable)	38-43	38-43	54-90	60-95	60-95	50-80	38-45	38-45	40-60	49-68	40-60	40-60	38-50	38-50	60-85	70-90	70-90	80-85	85-107	85-107	85-107	85-107	67-98
Fair (Mod. unstable)	44-47	44-47	91-125	96-132	96-142	81-110	46-58	46-58	61-78	65-84	69-88	61-78	51-61	51-61	86-105	91-110	91-110	86-105	108-132	108-132	108-132	108-132	99-125
Poor (Unstable)	48+	48+	130+	143+	143+	111+	59+	59+	79+	85+	89+	79+	62+	62+	106+	111+	111+	106+	133+	133+	133+	133+	126+
Stream type	DA3	DA4	DA5	DA6	E3	E4	E5	E6	F1	F2	F3	F4	F5	F6	G1	G2	G3	G4	G5	G6			
Good (Stable)	40-63	40-63	40-63	40-63	40-63	50-75	50-75	40-63	60-85	60-85	85-110	85-110	90-115	80-95	40-60	40-60	40-60	85-107	90-112	90-112	85-107		
Fair (Mod. unstable)	64-86	64-86	64-86	64-86	64-86	76-96	76-96	64-86	86-105	86-105	111-125	111-125	116-130	96-110	61-78	61-78	108-120	108-120	113-125	108-120			
Poor (Unstable)	87+	87+	87+	87+	87+	97+	97+	87+	106+	106+	126+	126+	131+	111+	79+	79+	121+	121+	126+	126+	121+		
		<b>Grand total = 133</b>		<b>Existing stream type = A4a+</b>		<b>*Potential stream type = A4a+</b>		<b>Modified channel stability rating = Poor</b>															

\*Rating is adjusted to potential stream type, not existing.

## BANCS Model – Streambank Erosion

**Worksheet 5-18.** Annual streambank erosion estimates.

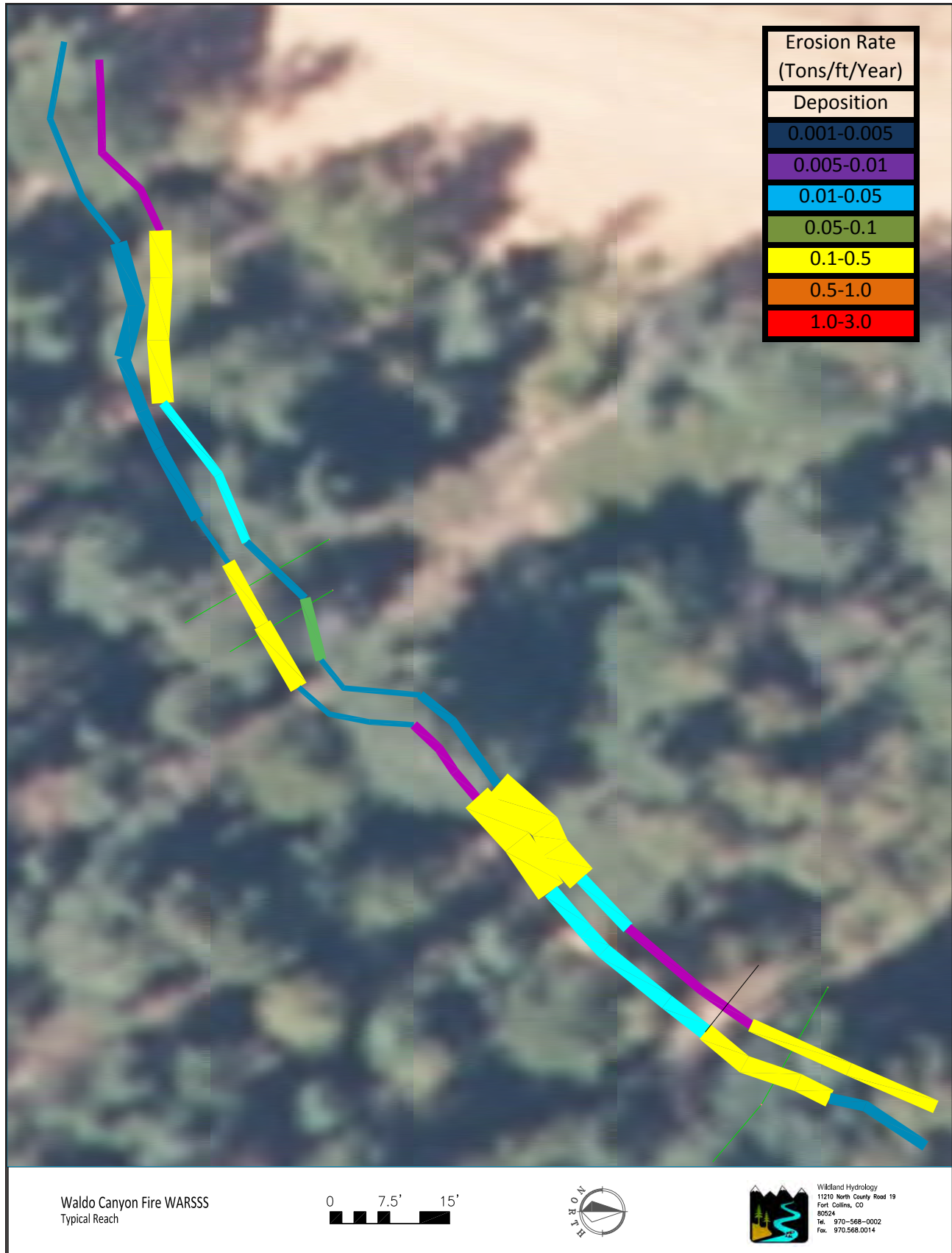
Stream: <b>Northfield Gulch A4a+ Poor</b>		Location: <b>A4a+ Poor</b>					
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>190</b>				Date: <b>11/8/2012</b>	
Observers: <b>Lee, Sumner, Jaram Leah</b>		Valley Type: <b>I</b>			Stream Type: <b>A4a+</b>		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 3-11) (adjective)	NBS rating (Worksheet 3-12) (adjective)	Bank erosion rate (Figure 3-9 or 3-10) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [(4)×(5)×(6)] (ft <sup>3</sup> /yr)	Erosion Rate (tons/yr/ft) {[(7)/27] × 1.3 / (5)}
1. L0+00 to 0+04	Moderate	Moderate	0.303	4.0	2.3	2.79	0.03360
2. L0+04 to 0+27	Moderate	Low	0.173	23.0	1.0	3.90	0.00820
3. L0+27 to 0+51	Very High	Very High	0.872	24.0	2.8	58.60	0.11760
4. L0+51 to 0+73	Moderate	Moderate	0.253	22.0	1.2	6.68	0.01460
5. L0+73 to 0+83	Low	Low	0.036	10.0	1.0	0.36	0.00170
6. L0+83 to 0+92	High	Very High	0.872	9.0	1.4	10.99	0.05880
7. L0+92 to 1+02	Very Low	Low	0.004	10.0	0.7	0.03	0.00013
8. L1+02 to 1+21	Low	Low	0.036	19.0	1.2	0.81	0.00210
9. L1+21 to 1+39	Very High	Very High	0.872	18.0	3.8	59.65	0.15950
10. L1+39 to 1+48	High	Moderate	0.380	8.0	1.6	4.86	0.02930
11. L1+48 to 1+68	Moderate	Low	0.153	20.0	1.2	3.67	0.00880
12. L1+68 to 1+90	High	Moderate	0.380	19.0	1.7	12.27	0.03110
13. R0+00 to 0+28	Low	Low	0.036	28.0	0.8	0.80	0.00140
14. R0+28 to 0+44	Low	Low	0.036	16.0	2.2	1.26	0.00380
15. R0+44 to 0+67	Low	Very Low	0.018	23.0	1.7	0.68	0.00140
16. R0+67 to 0+74	Very Low	Very Low	0.002	7.0	0.7	0.01	0.00272
17. R0+74 to 0+83	Moderate	Low	0.153	9.0	1.8	2.48	0.01330
18. R0+83 to 0+93	High	Low	0.250	10.0	2.3	5.75	0.02770
19. R0+93 to 1+07	Low	Low	0.036	14.0	0.7	0.35	0.00120
20. R1+07 to 1+21	Moderate	Low	0.153	14.0	1.2	2.57	0.00880
21. R1+21 to 1+37	Very High	Very High	0.872	16.0	3.8	53.02	0.15950



**Worksheet 5-18, con't.** Annual streambank erosion estimates.

Stream: <b>Northfield Gulch A4a+ Poor</b>		Location: <b>A4a+ Poor</b>					
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>190</b>				Date: <b>11/8/2012</b>	
Observers: <b>Lee, Sumner, Jaram Leah</b>		Valley Type: <b>I</b>			Stream Type: <b>A4a+</b>		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 3-11) (adjective)	NBS rating (Worksheet 3-12) (adjective)	Bank erosion rate (Figure 3-9 or 3-10) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [(4)×(5)×(6)] (ft <sup>3</sup> /yr)	Erosion Rate (tons/yr/ft) {[ (7)/27 ] × 1.3 / (5)}
22 R1+37 to 1+43	High	Moderate	0.380	6.0	2.0	4.56	0.03660
23 R1+43 to 1+64	Low	Low	0.036	21.0	1.0	0.75	0.00170
24 R1+64 to 1+82	Moderate	Low	0.153	18.0	2.3	6.33	0.01690
25 R1+82 to 1+90	Low	Low	0.036	8.0	1.4	0.40	0.00240
26							
27							
28							
29							
30							
31							
32							
33							
34							
35							
36							
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					Total Erosion (ft <sup>3</sup> /yr)	<b>243.55</b>	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					Total Erosion (yds <sup>3</sup> /yr)	<b>9.02</b>	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					Total Erosion (tons/yr)	<b>11.73</b>	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					Unit Erosion Rate (tons/yr/ft)	<b>0.0617</b>	

### Streambank Erosion Map



# FLOWSED Model – Total Annual Sediment Yield

Worksheet 19a. Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Stream: <b>Waldo Reference and Representative Reaches</b>		Location: <b>A4a+ Poor (Northfield)</b>		Gage Station #: <b>N/A</b>		Stream Type: <b>A4a+</b>		Date: <b>11/08/2012</b>						
Observer: <b>L,L,S,J</b>		Valley Type: <b>II</b>		Bankfull discharge (cfs)		Bankfull bedload (kg/s)		Bankfull suspended bedload (mg/l)						
Equation type		Intercept		Coefficient		Exponent		Form (e.g., linear, non-linear, etc.)		Equation name				
1. Bedload (dimensionless)		-0.0113		1.0139		2.1929		Non-Linear		Pagosa Springs Reference Curve				
2. Suspended sediment (dimensionless)		0.0636		0.9326		2.4085		Non-Linear		Pagosa Springs Reference Curve				
3. User-defined relations (bedload)														
4. User-defined relations (suspended sediment)														
Notes: Pre-Fire Flow Duration Curve, Good/Fair Sediment Curves, Good/Fair Regional Sediment Curves														
From dimensioned flow-duration curve			From sediment rating curves			Calculate			Calculate sediment yield					
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Flow exceedence (%)	Daily mean discharge (cfs)	Mid-ordinate (%)	Time increment (percent)	Time increment (days)	Mid-ordinate streamflow (cfs)	Dimensionless streamflow (Q/Q <sub>50</sub> )	Dimensionless suspended sediment discharge (S/S <sub>50</sub> )	Suspended sediment discharge (tons/day)	Dimensionless bedload discharge (b <sub>j</sub> /b <sub>50</sub> )	Bedload (tons/day)	Time adjusted streamflow (cfs)	Suspended sediment [(6)×(9)] (tons)	Bedload sediment [(6)×(11)] (tons)	Suspended + bedload [(13)+(14)] (tons)
100.000	0.0													
90.000	0.0	95.00	10.00	36.50	0.0	0.06	7.7	0.0	0.0051	0.00	0.10	0.00	0.00	0.00
80.000	0.0	85.00	10.00	36.50	0.0	0.06	7.7	0.0	0.0051	0.00	0.10	0.00	0.00	0.00
70.000	0.0	75.00	10.00	36.50	0.0	0.06	7.7	0.0	0.0051	0.00	0.10	0.00	0.00	0.00
60.000	0.0	65.00	10.00	36.50	0.0	0.06	7.7	0.0	0.0051	0.00	0.10	0.00	0.00	0.00
50.000	0.0	55.00	10.00	36.50	0.0	0.06	7.7	0.0	0.0051	0.00	0.10	0.00	0.00	0.00
40.000	0.0	45.00	10.00	36.50	0.0	0.06	7.7	0.0	0.0051	0.00	0.10	0.00	0.00	0.00
30.000	0.0	35.00	10.00	36.50	0.0	0.18	7.8	0.0	0.0055	0.00	0.30	0.00	0.00	0.00
20.000	0.0	25.00	10.00	36.50	0.0	0.24	7.8	0.0	0.0061	0.00	0.40	0.00	0.00	0.00
10.000	0.1	15.00	10.00	36.50	0.1	0.35	8.4	0.0	0.0081	0.00	0.60	0.00	0.00	0.00
5.000	0.1	7.50	5.00	18.25	0.1	0.59	11.9	0.0	0.0156	0.04	0.50	0.00	0.73	0.73
4.000	0.1	4.50	1.00	3.65	0.1	0.76	18.2	0.0	0.0246	0.09	0.13	0.00	0.33	0.33
3.000	0.2	3.50	1.00	3.65	0.2	0.88	25.5	0.0	0.0326	0.09	0.15	0.00	0.33	0.33
2.000	0.2	2.50	1.00	3.65	0.2	1.00	35.9	0.0	0.0423	0.13	0.17	0.00	0.47	0.47
1.500	0.2	1.75	0.50	1.83	0.2	1.18	58.3	0.0	0.0598	0.22	0.10	0.00	0.40	0.40
1.000	0.3	1.25	0.50	1.83	0.2	1.35	92.7	0.0	0.0816	0.26	0.12	0.00	0.47	0.47
0.900	0.3	0.95	0.10	0.37	0.3	1.59	146.9	0.0	0.1109	0.39	0.03	0.00	0.14	0.14
0.800	0.3	0.85	0.10	0.37	0.3	1.65	146.9	0.0	0.1109	0.43	0.03	0.00	0.16	0.16
0.700	0.3	0.75	0.10	0.37	0.3	1.76	146.9	0.0	0.1109	0.52	0.03	0.00	0.19	0.19
0.600	0.3	0.65	0.10	0.37	0.3	1.88	146.9	0.0	0.1109	0.56	0.03	0.00	0.20	0.20
0.500	0.4	0.55	0.10	0.37	0.3	2.00	146.9	0.0	0.1109	0.65	0.03	0.00	0.24	0.24
0.250	0.4	0.38	0.25	0.91	0.4	2.24	146.9	0.0	0.1109	0.86	0.10	0.00	0.78	0.78
0.100	0.5	0.18	0.15	0.55	0.4	2.53	146.9	0.0	0.1109	1.12	0.06	0.00	0.61	0.61
0.050	0.5	0.08	0.05	0.18	0.5	2.82	146.9	0.0	0.1109	1.43	0.02	0.00	0.26	0.26
0.010	0.5	0.03	0.04	0.15	0.5	3.06	146.9	0.0	0.1109	1.68	0.02	0.00	0.25	0.25
0.005	0.5	0.01	0.01	0.02	0.5	3.18	146.9	0.0	0.1109	1.81	0.00	0.00	0.03	0.03
0.001	0.5	0.00	0.00	0.01	0.5	3.18	146.9	0.0	0.1109	1.81	0.00	0.00	0.03	0.03
Annual totals:											0.0	5.6	5.6	
											(tons/yr)	(tons/yr)	(tons/yr)	

**Worksheet 19b.** Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Stream: <b>Waldo Reference and Representative Reaches</b>		Gage Station #: <b>N/A</b>		Stream Type: <b>A4a+</b>		Date: <b>11/08/2012</b>									
Observers: <b>L.L.S.J</b>		Equation name		Bankfull discharge (cfs)		Valley Type: <b>II</b>									
Equation type		Form (e.g., linear, non-linear, etc.)		Bankfull bedload (kg/s)		Bankfull suspended (mg/l)									
1. Bedload (dimensionless)		Pagosa Springs Reference Curve		0.17		0.0305									
2. Suspended sediment (dimensionless)		Pagosa Springs Reference Curve		0.17		77.5349									
3. User-defined relations (bedload)															
4. User-defined relations (suspended sediment)															
Notes: Post-Fire Flow Duration Curve, Poor Sediment Curves, Poor Regional Sediment Curves															
From dimensioned flow-duration curve				From sediment rating curves											
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)								
Flow exceedence (%)	Daily mean discharge (cfs)	Mid-ordinate (%)	Time increment (percent)	Time increment (days)	Mid-ordinate streamflow (cfs)	Dimensionless streamflow	Dimensionless suspended sediment discharge (S/S <sub>50</sub> )								
(15)	(14)	(13)	(12)	(11)	(10)	(9)	(8)								
Suspended bedload [(15)×(14)] (tons)	Bedload sediment [(13)×(11)] (tons)	Suspended sediment [(6)×(9)] (tons)	Time adjusted streamflow (cfs)	Bedload (tons/day)	Dimensionless bedload discharge (b <sub>f</sub> /b <sub>50</sub> )	Suspended sediment discharge (tons/day)	Dimensionless suspended sediment discharge (S/S <sub>50</sub> )								
(15)	(14)	(13)	(12)	(11)	(10)	(9)	(8)								
Calculate sediment yield	Calculate	Calculate	Calculate	Calculate	Calculate	Calculate	Calculate								
100.000	0.0	95.00	10.00	36.50	0.0	0.06	7.7	0.0	0.0051	0.22	0.10	0.00	8.03	8.03	
90.000	0.0	85.00	10.00	36.50	0.0	0.06	7.7	0.0	0.0051	0.22	0.10	0.00	8.03	8.03	
80.000	0.0	75.00	10.00	36.50	0.0	0.06	7.7	0.0	0.0051	0.22	0.10	0.00	8.03	8.03	
70.000	0.0	65.00	10.00	36.50	0.0	0.06	7.7	0.0	0.0051	0.22	0.10	0.00	8.03	8.03	
60.000	0.0	55.00	10.00	36.50	0.0	0.06	7.7	0.0	0.0051	0.22	0.10	0.00	8.03	8.03	
50.000	0.0	45.00	10.00	36.50	0.0	0.06	7.7	0.0	0.0051	0.22	0.10	0.00	8.03	8.03	
40.000	0.0	35.00	10.00	36.50	0.0	0.18	7.8	0.0	0.0055	0.22	0.30	0.00	8.03	8.03	
30.000	0.1	25.00	10.00	36.50	0.0	0.24	7.8	0.0	0.0061	0.26	0.40	0.00	9.49	9.49	
20.000	0.1	15.00	10.00	36.50	0.1	0.41	8.8	0.0	0.0095	0.39	0.70	0.00	14.24	14.24	
15.000	0.1	7.50	5.00	18.25	0.1	0.71	15.8	0.0	0.0213	0.91	0.60	0.18	16.61	16.79	
10.000	0.2	4.50	1.00	3.65	0.2	0.88	25.5	0.0	0.0326	1.38	0.15	0.04	5.04	5.08	
8.000	0.2	3.50	1.00	3.65	0.2	1.00	35.9	0.0	0.0423	1.81	0.17	0.07	6.61	6.68	
6.000	0.2	2.50	1.00	3.65	0.2	1.18	58.3	0.0	0.0598	2.59	0.20	0.11	9.45	9.56	
4.500	0.2	1.75	0.50	1.83	0.2	1.29	79.1	0.1	0.0736	3.20	0.11	0.09	5.84	5.93	
3.000	0.3	1.25	0.50	1.83	0.3	1.59	146.9	0.1	0.1109	5.05	0.14	0.22	9.22	9.44	
2.000	0.3	0.95	0.10	0.37	0.3	1.71	146.9	0.2	0.1109	5.92	0.03	0.06	2.16	2.22	
1.500	0.3	0.85	0.10	0.37	0.3	1.82	146.9	0.2	0.1109	6.91	0.03	0.08	2.52	2.60	
1.000	0.3	0.75	0.10	0.37	0.3	1.94	146.9	0.3	0.1109	7.99	0.03	0.11	2.92	3.03	
0.750	0.4	0.65	0.10	0.37	0.4	2.06	146.9	0.4	0.1109	9.16	0.03	0.14	3.34	3.48	
0.500	0.4	0.55	0.10	0.37	0.4	2.18	146.9	0.5	0.1109	10.41	0.04	0.18	3.80	3.98	
0.250	0.4	0.38	0.25	0.91	0.4	2.41	146.9	0.8	0.1109	13.26	0.10	0.71	12.10	12.81	
0.100	0.5	0.18	0.15	0.55	0.5	2.71	146.9	1.3	0.1109	17.37	0.07	0.73	9.51	10.24	
0.050	0.5	0.08	0.05	0.18	0.5	3.06	146.9	2.4	0.1109	23.16	0.03	0.43	4.23	4.66	
0.010	0.6	0.03	0.04	0.15	0.6	3.24	146.9	3.0	0.1109	26.44	0.02	0.44	3.86	4.30	
0.005	0.6	0.01	0.01	0.02	0.6	3.35	146.9	3.6	0.1109	28.77	0.00	0.07	0.53	0.60	
0.001	0.6	0.00	0.00	0.01	0.6	3.35	146.9	3.6	0.1109	28.77	0.00	0.05	0.42	0.47	
				<b>Annual totals:</b>				<b>3.7</b>	<b>178.1</b>	<b>3.7</b>	<b>178.1</b>	<b>3.7</b>	<b>178.1</b>	<b>3.7</b>	<b>178.1</b>

## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>Northfield Gulch A4a+ Poor</b>		Stream Type: <b>A4a+</b>	
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>	
Observers: <b>Lee, Sumner, Jara, Leah</b>		Date: <b>11/08/2012</b>	
<b>Enter Required Information for Existing Condition</b>			
4.1	$D_{50}$	Riffle bed material $D_{50}$ (mm)	
0.0	$\hat{D}_{50}$	Bar sample $D_{50}$ (mm)	
0.312	$D_{max}$	Largest particle from <b>Bed Material</b> (ft)	95 (mm) 304.8 mm/ft
0.13000	$S$	Existing bankfull water surface slope (ft/ft)	
0.19	$d$	Existing bankfull mean depth (ft)	
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment	
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>			
0.00	$D_{50}/\hat{D}_{50}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 (D_{50}/\hat{D}_{50})^{-0.872}$
23.11	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 (D_{max}/D_{50})^{-0.887}$
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED: <b>2</b>
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>			
N/A	$d$	Required bankfull mean depth (ft)	$d = \frac{\tau^* (\gamma_s - 1) D_{max}}{S}$ (use $D_{max}$ in ft)
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>			
N/A	$S$	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^* (\gamma_s - 1) D_{max}}{d}$ (use $D_{max}$ in ft)
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading			
<b>Sediment Competence Using Dimensional Shear Stress</b>			
1.541	Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d) $\gamma = 62.4$ , $d =$ existing depth, $S =$ existing slope		
Shields 122.4	CO 209	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ (Figure 5-49)	
Shields 1.209	CO 0.528	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) (Figure 5-49)	
Shields 0.15	CO 0.07	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm) $\tau =$ predicted shear stress, $\gamma = 62.4$ , $S =$ existing slope	$d = \frac{\tau}{\gamma S}$
Shields 0.1020	CO 0.0445	Predicted slope required to initiate movement of measured $D_{max}$ (mm) $\tau =$ predicted shear stress, $\gamma = 62.4$ , $d =$ existing depth	$S = \frac{\tau}{\gamma d}$
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input checked="" type="checkbox"/> Degrading			

## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>Northfield Gulch A4a+ Poor</b>	Stream Type: <b>A4a+</b>
Location: <b>Pike National Forest, CO</b>	Valley Type: <b>I</b>
Observers: <b>Lee, Sumner, Jara, Leah</b>	Date: <b>11/08/2012</b>
Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)	Stability Rating (Check Appropriate Rating)
Stream Type at potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	<input checked="" type="checkbox"/> Stable
(E→C), (C→High W/d C)	<input type="checkbox"/> Moderately Unstable
(G→F), (F→D), (C→F)	<input type="checkbox"/> Unstable
(C→D), (B→G), (D→G), (C→G), (E→G)	<input type="checkbox"/> Highly Unstable

Worksheet 5-25. Lateral stability.

Stream: <b>Northfield Gulch A4a+ Poor</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Lee, Sumner, Jara, Leah</b>		Date: <b>11/08/2012</b>			
Lateral stability criteria (choose one stability category for each criterion 1–5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	4
	(2)	(4)	(6)	(8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	N/A
	(1)	(2)	(3)	(4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		N/A
	(1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	6
	(2)	(4)	(6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	1
	(1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>11</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input checked="" type="checkbox"/>	<i>Unstable</i> 13 – 21 <input type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	

**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>Northfield Gulch A4a+ Poor</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Lee, Sumner, Jara, Leah</b>		Date: <b>11/08/2012</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
<b>1 Sediment competence (Worksheet 5-22)</b>	Sufficient depth and/or slope to transport largest size available <b>(2)</b>	Trend toward insufficient depth and/or slope-slightly incompetent <b>(4)</b>	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material <b>(6)</b>	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size <b>(8)</b>	<b>2</b>
<b>2 Sediment Capacity (POWERSED) (Worksheet 5-20)</b>	Sufficient capacity to transport annual load <b>(2)</b>	Trend toward insufficient sediment capacity <b>(4)</b>	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand <b>(6)</b>	Reduction over 25% of annual sediment yield for bedload and/or suspended sand <b>(7)</b>	<b>2</b>
<b>3 W/d Ratio State (Worksheet 5-13)</b>	1.0 – 1.2 <b>(2)</b>	1.2 – 1.4 <b>(4)</b>	1.4 – 1.6 <b>(6)</b>	>1.6 <b>(8)</b>	<b>4</b>
<b>4 Stream Succession States (Worksheet 5-24)</b>	Current stream type at potential or does not indicate deposition/aggradation <b>(2)</b>	(E→C) <b>(4)</b>	(C→High W/d C), (B→High W/d B), (C→F) <b>(6)</b>	(C→D), (F→D) <b>(8)</b>	<b>2</b>
<b>5 Depositional Patterns (Worksheet 5-10)</b>	B1 <b>(1)</b>	B2, B4 <b>(2)</b>	B3, B5 <b>(3)</b>	B6, B7, B8 <b>(4)</b>	<b>NA</b>
<b>6 Debris / Blockages (Worksheet 5-11)</b>	D1, D2, D3 <b>(1)</b>	D4, D7 <b>(2)</b>	D5, D8 <b>(3)</b>	D6, D9, D10 <b>(4)</b>	<b>1</b>
<b>Total Points</b>					<b>11</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
<b>Vertical Stability for Excess Deposition / Aggradation (use total points and check stability rating)</b>	<i>No Deposition</i> 10 – 14 <input checked="" type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input type="checkbox"/>	<i>Aggradation</i> > 30 <input type="checkbox"/>	



Worksheet 5-27. Vertical stability – degradation.

Stream: <b>Northfield Gulch A4a+ Poor</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Lee, Sumner, Jara, Leah</b>		Date: <b>11/08/2012</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>1 Sediment Competence (Worksheet 5-22)</b>	Does not indicate excess competence <b>(2)</b>	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed <b>(4)</b>	$D_{100}$ of bed moved <b>(6)</b>	Particles much larger than $D_{100}$ of bed moved <b>(8)</b>	<b>8</b>
<b>2 Sediment Capacity (POWERSED) (Worksheet 5-20)</b>	Does not indicate excess capacity <b>(2)</b>	Slight excess energy: up to 10% increase above reference <b>(4)</b>	Excess energy sufficient to increase load up to 50% of annual load <b>(6)</b>	Excess energy transporting more than 50% of annual load <b>(8)</b>	<b>2</b>
<b>3 Degree of Channel Incision (BHR) (Worksheet 5-12)</b>	1.00 – 1.10 <b>(2)</b>	1.11 – 1.30 <b>(4)</b>	1.31 – 1.50 <b>(6)</b>	> 1.50 <b>(8)</b>	<b>2</b>
<b>4 Stream Succession States (Worksheets 5-12 and 5-24)</b>	Does not indicate incision or degradation <b>(2)</b>	If BHR > 1.1 and stream type has W/d between 5–10 <b>(4)</b>	If BHR > 1.1 and stream type has W/d less than 5 <b>(6)</b>	(B→G), (C→G), (E→G), (D→G) <b>(8)</b>	<b>2</b>
<b>5 Confinement (MWR / MWR<sub>ref</sub>) (Worksheet 5-14)</b>	0.80 – 1.00 <b>(1)</b>	0.30 – 0.79 <b>(2)</b>	0.10 – 0.29 <b>(3)</b>	< 0.10 <b>(4)</b>	<b>2</b>
<b>Total Points</b>					<b>16</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation (use total points and check stability rating)</b>	<i>Not Incised</i> 9 – 11 <input type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input checked="" type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input type="checkbox"/>	<i>Degradation</i> > 27 <input type="checkbox"/>	

**Worksheet 5-28.** Channel enlargement.

Stream: <b>Northfield Gulch A4a+ Poor</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Lee, Sumner, Jara, Leah</b>		Date: <b>11/08/2012</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1-4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	8
	(2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	4
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	2
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	8
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>22</b>
<b>Category Point Range</b>					
<b>Channel Enlargement Prediction (use total points and check stability rating)</b>	<i>No Increase</i> 8 – 10 <input type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input checked="" type="checkbox"/>	<i>Extensive</i> > 24 <input type="checkbox"/>	

Worksheet 5-29. Overall sediment supply.

Stream: <b>Northfield Gulch A4a+ Poor</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Lee, Sumner, Jara, Leah</b>		Date: <b>11/08/2012</b>			
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1–5)		Stability Rating		Points	Selected Points
1	Lateral Stability (Worksheet 5-25)	<i>Stable</i>		1	2
		<i>Mod. Unstable</i>		2	
		<i>Unstable</i>		3	
		<i>Highly Unstable</i>		4	
2	Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>		1	2
		<i>Mod. Deposition</i>		2	
		<i>Excess Deposition</i>		3	
		<i>Aggradation</i>		4	
3	Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>		1	4
		<i>Slightly Incised</i>		2	
		<i>Mod. Incised</i>		3	
		<i>Degradation</i>		4	
4	Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>		1	3
		<i>Slight Increase</i>		2	
		<i>Mod. Increase</i>		3	
		<i>Extensive</i>		4	
5	Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>		1	4
		<i>Fair: Mod. Unstable</i>		2	
		<i>Poor: Unstable</i>		4	
				<b>Total Points</b>	<b>15</b>
<b>Category Point Range</b>					
Overall Sediment Supply Rating (use total points and check stability rating)		<i>Low</i> 5 <input type="checkbox"/>	<i>Moderate</i> 6 – 10 <input type="checkbox"/>	<i>High</i> 11 – 15 <input checked="" type="checkbox"/>	<i>Very High</i> 16 – 20 <input type="checkbox"/>

Worksheet 5-32. Summary of stability condition categories.

Stream: <b>Northfield Gulch A4a+ Poor</b>		Location: <b>Pike National Forest, Colorado</b>	
Observers: <b>Lee, Sumner, Jara, Leah</b>	Date: <b>11/8/2012</b>	Stream Type: <b>A4a+</b>	Valley Type: <b>I</b>
<b>Channel Dimension</b>	Mean Bankfull Depth (ft): <b>0.19</b>	Bankfull Width (ft): <b>1.55</b>	Cross-Sectional Area (ft <sup>2</sup> ): <b>0.3</b>
<b>Channel Pattern</b>	Mean: $\lambda/W_{bkf}$ : <b>N/A</b>	$L_m/W_{bkf}$ : <b>N/A</b>	$R_c/W_{bkf}$ : <b>N/A</b>
<b>River Profile &amp; Bed Features</b>	Check: <input type="checkbox"/> Riffle/Pool <input checked="" type="checkbox"/> Step/Pool <input type="checkbox"/> Plane Bed <input type="checkbox"/> Convergence/Divergence <input type="checkbox"/> Dunes/Antidunes/Smooth Bed	Width of Flood-Prone Area (ft): <b>8.16</b>	Entrenchment Ratio: <b>1.1</b>
<b>Level III Stream Stability Indices</b>	Max Bankfull Depth (ft): <b>0.27</b>	Depth Ratio (max to mean): <b>1.42</b>	Pool Spacing: <b>NA</b>
<b>Bank Erosion Summary</b>	Flow Regime: <b>E1, E2, E8 &amp; Order: S-2(1)</b>	Meander Patterns: <b>N/A</b>	Debris/Channel Blockages: <b>D2</b>
<b>Sediment Capacity (POWERSED)</b>	Degree of Incision (Bank-Height Ratio): <b>1.0</b>	Degree of Incision Stability Rating: <b>Stable</b>	Modified Pfankuch Stability Rating (Numeric & Adjective Rating): <b>133 (Poor)</b>
<b>Entrainment/Competence</b>	Width/depth Ratio (W/d): <b>52</b>	Reference W/d Ratio (W/d <sub>ref</sub> ): <b>12.6</b>	W/d Ratio State Stability Rating: <b>Highly Unstable</b>
<b>Successional Stage Shift</b>	Meander Width Ratio (MWR): <b>10.45</b>	Reference MWR <sub>ref</sub> : <b>1.5</b>	MWR / MWR <sub>ref</sub> Stability Rating: <b>Slight Departure from Reference</b>
<b>Lateral Stability</b>	Length of Reach Studied (ft): <b>190</b>	Annual Streambank Erosion Rate: <b>11.73</b> (tons/yr)	Curve Used: <b>Colorado</b>
<b>Vertical Stability (Aggradation)</b>	<input type="checkbox"/> Sufficient Capacity <input type="checkbox"/> Insufficient Capacity <input checked="" type="checkbox"/> Excess Capacity	Remarks:	Remarks: <b>Used Yellowstone curve for very low BEHI</b>
<b>Vertical Stability (Degradation)</b>	Largest Particle from Bar Sample (mm): <b>95</b>	$\tau = 0.528$	$\tau^* = N/A$
<b>Channel Enlargement</b>	Existing Stream State (Type): <b>A4a+</b>	Required Stream State (Type): <b>A4a+</b>	Potential Stream State (Type): <b>A4a+</b>
<b>Sediment Supply (Channel Source)</b>	<input type="checkbox"/> Stable <input checked="" type="checkbox"/> Mod. Unstable <input type="checkbox"/> Unstable	Remarks/causes: <b>Highly Unstable</b>	Remarks/causes:
	<input checked="" type="checkbox"/> No Deposition <input type="checkbox"/> Mod. Deposition <input type="checkbox"/> Ex. Deposition	Remarks/causes: <b>Aggradation</b>	Remarks/causes:
	<input type="checkbox"/> Not Incised <input type="checkbox"/> Slightly Incised <input type="checkbox"/> Mod. Incised <input checked="" type="checkbox"/> Degradation	Remarks/causes: <b>Degradation</b>	Remarks/causes: <b>Noted obvious headcuts</b>
	<input type="checkbox"/> No Increase <input type="checkbox"/> Slight Increase <input checked="" type="checkbox"/> Mod. Increase <input type="checkbox"/> Extensive	Remarks/causes: <b>Mod. Increase</b>	Remarks/causes: <b>Noted channel widening &amp; incision</b>
	<input type="checkbox"/> Low <input type="checkbox"/> Moderate <input checked="" type="checkbox"/> High <input type="checkbox"/> Very High	Remarks/causes: <b>High</b>	Remarks/causes: <b>significant contribution from road, also noted sediment supply from both bed and banks</b>

## *Appendix C3*

# **A4a+ Stream Type**

## *Poor Stability South Reach*



# Table of Contents

## *Appendix C3: A4a+ Poor South Reach*

<b>Reach Location &amp; Overview.....</b>	<b>C3-2</b>
<b>Survey Summary.....</b>	<b>C3-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C3-6</b>
<b><i>Velocity, Classification &amp; Morphological Relations.....</i></b>	<b>C3-6</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b><i>Stability Indices.....</i></b>	<b>C3-10</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b><i>BANCS Model – Streambank Erosion.....</i></b>	<b>C3-20</b>
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b><i>FLOWSED Model – Total Annual Sediment Yield.....</i></b>	<b>C3-22</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b><i>Sediment Competence/Entrainment.....</i></b>	<b>C3-24</b>
Worksheet 5-22. Sediment competence calculations.	
<b><i>Channel Stability Ratings.....</i></b>	<b>C3-25</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b><i>Summary.....</i></b>	<b>C3-31</b>
Worksheet 5-32. Summary of stability condition categories.	

## A4a+ Poor South Reach Location & Overview

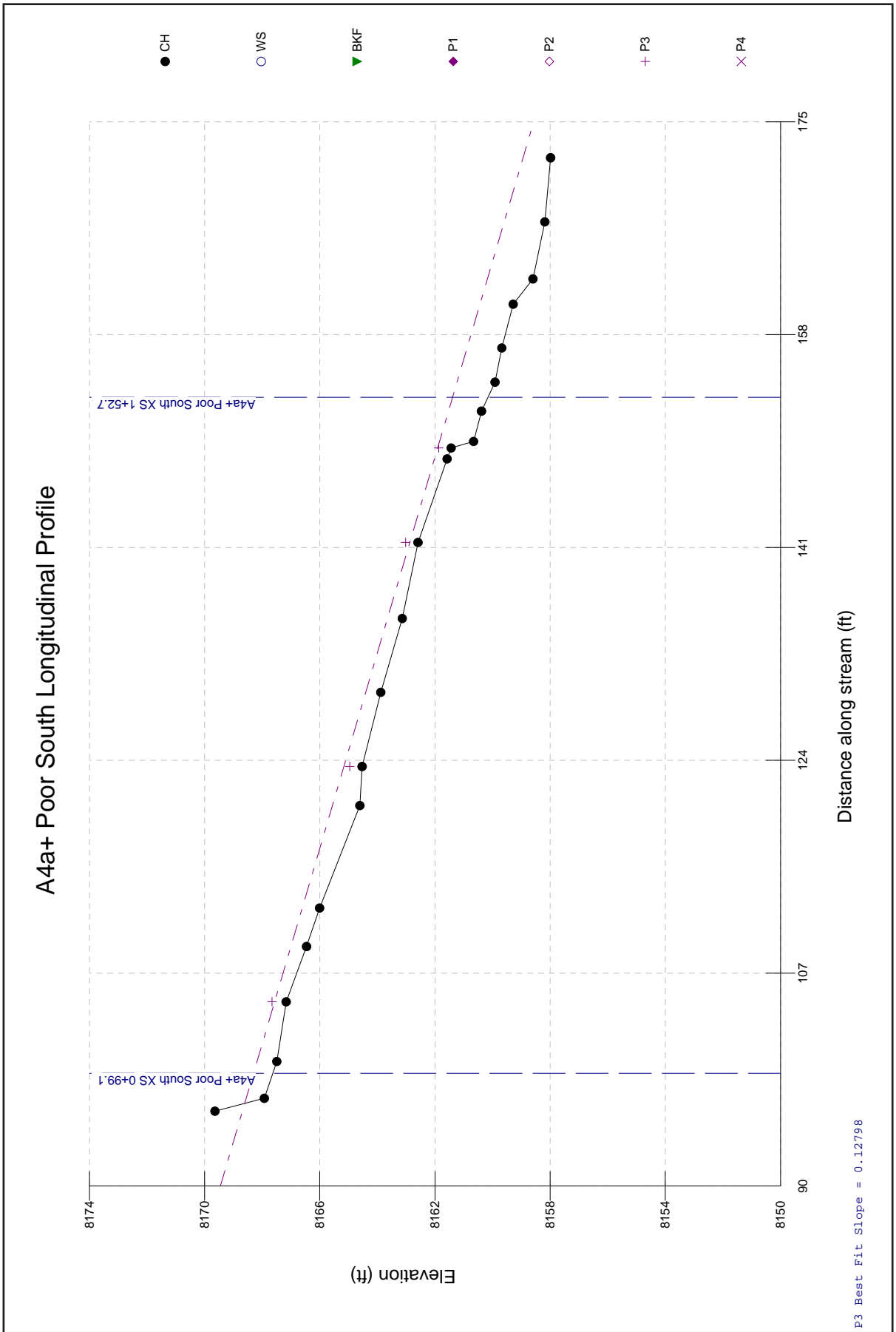
The A4a+ Poor south reach is a 1<sup>st</sup> order, ephemeral stream located in the Trail Creek Watershed (Figure C-2) with a high sediment supply due to channel processes. The photograph depicts the advancing headcut documenting both bed instability and accelerated streambank erosion. The stability rating is “Poor” due to degradation, active incision, and lateral instability. The streambank erosion rate is  $0.0355 \text{ tons/yr/ft}$ , more than an order of magnitude higher than its reference condition. The sediment supply also rates as *High* due to the same processes, including a *Moderate Increase* in channel enlargement. The overall “Poor” condition rating indicates a potential accelerated increase in flow-related sediment based on increased post-fire streamflow peak flows. The increase in water yield using the WRENSS model for this small, ephemeral channel of 0.32 cfs is  $0.6 \text{ acre-ft}$ . This increase corresponds with an increase in bedload using the FLOWSED model of  $1.7 \text{ tons/yr}$  and  $3.1 \text{ tons/yr}$  of suspended sediment.

The following graphs and summary worksheets provide the detail of the morphology, hydraulics, streambank erosion rates, and stability conditions responsible for the overall “Poor” rating.

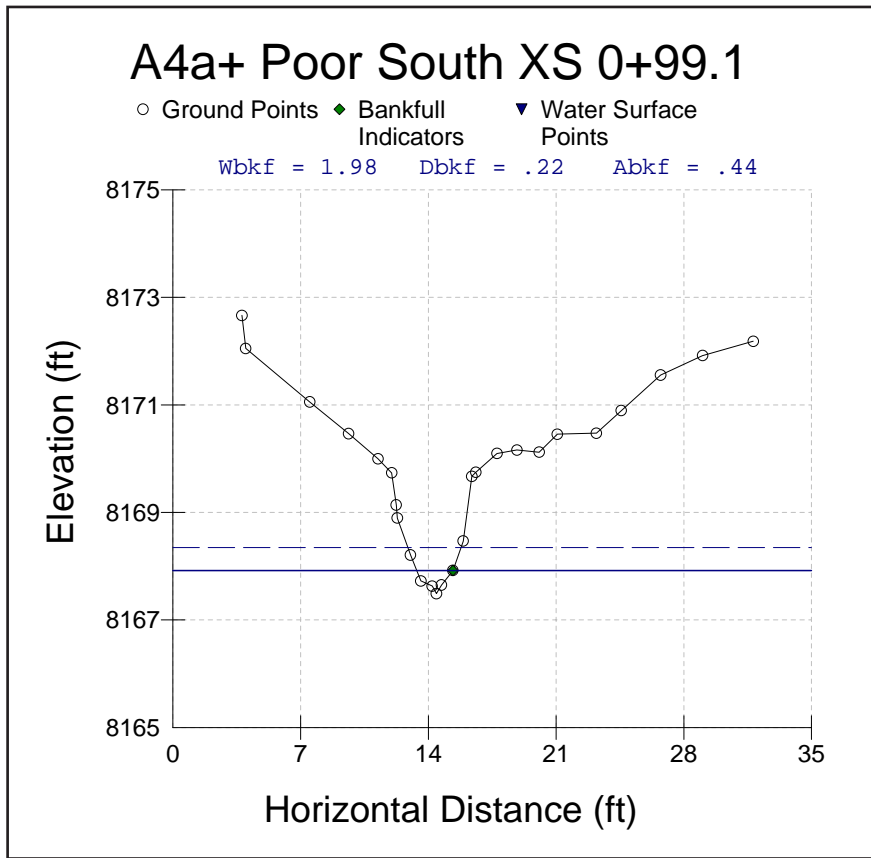




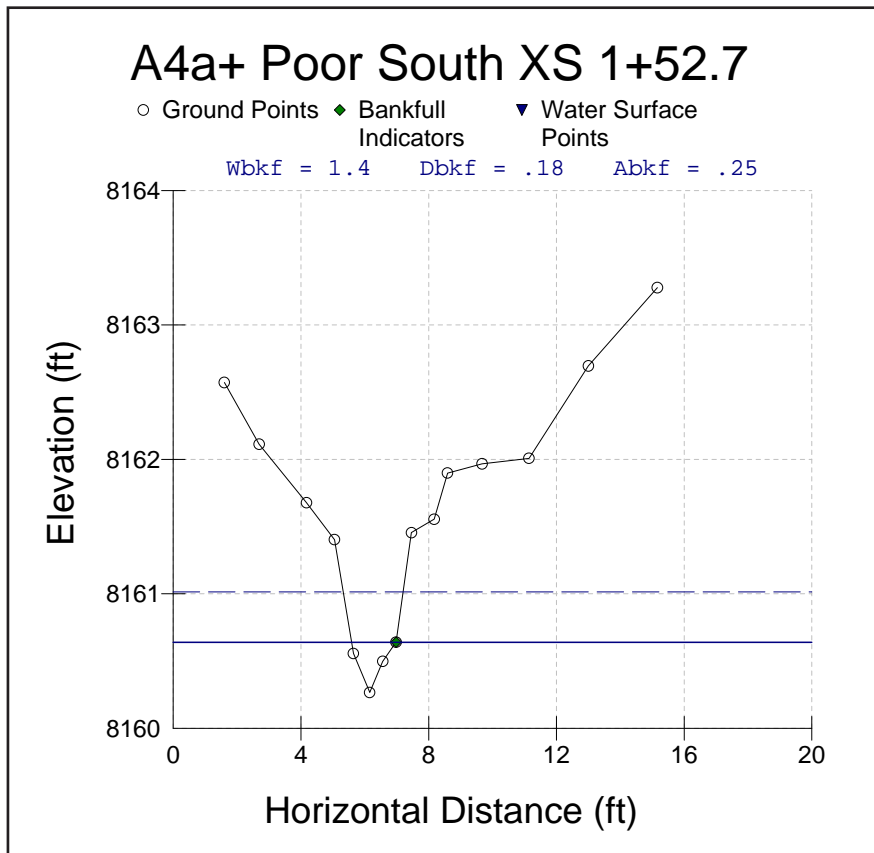
# Survey Summary



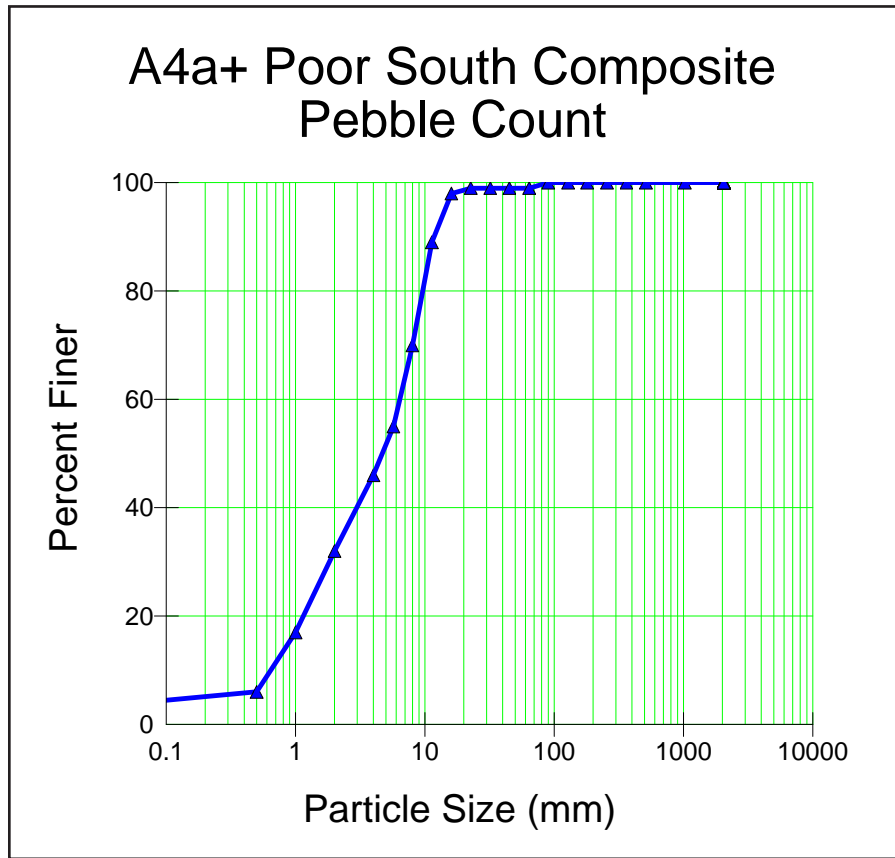
Longitudinal Profile (graph generated from RIVERMorph™)



Representative Cross-section 0+99.1 (graph generated from RIVERMorph™)



Cross-section 1+52.7 (graph generated from RIVERMorph™)



**Composite Pebble Count** (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates						
Stream:	Trail Creek, A4a+ Poor South			Location:	XS 0+99.1, Pike N.F., Colorado	
Date:	9/2/2010	Stream Type:	A4a+	Valley Type:	I	
Observers:	Chavez, Kasun & Gallagher			HUC:	___ - - - - -	
INPUT VARIABLES			OUTPUT VARIABLES			
Bankfull Riffle Cross-Sectional AREA	0.44	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.22	$d_{bkf}$ (ft)	
Bankfull Riffle WIDTH	1.98	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim (2 * d_{bkf}) + W_{bkf}$	2.42	$W_p$ (ft)	
$D_{84}$ at Riffle	10.4	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.03	$D_{84}$ (ft)	
Bankfull SLOPE	0.1280	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	0.18	R (ft)	
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness $R(ft) / D_{84}(ft)$	5.30	$R / D_{84}$	
Drainage Area	0.002	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.865	$u^*$ (ft/sec)	
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE	
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$			5.99	ft / sec	2.64	cfs
2. Roughness Coefficient: a) Manning's n from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n =$ <input type="text"/>				ft / sec		cfs
2. Roughness Coefficient: b) Manning's n from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n =$ <input type="text"/>				ft / sec		cfs
2. Roughness Coefficient: c) Manning's n from Jarrett (USGS): $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for Stream Types A1, A2, A3, B1, B2, B3, C2 & E3 $n =$ <input type="text" value="0.235"/>			0.73	ft / sec	0.32	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Darcy-Weisbach			7.17	ft / sec	3.15	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Hey			7.21	ft / sec	3.17	cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q =$ <input type="text"/> year $u = Q / A$				ft / sec		cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$				ft / sec		cfs
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation ( $R/D_{84}$ ) – Estimation Method 1						
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.						
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.						
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.						
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.						

**Worksheet 5-3.** Level II stream classification.

<b>Stream:</b> Trail Creek, A4a+ Poor South Reach	
<b>Basin:</b>	<b>Drainage Area:</b> acres <b>0.002</b> mi <sup>2</sup>
<b>Location:</b> Pike National Forest, Colorado	
<b>Twp.&amp;Rge:</b>	<b>Sec.&amp;Qtr.:</b>
<b>Cross-Section Monuments (Lat./Long.):</b> XS 0+99.1 <span style="float: right;"><b>Date:</b> 9/2/2010</span>	
<b>Observers:</b> Chavez, Kasun & Gallagher <span style="float: right;"><b>Valley Type:</b> I</span>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>1.98</b> ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A_{bkf} / W_{bkf}$ ).	<b>0.22</b> ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>0.44</b> ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>9.0</b> ft/ft
<b>Maximum DEPTH (<math>d_{max}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>0.43</b> ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>2.91</b> ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>1.47</b> ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the median or dominant diameter of channel materials, as sampled proportionately from the channel surface, between the bankfull stage and Thalweg elevations.	<b>4.76</b> mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.1280</b> ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope ( $S_{val} / S$ ).	<b>1.01</b>

<b>Stream Type</b>	<div style="border: 1px solid black; padding: 5px; display: inline-block;"><b>A4a+</b></div>	<b>See Classification Key (Figure 2-14)</b>
--------------------	--	---

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, A4a+ Poor South Reach</b>		Location: <b>Pike National Forest, Colorado</b>							
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/2/2010</b>		Valley Type: <b>I</b>		Stream Type: <b>A4a+</b>			
<b>River Reach Dimension Summary Data.....1</b>									
<b>Riffle Dimensions* ** *</b>	<b>Riffle Dimensions* ** *</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Width (W <sub>bkf</sub> )	1.7	1.4	2.0	ft	Riffle Cross-Sectional Area (A <sub>bkf</sub> ) (ft <sup>2</sup> )	0.3	0.3	0.4
	Mean Riffle Depth (d <sub>bkf</sub> )	0.20	0.18	0.22	ft	Riffle Width/Depth Ratio (W <sub>bkf</sub> / d <sub>bkf</sub> )	8.4	7.8	9.0
	Maximum Riffle Depth (d <sub>max</sub> )	0.40	0.37	0.43	ft	Max Riffle Depth to Mean Riffle Depth (d <sub>max</sub> /d <sub>bkf</sub> )	2.005	1.955	2.056
	Width of Flood-Prone Area (W <sub>fpa</sub> )	2.40	1.88	2.91	ft	Entrenchment Ratio (W <sub>fpa</sub> / W <sub>bkf</sub> )	1.41	1.35	1.47
	Riffle Inner Berm Width (W <sub>ib</sub> )				ft	Riffle Inner Berm Width to Riffle Width (W <sub>ib</sub> / W <sub>bkf</sub> )			
	Riffle Inner Berm Depth (d <sub>ib</sub> )				ft	Riffle Inner Berm Depth to Mean Depth (d <sub>ib</sub> / d <sub>bkf</sub> )			
	Riffle Inner Berm Area (A <sub>ib</sub> )				ft <sup>2</sup>	Riffle Inner Berm Area to Riffle Area (A <sub>ib</sub> / A <sub>bkf</sub> )			
	Riffle Inner Berm W/D Ratio (W <sub>ib</sub> / d <sub>ib</sub> )								
<b>Pool Dimensions* ** *</b>	<b>Pool Dimensions* ** *</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Pool Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Pool Width (W <sub>bkfp</sub> )				ft	Pool Width to Riffle Width (W <sub>bkfp</sub> / W <sub>bkf</sub> )			
	Mean Pool Depth (d <sub>bkfp</sub> )				ft	Mean Pool Depth to Mean Riffle Depth (d <sub>bkfp</sub> / d <sub>bkf</sub> )			
	Pool Cross-Sectional Area (A <sub>bkfp</sub> )				ft	Pool Area to Riffle Area (A <sub>bkfp</sub> / A <sub>bkf</sub> )			
	Maximum Pool Depth (d <sub>maxp</sub> )				ft	Max Pool Depth to Mean Riffle Depth (d <sub>maxp</sub> / d <sub>bkf</sub> )			
	Pool Inner Berm Width (W <sub>ibp</sub> )				ft	Pool Inner Berm Width to Pool Width (W <sub>ibp</sub> / W <sub>bkfp</sub> )			
	Pool Inner Berm Depth (d <sub>ibp</sub> )				ft	Pool Inner Berm Depth to Pool Depth (d <sub>ibp</sub> / d <sub>bkfp</sub> )			
	Pool Inner Berm Area (A <sub>ibp</sub> )				ft <sup>2</sup>	Pool Inner Berm Area to Pool Area (A <sub>ibp</sub> / A <sub>bkfp</sub> )			
	Point Bar Slope (S <sub>pb</sub> )				ft/ft	Pool Inner Berm Width/Depth Ratio (W <sub>ibp</sub> / d <sub>ibp</sub> )			
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Run Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Run Width (W <sub>bkfr</sub> )				ft	Run Width to Riffle Width (W <sub>bkfr</sub> / W <sub>bkf</sub> )			
	Mean Run Depth (d <sub>bkfr</sub> )				ft	Mean Run Depth to Mean Riffle Depth (d <sub>bkfr</sub> / d <sub>bkf</sub> )			
	Run Cross-Sectional Area (A <sub>bkfr</sub> )				ft	Run Area to Riffle Area (A <sub>bkfr</sub> / A <sub>bkf</sub> )			
	Maximum Run Depth (d <sub>maxr</sub> )				ft	Max Run Depth to Mean Riffle Depth (d <sub>maxr</sub> / d <sub>bkf</sub> )			
	Run Width/Depth Ratio (W <sub>bkfr</sub> / d <sub>bkfr</sub> )				ft				
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Glide Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Glide Width (W <sub>bkgf</sub> )				ft	Glide Width to Riffle Width (W <sub>bkgf</sub> / W <sub>bkf</sub> )			
	Mean Glide Depth (d <sub>bkgf</sub> )				ft	Mean Glide Depth to Mean Riffle Depth (d <sub>bkgf</sub> / d <sub>bkf</sub> )			
	Glide Cross-Sectional Area (A <sub>bkgf</sub> )				ft	Glide Area to Riffle Area (A <sub>bkgf</sub> / A <sub>bkf</sub> )			
	Maximum Glide Depth (d <sub>maxg</sub> )				ft	Max Glide Depth to Mean Riffle Depth (d <sub>maxg</sub> / d <sub>bkf</sub> )			
	Glide Width/Depth Ratio (W <sub>bkgf</sub> / d <sub>bkgf</sub> )				ft/ft	Glide Inner Berm Width/Depth Ratio (W <sub>ibg</sub> / d <sub>ibg</sub> )			
	Glide Inner Berm Width (W <sub>ibg</sub> )				ft	Glide Inner Berm Width to Glide Width (W <sub>ibg</sub> / W <sub>bkgf</sub> )			
	Glide Inner Berm Depth (d <sub>ibg</sub> )				ft	Glide Inner Berm Depth to Glide Depth (d <sub>ibg</sub> / d <sub>bkgf</sub> )			
Glide Inner Berm Area (A <sub>ibg</sub> )				ft <sup>2</sup>	Glide Inner Berm Area to Glide Area (A <sub>ibg</sub> / A <sub>bkgf</sub> )				
<b>Step**</b>	<b>Step Dimensions**</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Step Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Step Width (W <sub>bks</sub> )				ft	Step Width to Riffle Width (W <sub>bks</sub> / W <sub>bkf</sub> )			
	Mean Step Depth (d <sub>bks</sub> )				ft	Mean Step Depth to Riffle Depth (d <sub>bks</sub> / d <sub>bkf</sub> )			
	Step Cross-Sectional Area (A <sub>bks</sub> )				ft	Step Area to Riffle Area (A <sub>bks</sub> / A <sub>bkf</sub> )			
	Maximum Step Depth (d <sub>maxs</sub> )				ft	Max Step Depth to Mean Riffle Depth (d <sub>maxs</sub> / d <sub>bkf</sub> )			
	Step Width/Depth Ratio (W <sub>bks</sub> / d <sub>bks</sub> )								

**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, A4a+ Poor South Reach</b>		Location: <b>Pike National Forest, Colorado</b>							
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/2/2010</b>		Valley Type: <b>I</b>		Stream Type: <b>A4a+</b>			
<b>River Reach Summary Data.....2</b>									
<b>Hydraulics</b>	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )		<b>0.73</b>	ft/sec	Estimation Method		<b>Manning's n from Jarrett</b>		
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )		<b>0.32</b>	cfs	Drainage Area		<b>0.002</b> mi <sup>2</sup>		
<b>Channel Pattern</b>	<b>Geometry</b>			<b>Dimensionless Geometry Ratios</b>					
	Linear Wavelength ( $\lambda$ )	Mean	Min	Max	ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )	Mean		
	Stream Meander Length ( $L_m$ )				ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )	Min		
	Radius of Curvature ( $R_c$ )				ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )	Max		
	Belt Width ( $W_{bit}$ )	<b>2.6</b>			ft	Meander Width Ratio ( $W_{bit} / W_{bkt}$ )	<b>1.51</b>		
	Arc Length ( $L_a$ )				ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )			
	Riffle Length ( $L_r$ )				ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )			
	Individual Pool Length ( $L_p$ )				ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )			
Pool to Pool Spacing ( $P_s$ )				ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )				
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )	<b>0.1293</b>	ft/ft	Average Water Surface Slope (S)	<b>0.1280</b>	ft/ft	Sinuosity ( $S_{val} / S$ )	<b>1.01</b>	
	Stream Length (SL)	<b>20.0</b>	ft	Valley Length (VL)	<b>19.8</b>	ft	Sinuosity (SL / VL)	<b>1.01</b>	
	Low Bank Height (LBH)	start: <b>2.00</b> ft end: <b>1.50</b> ft		Max Bankfull Depth ( $d_{max}$ )	start: <b>0.43</b> ft end: <b>0.43</b> ft		Bank-Height Ratio (BHR) ( $LBH / d_{max}$ )	start: <b>4.7</b> end: <b>3.5</b>	
	<b>Facet Slopes</b>			<b>Dimensionless Facet Slope Ratios</b>					
	Riffle Slope ( $S_{rif}$ )	Mean	Min	Max	ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rif} / S$ )	Mean	Min	
	Run Slope ( $S_{run}$ )				ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )	Max		
	Pool Slope ( $S_p$ )				ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )			
	Glide Slope ( $S_g$ )				ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )			
	Step Slope ( $S_s$ )				ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )			
	<b>Max Depths<sup>a</sup></b>			<b>Dimensionless Depth Ratios</b>					
	Max Riffle Depth ( $d_{max}$ )	<b>0.48</b>	<b>0.37</b>	<b>0.61</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>2.400</b>	<b>1.850</b>	<b>3.050</b>
	Max Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )			
	Max Pool Depth ( $d_{maxp}$ )				ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )			
	Max Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )			
	Max Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
<b>Channel Materials</b>	<b>Reach<sup>b</sup></b>			<b>Riffle<sup>c</sup></b>			<b>Bar</b>		
	% Silt/Clay	<b>0</b>			$D_{16}$	<b>1</b>		mm	
	% Sand	<b>32</b>			$D_{35}$	<b>2</b>		mm	
	% Gravel	<b>67</b>			$D_{50}$	<b>5</b>		mm	
	% Cobble	<b>1</b>			$D_{84}$	<b>10</b>		mm	
	% Boulder	<b>0</b>			$D_{95}$	<b>14</b>		mm	
	% Bedrock	<b>0</b>			$D_{100}$	<b>90</b>		mm	
<b>Reach<sup>b</sup></b>			<b>Riffle<sup>c</sup></b>			<b>Bar</b>			
<b>Protrusion Height<sup>d</sup></b>									

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.  
<sup>b</sup> Composite sample of riffles and pools within the designated reach.      <sup>c</sup> Active bed of a riffle.      <sup>d</sup> Height of roughness feature above bed.

## Stability Indices

**Worksheet 5-6.** Riparian vegetation.


Riparian Vegetation						
Stream: <b>Trail Creek, A4a+ Poor South Reach</b>		Location: <b>Pike National Forest, Colorado</b>				
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Reference reach <input type="checkbox"/>	Disturbed (impacted reach) <input checked="" type="checkbox"/>	Date: <b>9/2/2010</b>		
Existing species composition: <b>Aspen, Raspberry</b>		Potential species composition: <b>Aspen, Ponderosa Pine</b>				
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition	
<b>1. Overstory</b>	Canopy layer	<b>0%</b>	<b>0%</b>		<b>0%</b>	
					<b>100%</b>	
<b>2. Understory</b>	Shrub layer		<b>10%</b>	<b>Raspberry</b>	<b>80%</b>	
					<b>Aspen</b>	<b>20%</b>
				<b>100%</b>		
<b>3. Ground level</b>	Herbaceous		<b>60%</b>	<b>Forbs(Kinnikinin, Senecio, Physelia, Scarlet Gilia)</b>	<b>50%</b>	
					<b>Grasses(Rush, Bunchgrass)</b>	<b>50%</b>
					<b>100%</b>	
Leaf or needle litter			<b>5%</b>	<b>Remarks:</b> Condition, vigor and/or usage of existing reach: <b>Rilling from side slopes noticeable, esp. on south aspects. Vegetation showing signs of recovery.</b>		
Bare ground			<b>25%</b>			
*Based on crown closure. **Based on basal area to surface area.			<b>Column total = 100%</b>			



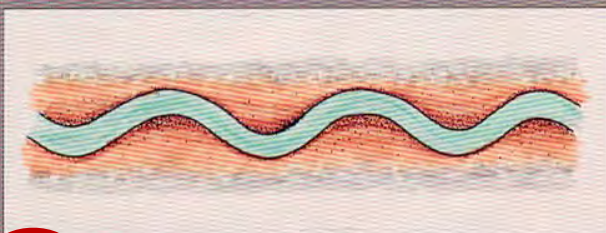




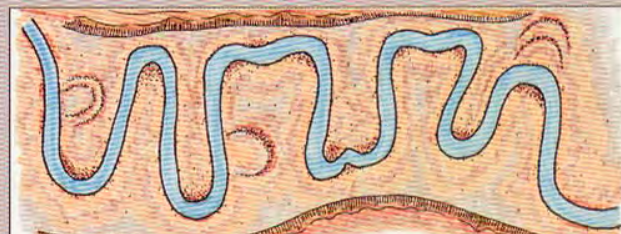
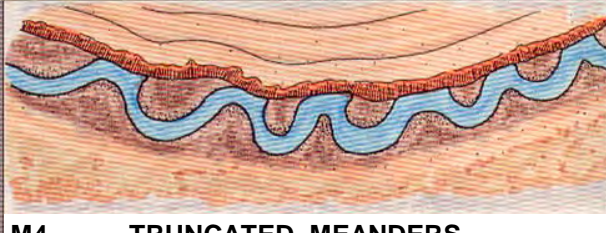
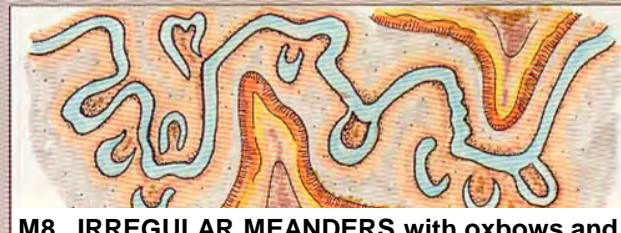
**Worksheet 5-7.** Flow regime.

<b>FLOW REGIME</b>								
Stream: <b>Trail Creek, A4a+ Poor South</b>			Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>Chavez, Kasun &amp; Gallagher</b>						Date: <b>9/2/2010</b>		
<b>List ALL COMBINATIONS that APPLY.....</b>			<b>E1</b>	<b>E2</b>	<b>E8</b>			
<b>General Category</b>								
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation							
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
<b>P</b>	Perennial stream channels: Surface water persists yearlong.							
<b>Specific Category</b>								
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
<b>4</b>	Streamflow regulated by glacial melt.							
<b>5</b>	Ice flows/ice torrents from ice dam breaches.							
<b>6</b>	Alternating flow/backwater due to tidal influence.							
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.							
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
<b>9</b>	Rain-on-snow generated runoff.							

**Worksheet 5-8.** Stream order & stream size.

<b>Stream Size and Order</b>			
Stream:	<b>Trail Creek, A4a+ Poor South Reach</b>		
Location:	<b>Pike National Forest, Colorado</b>		
Observers:	<b>Chavez, Kasun &amp; Gallagher</b>		
Date:	<b>9/2/2010</b>		
<b>Stream Size Category and Order</b> 			<b>S-2(1)</b>
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0 - 305	<1	<input type="checkbox"/>
<b>S-2</b>	<b>0.3 - 1.5</b>	<b>1 - 5</b>	<input checked="" type="checkbox"/>
S-3	1.5 - 4.6	5 - 15	<input type="checkbox"/>
S-4	4.6 - 9	15 - 30	<input type="checkbox"/>
S-5	9 - 15	30 - 50	<input type="checkbox"/>
S-6	15 - 22.8	50 - 75	<input type="checkbox"/>
S-7	22.8 - 30.5	75 - 100	<input type="checkbox"/>
S-8	30.5 - 46	100 - 150	<input type="checkbox"/>
S-9	46 - 76	150 - 250	<input type="checkbox"/>
S-10	76 - 107	250 - 350	<input type="checkbox"/>
S-11	107 - 150	350 - 500	<input type="checkbox"/>
S-12	150 - 305	500 - 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
<b>Stream Order</b>			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			

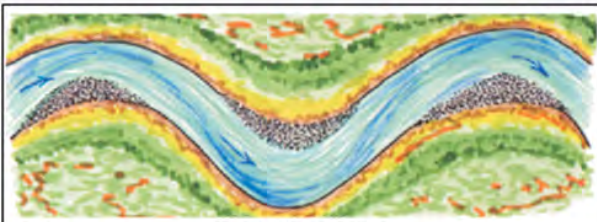
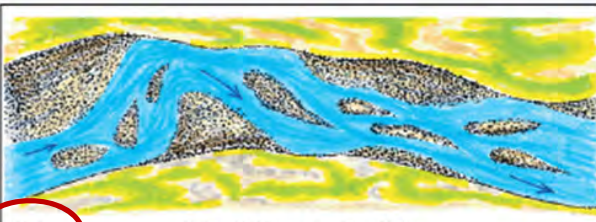

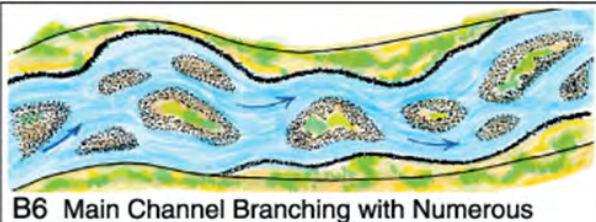
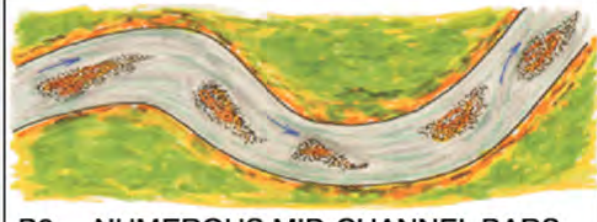
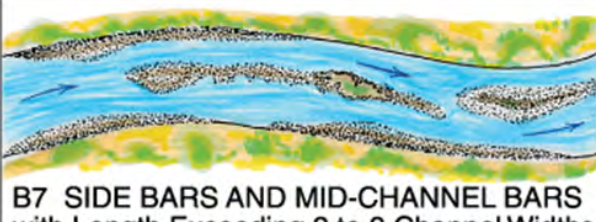


Worksheet 5-9. Meander patterns.

<b>Meander Patterns</b>					
Stream:	Trail Creek, A4a+ Poor South Reach	Location:	Pike National Forest, CO		
Observers:	Chavez, Kasun & Gallagher		Date:	9/2/2010	
List ALL CATEGORIES that APPLY	<b>M1</b>				
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>					
					
<b>M1</b> <b>REGULAR MEANDERS</b>	<b>M5</b> <b>UNCONFINED MEANDER SCROLLS</b>				
					
<b>M2</b> <b>TORTUOUS MEANDERS</b>	<b>M6</b> <b>CONFINED MEANDER SCROLLS</b>				
					
<b>M3</b> <b>IRREGULAR MEANDERS</b>	<b>M7</b> <b>DISTORTED MEANDER LOOPS</b>				
					
<b>M4</b> <b>TRUNCATED MEANDERS</b>	<b>M8</b> <b>IRREGULAR MEANDERS with oxbows and</b>				

**Worksheet 5-10.** Depositional patterns.

<b>Depositional Patterns</b>					
Stream:	Trail Creek, A4a+ Poor South Reach	Location:	Pike National Forest, Colorado		
Observers:	Chavez, Kasun & Gallagher	Date:	9/2/2010		
List ALL CATEGORIES that APPLY	B4	B5			

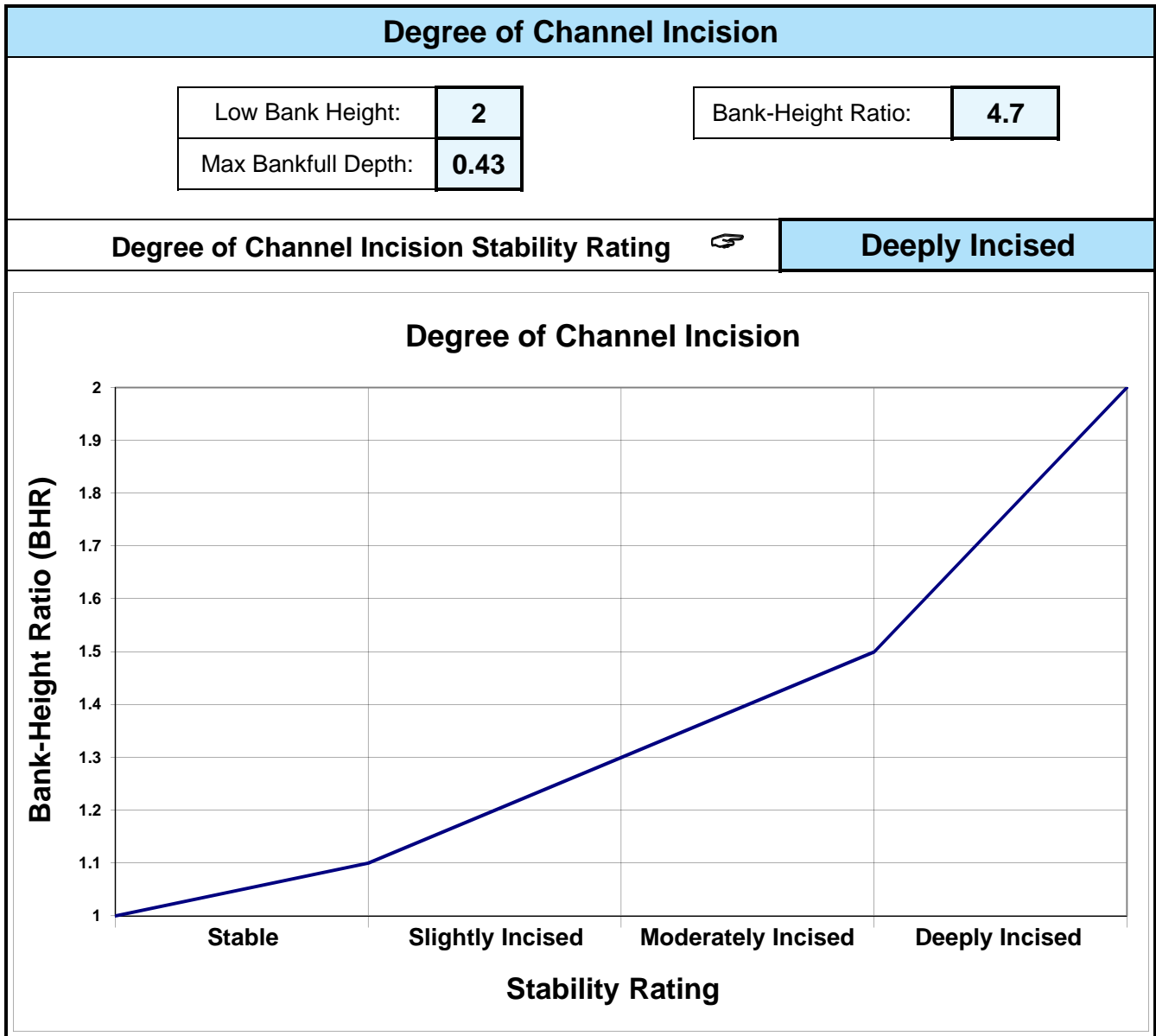
*Various Depositional Features modified from Galay et al. (1973)*

 <p><b>B1</b> POINT BARS</p>	 <p><b>B5</b> DIAGONAL BARS</p>
 <p><b>B2</b> POINT BARS with Few MID-CHANNEL BARS</p>	 <p><b>B6</b> Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</p>
 <p><b>B3</b> NUMEROUS MID-CHANNEL BARS</p>	 <p><b>B7</b> SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</p>
 <p><b>B4</b> SIDE BARS</p>	 <p><b>B8</b> DELTA BARS</p>

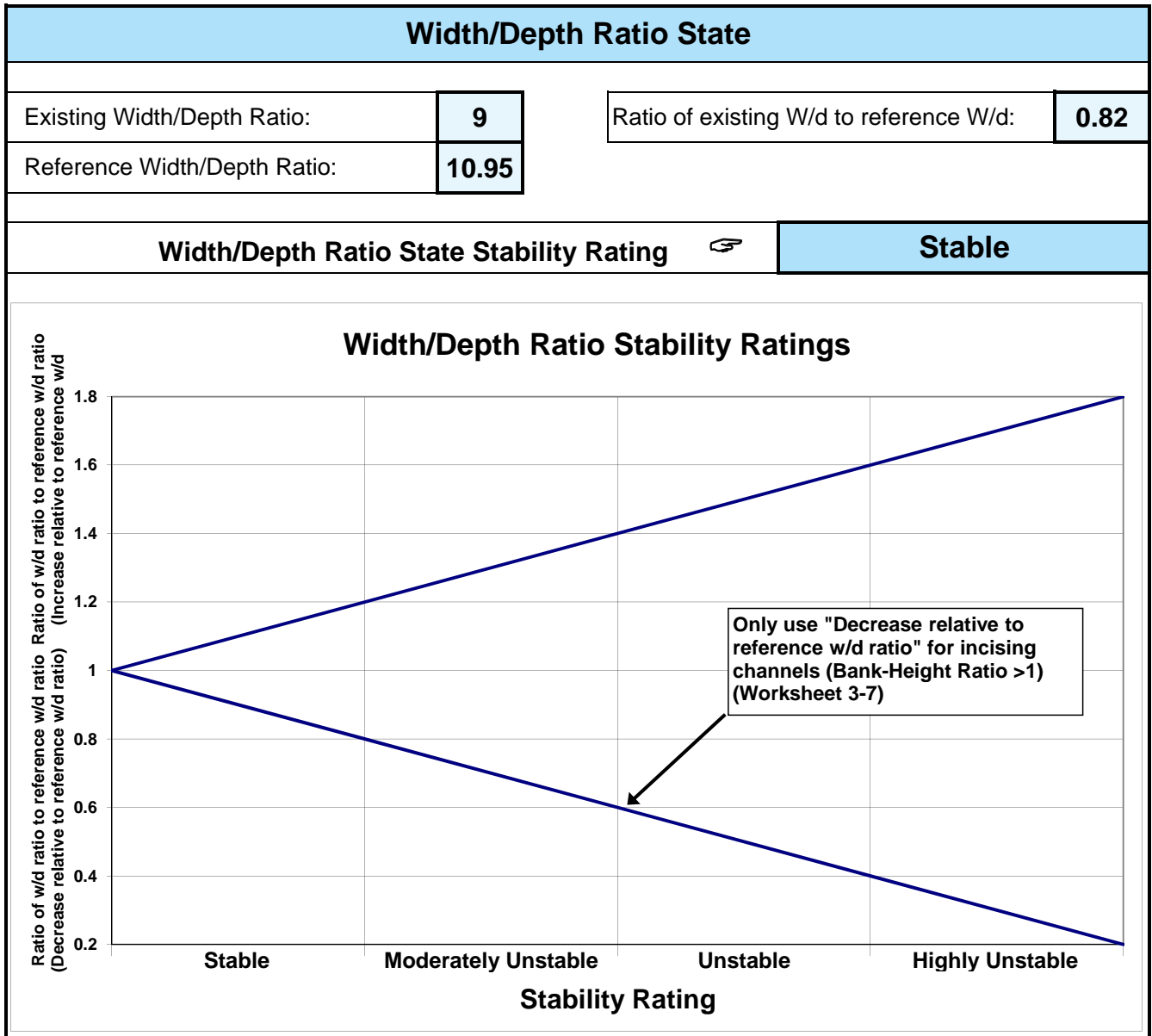
## Worksheet 5-11. Channel blockages.

Channel Blockages		
Stream: <b>Trail Creek, A4a+ Poor South Reach</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/2/2010</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input checked="" type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input type="checkbox"/>
<b>D4</b> Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

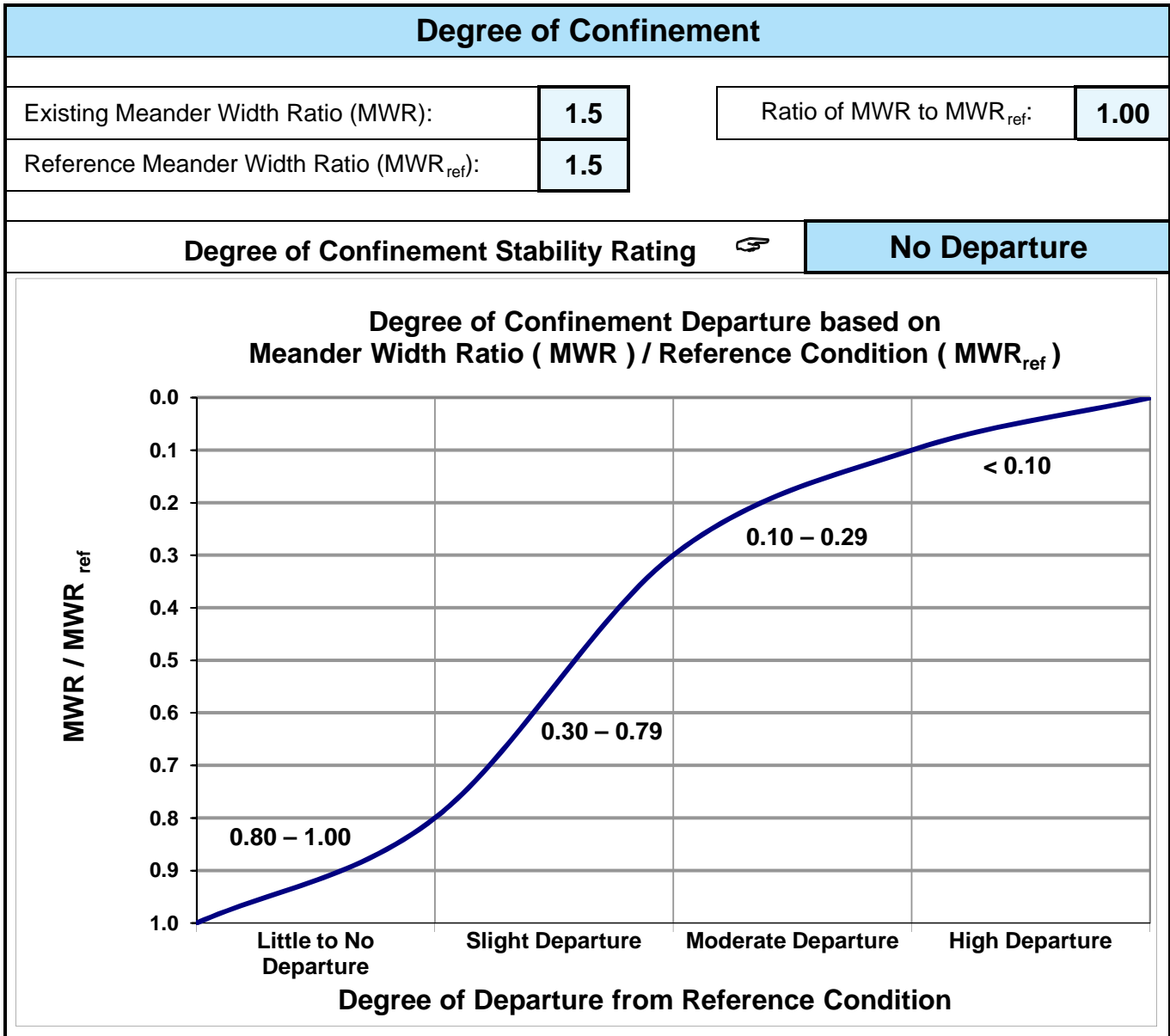
**Worksheet 5-12.** Degree of channel incision.



Worksheet 5-13. Width/depth ratio state.



**Worksheet 5-14.** Degree of channel confinement (lateral containment).





Worksheet 5-15. Pfankuch channel stability rating.

Stream: Trail Creek, A4+ Poor South Reach		Location: Pike National Forest, CO			Valley Type: I			Observers: Chavez, Kasun & Gallagher			Date: 9/2/2010														
Loca- tion	Key	Excellent			Good			Fair			Poor														
		Description	Rating		Description	Rating		Description	Rating	Description	Rating														
Upper banks	1	Landform slope	Bank slope gradient <30%.	3	Bank slope gradient 30–40%.	4	Bank slope gradient 40–60%.	6	Bank slope gradient > 60%.	8															
	2	Mass erosion	No evidence of past or future mass erosion.	3	Infrequent. Mostly healed over. Low future potential.	6	Frequent or large, causing sediment nearly yearlong.	9	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.	12															
	3	Debris jam potential	Essentially absent from immediate channel area.	2	Present, but mostly small twigs and limbs.	4	Moderate to heavy amounts, mostly larger sizes.	6	Moderate to heavy amounts, predominantly larger sizes.	8															
	4	Vegetative bank protection	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	3	70–90% density. Fewer species or less vigor suggest less dense or deep root mass.	6	50–70% density. Lower vigor and fewer species from a shallow, discontinuous root mass.	10	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.	12															
Lower banks	5	Channel capacity	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0.	1	Bankfull stage is contained within banks. Width/depth ratio departure from reference width/depth ratio = 1.0–1.2. Bank-Height Ratio (BHR) = 1.0–1.1.	2	Bankfull stage is not contained. Width/depth ratio departure from reference width/depth ratio = 1.2–1.4. Bank-Height Ratio (BHR) > 1.3.	3	Bankfull stage is not contained; over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.	4															
	6	Bank rock content	> 65% with large angular boulders. 12"+ common.	2	40–65%. Mostly boulders and small cobbles 6–12".	4	20–40%. Most in the 3–6" diameter class.	6	<20% rock fragments of gravel sizes, 1–3" or less.	8															
	7	Obstructions to flow	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	3	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	4	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	6	Frequent obstructions and deflectors cause bank erosion yearlong. Sediment traps full, channel migration occurring.	8															
	8	Cutting	Little or none. Infrequent raw banks <6".	4	Some, intermittently at outcaves and constrictions. Raw banks may be up to 12".	6	Significant. Cuts 12–24" high. Root mat overhangs and sloughing evident.	14	Almost continuous cuts, some over 24" high. Failure of overhangs frequent.	16															
	9	Deposition	Little or no enlargement of channel or point bars.	4	Some new bar increase, mostly from coarse gravel.	8	Moderate deposition of new gravel and coarse sand on old and some new bars.	12	Extensive deposit of predominantly fine particles. Accelerated bar development.	16															
Bottom	10	Rock angularity	Sharp edges and corners. Plane surfaces rough.	1	Rounded corners and edges. Surfaces smooth and flat.	2	Corners and edges well rounded in 2 dimensions.	3	Well rounded in all dimensions, surfaces smooth.	4															
	11	Brightness	Surfaces dull, dark or stained. Generally not bright.	1	Mostly dull, but may have <35% bright surfaces.	2	Mixture dull and bright, i.e., 35–65% mixture range.	3	Predominantly bright, > 65%, exposed or scored surfaces.	4															
	12	Consolidation of particles	Assorted sizes tightly packed or overlapping.	2	Moderately packed with some overlapping.	4	Mostly loose assortment with no apparent overlap.	6	No packing evident. Loose assortment, easily moved.	8															
	13	Bottom size distribution	No size change evident. Stable material 80–100%.	4	Distribution shift light. Stable material 50–80%.	8	Moderate change in sizes. Stable materials 20–50%.	12	Marked distribution change. Stable materials 0–20%.	16															
	14	Scouring and deposition	<5% of bottom affected by scour or deposition.	6	5–30% affected. Scour at constrictions and where grades steepen. Some deposition in pools.	12	30–50% affected. Deposits and scour at obstructions, constrictions and bends. Some filling of pools.	18	More than 50% of the bottom in a state of flux or change nearly yearlong.	24															
	15	Aquatic vegetation	Abundant growth moss-like, dark green perennial. In swift water too.	1	Common. Algae forms in low velocity and pool areas. Moss here too.	2	Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick.	3	Perennial types scarce or absent. Yellow-green, short-term bloom may be present.	4															
				<b>Excellent total = 3</b>	<b>Good total = 6</b>				<b>Fair total = 32</b>				<b>Poor total = 92</b>												
<b>Stream type</b>		A1	A2	A3	A4	A5	A6	B1	B2	B3	B4	B5	B6	C1	C2	C3	C4	C5	C6	D3	D4	D5	D6	<b>Grand total = 133</b>	
Good (Stable)		38-43	38-43	54-90	60-95	60-95	50-80	38-45	38-45	40-60	40-64	48-68	40-60	38-50	38-50	60-85	70-90	60-85	85-107	85-107	85-107	85-107	85-107	85-107	67-98
Fair (Mod. unstable)		44-47	44-47	91-129	96-132	96-132	81-110	46-58	46-58	61-78	65-84	69-88	61-78	51-61	51-61	86-105	91-110	86-105	108-132	108-132	108-132	108-132	108-132	108-132	99-125
Poor (Unstable)		48+	48+	130+	143+	143+	111+	59+	59+	79+	85+	89+	79+	62+	62+	106+	111+	106+	133+	133+	133+	133+	133+	126+	
<b>Stream type</b>		DA3	DA4	DA5	DA6	E3	E4	E5	E6	F1	F2	F3	F4	F5	F6	G1	G2	G3	G4	G5	G6	G6	G6	<b>A4a+</b>	
Good (Stable)		40-63	40-63	40-63	40-63	40-63	50-75	50-75	40-63	40-63	40-65	85-110	85-110	90-115	80-95	40-60	40-60	85-107	90-112	90-112	90-112	90-112	90-112	<b>A4a+</b>	
Fair (Mod. unstable)		64-86	64-86	64-86	64-86	64-86	76-96	76-96	64-86	86-105	86-105	111-125	111-125	116-130	96-110	61-78	61-78	108-120	108-120	113-125	108-120	108-120	108-120	<b>Modified channel stability rating =</b>	
Poor (Unstable)		87+	87+	87+	87+	87+	97+	97+	87+	106+	106+	126+	126+	131+	111+	79+	79+	121+	121+	126+	126+	121+	121+	<b>POOR</b>	

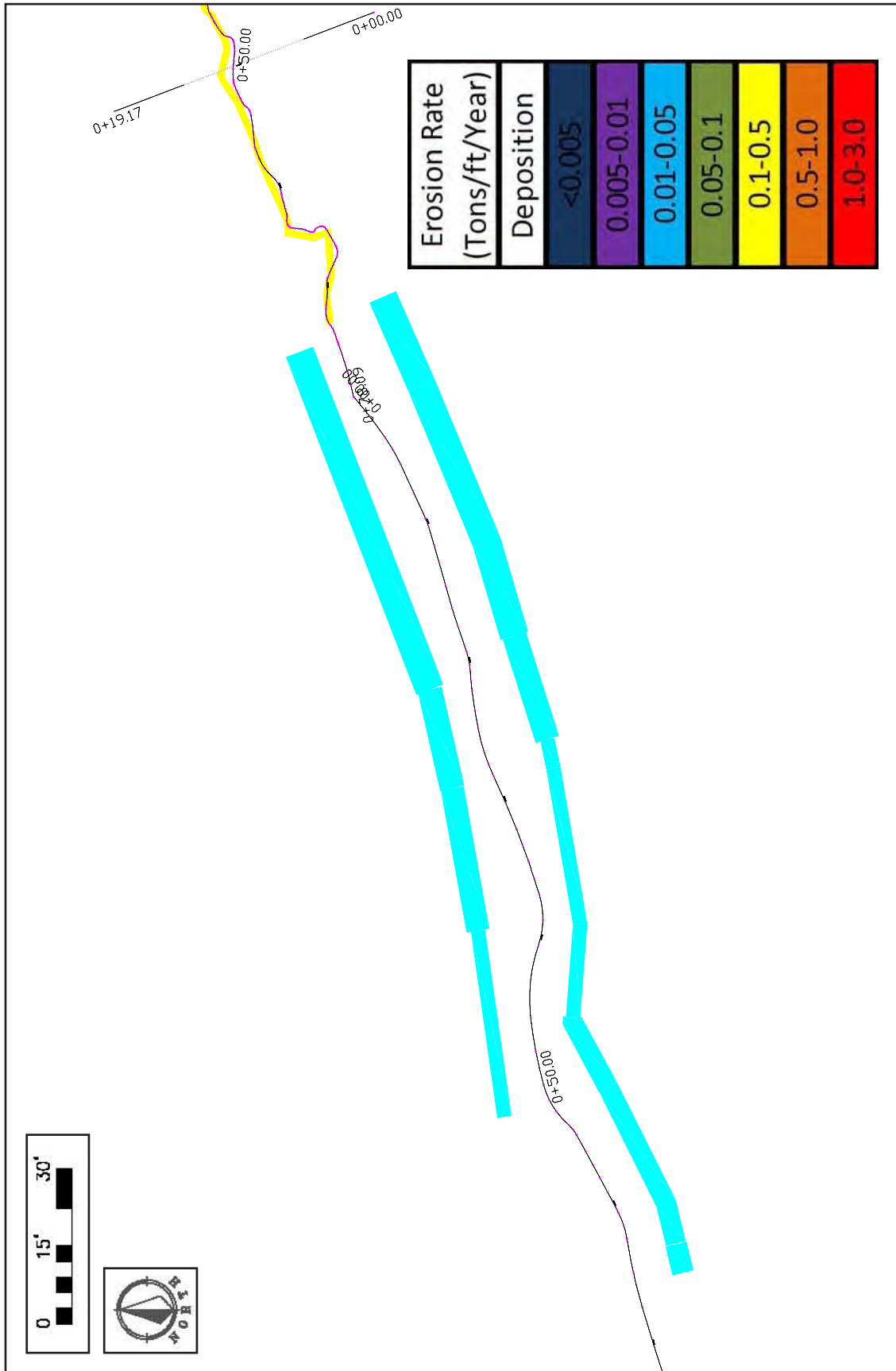
\*Rating is adjusted to potential stream type, not existing.

## BANCS Model – Streambank Erosion

**Worksheet 5-18.** Annual streambank erosion estimates.

Stream: <b>Trail Creek, A4a+ Poor South Reach</b>		Location: <b>Pike National Forest, Colorado</b>					
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>77</b>				Date: <b>9/2/2010</b>	
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Valley Type: <b>I</b>			Stream Type: <b>A4a+</b>		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 5-16) (adjective)	NBS rating (Worksheet 5-17) (adjective)	Bank erosion rate (Figure 5-34 or 5-35) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [(4)×(5)×(6)] (ft <sup>3</sup> /yr)	Erosion Rate (tons/yr/ft) {[ (7)/27] × 1.3 / (5)}
1. 0+0 - 0+25R	High	Low	0.25042	25.0	2.0	12.52	0.02411
2. 0+0 - 0+25L	High	Low	0.25042	25.0	2.0	12.52	0.02411
3. 0+25 - 0+32R	High	Low	0.25042	7.0	1.7	2.98	0.02050
4. 0+25 - 0+32L	High	Low	0.25042	7.0	1.7	2.98	0.02050
5. 0+32 - 0+42R	High	Low	0.25042	10.0	1.6	4.01	0.01929
6. 0+42 - 0+55L	High	Low	0.25042	22.0	1.0	5.51	0.01206
7. 0+42 - 0+55R	High	Low	0.25042	13.0	1.0	3.26	0.01206
8. 0+55 - 0+60R	Moderate	Low	0.15287	5.0	1.4	1.07	0.01030
9. 0+55 - 0+60L	High	Low	0.25042	5.0	1.4	1.75	0.01688
10. 0+60 - 0+72R	Moderate	Low	0.15287	12.0	1.8	3.30	0.01325
11. 0+63 - 0+75L	High	Low	0.25042	12.0	1.4	4.21	0.01688
12. 0+72 - 0+77R	High	Low	0.25042	5.0	1.5	1.88	0.01809
13. 0+75 - 0+77L	High	Low	0.25042	2.0	1.5	0.75	0.01809
14							
15							
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					Total Erosion (ft <sup>3</sup> /yr)	<b>56.74</b>	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					Total Erosion (yds <sup>3</sup> /yr)	<b>2.10</b>	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					Total Erosion (tons/yr)	<b>2.73</b>	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					Total Erosion (tons/yr/ft)	<b>0.0355</b>	

**Streambank Erosion Map**



## FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Equation Type		Equation Source		Equation		Bankfull Discharge (cfs)		Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)				
1. Bedload Sediment		"Good/Fair" Pagosa		$y = -0.0113+1.0139x^{2.1929}$		0.32		0.0014		0.01406				
2. Suspended Sediment		"Good/Fair" Pagosa		$y = 0.0636+0.9326x^{2.4085}$										
		From Dimensional Flow-Duration Curve				From Sediment Rating Curves				Calculate		Calculate Sediment Yield		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Percentage of Time	Daily Mean Discharge (cfs)	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Suspended Sediment Discharge	Suspended Sediment Discharge	Dimensionless Bedload Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow	Suspended Sediment	Bedload Sediment	Suspended + Bedload Sediment
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/O <sub>bed</sub> )	(S/S <sub>bed</sub> )	(tons/day)	(b <sub>g</sub> /b <sub>bed</sub> )	(tons/day)	[(5)×(6)]	[(5)×(9)]	[(5)×(11)]	[(13)+(14)]
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/O <sub>bed</sub> )	(S/S <sub>bed</sub> )	(tons/day)	(b <sub>g</sub> /b <sub>bed</sub> )	(tons/day)	(cfs)	(tons)	(tons)	(tons)
0%	0.8													
0.10%	0.7	0.05%	0.09%	0.34	0.8	2.363	7.461	0.00	6.670	0.87	0.3	0.00	0.30	0.30
0.25%	0.6	0.08%	0.15%	0.55	0.7	2.036	5.232	0.00	4.809	0.62	0.4	0.00	0.34	0.34
0.50%	0.5	0.13%	0.25%	0.91	0.6	1.761	3.706	0.00	3.494	0.45	0.5	0.00	0.41	0.41
0.75%	0.4	0.13%	0.25%	0.91	0.5	1.513	2.592	0.00	2.502	0.32	0.4	0.00	0.30	0.30
1%	0.4	0.13%	0.25%	0.91	0.4	1.300	1.817	0.00	1.790	0.23	0.4	0.00	0.21	0.21
1.5%	0.3	0.25%	0.50%	1.83	0.4	1.120	1.289	0.00	1.289	0.17	0.7	0.00	0.31	0.31
2%	0.3	0.25%	0.50%	1.83	0.3	0.949	0.886	0.00	0.893	0.12	0.6	0.00	0.21	0.21
3%	0.2	0.50%	1.00%	3.65	0.3	0.795	0.600	0.00	0.602	0.08	0.9	0.00	0.28	0.28
4%	0.2	0.50%	1.00%	3.65	0.2	0.674	0.424	0.00	0.415	0.05	0.8	0.00	0.20	0.20
5%	0.2	0.50%	1.00%	3.65	0.2	0.587	0.322	0.00	0.304	0.04	0.7	0.00	0.14	0.14
10%	0.1	2.50%	5.00%	18.25	0.1	0.450	0.200	0.00	0.165	0.02	2.6	0.00	0.39	0.39
20%	0.1	5.00%	10.00%	36.50	0.1	0.269	0.103	0.00	0.045	0.01	3.1	0.00	0.22	0.22
30%	0.0	5.00%	10.00%	36.50	0.1	0.158	0.075	0.00	0.006	0.00	1.8	0.00	0.03	0.03
40%	0.0	5.00%	10.00%	36.50	0.0	0.108	0.068	0.00	0.000	0.00	1.3	0.00	0.00	0.00
50%	0.0	5.00%	10.00%	36.50	0.0	0.079	0.066	0.00	0.000	0.00	0.9	0.00	0.00	0.00
60%	0.0	5.00%	10.00%	36.50	0.0	0.061	0.065	0.00	0.000	0.00	0.7	0.00	0.00	0.00
70%	0.0	5.00%	10.00%	36.50	0.0	0.047	0.064	0.00	0.000	0.00	0.6	0.00	0.00	0.00
80%	0.0	5.00%	10.00%	36.50	0.0	0.039	0.064	0.00	0.000	0.00	0.5	0.00	0.00	0.00
90%	0.0	5.00%	10.00%	36.50	0.0	0.032	0.064	0.00	0.000	0.00	0.4	0.00	0.00	0.00
100%	0.0	5.00%	10.00%	36.50	0.0	0.016	0.064	0.00	0.000	0.00	0.2	0.00	0.00	0.00
<b>Annual Totals:</b>											17.6	0.0	3.3	3.3
											(cfs)	(tons/yr)	(tons/yr)	(tons/yr)
											35.0			
											(acre-ft)			

Worksheet 19b. Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Equation Type		Equation Source				Equation		Bankfull Discharge (cfs)		Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)						
1. Bedload Sediment		"Poor" Pagosa				$Y = 0.07176 + 1.02176x^{2.3772}$		0.32		0.00096		53.83						
2. Suspended Sediment		"Poor" Pagosa				$Y = 0.0989 + 0.9213x^{3.659}$												
From Dimensional Flow-Duration Curve												From Sediment Rating Curves			Calculate		Calculate Sediment Yield	
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)				
Percentage of Time	Daily Mean Discharge (cfs)	Mid-Ordinate (%)	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow (cfs)	Dimension-less Streamflow	Dimension-less Sediment Discharge ( $S/S_{bed}$ )	Suspended Sediment Discharge (tons/day)	Dimension-less Bedload Discharge ( $b_b/b_{bed}$ )	Bedload Sediment Discharge (tons/day)	Time Adjusted Streamflow $[(5) \times (6)]$ (cfs)	Suspended Sediment $[(5) \times (9)]$ (tons)	Bedload Sediment $[(5) \times (11)]$ (tons)	Suspended Sediment + Bedload Sediment $[(13) \times (14)]$ (tons)				
0%	0.8																	
0.10%	0.7	0.05%	0.09%	0.34	0.8	2.385	22.277	2.47	8.142	0.75	0.3	0.85	0.26	1.10				
0.25%	0.6	0.08%	0.15%	0.55	0.7	2.059	13.032	1.25	5.757	0.53	0.4	0.68	0.29	0.97				
0.50%	0.5	0.13%	0.25%	0.91	0.6	1.783	7.748	0.64	4.113	0.38	0.5	0.59	0.34	0.93				
0.75%	0.5	0.13%	0.25%	0.91	0.5	1.536	4.525	0.32	2.904	0.27	0.4	0.29	0.24	0.54				
1%	0.4	0.13%	0.25%	0.91	0.4	1.322	2.660	0.16	2.057	0.19	0.4	0.15	0.17	0.32				
1.5%	0.3	0.25%	0.50%	1.83	0.4	1.143	1.599	0.08	1.475	0.14	0.7	0.16	0.25	0.40				
2%	0.3	0.25%	0.50%	1.83	0.3	0.971	0.927	0.04	1.025	0.09	0.6	0.08	0.17	0.25				
3%	0.2	0.50%	1.00%	3.65	0.3	0.817	0.539	0.02	0.704	0.06	1.0	0.07	0.24	0.31				
4%	0.2	0.50%	1.00%	3.65	0.2	0.695	0.342	0.01	0.502	0.05	0.8	0.04	0.17	0.21				
5%	0.2	0.50%	1.00%	3.65	0.2	0.606	0.246	0.01	0.382	0.04	0.7	0.03	0.13	0.15				
10%	0.1	2.50%	5.00%	18.25	0.1	0.465	0.155	0.00	0.237	0.02	2.7	0.06	0.40	0.46				
20%	0.1	5.00%	10.00%	36.50	0.1	0.275	0.107	0.00	0.119	0.01	3.2	0.05	0.40	0.45				
30%	0.0	5.00%	10.00%	36.50	0.1	0.159	0.100	0.00	0.085	0.01	1.9	0.03	0.28	0.31				
40%	0.0	5.00%	10.00%	36.50	0.0	0.108	0.099	0.00	0.077	0.01	1.3	0.02	0.26	0.28				
50%	0.0	5.00%	10.00%	36.50	0.0	0.079	0.099	0.00	0.074	0.01	0.9	0.01	0.25	0.26				
60%	0.0	5.00%	10.00%	36.50	0.0	0.061	0.099	0.00	0.073	0.01	0.7	0.01	0.24	0.25				
70%	0.0	5.00%	10.00%	36.50	0.0	0.047	0.099	0.00	0.072	0.01	0.6	0.01	0.24	0.25				
80%	0.0	5.00%	10.00%	36.50	0.0	0.039	0.099	0.00	0.072	0.01	0.5	0.01	0.24	0.25				
90%	0.0	5.00%	10.00%	36.50	0.0	0.032	0.099	0.00	0.072	0.01	0.4	0.01	0.24	0.25				
100%	0.0	5.00%	10.00%	36.50	0.0	0.016	0.099	0.00	0.072	0.01	0.2	0.00	0.24	0.24				
<b>Annual Totals:</b>												<b>17.9</b> (cfs)	<b>3.1</b> (tons/yr)	<b>5.0</b> (tons/yr)	<b>8.2</b> (tons/yr)			
												<b>35.6</b> (acre-ft)						

## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>Trail Creek, A4a+ Poor South Reach</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/2/2010</b>			
<b>Enter Required Information for Existing Condition</b>					
4.8	$D_{50}$	Riffle bed material $D_{50}$ (mm)			
	$\hat{D}_{50}$	Bar sample $D_{50}$ (mm)			
0.30	$D_{max}$	Largest particle from <b>Bed Material</b> (ft)	90	(mm)	304.8 mm/ft
0.1280	$S$	Existing bankfull water surface slope (ft/ft)			
0.22	$d$	Existing bankfull mean depth (ft)			
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment			
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>					
N/A	$D_{50}/\hat{D}_{50}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 ( D_{50}/\hat{D}_{50} )^{-0.872}$		
N/A	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 ( D_{max}/D_{50} )^{-0.887}$		
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED:		
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	$d$	Required bankfull mean depth (ft)	$d = \frac{\tau^*(\gamma_s - 1)D_{max}}{S}$ (use $D_{max}$ in ft)		
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	$S$	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^*(\gamma_s - 1)D_{max}}{d}$ (use $D_{max}$ in ft)		
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					
<b>Sediment Competence Using Dimensional Shear Stress</b>					
1.757	Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d ) $\gamma = 62.4$ , $d =$ existing depth, $S =$ existing slope				
Shields 140	CO 230	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ (Figure 5-49)			
Shields 1.2	CO 0.48	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) (Figure 5-49)			
Shields 0.15	CO 0.06	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm)		$d = \frac{\tau}{\gamma S}$	
Shields 0.0874	CO 0.0350	Predicted slope required to initiate movement of measured $D_{max}$ (mm)		$S = \frac{\tau}{\gamma d}$	
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input checked="" type="checkbox"/> Degrading					

## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>Trail Creek, A4a+ Poor South</b> Stream Type: <b>A4a+</b>	
Location: <b>Pike National Forest, CO</b> Valley Type: <b>I</b>	
Observers: <b>Chavez, Kasun &amp; Gallagher</b> Date: <b>9/2/2010</b>	
<b>Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)</b>	<b>Stability Rating (Check Appropriate Rating)</b>
<b>Stream Type at potential, (C→E),</b> (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	<input checked="" type="checkbox"/> Stable
(E→C), (C→High W/d C)	<input type="checkbox"/> Moderately Unstable
(G→F), (F→D), (C→F)	<input type="checkbox"/> Unstable
(C→D), (B→G), (D→G), (C→G), (E→G)	<input type="checkbox"/> Highly Unstable

**Worksheet 5-25.** Lateral stability.

Stream: <b>Trail Creek, A4a+ Poor South Reach</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/2/2010</b>			
Lateral stability criteria (choose one stability category for each criterion 1-5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	2
	<b>0.82</b> (2)	(4)	(6)	(8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	4
	(1)	(2)	(3)	B4, B5 (4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		1
	<b>M1</b> (1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, <b>H/L</b> , H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	6
	(2)	(4)	<b>H/L</b> (6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	1
	<b>1.0</b> (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>14</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input type="checkbox"/>	<i>Unstable</i> 13 – 21 <input checked="" type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	



**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>Trail Creek, A4a+ Poor South Reach</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/2/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
1 <b>Sediment Competence</b> (Worksheet 5-22)	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope-slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	2
	<b>Excess</b> (2)	(4)	(6)	(8)	
2 <b>Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	2
	<b>Excess</b> (2)	(4)	(6)	(8)	
3 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	2
	<b>0.82</b> (2)	(4)	(6)	(8)	
4 <b>Stream Succession States</b> (Worksheet 5-24)	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	2
	<b>at potential</b> (2)	(4)	(6)	(8)	
5 <b>Depositional Patterns</b> (Worksheet 5-10)	B1	B2, B4	B3, B5	B6, B7, B8	3
	(1)	(2)	<b>B4, B5</b> (3)	(4)	
6 <b>Debris / Blockages</b> (Worksheet 5-11)	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	1
	<b>D1</b> (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>12</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
Vertical Stability for Excess Deposition / Aggradation (use total points and check stability rating)	<i>No Deposition</i> 10 – 14 <input checked="" type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input type="checkbox"/>	<i>Aggradation</i> > 30 <input type="checkbox"/>	

**Worksheet 5-27. Vertical stability – degradation.**

Stream: <b>Trail Creek, A4a+ Poor South Reach</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/2/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>1 Sediment Competence (Worksheet 5-22)</b>	Does not indicate excess competence <b>(2)</b>	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed <b>(4)</b>	$D_{100}$ of bed moved <b>(6)</b>	Particles much larger than $D_{100}$ of bed moved <b>(8)</b>	<b>8</b>
<b>2 Sediment Capacity (POWERSED) (Worksheet 5-20)</b>	Does not indicate excess capacity <b>(2)</b>	Slight excess energy: up to 10% increase above reference <b>(4)</b>	Excess energy sufficient to increase load up to 50% of annual load <b>(6)</b>	Excess energy transporting more than 50% of annual load <b>(8)</b>	<b>8</b>
<b>3 Degree of Channel Incision (BHR) (Worksheet 5-12)</b>	1.00 – 1.10 <b>(2)</b>	1.11 – 1.30 <b>(4)</b>	1.31 – 1.50 <b>(6)</b>	> 1.50 <b>4.70 (8)</b>	<b>8</b>
<b>4 Stream Succession States (Worksheets 5-12 and 5-24)</b>	Does not indicate incision or degradation <b>(2)</b>	If BHR > 1.1 and stream type has W/d between 5–10 <b>BHR 4.7, W/D 9 (4)</b>	If BHR > 1.1 and stream type has W/d less than 5 <b>(6)</b>	(B→G), (C→G), (E→G), (D→G) <b>(8)</b>	<b>4</b>
<b>5 Confinement (MWR / MWR<sub>ref</sub>) (Worksheet 5-14)</b>	0.80 – 1.00 <b>1.00 (1)</b>	0.30 – 0.79 <b>(2)</b>	0.10 – 0.29 <b>(3)</b>	< 0.10 <b>(4)</b>	<b>1</b>
<b>Total Points</b>					<b>29</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation (use total points and check stability rating)</b>	<i>Not Incised</i> 9 – 11 <input type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input type="checkbox"/>	<i>Degradation</i> > 27 <input checked="" type="checkbox"/>	

Worksheet 5-28. Channel enlargement.

Stream: <b>Trail Creek, A4a+ Poor South Reach</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/2/2010</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1-4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	2
	at potential (2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	6
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	2
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	8
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>18</b>
<b>Category Point Range</b>					
Channel Enlargement Prediction (use total points and check stability rating)	<i>No Increase</i> 8 – 10 <input type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input checked="" type="checkbox"/>	<i>Extensive</i> > 24 <input type="checkbox"/>	

Worksheet 5-29. Overall sediment supply.

Stream: <b>Trail Creek, A4a+ Poor South Reach</b>		Stream Type: <b>A4a+</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>		
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/2/2010</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1-5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	3	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	1	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	4	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	3	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	4	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>15</b>	
<b>Category Point Range</b>				
Overall Sediment Supply Rating (use total points and check stability rating)	<b>Low</b> 5 <input type="checkbox"/>	<b>Moderate</b> 6 – 10 <input type="checkbox"/>	<b>High</b> 11 – 15 <input checked="" type="checkbox"/>	<b>Very High</b> 16 – 20 <input type="checkbox"/>

Worksheet 5-32. Summary of stability condition categories.

Stream:	Trail Creek, A4a+ Poor South Reach										Location: Pike National Forest, Colorado			
Observers:	Chavez, Kasun & Gallagher										Date: 9/2/2010	Stream Type: A4a+	Valley Type: I	
Channel Dimension (XS 0+99.1)	Mean Bankfull Depth (ft):	0.22	Bankfull Width (ft):	1.98	Cross-Sectional Area (ft <sup>2</sup> ):	0.44	Width of Flood-Prone Area (ft):	2.91	Entrenchment Ratio:	1.47				
Channel Pattern	Mean Range:	$\lambda/W_{bkf}$ : N/A	$L_m/W_{bkf}$ : N/A	$R_d/W_{bkf}$ : N/A	MWR: N/A	Sinuosity: 1.01								
River Profile & Bed Features	Check:	<input type="checkbox"/> Riffle/Pool	<input type="checkbox"/> Step/Pool	<input checked="" type="checkbox"/> Plane Bed	<input type="checkbox"/> Convergence/Divergence	<input type="checkbox"/> Dunes/Antidunes/Smooth Bed								
	Max Bankfull Depth (ft):	0.48	Riffle Pool	Depth Ratio (max to mean):	2.4	Riffle Pool	Pool-to-Pool Spacing:	Valley:	0.129	Water Surface:	0.128			
Level III Stream Stability Indices	Riparian Vegetation	Aspen, Raspberry	Aspen, Ponderosa Pine	Meander Patterns:	M1	Depositional Patterns:	B4, B5	Debris/Channel Blockages:	D1 (None)	Modified Pfankuch Stability Rating (Numeric & Adjective Rating):	133 (Poor)			
	Degree of Incision (Bank-Height Ratio):	4.7	Degree of Incision Stability Rating:	Deeply Incised										
	Width/depth Ratio (W/d):	9	Reference W/d Ratio (W/d <sub>ref</sub> ):	11	Width/Depth Ratio State (W/d) / (W/d <sub>ref</sub> ):	0.82	W/d Ratio State Stability Rating:	Stable						
	Meander Width Ratio (MWR):	1.5	Reference MWR <sub>ref</sub> :	1.5	Degree of confinement (MWR / MWR <sub>ref</sub> ):	1	MWR / MWR <sub>ref</sub> Stability Rating:	No Departure from Reference						
Bank Erosion Summary	Length of Reach Studied (ft):	77	Annual Streambank Erosion Rate: (tons/yr)	2.73	Curve Used:	Colorado	Remarks:							
Sediment Capacity (POWERSED)	<input type="checkbox"/> Sufficient Capacity	<input type="checkbox"/> Insufficient Capacity	<input checked="" type="checkbox"/> Excess Capacity											
Entrainment/Competence	Largest Particle from Bed Material (mm):	90	$\tau =$	1.757	$\tau^* =$	N/A	Existing Depth:	0.22	Required Depth:	0.15	Existing Slope:	0.128	Required Slope:	0.087
Successional Stage Shift	A4a+ → A4a+	→	→	→	→	→	Existing Stream State (Type):	A4a+	Potential Stream State (Type):	A4a+				
Lateral Stability	<input type="checkbox"/> Stable	<input type="checkbox"/> Mod. Unstable	<input checked="" type="checkbox"/> Unstable	<input type="checkbox"/> Highly Unstable										
Vertical Stability (Aggradation)	<input checked="" type="checkbox"/> No Deposition	<input type="checkbox"/> Mod. Deposition	<input type="checkbox"/> Ex. Deposition	<input type="checkbox"/> Aggradation										
Vertical Stability (Degradation)	<input type="checkbox"/> Not Incised	<input type="checkbox"/> Slightly Incised	<input type="checkbox"/> Mod. Incised	<input checked="" type="checkbox"/> Degradation										
Channel Enlargement	<input type="checkbox"/> No Increase	<input type="checkbox"/> Slight Increase	<input checked="" type="checkbox"/> Mod. Increase	<input type="checkbox"/> Extensive										
Sediment Supply (Channel Source)	<input type="checkbox"/> Low	<input type="checkbox"/> Moderate	<input checked="" type="checkbox"/> High	<input type="checkbox"/> Very High										



## *Appendix C4*

# **A4a+ Stream Type**

## ***Poor Stability Downstream Reach***





# Table of Contents

## *Appendix C4: A4a+ Poor Downstream Reach*

<b>Reach Location &amp; Overview.....</b>	<b>C4-2</b>
<b>Survey Summary.....</b>	<b>C4-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C4-6</b>
<b>Velocity, Classification &amp; Morphological Relations.....</b>	<b>C4-6</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b>Stability Indices.....</b>	<b>C4-10</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b>BANCS Model – Streambank Erosion.....</b>	<b>C4-20</b>
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b>FLOWSED Model – Total Annual Sediment Yield.....</b>	<b>C4-22</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b>Sediment Competence/Entrainment.....</b>	<b>C4-24</b>
Worksheet 5-22. Sediment competence calculations.	
<b>Channel Stability Ratings.....</b>	<b>C4-25</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b>Summary.....</b>	<b>C4-31</b>
Worksheet 5-32. Summary of stability condition categories.	

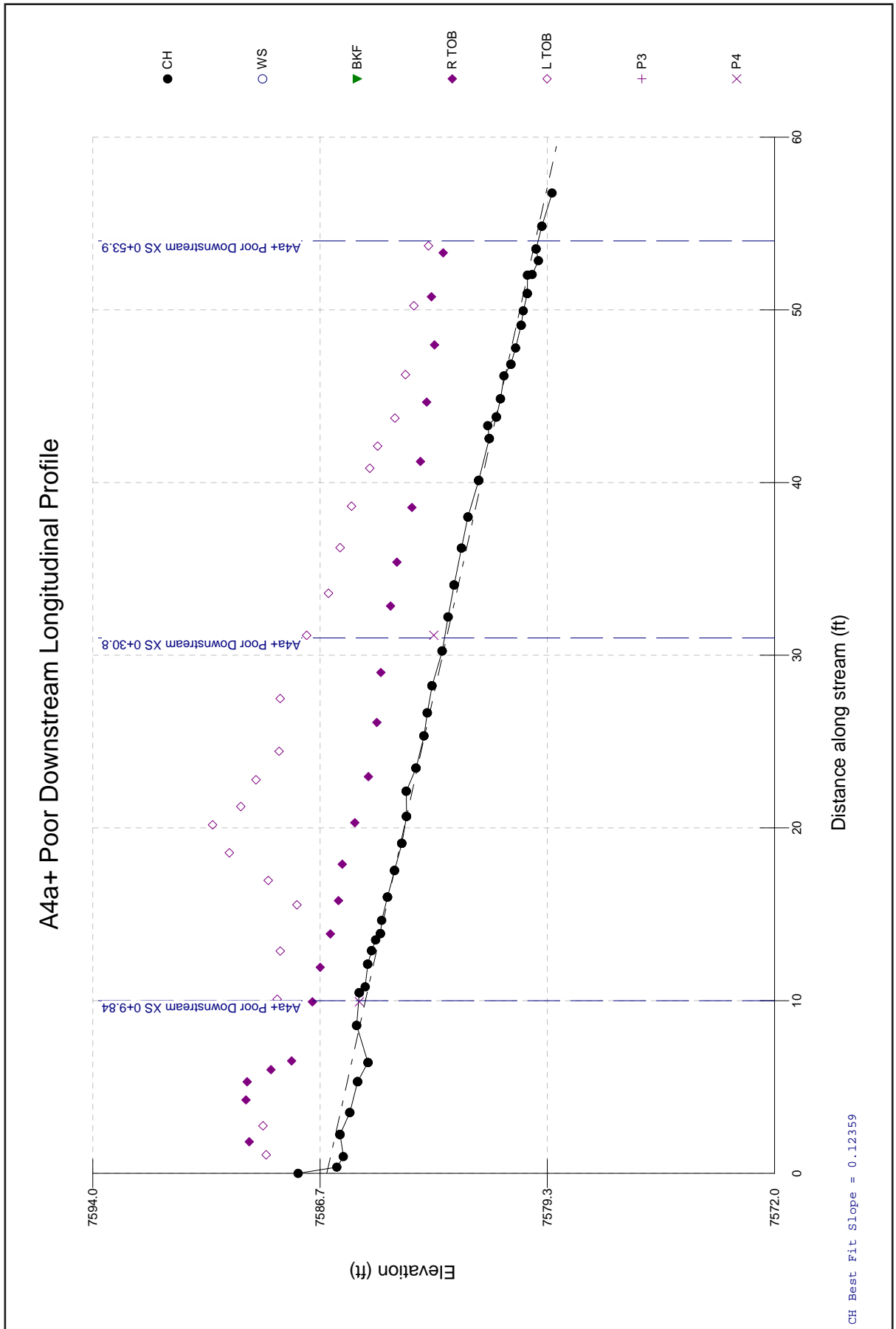
## A4a+ Poor Downstream Reach Location & Overview

The A4a+ Poor downstream reach is a 2<sup>nd</sup> order, ephemeral stream in the Trail Creek Watershed (**Figure C-2**) with a high sediment supply due to channel processes. The stability rating is “Poor” due to degradation, active incision, and lateral instability. The streambank erosion rate is *0.0785 tons/yr/ft*, more than an order of magnitude higher than its reference condition (*0.0017 tons/yr/ft*). The sediment supply rating is also *High* due to the same processes including a *Moderate Increase* in channel enlargement. The overall rating of “Poor” indicates a potential accelerated increase in flow-related sediment based on increased post-fire streamflow peak flows. The bankfull discharge for this small ephemeral stream is 0.41 cfs. The increase in flow using the WRENS model is *1.0 acre-ft*. The corresponding increase in bedload using the FLOWSED model is *2.6 tons/yr* and *4.2 tons/yr* of suspended sediment, with a total sediment increase of *6.8 tons/yr*. The pre-fire sediment yields were one-third of this value.

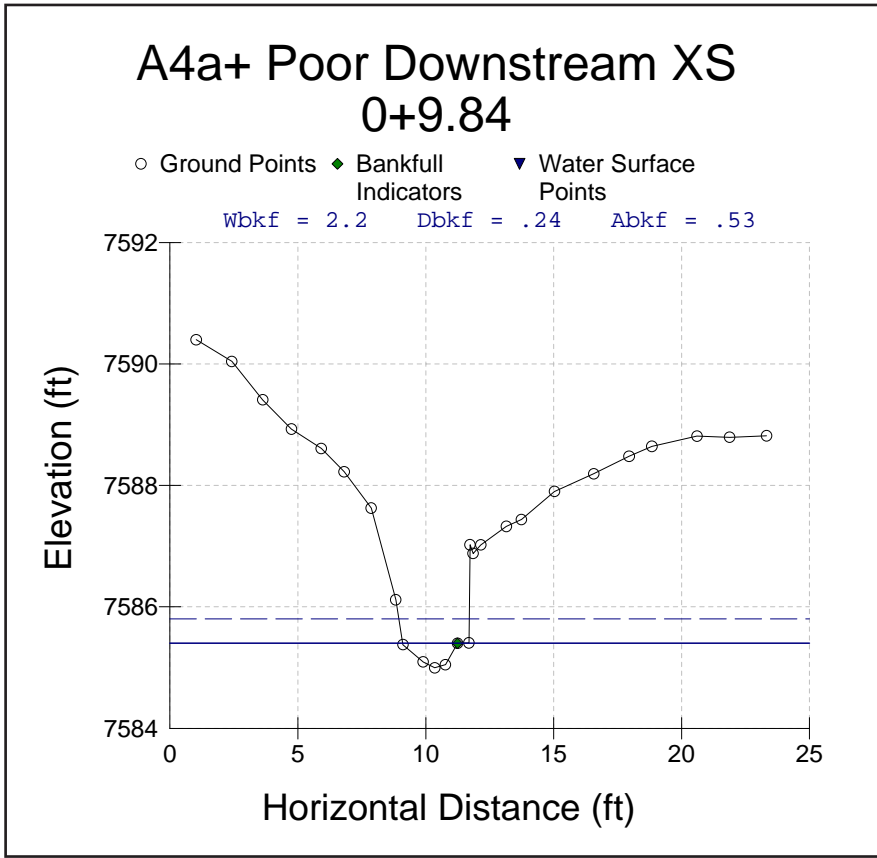
The photograph depicts the typical character of this representative A4a+ Poor stream type. The following graphs and summary worksheets provide the detail of the morphology, hydraulics, streambank erosion rates, and stability conditions responsible for the overall “Poor” rating.



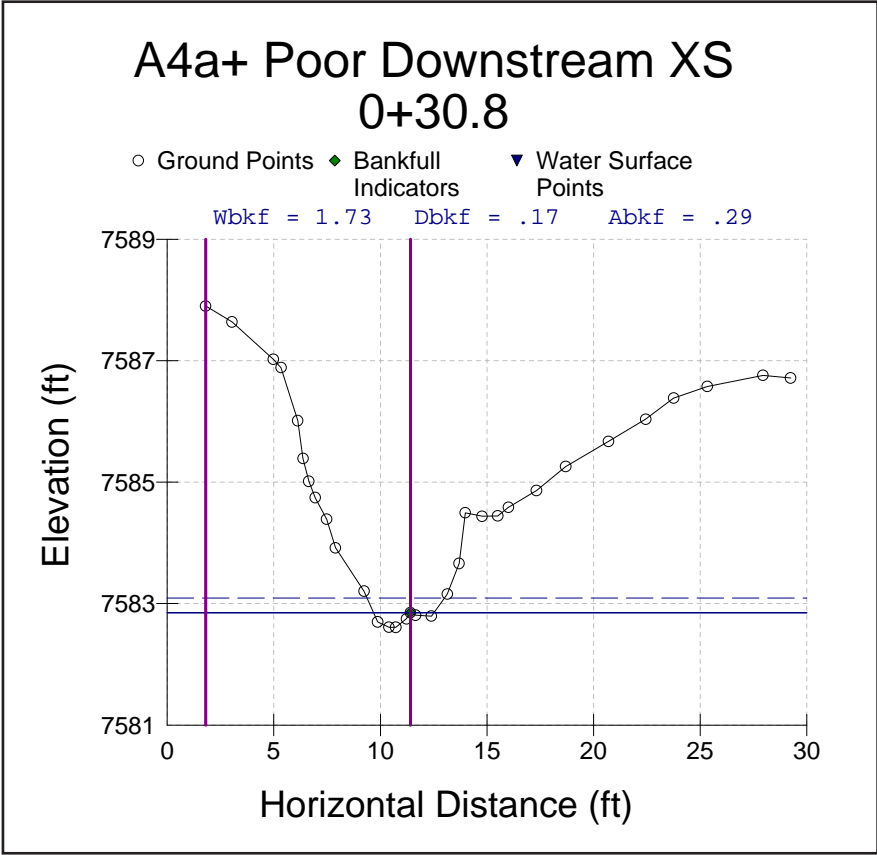
# Survey Summary



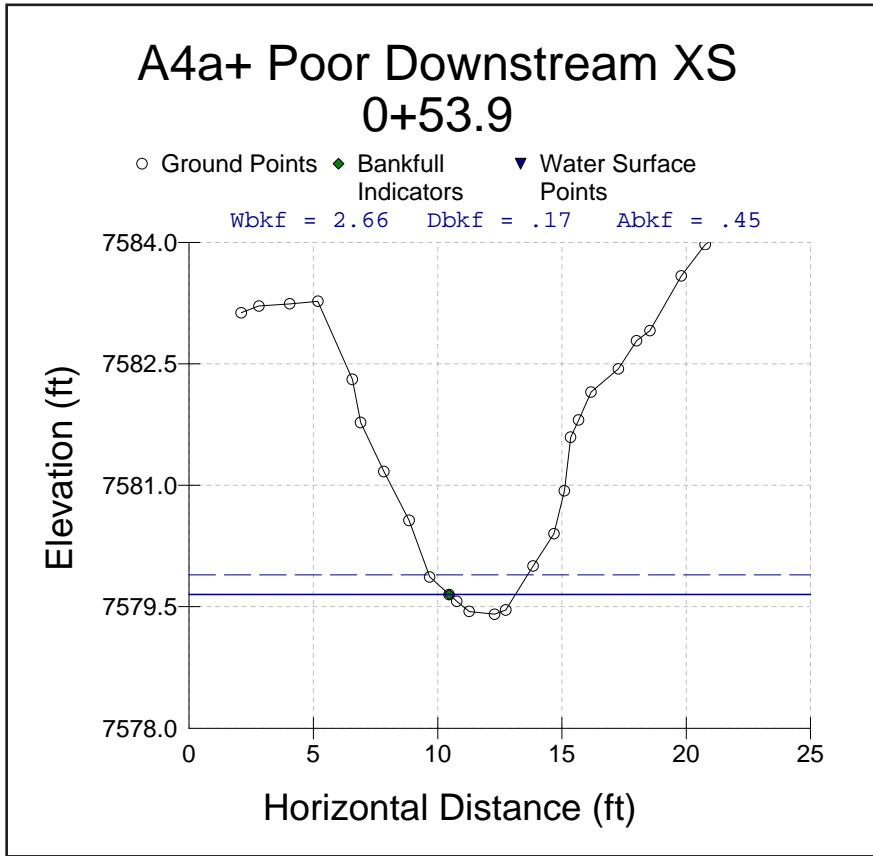
Longitudinal Profile (graph generated from RIVERMorph™)



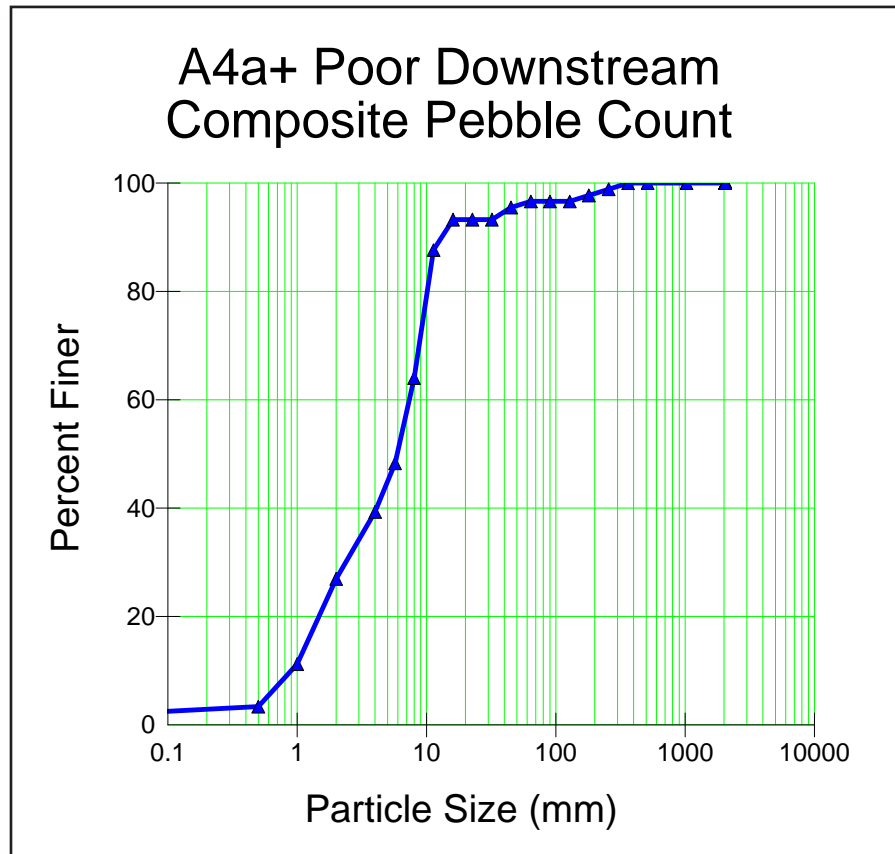
Representative Cross-section 0+9.84 (graph generated from RIVERMorph™)



Cross-section 0+30.8 (graph generated from RIVERMorph™)



Cross-section 0+53.9 (graph generated from RIVERMorph™)



Composite Pebble Count (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates							
Stream:	Trail Creek, A4a+ Poor Downstream			Location:	XS 0+9.84, Pike N.F., Colorado		
Date:	9/3/2010	Stream Type:	A4a+	Valley Type:	III		
Observers:	Chavez, Kasun & Gallagher			HUC:	_ _ _ _ _		
INPUT VARIABLES				OUTPUT VARIABLES			
Bankfull Riffle Cross-Sectional AREA	0.53	$A_{bkt}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.24	$d_{bkt}$ (ft)		
Bankfull Riffle WIDTH	2.20	$W_{bkt}$ (ft)	Wetted PERIMETER $\sim (2 * d_{bkt}) + W_{bkt}$	2.68	$W_p$ (ft)		
$D_{84}$ at Riffle	10.8	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.04	$D_{84}$ (ft)		
Bankfull SLOPE	0.1236	$S_{bkt}$ (ft / ft)	Hydraulic RADIUS $A_{bkt} / W_p$	0.20	R (ft)		
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness $R(ft) / D_{84} (ft)$	5.58	$R / D_{84}$		
Drainage Area	0.0027	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.887	$u^*$ (ft/sec)		
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE	
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$				6.26	ft / sec	3.32	cfs
2. Roughness Coefficient: a) Manning's $n$ from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.0094$				18.91	ft / sec	10.02	cfs
2. Roughness Coefficient: b) Manning's $n$ from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n =$ <input type="text"/>					ft / sec		cfs
2. Roughness Coefficient: c) Manning's $n$ from Jarrett (USGS): $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for $n = 0.228$				0.78	ft / sec	0.41	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) <input type="text"/>					ft / sec		cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) <input type="text"/>					ft / sec		cfs
4. Continuity Equations: a) Regional Curves $u = Q / A$ Return Period for Bankfull Discharge $Q =$ <input type="text"/> year					ft / sec		cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation ( $R/D_{84}$ ) – Estimation Method 1							
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.							
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.							
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.							
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.							

**Worksheet 5-3.** Level II stream classification.

Stream: <b>Trail Creek, A4a+ Poor Downstream Reach</b>	
Basin:	Drainage Area: acres <b>0.0027</b> mi <sup>2</sup>
Location: <b>Pike National Forest, Colorado</b>	
Twp.&Rge:	Sec.&Qtr.:
Cross-Section Monuments (Lat./Long.): <b>XS 0+9.84</b> Date: <b>9/3/2010</b>	
Observers: <b>Chavez, Kasun &amp; Gallagher</b>	Valley Type: <b>III</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>2.20</b> ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A_{bkf} / W_{bkf}$ ).	<b>0.24</b> ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>0.53</b> ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>9.17</b> ft/ft
<b>Maximum DEPTH (<math>d_{max}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>0.40</b> ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkd}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>2.75</b> ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>1.25</b> ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the median or dominant diameter of channel materials, as sampled proportionately from the channel surface, between the bankfull stage and Thalweg elevations.	<b>6</b> mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.1236</b> ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope ( $S_{val} / S$ ).	<b>1.09</b>

<div style="border: 1px solid black; padding: 5px; display: inline-block;">Stream Type</div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: #e0f0ff;"><b>A4a+</b></div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;">See Classification Key (Figure 2-14)</div>
--	---	---

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, A4a+ Poor Downstream Reach</b>		Location: <b>Pike National Forest, Colorado</b>								
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/3/2010</b>		Valley Type: <b>III</b>		Stream Type: <b>A4a+</b>				
<b>River Reach Dimension Summary Data.....1</b>										
<b>Riffle Dimensions*</b> , **, ***	<b>Riffle Dimensions**</b> , ***, ***		<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Width ( $W_{bkt}$ )		<b>2.2</b>	<b>1.7</b>	<b>2.7</b>	ft	Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	<b>0.42</b>	<b>0.29</b>	<b>0.53</b>
	Mean Riffle Depth ( $d_{bkt}$ )		<b>0.19</b>	<b>0.17</b>	<b>0.24</b>	ft	Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	<b>11.7</b>	<b>9.2</b>	<b>15.7</b>
	Maximum Riffle Depth ( $d_{max}$ )		<b>0.29</b>	<b>0.24</b>	<b>0.40</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>1.497</b>	<b>1.411</b>	<b>1.667</b>
	Width of Flood-Prone Area ( $W_{fpa}$ )		<b>2.91</b>	<b>2.01</b>	<b>3.97</b>	ft	Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )	<b>1.30</b>	<b>1.16</b>	<b>1.49</b>
	Riffle Inner Berm Width ( $W_{ib}$ )					ft	Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )			
	Riffle Inner Berm Depth ( $d_{ib}$ )					ft	Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )			
	Riffle Inner Berm Area ( $A_{ib}$ )					ft <sup>2</sup>	Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )			
	Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )									
<b>Pool Dimensions*</b> , **, ***	<b>Pool Dimensions**</b> , ***, ***		<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Pool Dimensions &amp; Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Pool Width ( $W_{bkfp}$ )					ft	Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )			
	Mean Pool Depth ( $d_{bkfp}$ )					ft	Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )			
	Pool Cross-Sectional Area ( $A_{bkfp}$ )					ft	Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )			
	Maximum Pool Depth ( $d_{maxp}$ )					ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )			
	Pool Inner Berm Width ( $W_{ibp}$ )					ft	Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )			
	Pool Inner Berm Depth ( $d_{ibp}$ )					ft	Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )			
	Pool Inner Berm Area ( $A_{ibp}$ )					ft <sup>2</sup>	Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )			
	Point Bar Slope ( $S_{pb}$ )					ft/ft	Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )			
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Run Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Run Width ( $W_{bkfr}$ )					ft	Run Width to Riffle Width ( $W_{bkfr} / W_{bkt}$ )			
	Mean Run Depth ( $d_{bkfr}$ )					ft	Mean Run Depth to Mean Riffle Depth ( $d_{bkfr} / d_{bkt}$ )			
	Run Cross-Sectional Area ( $A_{bkfr}$ )					ft	Run Area to Riffle Area ( $A_{bkfr} / A_{bkt}$ )			
	Maximum Run Depth ( $d_{maxr}$ )					ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )			
Run Width/Depth Ratio ( $W_{bkfr} / d_{bkfr}$ )					ft					
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Glide Dimensions &amp; Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Glide Width ( $W_{bkfg}$ )					ft	Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )			
	Mean Glide Depth ( $d_{bkfg}$ )					ft	Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )			
	Glide Cross-Sectional Area ( $A_{bkfg}$ )					ft	Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )			
	Maximum Glide Depth ( $d_{maxg}$ )					ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )			
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )					ft/ft	Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )			
	Glide Inner Berm Width ( $W_{ibg}$ )					ft	Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )			
	Glide Inner Berm Depth ( $d_{ibg}$ )					ft	Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )			
Glide Inner Berm Area ( $A_{ibg}$ )					ft <sup>2</sup>	Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )				
<b>Step**</b>	<b>Step Dimensions**</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Step Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Step Width ( $W_{bkfs}$ )					ft	Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )			
	Mean Step Depth ( $d_{bkfs}$ )					ft	Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )			
	Step Cross-Sectional Area ( $A_{bkfs}$ )					ft	Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )			
	Maximum Step Depth ( $d_{maxs}$ )					ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )										



**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, A4a+ Poor Downstream Reach</b>		Location: <b>Pike National Forest, Colorado</b>										
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/3/2010</b>		Valley Type: <b>III</b>		Stream Type: <b>A4a+</b>						
<b>River Reach Summary Data.....2</b>												
<b>Hydraulics</b>	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )		<b>0.78</b>		ft/sec		Estimation Method	<b>Manning's n from Jarrett</b>				
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )		<b>0.41</b>		cfs		Drainage Area	<b>0.0027</b> mi <sup>2</sup>				
<b>Channel Pattern</b>	<b>Geometry</b>			<b>Dimensionless Geometry Ratios</b>								
	Linear Wavelength ( $\lambda$ )	Mean	Min	Max	ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )	Mean	Min	Max			
	Stream Meander Length ( $L_m$ )				ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )						
	Radius of Curvature ( $R_c$ )				ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )						
	Belt Width ( $W_{bkt}$ )	<b>13.8</b>			ft	Meander Width Ratio ( $W_{bkt} / W_{bkt}$ )	<b>6.30</b>					
	Arc Length ( $L_a$ )				ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )						
	Riffle Length ( $L_r$ )				ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )						
	Individual Pool Length ( $L_p$ )				ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )						
Pool to Pool Spacing ( $P_s$ )				ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )							
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )	<b>0.1347</b>	ft/ft	Average Water Surface Slope (S)	<b>0.1236</b>	ft/ft	Sinuosity ( $S_{val} / S$ )	<b>1.09</b>				
	Stream Length (SL)	<b>72.1</b>	ft	Valley Length (VL)	<b>66.0</b>	ft	Sinuosity (SL / VL)	<b>1.09</b>				
	Low Bank Height (LBH)	start: <b>2.05</b>	ft	Max Bankfull Depth ( $d_{max}$ )	start: <b>0.40</b>	ft	Bank-Height Ratio (BHR) ( $LBH / d_{max}$ )	start: <b>5.1</b>				
		end:	ft		end:	ft		end:				
	<b>Facet Slopes</b>			<b>Dimensionless Facet Slope Ratios</b>								
	Riffle Slope ( $S_{rif}$ )	Mean	Min	Max	ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rif} / S$ )	Mean	Min	Max			
	Run Slope ( $S_{run}$ )				ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )						
	Pool Slope ( $S_p$ )				ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )						
	Glide Slope ( $S_g$ )				ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )						
	Step Slope ( $S_s$ )				ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )						
	<b>Max Depths<sup>a</sup></b>			<b>Dimensionless Depth Ratios</b>								
	Max Riffle Depth ( $d_{max}$ )	Mean	Min	Max	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	Mean	Min	Max			
	Max Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )						
	Max Pool Depth ( $d_{maxp}$ )				ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )						
	Max Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )						
Max Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )							
<b>Channel Materials</b>	<b>Reach<sup>b</sup></b>			<b>Riffle<sup>c</sup></b>			<b>Bar</b>			<b>Protrusion Height<sup>d</sup></b>		
	% Silt/Clay	<b>0</b>			$D_{16}$	<b>1.30</b>					mm	
	% Sand	<b>27</b>			$D_{35}$	<b>3.30</b>					mm	
	% Gravel	<b>70</b>			$D_{50}$	<b>5.95</b>					mm	
	% Cobble	<b>2</b>			$D_{84}$	<b>10.79</b>					mm	
	% Boulder	<b>1</b>			$D_{95}$	<b>42.05</b>					mm	
	% Bedrock	<b>0</b>			$D_{100}$	<b>361.99</b>					mm	

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

## Stability Indices

**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation					
Stream: <b>Trail Creek, A4a+ Poor Downstream Reach</b>		Location: <b>Pike National Forest, Colorado</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>	Reference reach: <input type="checkbox"/>	Disturbed (impacted reach): <input checked="" type="checkbox"/>	Date: <b>9/3/2010</b>		
Existing species composition: <b>Ponderosa Pine Seedlings, Forbs/Grass</b>		Potential species composition: <b>Mature Ponderosa Pine, Shrubs, Forb/Grass</b>			
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition
<b>1. Overstory</b>	Canopy layer	5%	1%	<b>Ponderosa Pine</b>	100%
					100%
<b>2. Understory</b>	Shrub layer		1%	<b>Raspberry</b>	100%
					100%
<b>3. Ground level</b>	Herbaceous		48%	<b>Geranium</b>	50%
				<b>Grass (little bluestem, grama, cheat)</b>	50%
					100%
	Leaf or needle litter		20%	<b>Remarks:</b> Condition, vigor and/or usage of existing reach: <b>Ponderosa Pine beginning to regenerate</b>	
	Bare ground		30%		
			<b>Column total = 100%</b>		

\*Based on crown closure.  
\*\*Based on basal area to surface area.

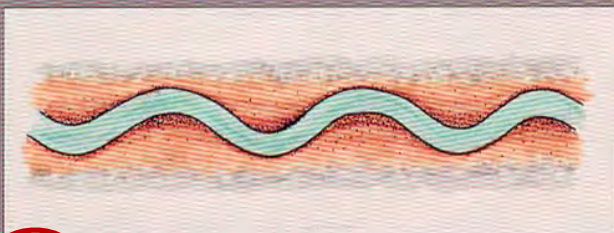

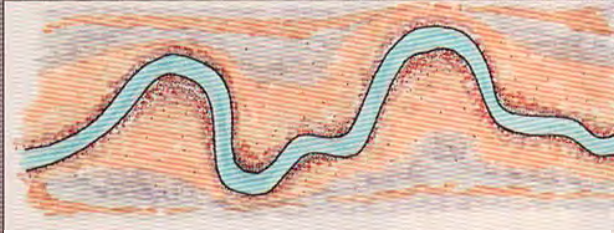
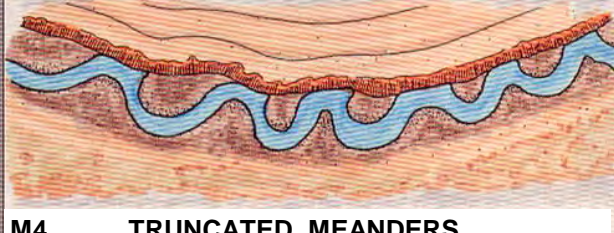

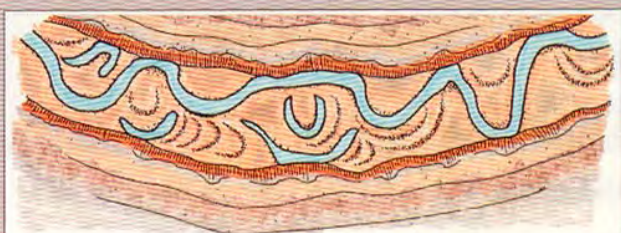
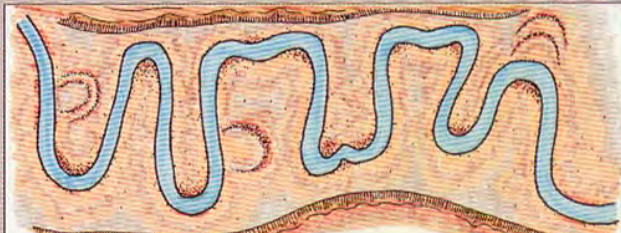

**Worksheet 5-7.** Flow regime.

<b>FLOW REGIME</b>								
Stream: <b>Trail Creek, A4a+ Poor Dwnstm</b>			Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>Chavez, Kasun &amp; Gallagher</b>						Date: <b>9/3/2010</b>		
<b>List ALL COMBINATIONS that APPLY.....</b>	<b>E1</b>	<b>E2</b>	<b>E8</b>					
<b>General Category</b>								
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation							
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
<b>P</b>	Perennial stream channels: Surface water persists yearlong.							
<b>Specific Category</b>								
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
<b>4</b>	Streamflow regulated by glacial melt.							
<b>5</b>	Ice flows/ice torrents from ice dam breaches.							
<b>6</b>	Alternating flow/backwater due to tidal influence.							
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.							
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
<b>9</b>	Rain-on-snow generated runoff.							

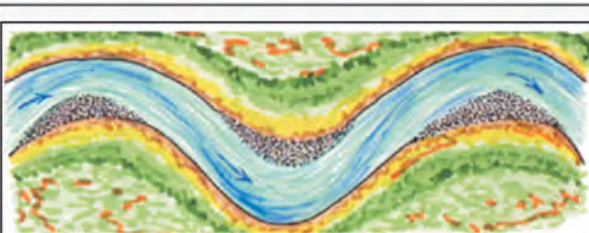

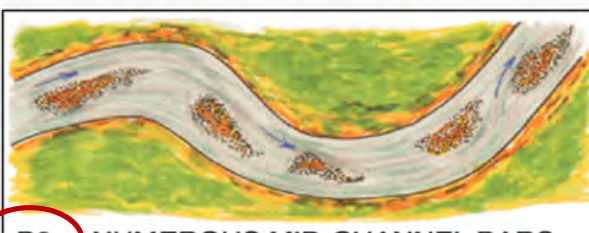

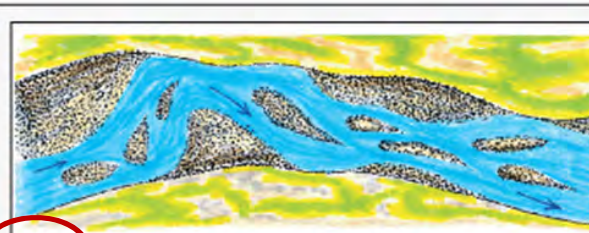
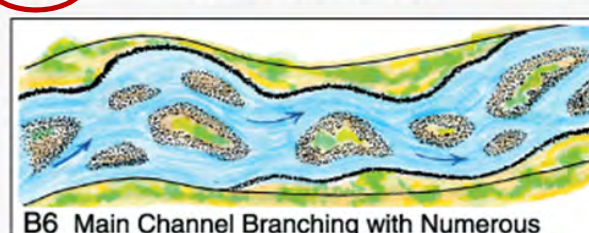
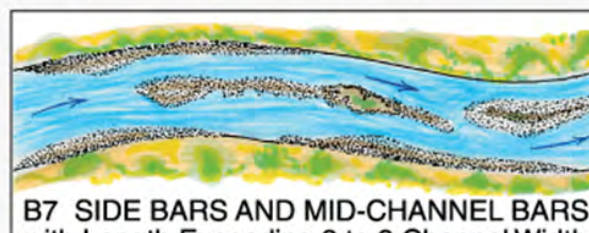
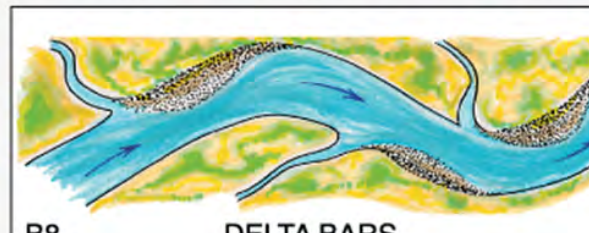
**Worksheet 5-8.** Stream order & stream size.

<b>Stream Size and Order</b>			
Stream:	<b>Trail Creek, A4a+ Poor Downstream</b>		
Location:	<b>Pike National Forest, Colorado</b>		
Observers:	<b>Chavez, Kasun &amp; Gallagher</b>		
Date:	<b>9/3/2010</b>		
<b>Stream Size Category and Order</b> ↗			<b>S-2(2)</b>
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0.305	<1	<input type="checkbox"/>
<b>S-2</b>	<b>0.3 – 1.5</b>	<b>1 – 5</b>	<input checked="" type="checkbox"/>
S-3	1.5 – 4.6	5 – 15	<input type="checkbox"/>
S-4	4.6 – 9	15 – 30	<input type="checkbox"/>
S-5	9 – 15	30 – 50	<input type="checkbox"/>
S-6	15 – 22.8	50 – 75	<input type="checkbox"/>
S-7	22.8 – 30.5	75 – 100	<input type="checkbox"/>
S-8	30.5 – 46	100 – 150	<input type="checkbox"/>
S-9	46 – 76	150 – 250	<input type="checkbox"/>
S-10	76 – 107	250 – 350	<input type="checkbox"/>
S-11	107 – 150	350 – 500	<input type="checkbox"/>
S-12	150 – 305	500 – 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
<b>Stream Order</b>			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			

Worksheet 5-9. Meander patterns.

<b>Meander Patterns</b>					
Stream:	Trail Creek, A4a+ Poor Downstream	Location:	Pike National Forest, CO		
Observers:	Chavez, Kasun & Gallagher		Date:	9/3/2010	
List ALL CATEGORIES that APPLY	<b>M1</b>				
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>					
					
<b>M1</b> REGULAR MEANDERS					
					
<b>M2</b> TORTUOUS MEANDERS					
					
<b>M3</b> IRREGULAR MEANDERS					
					
<b>M4</b> TRUNCATED MEANDERS					
					
<b>M5</b> UNCONFINED MEANDER SCROLLS					
					
<b>M6</b> CONFINED MEANDER SCROLLS					
					
<b>M7</b> DISTORTED MEANDER LOOPS					
					
<b>M8</b> IRREGULAR MEANDERS with oxbows and					

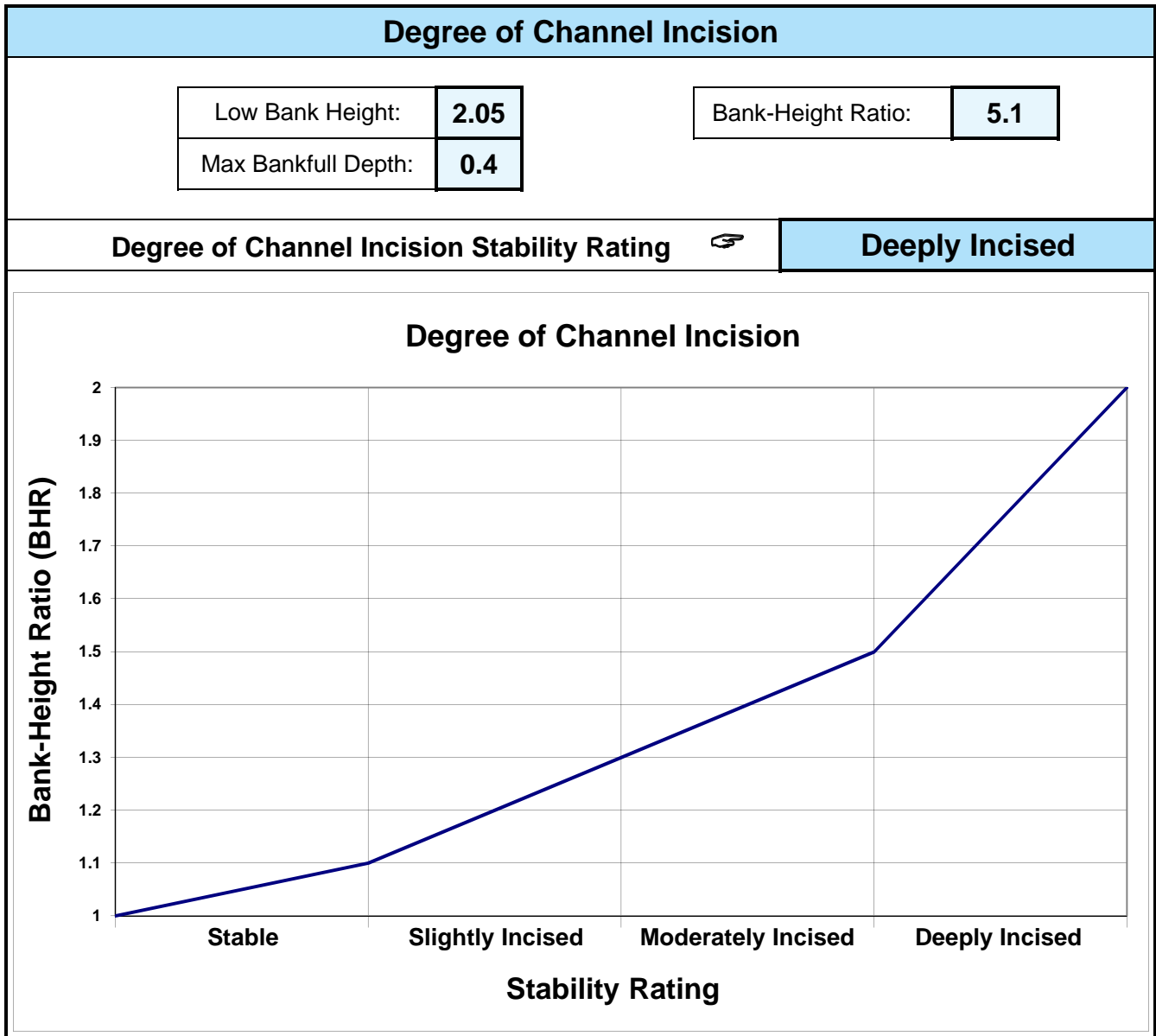
**Worksheet 5-10.** Depositional patterns.

<b>Depositional Patterns</b>					
Stream:	Trail Creek, A4a+ Poor Downstream	Location:	Pike National Forest, Colorado		
Observers:	Chavez, Kasun & Gallagher	Date:	9/3/2010		
List ALL CATEGORIES that APPLY	<b>B3</b>	<b>B4</b>	<b>B5</b>		
<i>Various Depositional Features modified from Galay et al. (1973)</i>					
	<b>B1</b> POINT BARS				
	<b>B2</b> POINT BARS with Few MID-CHANNEL BARS				
	<b>B3</b> NUMEROUS MID-CHANNEL BARS				
	<b>B4</b> SIDE BARS				
	<b>B5</b> DIAGONAL BARS				
	<b>B6</b> Main Channel Branching with Numerous MID-CHANNEL BARS and Islands				
	<b>B7</b> SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths				
	<b>B8</b> DELTA BARS				

## Worksheet 5-11. Channel blockages.

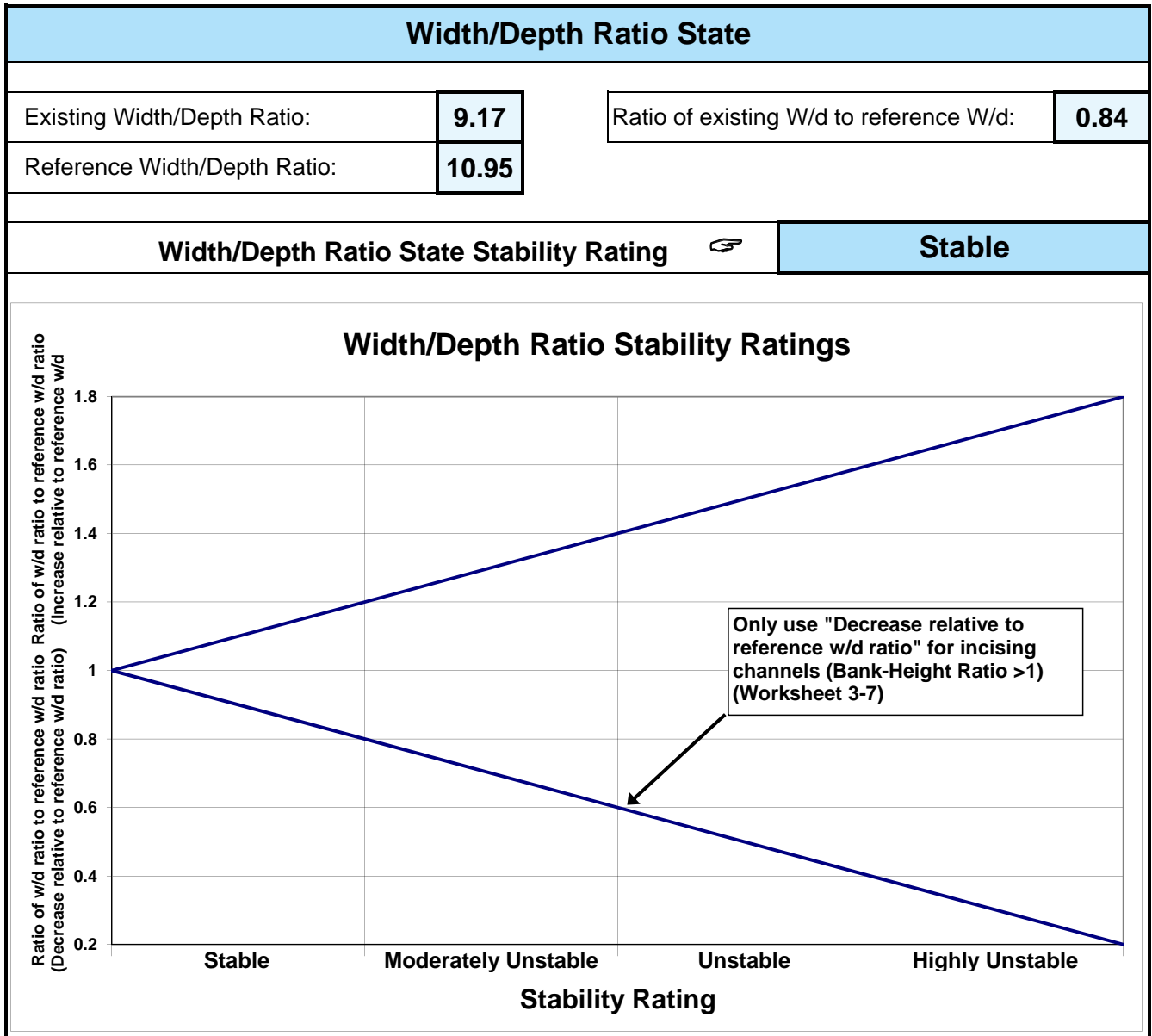
Channel Blockages		
Stream: <b>Trail Creek, A4a+ Poor Downstream Reach</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/3/2010</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input checked="" type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input type="checkbox"/>
<b>D4</b> Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

**Worksheet 5-12.** Degree of channel incision.

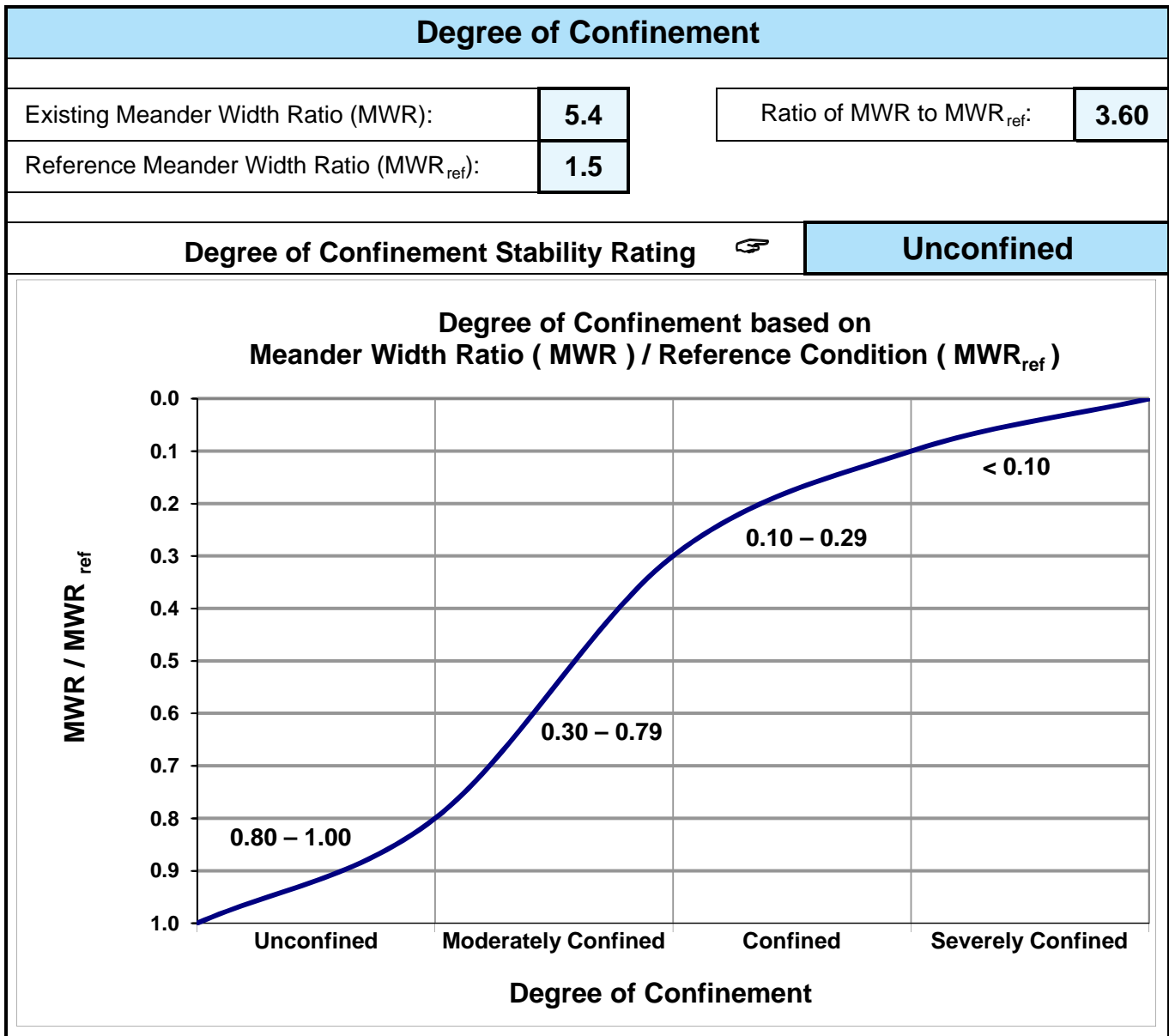




Worksheet 5-13. Width/depth ratio state.



**Worksheet 5-14.** Degree of channel confinement (lateral containment).



**Worksheet 5-15. Pfrankuch channel stability rating.**

Stream: Trail Creek, A4a+ Poor Downstream		Location: Pike National Forest, CO		Valley Type: III		Observers: Chavez, Kasun & Gallagher		Date: 9/3/2010																	
Local- tion	Key	Category	Excellent	Good	Fair	Poor	Rating	Description	Rating																
Upper banks	1	Landform slope	Bank slope gradient <30%.	Bank slope gradient 30–40%.	Bank slope gradient 40–60%.	Bank slope gradient > 60%.	4	Bank slope gradient > 60%.	6																
	2	Mass erosion	No evidence of past or future mass erosion.	Infrequent. Mostly healed over. Low future potential.	Frequent or large, causing sediment nearly yearlong.	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.	3		9																
	3	Debris jam potential	Essentially absent from immediate channel area.	Present, but mostly small twigs and limbs.	Moderate to heavy amounts, mostly larger sizes.	Moderate to heavy amounts, predominantly larger sizes.	2		6																
	4	Vegetative bank protection	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	70–90% density. Fewer species or less vigor suggest less dense or deep root mass.	50–70% density. Lower vigor and fewer species from a shallow, discontinuous root mass.	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.	3		9																
Lower banks	5	Channel capacity	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0.	Bankfull stage is contained within banks. Width/depth ratio departure from reference width/depth ratio = 1.0–1.2. Bank-Height Ratio (BHR) = 1.0–1.1.	Bankfull stage is not contained. Width/depth ratio departure from reference width/depth ratio = 1.2–1.4. Bank-Height Ratio (BHR) > 1.1–1.3.	Bankfull stage is not contained; over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.	1		3																
	6	Bank rock content	> 65% with large angular boulders. 12"+ common.	40–65%. Mostly boulders and small cobbles 6–12".	20–40%. Most in the 3–6" diameter class.	<20% rock fragments of gravel sizes, 1–3" or less.	2		6																
	7	Obstructions to flow	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	Frequent obstructions and deflectors cause bank erosion yearlong. Sediment traps full, channel migration occurring.	2		6																
	8	Cutting	Little or none. Infrequent raw banks	Some, intermittently at outcrops and constrictions. Raw banks may be up to 12".	Significant. Cuts 12–24" high. Root mat overhangs and sloughing evident.	High. Failure of overhangs frequent.	4		12																
	9	Deposition	Little or no enlargement of channel or point bars.	Some new bar increase, mostly from coarse gravel.	Moderate deposition of new gravel and coarse sand on old and some new bars.	Extensive deposit of predominantly fine particles. Accelerated bar development.	4		12																
Bottom	10	Rock angularity	Sharp edges and corners. Plane surfaces rough.	Rounded corners and edges. Surfaces smooth and flat.	Comers and edges well rounded in 2 dimensions.	Well rounded in all dimensions, surfaces smooth.	1		3																
	11	Brightness	Surfaces dull, dark or stained. Generally not bright.	Mostly dull, but may have <35% bright surfaces.	Mixture dull and bright, i.e., 35–65% mixture range.	Predominantly bright, > 65%, exposed or scoured surfaces.	1		3																
	12	Consolidation of particles	Assorted sizes tightly packed or overlapping.	Moderately packed with some overlapping.	Mostly loose assortment with no apparent overlap.	No packing evident. Loose assortment, easily moved.	2		6																
	13	Bottom size distribution	No size change evident. Stable material 80–100%.	Distribution shift light. Stable material 50–80%.	Moderate change in sizes. Stable materials 20–50%.	Marked distribution change. Stable materials 0–20%.	4		12																
	14	Scouring and deposition	<5% of bottom affected by scour or deposition.	5–30% affected. Scour at constrictions and where grades steepen. Some deposition in pools.	30–50% affected. Deposits and scour at obstructions, constrictions and bends. Some filling of pools.	More than 50% of the bottom in a state of flux or change nearly yearlong.	6		18																
	15	Aquatic vegetation	Abundant growth moss-like, dark green perennial. In swift water too.	Common. Algae forms in low velocity and pool areas. Moss here too.	Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick.	Perennial types scarce or absent. Yellow-green, short-term bloom may be present.	2		3																
			<b>Excellent total = 0</b>	<b>Good total = 12</b>	<b>Fair total = 0</b>	<b>Poor total = 128</b>																			
Stream type	A1	A2	A3	A4	A5	A6	B1	B2	B3	B4	B5	B6	C1	C2	C3	C4	C5	C6	D3	D4	D5	D6	Grand total =		
Good (Stable)	38-43	38-43	54-90	60-95	60-95	50-80	38-45	38-45	40-60	40-64	48-68	40-60	38-50	38-50	60-85	70-90	70-90	60-85	85-107	85-107	85-107	85-107	85-107	67-98	140
Fair (Mod. unstable)	44-47	44-47	91-129	96-132	96-142	81-110	46-58	46-58	61-78	65-84	69-88	61-78	51-61	51-61	86-105	91-110	91-110	86-105	108-132	108-132	108-132	108-132	108-132	99-125	A4a+
Poor (Unstable)	48+	48+	130+	130+	143+	111+	59+	59+	79+	85+	89+	79+	62+	62+	106+	111+	111+	106+	133+	133+	133+	133+	133+	126+	A4a+
Stream type	DA3	DA4	DA5	DA6	E3	E4	E5	E6	F1	F2	F3	F4	F5	F6	G1	G2	G3	G4	G5	G6	G6	G6	G6	Modified channel stability rating =	
Good (Stable)	40-63	40-63	40-63	40-63	50-75	50-75	50-75	40-63	60-85	60-85	85-110	85-110	90-115	80-95	40-60	40-60	40-60	85-107	90-112	90-112	90-112	90-112	90-112	A4a+	
Fair (Mod. unstable)	64-86	64-86	64-86	64-86	76-96	76-96	76-96	64-86	86-105	86-105	111-125	111-125	116-130	96-110	61-78	61-78	108-120	108-120	113-125	113-125	108-120	108-120	108-120	A4a+	
Poor (Unstable)	87+	87+	87+	87+	87+	87+	87+	87+	106+	106+	126+	126+	131+	111+	79+	79+	121+	121+	126+	126+	121+	121+	121+	Poor	

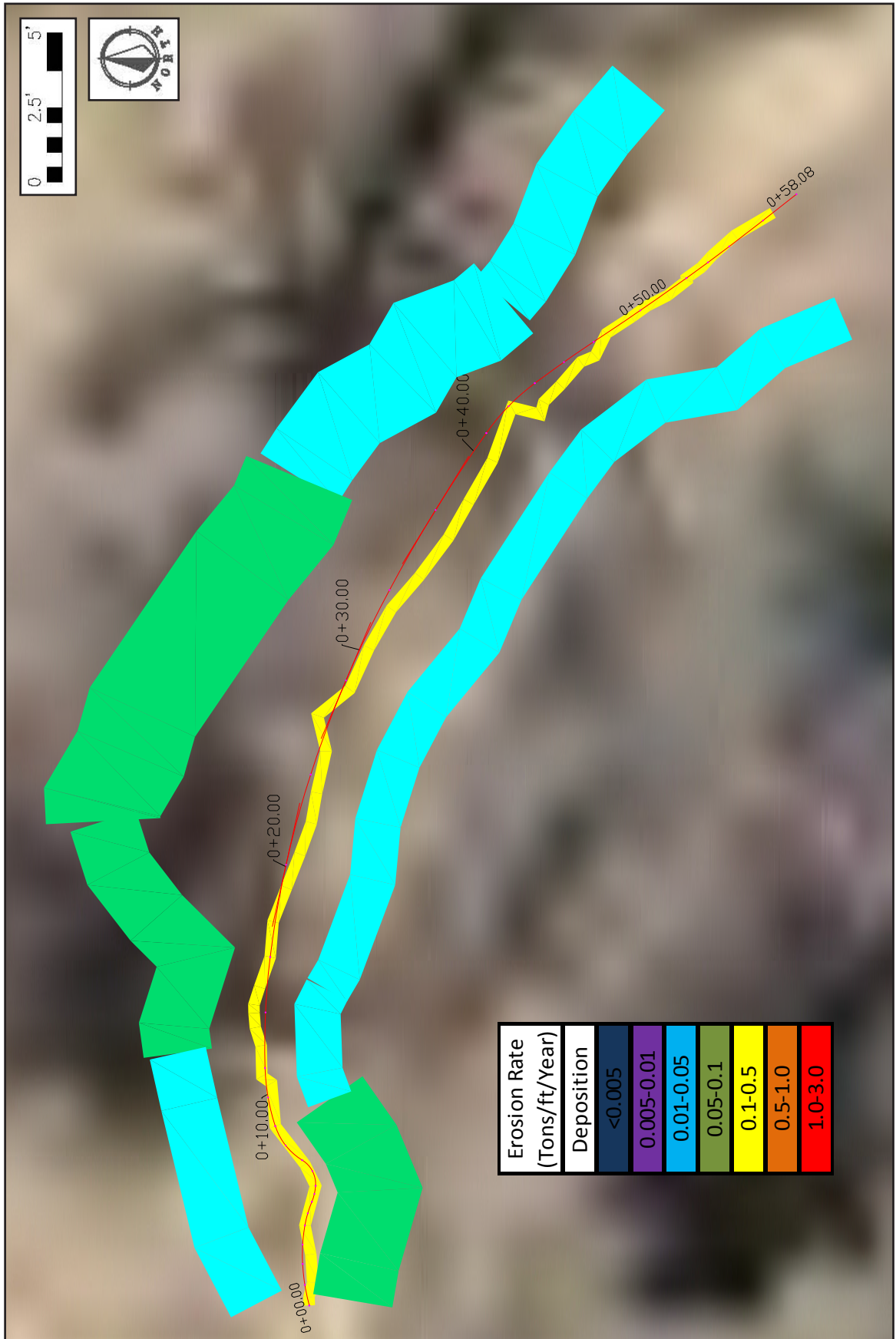
\*Rating is adjusted to potential stream type, not existing.

## BANCS Model – Streambank Erosion

**Worksheet 5-18.** Annual streambank erosion estimates.

Stream: <b>Trail Creek, A4a+ Poor Downstream</b>		Location: <b>Pike National Forest, Colorado</b>					
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>58</b>				Date: <b>9/3/2010</b>	
Observers: <b>Chavez, Kasun, Gallagher</b>		Valley Type: <b>III</b>			Stream Type: <b>A4a+</b>		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 5-16) (adjective)	NBS rating (Worksheet 5-17) (adjective)	Bank erosion rate (Figure 5-34 or 5-35) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [(4)×(5)×(6)] (ft <sup>3</sup> /yr)	Erosion Rate (tons/yr/ft) {[ (7)/27 ] × 1.3 / (5)}
1. R_0+00 - 0+09	Extreme	Low	0.41998	9.0	3.5	13.23	0.07077
2. L_0+00 - 0+11	Very High	Low	0.25042	11.0	2.5	6.89	0.03014
3. R_0+09 - 0+15	Very High	Low	0.25042	6.0	2.0	3.01	0.02411
4. L_0+11 - 0+19	Extreme	Low	0.41998	8.0	3.0	10.08	0.06066
5. R_0+15 - 0+58	Very High	Low	0.25042	43.0	2.0	21.54	0.02411
6. L_0+19 - 0+35	Very High	Low	0.25042	16.0	5.0	20.03	0.06029
7. L_0+35 - 0+45	Very High	Low	0.25042	10.0	4.0	10.02	0.04823
8. L_0+45 - 0+58	Very High	Low	0.25042	13.0	3.0	9.77	0.03617
9							
10							
11							
12							
13							
14							
15							
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					Total Erosion (ft <sup>3</sup> /yr)	94.55	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					Total Erosion (yds <sup>3</sup> /yr)	3.50	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					Total Erosion (tons/yr)	4.55	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					Total Erosion (tons/yr/ft)	0.0785	

Streambank Erosion Map



## FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Equation Type		Equation Source				Equation		Bankfull Discharge (cfs)			Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)	
1. Bedload Sediment		"Good/Fair" Pagosa				$y = -0.0113 + 1.0139x^{2.1929}$		0.41			0.0015		0.0182	
2. Suspended Sediment		"Good/Fair" Pagosa				$y = 0.06336 + 0.9326x^{2.4085}$								
		From Dimensional Flow-Duration Curve				From Sediment Rating Curves				Calculate		Calculate Sediment Yield		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Percentage of Time	Daily Mean Discharge (cfs)	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimension-less Streamflow	Dimension-less Sediment Discharge (S/S <sub>bed</sub> )	Suspended Sediment Discharge (tons/day)	Dimension-less Discharge (b <sub>y</sub> /b <sub>bed</sub> )	Bedload Sediment Discharge	Time Adjusted Streamflow [(5)×(6)]	Suspended Sediment [(5)×(9)]	Bedload Sediment [(5)×(11)]	Suspended Sediment + Bedload Sediment [(13)×(14)]
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>bed</sub> )	(S/S <sub>bed</sub> )	(tons/day)	(b <sub>y</sub> /b <sub>bed</sub> )	(tons/day)	(cfs)	(tons)	(tons)	(tons)
0%	1.0													
0.10%	0.9	0.05%	0.09%	0.34	1.0	2.363	7.461	0.00	6.670	0.94	0.3	0.00	0.32	0.32
0.25%	0.8	0.08%	0.15%	0.55	0.8	2.036	5.232	0.00	4.809	0.68	0.5	0.00	0.37	0.37
0.50%	0.7	0.13%	0.25%	0.91	0.7	1.761	3.706	0.00	3.494	0.49	0.7	0.00	0.45	0.45
0.75%	0.6	0.13%	0.25%	0.91	0.6	1.513	2.592	0.00	2.502	0.35	0.6	0.00	0.32	0.32
1%	0.5	0.13%	0.25%	0.91	0.5	1.300	1.817	0.00	1.790	0.25	0.5	0.00	0.23	0.23
1.5%	0.4	0.25%	0.50%	1.83	0.5	1.120	1.289	0.00	1.289	0.18	0.8	0.00	0.33	0.33
2%	0.4	0.25%	0.50%	1.83	0.4	0.949	0.886	0.00	0.893	0.13	0.7	0.00	0.23	0.23
3%	0.3	0.50%	1.00%	3.65	0.3	0.795	0.600	0.00	0.602	0.09	1.2	0.00	0.31	0.31
4%	0.3	0.50%	1.00%	3.65	0.3	0.674	0.424	0.00	0.415	0.06	1.0	0.00	0.21	0.21
5%	0.2	0.50%	1.00%	3.65	0.2	0.587	0.322	0.00	0.304	0.04	0.9	0.00	0.16	0.16
10%	0.1	2.50%	5.00%	18.25	0.2	0.450	0.200	0.00	0.165	0.02	3.4	0.00	0.43	0.43
20%	0.1	5.00%	10.00%	36.50	0.1	0.269	0.103	0.00	0.045	0.01	4.0	0.00	0.23	0.23
30%	0.1	5.00%	10.00%	36.50	0.1	0.158	0.075	0.00	0.006	0.00	2.4	0.00	0.03	0.03
40%	0.0	5.00%	10.00%	36.50	0.0	0.108	0.068	0.00	0.000	0.00	1.6	0.00	0.00	0.00
50%	0.0	5.00%	10.00%	36.50	0.0	0.079	0.066	0.00	0.000	0.00	1.2	0.00	0.00	0.00
60%	0.0	5.00%	10.00%	36.50	0.0	0.061	0.065	0.00	0.000	0.00	0.9	0.00	0.00	0.00
70%	0.0	5.00%	10.00%	36.50	0.0	0.047	0.064	0.00	0.000	0.00	0.7	0.00	0.00	0.00
80%	0.0	5.00%	10.00%	36.50	0.0	0.039	0.064	0.00	0.000	0.00	0.6	0.00	0.00	0.00
90%	0.0	5.00%	10.00%	36.50	0.0	0.032	0.064	0.00	0.000	0.00	0.5	0.00	0.00	0.00
100%	0.0	5.00%	10.00%	36.50	0.0	0.016	0.064	0.00	0.000	0.00	0.2	0.00	0.00	0.00
<b>Annual Totals:</b>											22.6 (cfs)	0.0 (tons/yr)	3.6 (tons/yr)	3.6 (tons/yr)
											44.8 (acre-ft)			

Worksheet 19b. Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Equation Type		Equation Source			Equation		Bankfull Discharge (cfs)		Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)			
1. Bedload Sediment		"Poor" Pagosa			$Y = 0.07176x + 1.02176x^{2.3772}$		0.41		0.0012		56.45			
2. Suspended Sediment		"Poor" Pagosa			$Y = 0.0989x + 0.9213x^{3.659}$									
From Dimensional Flow-Duration Curve														
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Percentage of Time	Daily Mean Discharge (cfs)	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimension-less Streamflow	Dimension-less Suspended Sediment Discharge ( $S/S_{bed}$ )	Suspended Sediment Discharge (tons/day)	Dimension-less Bedload Discharge ( $b_b/b_{bed}$ )	Bedload Sediment Discharge (tons/day)	Time Adjusted Streamflow $[(5) \times (6)]$ (cfs)	Suspended Sediment $[(5) \times (9)]$ (tons)	Bedload Sediment $[(5) \times (11)]$ (tons)	Suspended Sediment + Bedload Sediment $[(13) \times (14)]$ (tons)
0%	1.1													
0.10%	0.9	0.05%	0.09%	0.34	1.0	2.387	22.319	3.33	8.152	0.92	0.3	1.14	0.32	1.46
0.25%	0.8	0.08%	0.15%	0.55	0.8	2.060	13.060	1.68	5.765	0.65	0.5	0.92	0.36	1.28
0.50%	0.7	0.13%	0.25%	0.91	0.7	1.785	7.767	0.87	4.120	0.46	0.7	0.79	0.42	1.21
0.75%	0.6	0.13%	0.25%	0.91	0.6	1.537	4.537	0.44	2.910	0.33	0.6	0.40	0.30	0.70
1%	0.5	0.13%	0.25%	0.91	0.5	1.324	2.669	0.22	2.061	0.23	0.5	0.20	0.21	0.41
1.5%	0.4	0.25%	0.50%	1.83	0.5	1.144	1.605	0.11	1.478	0.17	0.9	0.21	0.30	0.51
2%	0.4	0.25%	0.50%	1.83	0.4	0.972	0.930	0.06	1.028	0.12	0.7	0.10	0.21	0.31
3%	0.3	0.50%	1.00%	3.65	0.3	0.818	0.541	0.03	0.706	0.08	1.2	0.10	0.29	0.39
4%	0.3	0.50%	1.00%	3.65	0.3	0.696	0.344	0.01	0.504	0.06	1.0	0.05	0.21	0.26
5%	0.2	0.50%	1.00%	3.65	0.2	0.607	0.247	0.01	0.384	0.04	0.9	0.03	0.16	0.19
10%	0.1	2.50%	5.00%	18.25	0.2	0.465	0.155	0.00	0.238	0.03	3.5	0.08	0.49	0.57
20%	0.1	5.00%	10.00%	36.50	0.1	0.275	0.107	0.00	0.119	0.01	4.1	0.07	0.49	0.56
30%	0.1	5.00%	10.00%	36.50	0.1	0.159	0.100	0.00	0.085	0.01	2.4	0.04	0.35	0.38
40%	0.0	5.00%	10.00%	36.50	0.0	0.108	0.099	0.00	0.077	0.01	1.6	0.02	0.32	0.34
50%	0.0	5.00%	10.00%	36.50	0.0	0.079	0.099	0.00	0.074	0.01	1.2	0.02	0.31	0.32
60%	0.0	5.00%	10.00%	36.50	0.0	0.061	0.099	0.00	0.073	0.01	0.9	0.01	0.30	0.31
70%	0.0	5.00%	10.00%	36.50	0.0	0.047	0.099	0.00	0.072	0.01	0.7	0.01	0.30	0.31
80%	0.0	5.00%	10.00%	36.50	0.0	0.039	0.099	0.00	0.072	0.01	0.6	0.01	0.30	0.31
90%	0.0	5.00%	10.00%	36.50	0.0	0.032	0.099	0.00	0.072	0.01	0.5	0.01	0.30	0.30
100%	0.0	5.00%	10.00%	36.50	0.0	0.016	0.099	0.00	0.072	0.01	0.2	0.00	0.30	0.30
<b>Annual Totals:</b>											<b>23.0</b> (cfs)	<b>4.2</b> (tons/yr)	<b>6.2</b> (tons/yr)	<b>10.4</b> (tons/yr)
											<b>45.6</b> (acre-ft)			

## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>Trail Creek, A4a+ Poor Downstream</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>III</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/2/2010</b>			
<b>Enter Required Information for Existing Condition</b>					
6.0	$D_{50}$	Riffle bed material $D_{50}$ (mm)			
	$\hat{D}_{50}$	Bar sample $D_{50}$ (mm)			
0.04	$D_{max}$	<b>D84</b> particle from <b>Bed Material</b> (ft)	10.79	(mm)	304.8 mm/ft
0.12360	$S$	Existing bankfull water surface slope (ft/ft)			
0.24	$d$	Existing bankfull mean depth (ft)			
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment			
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>					
N/A	$D_{50}/\hat{D}_{50}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 ( D_{50}/\hat{D}_{50} )^{-0.872}$		
N/A	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 ( D_{max}/D_{50} )^{-0.887}$		
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED:		
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	$d$	Required bankfull mean depth (ft)	$d = \frac{\tau^*(\gamma_s - 1)D_{max}}{S}$ (use $D_{max}$ in ft)		
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	$S$	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^*(\gamma_s - 1)D_{max}}{d}$ (use $D_{max}$ in ft)		
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					
<b>Sediment Competence Using Dimensional Shear Stress</b>					
1.851	Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d ) $\gamma = 62.4$ , $d =$ existing depth, $S =$ existing slope				
Shields 140	CO 240	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ ( <b>Figure 5-49</b> )			
Shields 0.18	CO 0.028	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) ( <b>Figure 5-49</b> )			
Shields 0.02	CO 0.004	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm)		$d = \frac{\tau}{\gamma S}$	
Shields 0.0120	CO 0.0019	Predicted slope required to initiate movement of measured $D_{max}$ (mm)		$S = \frac{\tau}{\gamma d}$	
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input checked="" type="checkbox"/> Degrading					



## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>Trail Creek, A4a+ Poor Dwnstrm</b>	Stream Type: <b>A4a+</b>
Location: <b>Pike National Forest, CO</b>	Valley Type: <b>III</b>
Observers: <b>Chavez, Kasun &amp; Gallagher</b>	Date: <b>9/3/2010</b>
<b>Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)</b>	<b>Stability Rating (Check Appropriate Rating)</b>
<b>Stream Type at potential, (C→E), (F<sub>b</sub>→B), (G→B), (F→B<sub>c</sub>), (F→C), (D→C)</b>	<input checked="" type="checkbox"/> Stable
(E→C), (C→High W/d C)	<input type="checkbox"/> Moderately Unstable
(G→F), (F→D), (C→F)	<input checked="" type="checkbox"/> Unstable
(C→D), (B→G), (D→G), (C→G), (E→G)	<input type="checkbox"/> Highly Unstable

**Worksheet 5-25.** Lateral stability.

Stream: <b>Trail Creek, A4a+ Poor Downstream Reach</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>III</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/3/2010</b>			
Lateral stability criteria (choose one stability category for each criterion 1-5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	2
	0.84 (2)	(4)	(6)	(8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	4
	(1)	(2)	(3)	B3, B4, B5 (4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		1
	M1 (1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	6
	(2)	(4)	VH/L (6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	1
	(1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>14</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input type="checkbox"/>	<i>Unstable</i> 13 – 21 <input checked="" type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	

**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>Trail Creek, A4a+ Poor Downstream Reach</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>III</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/3/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
1 <b>Sediment competence</b> (Worksheet 5-22)	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope—slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	2
	<b>Excess</b> (2)	(4)	(6)	(8)	
2 <b>Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	2
	<b>Excess</b> (2)	(4)	(6)	(8)	
3 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	2
	<b>0.84</b> (2)	(4)	(6)	(8)	
4 <b>Stream Succession States</b> (Worksheet 5-24)	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	2
	<b>at potential</b> (2)	(4)	(6)	(8)	
5 <b>Depositional Patterns</b> (Worksheet 5-10)	B1	B2, B4	B3, B5	B6, B7, B8	3
	(1)	(2)	<b>B3, B4, B5</b> (3)	(4)	
6 <b>Debris / Blockages</b> (Worksheet 5-11)	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	1
	<b>D2</b> (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>12</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
Vertical Stability for Excess Deposition / Aggradation (use total points and check stability rating)	<i>No Deposition</i> 10 – 14 <input checked="" type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input type="checkbox"/>	<i>Aggradation</i> > 30 <input type="checkbox"/>	

**Worksheet 5-27.** Vertical stability – degradation.

Stream: <b>Trail Creek, A4a+ Poor Downstream Reach</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>III</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/3/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>1 Sediment Competence</b> (Worksheet 5-22)	Does not indicate excess competence	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed	$D_{100}$ of bed moved	Particles much larger than $D_{100}$ of bed moved	<b>8</b>
	(2)	(4)	(6)	(8)	
<b>2 Sediment Capacity</b> (POWERSED) (Worksheet 5-20)	Does not indicate excess capacity	Slight excess energy: up to 10% increase above reference	Excess energy sufficient to increase load up to 50% of annual load	Excess energy transporting more than 50% of annual load	<b>8</b>
	(2)	(4)	(6)	(8)	
<b>3 Degree of Channel Incision (BHR)</b> (Worksheet 5-12)	1.00 – 1.10	1.11 – 1.30	1.31 – 1.50	> 1.50	<b>8</b>
	(2)	(4)	(6)	<b>5.10</b> (8)	
<b>4 Stream Succession States</b> (Worksheets 5-12 and 5-24)	Does not indicate incision or degradation	If BHR > 1.1 and stream type has W/d between 5–10	If BHR > 1.1 and stream type has W/d less than 5	(B→G), (C→G), (E→G), (D→G)	<b>4</b>
	(2)	BHR 5.1, W/d 9.17 (4)	(6)	(8)	
<b>5 Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.80 – 1.00	0.30 – 0.79	0.10 – 0.29	< 0.10	<b>1</b>
	(1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>29</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation</b> (use total points and check stability rating)	<i>Not Incised</i> 9 – 11 <input type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input type="checkbox"/>	<i>Degradation</i> > 27 <input checked="" type="checkbox"/>	

Worksheet 5-28. Channel enlargement.

Stream: <b>Trail Creek, A4a+ Poor Downstream Reach</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>III</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/3/2010</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1–4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	2
	(2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	6
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	2
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	8
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>18</b>
<b>Category Point Range</b>					
Channel Enlargement Prediction (use total points and check stability rating)	<i>No Increase</i> 8 – 10 <input type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input checked="" type="checkbox"/>	<i>Extensive</i> > 24 <input type="checkbox"/>	

Worksheet 5-29. Overall sediment supply.

Stream: <b>Trail Creek, A4a+ Poor Downstream Reach</b>		Stream Type: <b>A4a+</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>III</b>		
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/3/2010</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1–5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	3	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	1	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	4	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	3	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	4	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>15</b>	
<b>Category Point Range</b>				
Overall Sediment Supply Rating (use total points and check stability rating)	<b>Low</b> 5 <input type="checkbox"/>	<b>Moderate</b> 6 – 10 <input type="checkbox"/>	<b>High</b> 11 – 15 <input checked="" type="checkbox"/>	<b>Very High</b> 16 – 20 <input type="checkbox"/>

Worksheet 5-32. Summary of stability condition categories.

Stream: <b>Trail Creek, A4a+ Poor Downstream Reach</b>		Location: <b>Pike National Forest, Colorado</b>	
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Stream Type: <b>A4a+</b> Valley Type: <b>III</b>	
Date: <b>9/3/2010</b>		Entrenchment Ratio: <b>1.25</b>	
<b>Channel Dimension (XS 0+9.84)</b>	Mean Bankfull Depth (ft): <b>0.24</b>	Cross-Sectional Area (ft <sup>2</sup> ): <b>0.53</b>	Width of Flood-Prone Area (ft): <b>2.75</b>
<b>Channel Pattern</b>	λ/W <sub>bkf</sub> : <b>N/A</b>	R <sub>c</sub> /W <sub>bkf</sub> : <b>N/A</b>	MWR: <b>5.4</b> Sinuosity: <b>1.09</b>
<b>River Profile &amp; Bed Features</b>	Check: <input type="checkbox"/> Riffle/Pool <input type="checkbox"/> Step/Pool <input checked="" type="checkbox"/> Plane Bed <input type="checkbox"/> Convergence/Divergence <input type="checkbox"/> Dunes/Antidunes/Smooth Bed	Pool	Slope
	Max Bankfull Depth (ft):	Depth Ratio (max to mean):	Pool Spacing: <b>0.1347</b> Valley: <b>0.1347</b> Water Surface: <b>0.1236</b>
<b>Level III Stream Stability Indices</b>	Riparian Vegetation: <b>P.Pine Seedlings/Grass/Forb</b>	Potential Composition/Density:	Remarks: Condition, Vigor & Usage of Existing Reach:
	Flow Regime: <b>E1, E2, E8 &amp; Order: S-2(2)</b>	Meander Patterns: <b>M1</b>	<b>Ponderosa Pine beginning to regenerate</b>
	Degree of Incision (Bank-Height Ratio): <b>5.1</b>	Degree of Incision Stability Rating: <b>Deeply Incised</b>	Modified Pfankuch Stability Rating (Numeric & Adjective Rating): <b>140 (Poor)</b>
<b>Bank Erosion Summary</b>	Width/depth Ratio (W/d): <b>9.17</b>	Reference W/d Ratio (W/d) <sub>ref</sub> : <b>11</b>	W/d Ratio State Stability Rating: <b>0.84</b> <b>Stable</b>
	Meander Width Ratio (MWR): <b>5.4</b>	Reference MWR <sub>ref</sub> : <b>1.5</b>	MWR / MWR <sub>ref</sub> Stability Rating: <b>3.6</b> <b>Unconfined</b>
<b>Sediment Capacity (POWERSED)</b>	Length of Reach Studied (ft): <b>58</b>	Annual Streambank Erosion Rate: (tons/yr) <b>0.0785</b> (tons/yr/ft) <b>Colorado</b>	Remarks:
	<input type="checkbox"/> Sufficient Capacity <input type="checkbox"/> Insufficient Capacity <input checked="" type="checkbox"/> Excess Capacity		
<b>Entrainment/Competence</b>	Largest Particle from Bar Sample (mm): <b>10.79</b>	τ = <b>1.851</b> τ* = <b>N/A</b>	Required Depth: <b>0.24</b> Existing Depth: <b>0.02</b>
	<b>A4a+ → A4a+ →</b>	<b>→</b>	Existing Stream State (Type): <b>A4a+</b> Potential Stream State (Type): <b>A4a+</b>
<b>Lateral Stability</b>	<input type="checkbox"/> Stable <input type="checkbox"/> Mod. Unstable <input checked="" type="checkbox"/> Unstable <input type="checkbox"/> Highly Unstable		Remarks/causes:
<b>Vertical Stability (Aggradation)</b>	<input checked="" type="checkbox"/> No Deposition <input type="checkbox"/> Mod. Deposition <input type="checkbox"/> Ex. Deposition <input type="checkbox"/> Aggradation		Remarks/causes:
<b>Vertical Stability (Degradation)</b>	<input type="checkbox"/> Not Incised <input type="checkbox"/> Slightly Incised <input type="checkbox"/> Mod. Incised <input checked="" type="checkbox"/> Degradation		Remarks/causes:
<b>Channel Enlargement</b>	<input type="checkbox"/> No Increase <input type="checkbox"/> Slight Increase <input checked="" type="checkbox"/> Mod. Increase <input type="checkbox"/> Extensive		Remarks/causes:
<b>Sediment Supply (Channel Source)</b>	<input type="checkbox"/> Low <input type="checkbox"/> Moderate <input checked="" type="checkbox"/> High <input type="checkbox"/> Very High		Remarks/causes:





## *Appendix C5*

# **B4 Stream Type**

## *Fair Stability Reach*



# Table of Contents

## *Appendix C5: B4 Fair Reach*

<b>Reach Location &amp; Overview.....</b>	<b>C5-2</b>
<b>Survey Summary.....</b>	<b>C5-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C5-8</b>
<b><i>Velocity, Classification &amp; Morphological Relations.....</i></b>	<b>C5-8</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b><i>Stability Indices.....</i></b>	<b>C5-12</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b><i>BANCS Model – Streambank Erosion.....</i></b>	<b>C5-24</b>
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b><i>FLOWSED Model – Total Annual Sediment Yield.....</i></b>	<b>C5-24</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b><i>POWERSED Model– Sediment Transport Capacity to Assess Bed Stability.....</i></b>	<b>C5-26</b>
Worksheet 5-20a. Sediment transport prediction for the upstream condition.	
Worksheet 5-20b. Sediment transport prediction for the existing condition.	
<b><i>Sediment Competence/Entrainment.....</i></b>	<b>C5-28</b>
Worksheet 5-22. Sediment competence calculations.	
<b><i>Channel Stability Ratings.....</i></b>	<b>C5-29</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b><i>Summary.....</i></b>	<b>C5-35</b>
Worksheet 5-32. Summary of stability condition categories.	

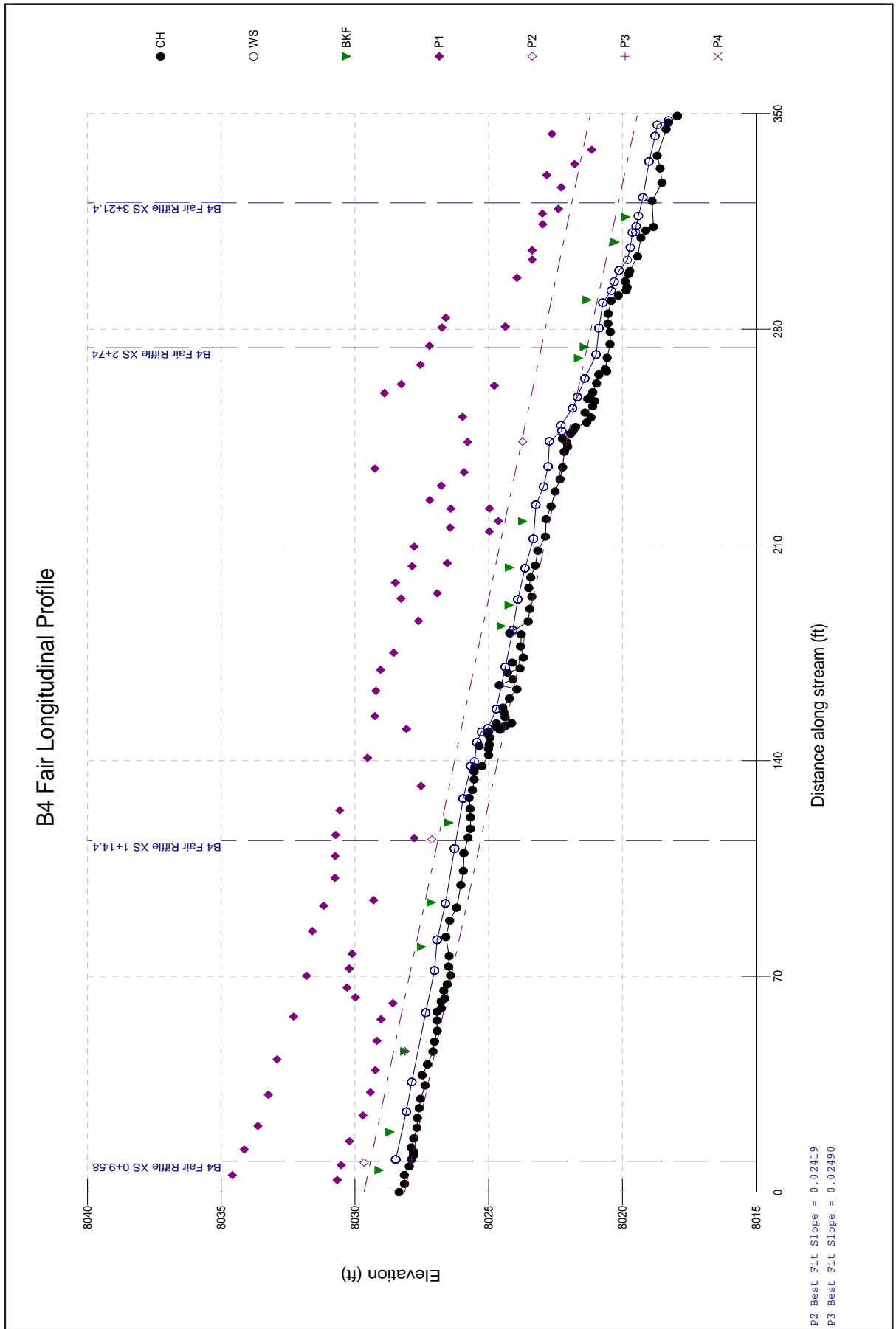
## B4 Fair Reach Location & Overview

The B4 Fair representative reach is a 3<sup>rd</sup> order, perennial stream located in main Trail Creek (**Figure C-2**). The photograph depicts high eroding banks, although the riparian vegetation is slowly reoccupying this reach as the stream has gradually evolved from an F4b to a B4 stream type. However, the higher width/depth ratio than the reference condition has led to excess sediment deposition in the channel. The stability rating is “Fair” due to a “Fair” Pfankuch stability rating and the relatively high streambank erosion rate of  $0.0973 \text{ tons/yr/ft}$  compared to the B4 reference rate of  $0.0048 \text{ tons/yr/ft}$ . The sediment transport capacity model (POWERSED) indicates aggradation. The sediment supply rating is *High* due primarily to the streambank erosion source and increase in stored sediment in the channel bed. This rating indicates a potential accelerated increase in flow-related sediment based on increased post-fire streamflow peak flows compared to the reference B4 condition. The WRENSS model suggests a water yield increase due to the fire of  $1,736 \text{ acre-ft}$ . Bedload was subsequently increased from  $39 \text{ tons/yr}$  to  $222 \text{ tons/yr}$ , and the suspended sediment was increased from  $62 \text{ tons/yr}$  to  $438 \text{ tons/yr}$ , representing a total increase in sediment of  $560 \text{ tons/yr}$ . These are high sediment values for a B4 stream type of this size (30 cfs bankfull) and reflect the accelerated sediment yield due to flow-related sediment.

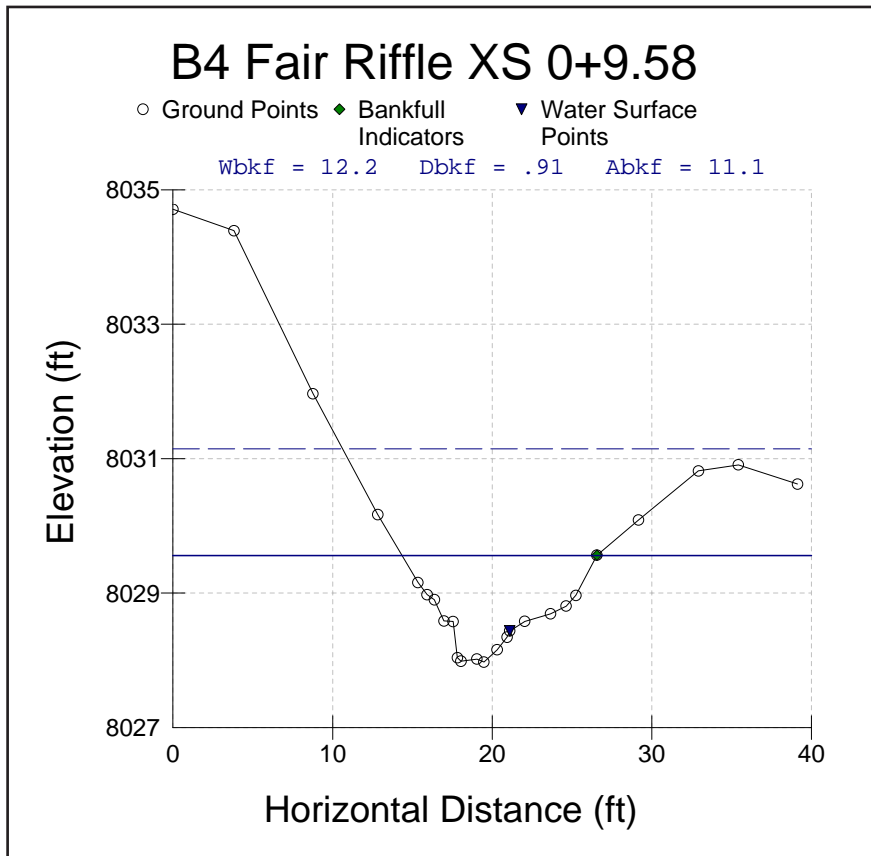
The photograph depicts the typical character of this representative B4 stream type. The following graphs and summary worksheets provide the detail of the morphology, hydraulics, streambank erosion rates, and stability conditions responsible for the overall “Fair” rating.



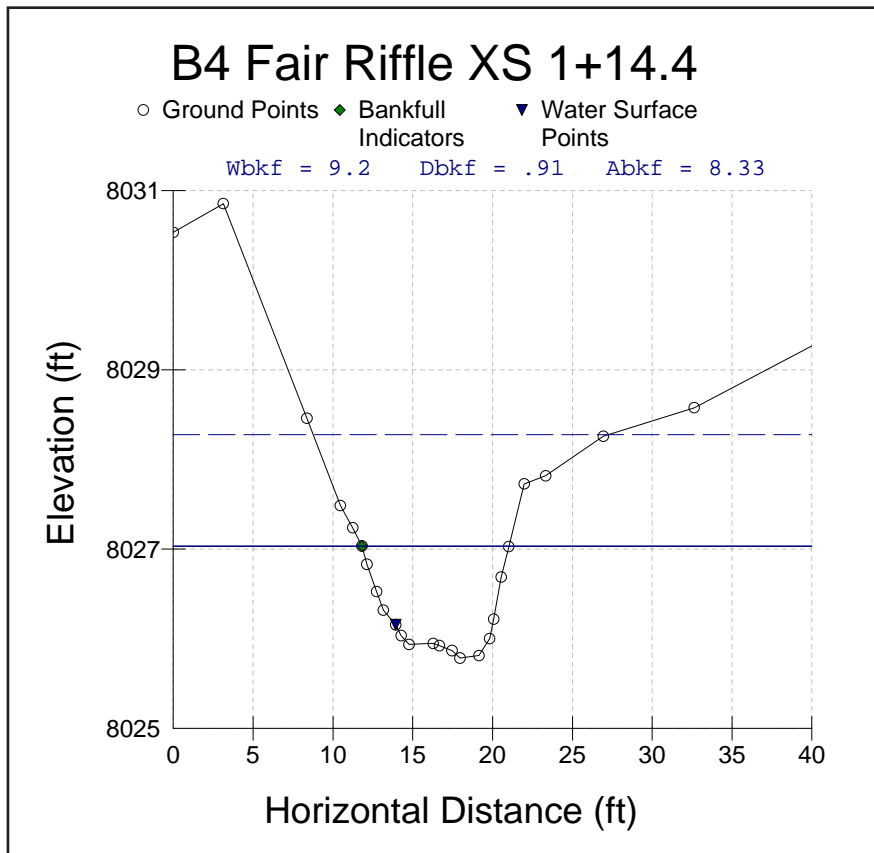
# Survey Summary



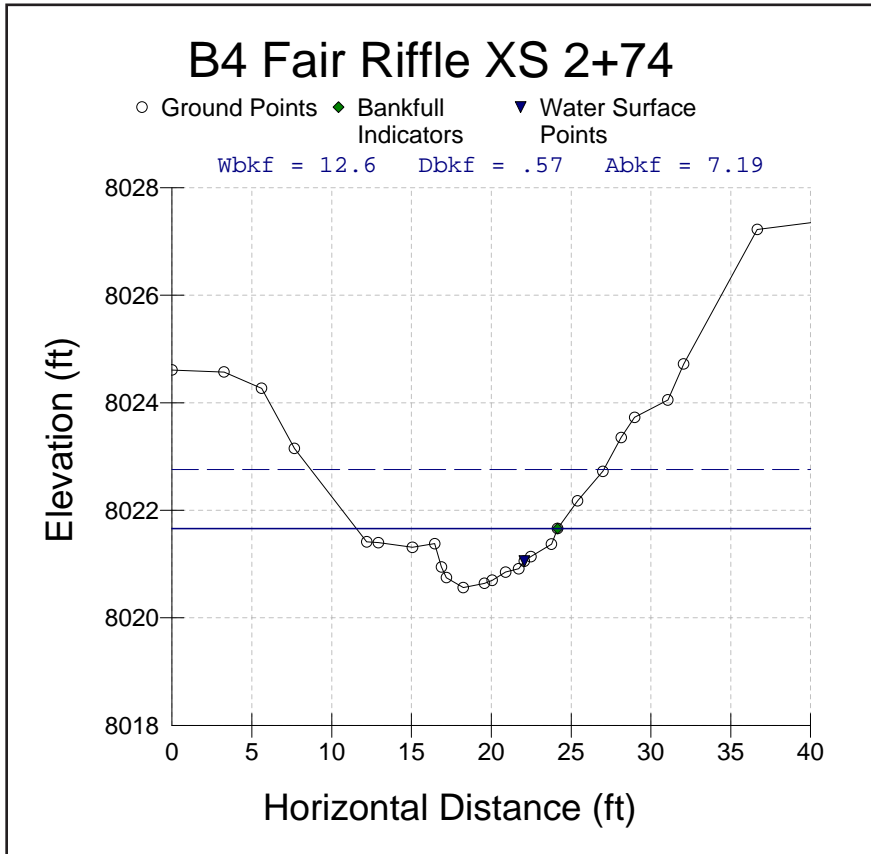
Longitudinal Profile (graph generated from RIVERMorph™)



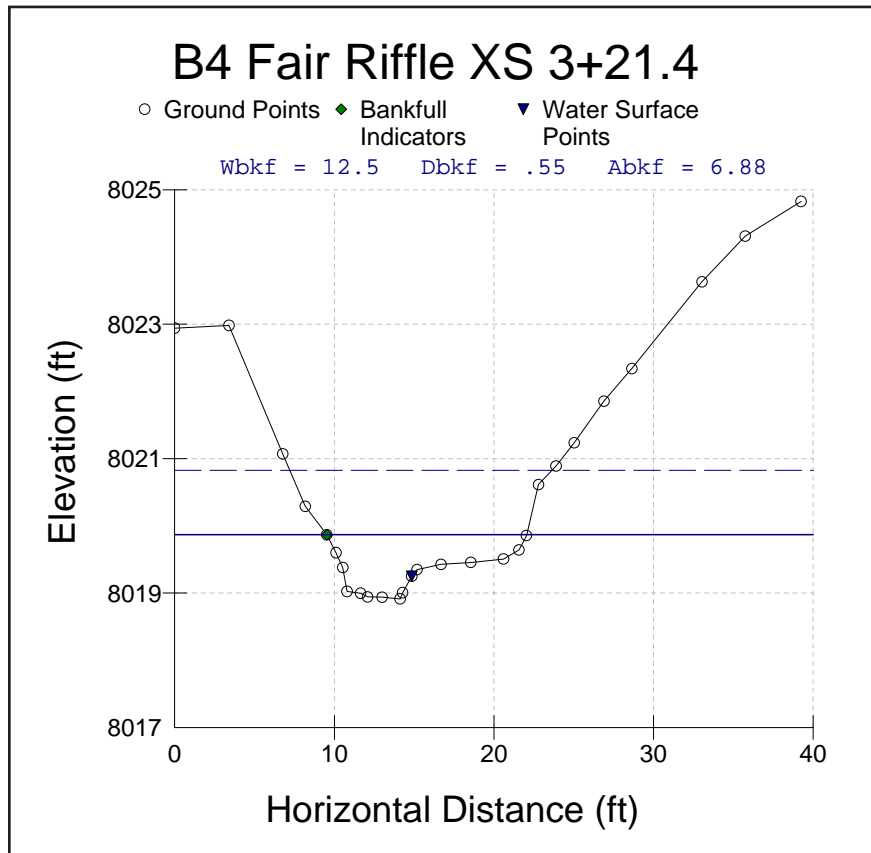
Riffle Cross-section 0+9.58 (graph generated from RIVERMorph™)



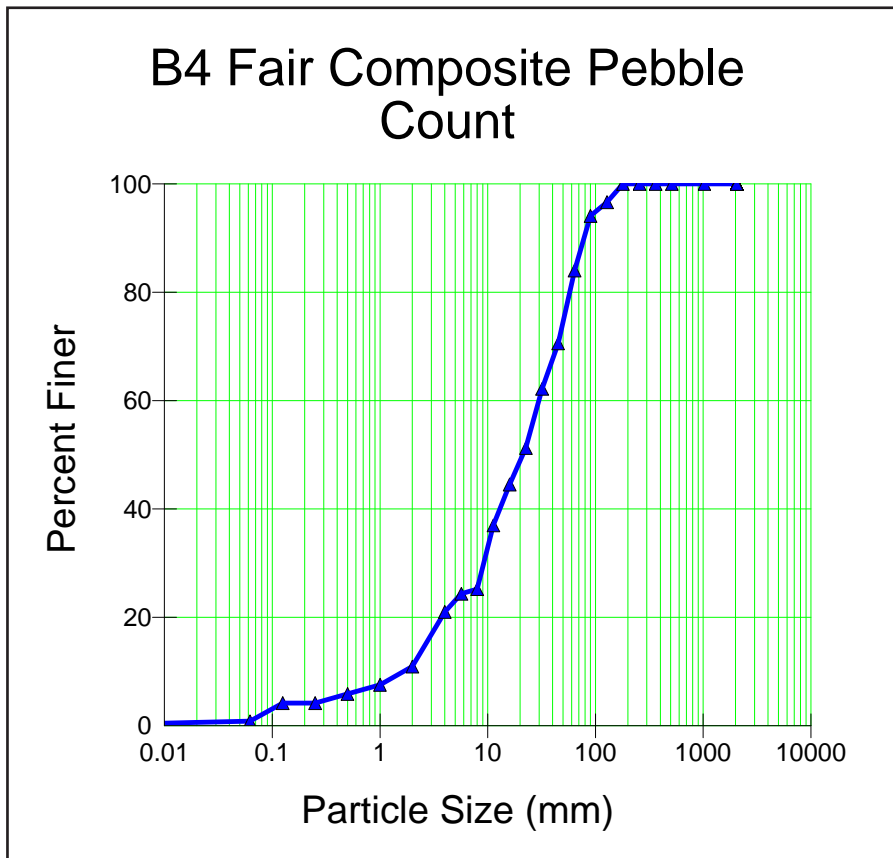
Riffle Cross-section 1+14.4 (graph generated from RIVERMorph™)



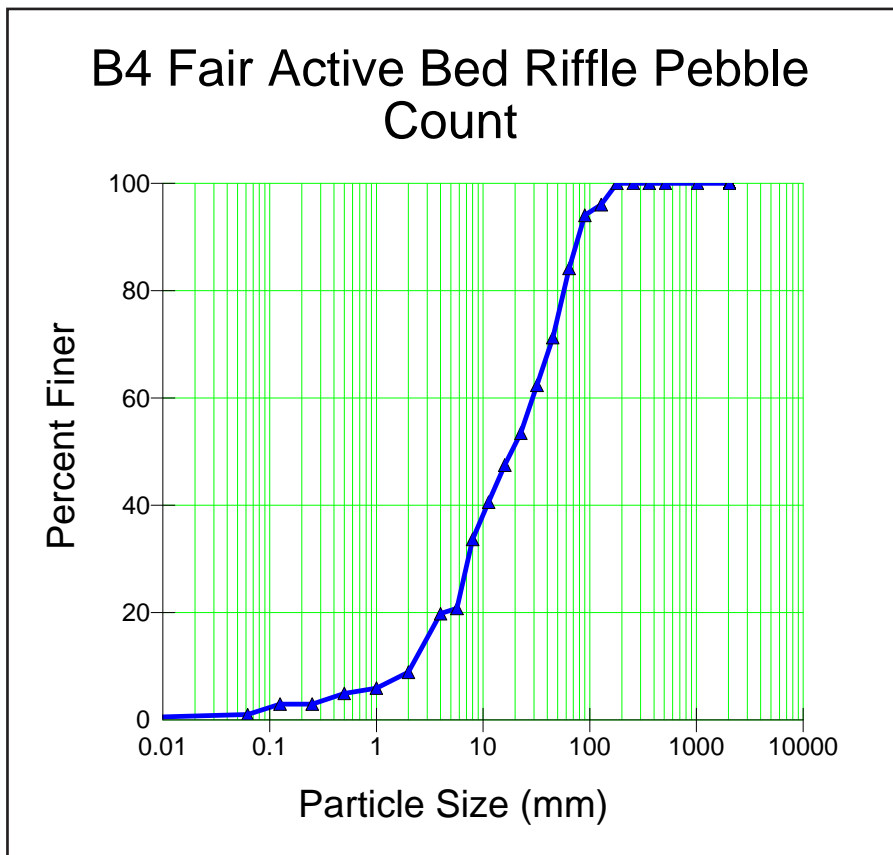
Representative Riffle Cross-section 2+74 (graph generated from RIVERMorph™)



Riffle Cross-section 3+21.4 (graph generated from RIVERMorph™)

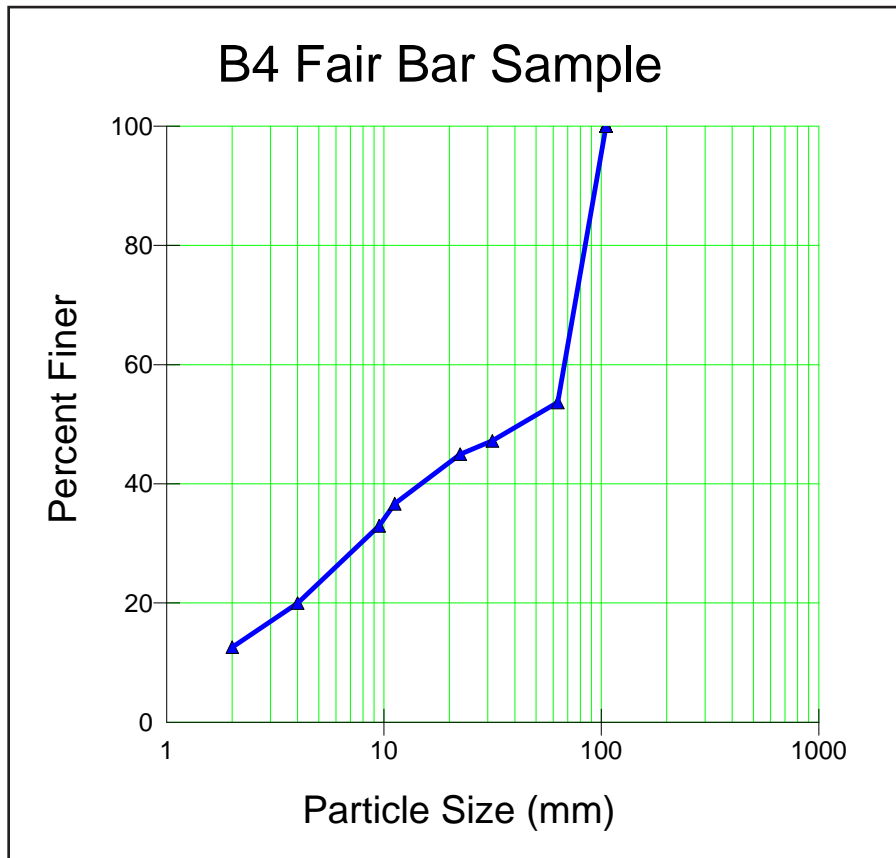


Composite Pebble Count (graph generated from RIVERMorph™)



Active Bed Riffle Pebble Count (graph generated from RIVERMorph™)





**Bar Sample** (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates					
Stream:	Trail Creek, B4 Fair Reach		Location:	XS 2+74, Pike N.F., Colorado	
Date:	8/20/2010	Stream Type:	B4	Valley Type:	VIII
Observers:	K. Wright & B. Kasun		HUC:	___	
INPUT VARIABLES			OUTPUT VARIABLES		
Bankfull Riffle Cross-Sectional AREA	7.19	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.57	$d_{bkf}$ (ft)
Bankfull Riffle WIDTH	12.60	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim (2 * d_{bkf}) + W_{bkf}$	13.07	$W_p$ (ft)
$D_{84}$ at Riffle	63.8	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.21	$D_{84}$ (ft)
Bankfull SLOPE	0.024	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	0.55	R (ft)
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness $R(ft) / D_{84}(ft)$	2.63	$R / D_{84}$
Drainage Area	10.1	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.652	$u^*$ (ft/sec)
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$			3.39	ft / sec	24.41 cfs
2. Roughness Coefficient: a) Manning's n from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.048$			3.23	ft / sec	23.21 cfs
2. Roughness Coefficient: b) Manning's n from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.057$			2.72	ft / sec	19.55 cfs
2. Roughness Coefficient: c) Manning's n from Jarrett (USGS): $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ <small>Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for Stream Types A1, A2, A3, B1, B2, B3, C2 &amp; E3</small> $n = 0.057$			2.72	ft / sec	19.55 cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)				ft / sec	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)				ft / sec	cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q =$ <input type="text"/> year $u = Q / A$				ft / sec	cfs
4. Continuity Equations: b) $u = Q / A$ (based on riffle 1+14.2- good bkf)			4.20	ft / sec	30.2 cfs
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation ( $R/D_{84}$ ) – Estimation Method 1					
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.					
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.					
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.					
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.					

**Worksheet 5-3.** Level II stream classification.

Stream: <b>Trail Creek, B4 Fair Reach</b>	
Basin:	Drainage Area: <b>6464</b> acres <b>10.1</b> mi <sup>2</sup>
Location: <b>Pike National Forest, Colorado</b>	
Twp.&Rge:	Sec.&Qtr.:
Cross-Section Monuments (Lat./Long.): <b>XS 2+74</b>	Date: <b>08/20/10</b>
Observers: <b>K. Wright &amp; B. Kasun</b>	Valley Type: <b>VIII</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>12.59</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>0.57</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>7.19</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>22.09</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>1.1</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>18.36</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>1.46</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>21.36</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.024</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length ( $SL / VL$ ); or estimated from a ratio of valley slope divided by channel slope ( $VS / S$ ).	<b>1.21</b>	

<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>Stream Type</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: #e0f0ff;"> <b>B4</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;">                 (See Figure 2-14)             </div>
---	---	--

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, B4 Fair Reach</b>				Location: <b>Pike National Forest, Colorado</b>							
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/20/2010</b>		Valley Type: <b>VIII</b>		Stream Type: <b>B4</b>					
<b>River Reach Dimension Summary Data.....1</b>											
<b>Riffle Dimensions*<sup>*, **</sup>, ***</b>	<b>Riffle Dimensions*<sup>*, **</sup>, ***</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Width ( $W_{bkt}$ )	<b>14.0</b>	<b>12.2</b>	<b>18.5</b>	ft	Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	<b>8.4</b>	<b>6.9</b>	<b>11.1</b>		
	Mean Riffle Depth ( $d_{bkt}$ )	<b>0.74</b>	<b>0.55</b>	<b>0.91</b>	ft	Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	<b>17.1</b>	<b>10.1</b>	<b>22.8</b>		
	Maximum Riffle Depth ( $d_{max}$ )	<b>1.23</b>	<b>0.96</b>	<b>1.59</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>1.699</b>	<b>1.370</b>	<b>1.930</b>		
	Width of Flood-Prone Area ( $W_{fpa}$ )	<b>18.7</b>	<b>16.4</b>	<b>21.7</b>	ft	Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )	<b>1.64</b>	<b>1.31</b>	<b>2.01</b>		
	Riffle Inner Berm Width ( $W_{ib}$ )	<b>6.2</b>	<b>5.5</b>	<b>6.9</b>	ft	Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )	<b>0.443</b>	<b>0.392</b>	<b>0.495</b>		
	Riffle Inner Berm Depth ( $d_{ib}$ )	<b>0.38</b>	<b>0.32</b>	<b>0.47</b>	ft	Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )	<b>0.517</b>	<b>0.435</b>	<b>0.639</b>		
	Riffle Inner Berm Area ( $A_{ib}$ )	<b>2.4</b>	<b>1.8</b>	<b>3.2</b>	ft <sup>2</sup>	Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )	<b>0.285</b>	<b>0.209</b>	<b>0.386</b>		
	Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )	<b>16.5</b>	<b>14.7</b>	<b>17.7</b>							
<b>Pool Dimensions*<sup>*, **</sup>, ***</b>	<b>Pool Dimensions*<sup>*, **</sup>, ***</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Pool Dimensions &amp; Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Pool Width ( $W_{bkfp}$ )				ft	Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )					
	Mean Pool Depth ( $d_{bkfp}$ )				ft	Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )					
	Pool Cross-Sectional Area ( $A_{bkfp}$ )				ft	Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )					
	Maximum Pool Depth ( $d_{maxp}$ )				ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )					
	Pool Inner Berm Width ( $W_{ibp}$ )				ft	Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )					
	Pool Inner Berm Depth ( $d_{ibp}$ )				ft	Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )					
	Pool Inner Berm Area ( $A_{ibp}$ )				ft <sup>2</sup>	Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )					
	Point Bar Slope ( $S_{pb}$ )				ft/ft	Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )					
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Run Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Run Width ( $W_{bkfr}$ )				ft	Run Width to Riffle Width ( $W_{bkfr} / W_{bkt}$ )					
	Mean Run Depth ( $d_{bkfr}$ )				ft	Mean Run Depth to Mean Riffle Depth ( $d_{bkfr} / d_{bkt}$ )					
	Run Cross-Sectional Area ( $A_{bkfr}$ )				ft	Run Area to Riffle Area ( $A_{bkfr} / A_{bkt}$ )					
	Maximum Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )					
	Run Width/Depth Ratio ( $W_{bkfr} / d_{bkfr}$ )				ft						
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Glide Dimensions &amp; Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Glide Width ( $W_{bkfg}$ )				ft	Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )					
	Mean Glide Depth ( $d_{bkfg}$ )				ft	Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )					
	Glide Cross-Sectional Area ( $A_{bkfg}$ )				ft	Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )					
	Maximum Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )					
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )				ft/ft	Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )					
	Glide Inner Berm Width ( $W_{ibg}$ )				ft	Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )					
	Glide Inner Berm Depth ( $d_{ibg}$ )				ft	Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )					
Glide Inner Berm Area ( $A_{ibg}$ )				ft <sup>2</sup>	Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )						
<b>Step**</b>	<b>Step Dimensions**</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Step Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Step Width ( $W_{bkfs}$ )				ft	Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )					
	Mean Step Depth ( $d_{bkfs}$ )				ft	Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )					
	Step Cross-Sectional Area ( $A_{bkfs}$ )				ft	Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )					
	Maximum Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )					
	Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )										

**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, B4 Fair Reach</b>		Location: <b>Pike National Forest, Colorado</b>								
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/20/2010</b>		Valley Type: <b>VIII</b>		Stream Type: <b>B4</b>				
<b>River Reach Summary Data.....2</b>										
<b>Hydraulics</b>	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )		<b>4.20</b>		ft/sec		Estimation Method	<b>Continuity</b>		
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )		<b>30.2</b>		cfs		Drainage Area	<b>10.1</b> mi <sup>2</sup>		
<b>Channel Pattern</b>	<b>Geometry</b>			<b>Dimensionless Geometry Ratios</b>						
	Linear Wavelength ( $\lambda$ )	<b>N/A</b>		ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )	<b>N/A</b>				
	Stream Meander Length ( $L_m$ )	<b>100.0</b>		ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )	<b>7.16</b>				
	Radius of Curvature ( $R_c$ )	<b>N/A</b>		ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )	<b>N/A</b>				
	Belt Width ( $W_{bkt}$ )	<b>41.4</b>		ft	Meander Width Ratio ( $W_{bkt} / W_{bkt}$ )	<b>2.97</b>				
	Arc Length ( $L_a$ )	<b>N/A</b>		ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )	<b>N/A</b>				
	Riffle Length ( $L_r$ )	<b>39.4</b>	<b>23.1</b>	<b>54.9</b>	ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )	<b>2.82</b>	<b>1.65</b>	<b>3.93</b>	
	Individual Pool Length ( $L_p$ )	<b>11.5</b>	<b>6.6</b>	<b>20.9</b>	ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )	<b>0.82</b>	<b>0.47</b>	<b>1.50</b>	
Pool to Pool Spacing ( $P_s$ )	<b>50.6</b>	<b>11.4</b>	<b>83.9</b>	ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )	<b>3.62</b>	<b>0.82</b>	<b>6.01</b>		
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )	<b>0.0290</b>	ft/ft		Average Water Surface Slope (S)	<b>0.0240</b>	ft/ft		Sinuosity ( $S_{val} / S$ )	<b>1.21</b>
	Stream Length (SL)	<b>349.2</b>	ft		Valley Length (VL)	<b>290.0</b>	ft		Sinuosity (SL / VL)	<b>1.20</b>
	Low Bank Height (LBH)	start: <b>1.25</b>	ft		Max Bankfull Depth ( $d_{max}$ )	start: <b>1.25</b>	ft		Bank-Height Ratio (BHR) (LBH / $d_{max}$ )	start: <b>1.0</b>
		end: <b>1.38</b>	ft			end: <b>1.38</b>	ft			end: <b>1.0</b>
	<b>Facet Slopes</b>			<b>Dimensionless Facet Slope Ratios</b>						
	Riffle Slope ( $S_{rif}$ )	<b>0.0350</b>	<b>0.0210</b>	<b>0.0550</b>	ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.4583</b>	<b>0.8750</b>	<b>2.2917</b>	
	Run Slope ( $S_{run}$ )	<b>0.1710</b>	<b>0.0750</b>	<b>0.2510</b>	ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )	<b>7.1250</b>	<b>3.1250</b>	<b>10.4583</b>	
	Pool Slope ( $S_p$ )	<b>0.0150</b>	<b>0.0060</b>	<b>0.0270</b>	ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )	<b>0.6250</b>	<b>0.2500</b>	<b>1.1250</b>	
	Glide Slope ( $S_g$ )	<b>0.0160</b>	<b>0.0140</b>	<b>0.0170</b>	ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )	<b>0.6667</b>	<b>0.5833</b>	<b>0.7083</b>	
	Step Slope ( $S_s$ )				ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )				
	<b>Max Depths<sup>a</sup></b>			<b>Dimensionless Depth Ratios</b>						
	Max Riffle Depth ( $d_{max}$ )	<b>1.46</b>	<b>1.25</b>	<b>1.62</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>1.986</b>	<b>1.701</b>	<b>2.204</b>	
	Max Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )	<b>1.68</b>	<b>1.54</b>	<b>1.79</b>	ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	<b>2.286</b>	<b>2.095</b>	<b>2.435</b>	
	Max Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )				
Max Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )					
<b>Channel Materials</b>	<b>Reach<sup>b</sup></b>			<b>Reach<sup>b</sup></b>			<b>Protrusion Height<sup>d</sup></b>			
	% Silt/Clay	<b>1</b>	<b>1</b>	<b>0</b>	$D_{16}$	<b>3.0</b>	<b>3.3</b>	<b>2.9</b>	mm	
	% Sand	<b>10</b>	<b>8</b>	<b>13</b>	$D_{35}$	<b>10.8</b>	<b>8.6</b>	<b>10.4</b>	mm	
	% Gravel	<b>73</b>	<b>75</b>	<b>43</b>	$D_{50}$	<b>21.4</b>	<b>18.8</b>	<b>45.1</b>	mm	
	% Cobble	<b>16</b>	<b>16</b>	<b>45</b>	$D_{84}$	<b>64.0</b>	<b>63.8</b>	<b>90.5</b>	mm	
	% Boulder	<b>0</b>	<b>0</b>	<b>0</b>	$D_{95}$	<b>103.3</b>	<b>108.0</b>	<b>100.5</b>	mm	
	% Bedrock	<b>0</b>	<b>0</b>	<b>0</b>	$D_{100}$	<b>180.0</b>	<b>180.0</b>	<b>105.0</b>	mm	

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

## Stability Indices


**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation					
Stream: <b>Trail Creek, B4 Fair Reach</b>			Location: <b>Pike National Forest, Colorado</b>		
Observers: <b>K. Wright &amp; B. Kasun</b>	Reference reach: <input type="checkbox"/>	Disturbed (impacted reach): <input checked="" type="checkbox"/>	Date: <b>8/20/10</b>		
Existing species composition: <b>Willow/Aspen/Grass</b>			Potential species composition: <b>Willow/Aspen/Grass</b>		
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition
<b>1. Overstory</b>	Canopy layer	<b>70%</b>	<b>22%</b>	<b>Willows</b>	<b>90%</b>
				<b>Aspen</b>	<b>10%</b>
100%					
<b>2. Understory</b>	Shrub layer	<b>33%</b>	<b>33%</b>	<b>Willow</b>	<b>100%</b>
100%					
<b>3. Ground level</b>	Herbaceous	<b>24%</b>	<b>24%</b>	<b>Mullen</b>	<b>10%</b>
				<b>Red Top</b>	<b>25%</b>
				<b>Poa</b>	<b>25%</b>
				<b>Thistle</b>	<b>5%</b>
	<b>Annual Forbs</b>	<b>35%</b>			
100%					
	Leaf or needle litter		<b>less than 3%</b>	<b>Remarks:</b> Condition, vigor and/or usage of existing reach: <b>Adjacent to road fill, invasive species control needed</b>	
	Bare ground		<b>18%</b>		
*Based on crown closure. **Based on basal area to surface area.			<b>Column total = 100%</b>		

**Worksheet 5-7.** Flow regime.

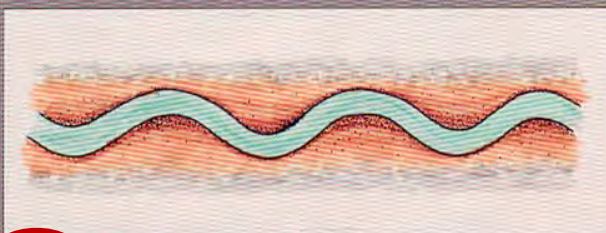


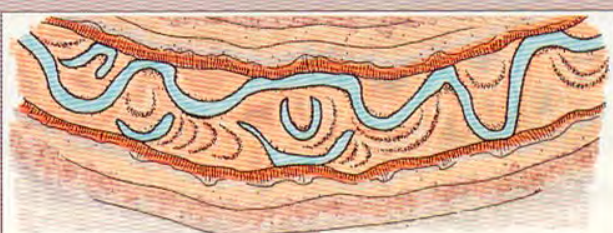


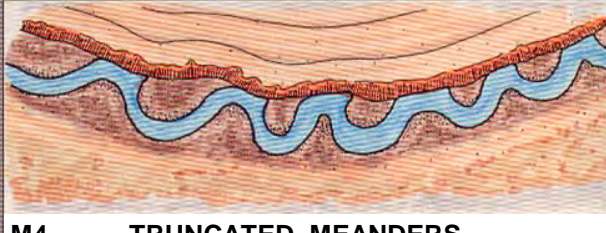

FLOW REGIME								
Stream: <b>Trail Creek, B4 Fair Reach</b>			Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>K. Wright &amp; B. Kasun</b>						Date: <b>8/20/2010</b>		
List ALL COMBINATIONS that APPLY.....☞			P1	P2	P8			
General Category								
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation							
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
<b>P</b>	Perennial stream channels: Surface water persists yearlong.							
Specific Category								
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
<b>4</b>	Streamflow regulated by glacial melt.							
<b>5</b>	Ice flows/ice torrents from ice dam breaches.							
<b>6</b>	Alternating flow/backwater due to tidal influence.							
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.							
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
<b>9</b>	Rain-on-snow generated runoff.							

**Worksheet 5-8.** Stream order & stream size.

Stream Size and Order			
Stream:	Trail Creek, B4 Fair Reach		
Location:	Pike National Forest, Colorado		
Observers:	K. Wright & B. Kasun		
Date:	8/20/2010		
Stream Size Category and Order 			S-3(3)
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0.305	<1	<input type="checkbox"/>
S-2	0.3 – 1.5	1 – 5	<input type="checkbox"/>
<b>S-3</b>	<b>1.5 – 4.6</b>	<b>5 – 15</b>	<input checked="" type="checkbox"/>
S-4	4.6 – 9	15 – 30	<input type="checkbox"/>
S-5	9 – 15	30 – 50	<input type="checkbox"/>
S-6	15 – 22.8	50 – 75	<input type="checkbox"/>
S-7	22.8 – 30.5	75 – 100	<input type="checkbox"/>
S-8	30.5 – 46	100 – 150	<input type="checkbox"/>
S-9	46 – 76	150 – 250	<input type="checkbox"/>
S-10	76 – 107	250 – 350	<input type="checkbox"/>
S-11	107 – 150	350 – 500	<input type="checkbox"/>
S-12	150 – 305	500 – 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
Stream Order			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			



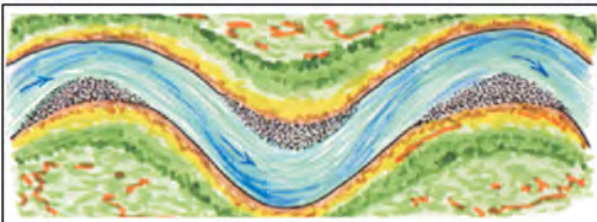

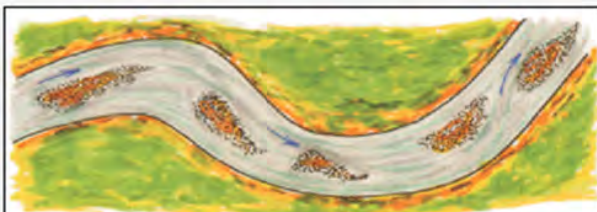

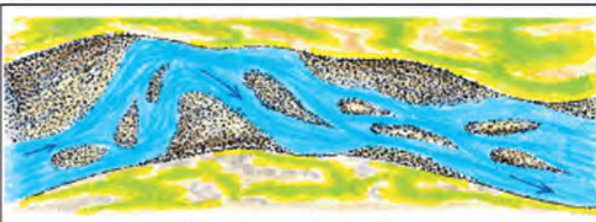
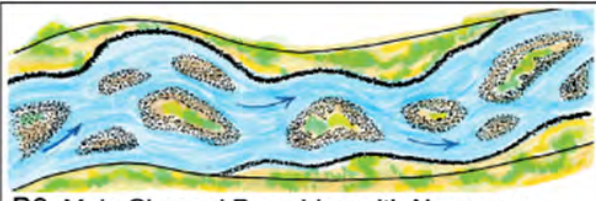
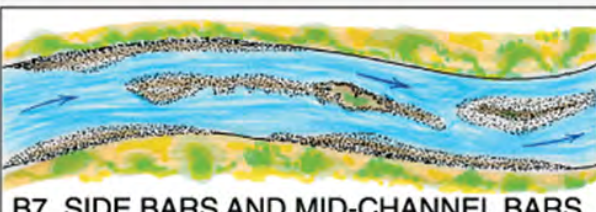

Worksheet 5-9. Meander patterns.

<b>Meander Patterns</b>					
Stream: <b>Trail Creek, B4 Fair Reach</b>			Location: <b>Pike National Forest, CO</b>		
Observers: <b>K. Wright &amp; B. Kasun</b>			Date: <b>8/20/2010</b>		
List ALL CATEGORIES that APPLY		<b>M1</b>			
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>					
 <b>M1</b> <b>REGULAR MEANDERS</b>	 <b>M5</b> <b>UNCONFINED MEANDER SCROLLS</b>				
 <b>M2</b> <b>TORTUOUS MEANDERS</b>	 <b>M6</b> <b>CONFINED MEANDER SCROLLS</b>				
 <b>M3</b> <b>IRREGULAR MEANDERS</b>	 <b>M7</b> <b>DISTORTED MEANDER LOOPS</b>				
 <b>M4</b> <b>TRUNCATED MEANDERS</b>	 <b>M8</b> <b>IRREGULAR MEANDERS with oxbows and</b>				

**Worksheet 5-10.** Depositional patterns.

<b>Depositional Patterns</b>					
Stream:	Trail Creek, B4 Fair Reach	Location:	Pike National Forest, CO		
Observers:	K. Wright & B. Kasun	Date:	8/20/2010		
List ALL CATEGORIES that APPLY	B4	B8			

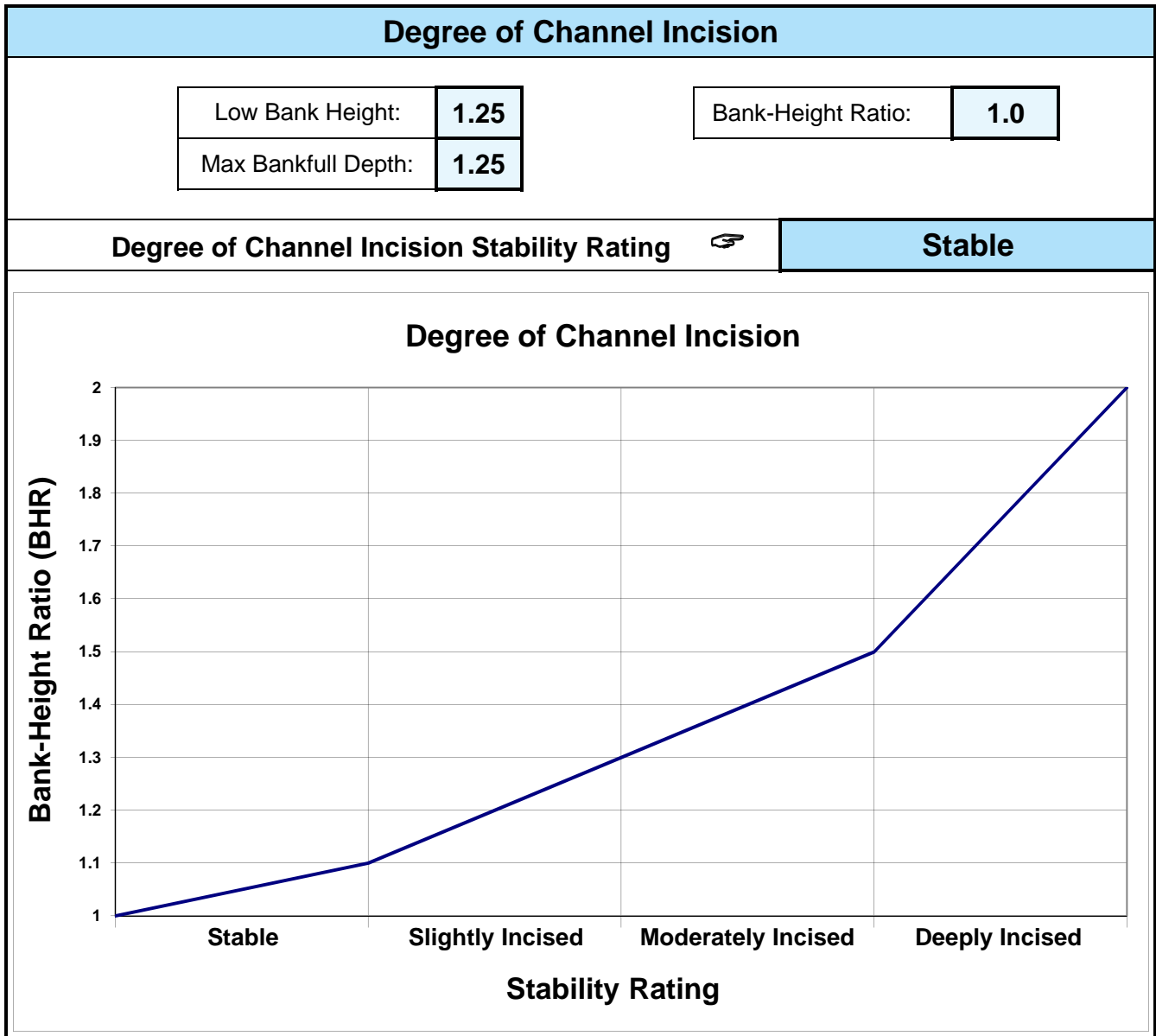
*Various Depositional Features modified from Galay et al. (1973)*

<div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B1</b> POINT BARS</p> </div> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B2</b> POINT BARS with Few MID-CHANNEL BARS</p> </div> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B3</b> NUMEROUS MID-CHANNEL BARS</p> </div> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B4</b> SIDE BARS</p> </div>	<div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B5</b> DIAGONAL BARS</p> </div> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B6</b> Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</p> </div> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B7</b> SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</p> </div> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B8</b> DELTA BARS</p> </div>
--	--

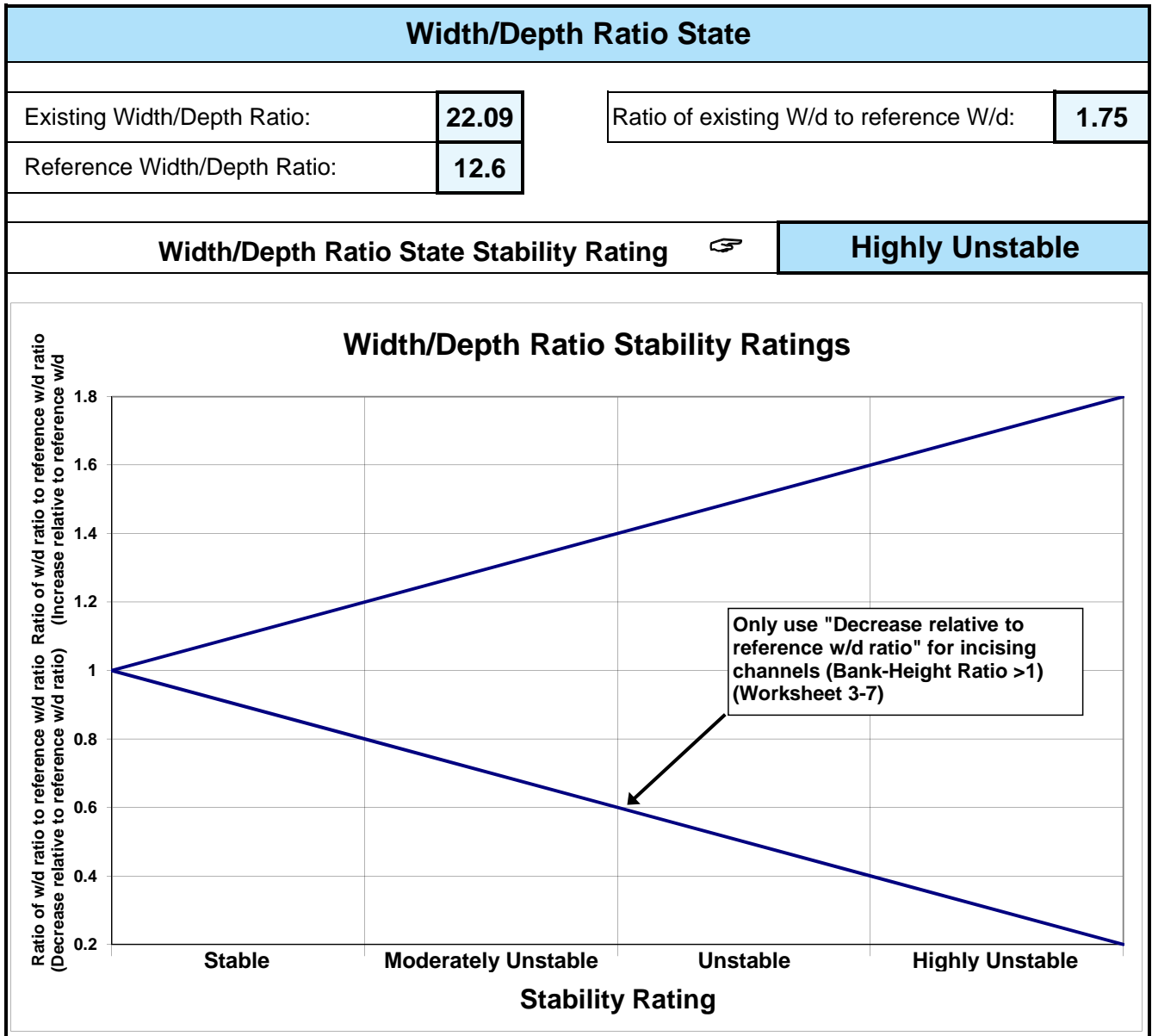
## Worksheet 5-11. Channel blockages.

Channel Blockages		
Stream: <b>Trail Creek, B4 Fair Reach</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/20/2010</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input checked="" type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input type="checkbox"/>
<b>D4</b> Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

**Worksheet 5-12.** Degree of channel incision.



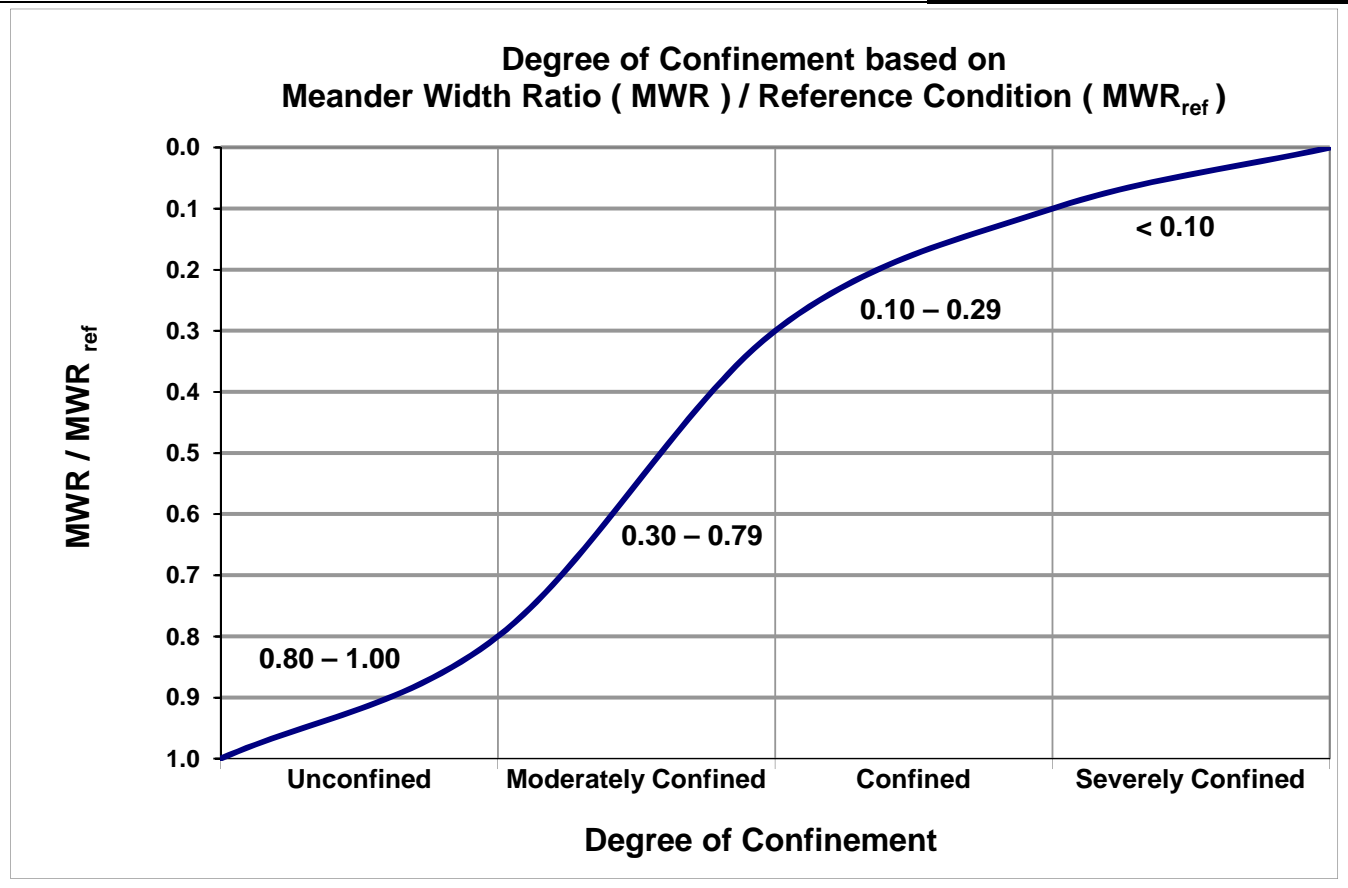
**Worksheet 5-13.** Width/depth ratio state.



**Worksheet 5-14.** Degree of channel confinement (lateral containment).

Degree of Confinement			
Existing Meander Width Ratio (MWR):	<b>2.97</b>	Ratio of MWR to $MWR_{ref}$ :	<b>1.10</b>
Reference Meander Width Ratio ( $MWR_{ref}$ ):	<b>2.7</b>		

<b>Degree of Confinement Stability Rating</b>	<b>Unconfined</b>
---	-------------------



**Worksheet 5-15. Pfankuch channel stability rating.**

Stream: Trail Creek, B4 Fair Reach		Location: Pike NF, CO			Valley Type: VIII			Observers: K. Wright & B. Kasun			Date: 8/20/2010														
Local-tion	Key	Category	Excellent	Good	Fair	Poor	Rating	Description	Rating	Description	Rating	Rating													
Upper banks	1	Landform slope	Bank slope gradient <30%.	Bank slope gradient 30–40%.	Bank slope gradient 40–60%.	Bank slope gradient > 60%.	2		4		6	8													
	2	Mass erosion	No evidence of past or future mass erosion.	Infrequent. Mostly healed over. Low future potential.	Frequent or large, causing sediment nearby yearlong.	Frequent or large, causing sediment nearby yearlong OR imminent danger of same.	3		4		9	12													
	3	Debris jam potential	Essentially absent from immediate channel area.	Present, but mostly small twigs and limbs.	Moderate to heavy amounts, mostly larger sizes.	Moderate to heavy amounts, predominantly larger sizes.	2		4		6	8													
	4	Vegetative bank protection	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	70–90% density. Fewer species or less vigor suggest less dense or deep root mass.	50–70% density. Lower vigor and fewer species from a shallow, discontinuous root mass.	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.	4		6		9	12													
Lower banks	5	Channel capacity	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0.	Bankfull stage is contained within banks. Width/depth ratio departure from reference width/depth ratio = 1.0–1.2. Bank-Height Ratio (BHR) = 1.0–1.1.	Bankfull stage is not contained. Width/depth ratio departure from reference width/depth ratio = 1.2–1.4. Bank-Height Ratio (BHR) = 1.1–1.3.	Bankfull stage is not contained; over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.	1		2		3	4													
	6	Bank rock content	> 65% with large angular boulders. 12" + common.	40–65%. Mostly boulders and small cobbles 6–12".	20–40%. Most in the 3–6" diameter class.	<20% rock fragments of gravel sizes, 1–3" or less.	2		4		5	8													
	7	Obstructions to flow	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	Frequent obstructions and deflectors cause bank erosion yearlong. Sediment traps full, channel migration occurring.	2		4		6	8													
	8	Cutting	Little or none. Infrequent raw banks <6".	Some, intermittently at outcrops and constrictions. Raw banks may be up to 12".	Significant. Cuts 12–24" high. Root mat overhangs and sloughing evident.	Almost continuous cuts, some over 24" high. Failure of overhangs frequent.	4		7		12	16													
	9	Deposition	Little or no enlargement of channel or point bars.	Some new bar increase, mostly from coarse gravel.	Moderate deposition of new gravel and coarse sand on old and some new bars.	Extensive deposit of predominantly fine particles. Accelerated bar development.	4		8		12	16													
	10	Rock angularity	Sharp edges and corners. Plane surfaces rough.	Rounded corners and edges. Surfaces smooth and flat.	2	Comers and edges well rounded in 2 dimensions.	1		2		3	4													
	11	Brightness	Surfaces dull, dark or stained. Generally not bright.	Mostly dull, but may have <35% bright surfaces.	2	Mixture dull and bright, i.e., 35–65% mixture range.	1		2		3	4													
Bottom	12	Consolidation of particles	Assorted sizes tightly packed or overlapping.	Moderately packed with some overlapping.	3	Mostly loose assortment with no apparent overlap.	3		4		6	8													
	13	Bottom size distribution	No size change evident. Stable material 80–100%.	Distribution shift light. Stable material 50–80%.	4	Moderate change in sizes. Stable materials 20–50%.	4		8		12	16													
	14	Scouring and deposition	<5% of bottom affected by scour or deposition.	5–30% affected. Scour at constrictions and where grades steepen. Some deposition in pools.	6	30–50% affected. Deposits and scour at obstructions, constrictions and bends. Some filling of pools.	6		9		18	24													
	15	Aquatic vegetation	Abundant growth moss-like, dark green perennial. In swift water too.	Common. Algae forms in low velocity and pool areas. Moss here too.	1	Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick.	1		2		3	4													
			<b>Excellent total = 18</b>	<b>Good total = 15</b>	<b>Fair total = 17</b>	<b>Poor total = 20</b>																			
Stream type	A1	A2	A3	A4	A5	A6	B1	B2	B3	B4	B5	B6	C1	C2	C3	C4	C5	C6	C6	D3	D4	D5	D6	Grand total = 70	
Good (Stable)	36-43	38-43	54-90	60-95	60-95	50-80	38-45	38-45	40-60	40-64	48-68	40-60	38-50	38-50	60-85	70-90	70-90	60-85	85-107	85-107	85-107	85-107	85-107	85-107	87-98
Fair (Mod. unstable)	44-47	44-47	91-129	96-132	96-142	81-110	46-58	46-58	61-78	65-84	69-88	61-78	51-61	51-61	86-105	91-110	91-110	86-105	108-132	108-132	108-132	108-132	108-132	99-125	
Poor (Unstable)	48+	48+	130+	133+	143+	111+	59+	59+	79+	85+	89+	79+	62+	62+	106+	111+	111+	106+	133+	133+	133+	133+	133+	126+	
Stream type	DA3	DA4	DA5	DA6	E3	E4	E5	E6	F1	F2	F3	F4	F5	F6	G1	G2	G3	G4	G5	G6				B4	
Good (Stable)	40-63	40-63	40-63	40-63	40-63	50-75	50-75	40-63	60-85	85-110	85-110	90-115	90-115	90-115	80-95	40-60	40-60	85-107	85-107	90-112	90-112	85-107	85-107	85-107	
Fair (Mod. unstable)	64-86	64-86	64-86	64-86	64-86	76-96	76-96	64-86	86-105	86-105	111-125	111-125	116-130	116-130	96-110	61-78	61-78	108-120	108-120	113-125	113-125	108-120	108-120	108-120	
Poor (Unstable)	87+	87+	87+	87+	87+	97+	97+	87+	106+	106+	126+	126+	131+	131+	111+	79+	79+	121+	121+	126+	126+	121+	126+	121+	
			<b>Excellent total = 18</b>	<b>Good total = 15</b>	<b>Fair total = 17</b>	<b>Poor total = 20</b>							Grand total = 70	Existing stream type = B4	*Potential stream type = B4	Modified channel stability rating = Fair									

\*Rating is adjusted to potential stream type, not existing.

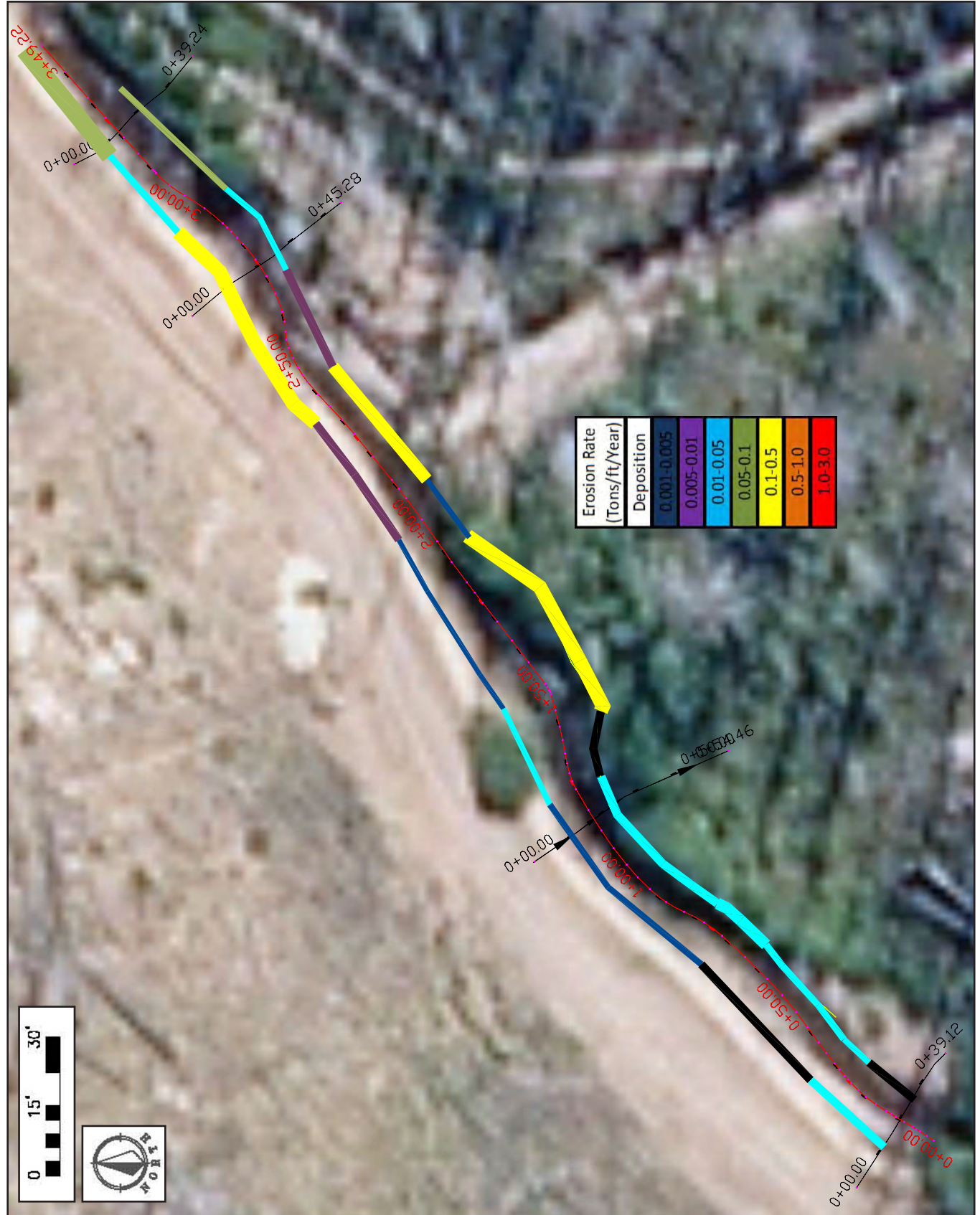
## BANCS Model – Streambank Erosion

**Worksheet 5-18.** Annual streambank erosion estimates.

Stream: <b>Trail Creek, B4 Fair Reach</b>				Location: <b>Pike National Forest, Colorado</b>			
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>340</b>		Date: <b>8/20/2010</b>			
Observers: <b>Wright, J.J. &amp; Kasun</b>		Valley Type: <b>VIII</b>		Stream Type: <b>B4</b>			
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 5-16) (adjective)	NBS rating (Worksheet 5-17) (adjective)	Bank erosion rate (Figure 5-34 or 5- 35) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal {[(4)×(5)×(6)] (ft <sup>3</sup> /yr)}	Erosion Rate (tons/yr/ft) {[(7)/27] × 1.3 / (5)}
0+00 to 1. 0+37 Left	High	Moderate	0.37957	37.0	2.0	28.09	0.03655
0+23 to 2. 0+36 Right	Moderate	High	0.42031	12.0	1.5	7.57	0.03036
0+35 to 3. 0+60 Right	Moderate	Moderate	0.25348	25.0	1.7	10.77	0.02075
0+65 to 4. 0+89 Right	Very High	Moderate	0.37957	23.0	2.8	24.44	0.05117
0+89 to 5. 1+23 Left	Low	Low	0.03566	34.0	1.5	1.82	0.00258
0+89 to 6. 1+23 Right	Moderate	Moderate	0.25348	34.0	2.1	18.10	0.02563
1+23 to 7. 1+36 Left	Low	Moderate	0.07435	13.0	1.4	1.35	0.00501
1+36 to 8. 1+85 Left	Low	Low	0.03566	49.0	1.2	2.10	0.00206
1+36 to 9. 1+87 Right	Very High	Very High	0.87205	1.0	3.5	3.05	0.14696
1+85 to 10. 2+20 Left	Moderate	Low	0.15287	35.0	2.0	10.70	0.01472
1+87 to 11. 2+05 Right	Low	Low	0.03566	18.0	1.3	0.83	0.00223
2+20 to 12. 2+56 Left	Very High	Very High	0.87205	36.0	3.5	109.88	0.14696
2+05 to 13. 2+33 Right	Extreme	Extreme	2.76027	28.0	3.0	231.86	0.39871
2+33 to 14. 2+56 Right	High	Very High	0.87205	23.0	2.0	40.11	0.08398
2+56 to 15. 2+71 Right	Moderate	Low	0.15287	15.0	1.4	3.21	0.01030
2+56 to 16. 2+84 Left	Low	Low	0.03566	28.0	1.6	1.60	0.00275
2+71 to 17. 3+40 Right	High	Very High	0.87205	69.0	1.5	90.26	0.06298
2+84 to 18. 3+40 Left	Moderate	High	0.42031	56.0	4.3	101.21	0.08702
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					Total Erosion (ft <sup>3</sup> /yr)	<b>686.96</b>	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					Total Erosion (yds <sup>3</sup> /yr)	<b>25.44</b>	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					Total Erosion (tons/yr)	<b>33.08</b>	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					Total Erosion (tons/yr/ft)	<b>0.0973</b>	



**Streambank Erosion Map**



## FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Equation Type		Equation Source				Equation		Bankfull Discharge (cfs)			Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)		
1. Bedload Sediment		"Good/Fair" Pagosa				$y = -0.0113 + 1.0139x^{2.1929}$		30.17			0.0160		21.46		
2. Suspended Sediment		"Good/Fair" Pagosa				$y = 0.0636 + 0.9326x^{2.4085}$									
		From Dimensional Flow-Duration Curve				From Sediment Rating Curves				Calculate		Calculate Sediment Yield			
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	
Percentage of Time	Daily Mean Discharge (cfs)	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Sediment Discharge (S/S <sub>bed</sub> )	Suspended Sediment Discharge (tons/day)	Dimensionless Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow [(5)×(6)]	Suspended Sediment [(5)×(9)]	Bedload Sediment [(5)×(11)]	Suspended Sediment + Bedload Sediment [(13)×(14)]	
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>bed</sub> )	(S/S <sub>bed</sub> )	(tons/day)	(b <sub>y</sub> /b <sub>bed</sub> )	(tons/day)	(cfs)	(tons)	(tons)	(tons)	
0%	76.7														
0.10%	65.9	0.05%	0.09%	0.34	71.3	2.363	7.461	30.82	6.670	10.16	24.5	10.58	3.49	14.06	
0.25%	57.0	0.08%	0.15%	0.55	61.4	2.036	5.232	18.62	4.809	7.33	33.6	10.20	4.01	14.21	
0.50%	49.2	0.13%	0.25%	0.91	53.1	1.761	3.706	11.41	3.494	5.32	48.5	10.41	4.86	15.27	
0.75%	42.0	0.13%	0.25%	0.91	45.6	1.513	2.592	6.86	2.502	3.81	41.7	6.26	3.48	9.73	
1%	36.4	0.13%	0.25%	0.91	39.2	1.300	1.817	4.13	1.790	2.73	35.8	3.77	2.49	6.26	
1.5%	31.2	0.25%	0.50%	1.83	33.8	1.120	1.289	2.52	1.289	1.96	61.7	4.61	3.58	8.19	
2%	26.1	0.25%	0.50%	1.83	28.6	0.949	0.886	1.47	0.893	1.36	52.3	2.68	2.48	5.16	
3%	21.9	0.50%	1.00%	3.65	24.0	0.795	0.600	0.83	0.602	0.92	87.5	3.05	3.35	6.39	
4%	18.7	0.50%	1.00%	3.65	20.3	0.674	0.424	0.50	0.415	0.63	74.2	1.82	2.31	4.13	
5%	16.7	0.50%	1.00%	3.65	17.7	0.587	0.322	0.33	0.304	0.46	64.6	1.21	1.69	2.90	
10%	10.5	2.50%	5.00%	18.25	13.6	0.450	0.200	0.16	0.165	0.25	247.9	2.87	4.58	7.46	
20%	5.7	5.00%	10.00%	36.50	8.1	0.269	0.103	0.05	0.045	0.07	295.7	1.76	2.53	4.29	
30%	3.8	5.00%	10.00%	36.50	4.8	0.158	0.075	0.02	0.006	0.01	173.9	0.75	0.36	1.11	
40%	2.7	5.00%	10.00%	36.50	3.3	0.108	0.068	0.01	0.000	0.00	118.9	0.47	0.00	0.47	
50%	2.1	5.00%	10.00%	36.50	2.4	0.079	0.066	0.01	0.000	0.00	87.0	0.33	0.00	0.33	
60%	1.6	5.00%	10.00%	36.50	1.8	0.061	0.065	0.01	0.000	0.00	66.7	0.25	0.00	0.25	
70%	1.3	5.00%	10.00%	36.50	1.4	0.047	0.064	0.01	0.000	0.00	52.2	0.19	0.00	0.19	
80%	1.1	5.00%	10.00%	36.50	1.2	0.039	0.064	0.00	0.000	0.00	43.5	0.16	0.00	0.16	
90%	0.8	5.00%	10.00%	36.50	1.0	0.032	0.064	0.00	0.000	0.00	34.8	0.13	0.00	0.13	
100%	0.2	5.00%	10.00%	36.50	0.5	0.016	0.064	0.00	0.000	0.00	17.4	0.06	0.00	0.06	
<b>Annual Totals:</b>										1,662.1 (cfs)		61.6 (tons/yr)		100.8 (tons/yr)	
										3,296.8 (acre-ft)		39.2 (tons/yr)			

Worksheet 19b. Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Equation Type		Equation Source				Equation		Bankfull Discharge (cfs)			Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)				
1. Bedload Sediment		"Good/Fair" Pagosa				$y = -0.0113 + 1.0139x^{2.1929}$		30.17			0.0290		38.00				
2. Suspended Sediment		"Good/Fair" Pagosa				$y = 0.0636 + 0.9326x^{2.4085}$											
From Dimensional Flow-Duration Curve						From Sediment Rating Curves						Calculate		Calculate Sediment Yield			
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)			
Percentage of Time	Daily Mean Discharge	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Suspended Sediment Discharge	Suspended Sediment Discharge	Dimensionless Bedload Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow	Suspended Sediment	Bedload Sediment	Suspended Sediment + Bedload Sediment			
(%)	(cfs)	(%)	(%)	(days)	(cfs)	( $Q/Q_{bkt}$ )	( $S/S_{bkt}$ )	(tons/day)	( $b_b/b_{bkt}$ )	(tons/day)	(cfs)	(tons)	(tons)	(tons)			
0%	98.1																
0.10%	87.2	0.05%	0.09%	0.34	92.6	3.070	13.965	132.73	11.856	32.75	31.8	45.54	11.24	56.78			
0.25%	78.3	0.08%	0.15%	0.55	82.8	2.743	10.664	90.56	9.260	25.58	45.3	49.58	14.01	63.59			
0.50%	70.6	0.13%	0.25%	0.91	74.5	2.468	8.281	63.26	7.341	20.28	67.9	57.73	18.51	76.24			
0.75%	63.4	0.13%	0.25%	0.91	67.0	2.220	6.433	44.22	5.819	16.08	61.1	40.35	14.67	55.02			
1%	57.7	0.13%	0.25%	0.91	60.6	2.007	5.058	31.43	4.661	12.88	55.3	28.68	11.75	40.43			
1.5%	52.3	0.25%	0.50%	1.83	55.0	1.823	4.023	22.69	3.770	10.42	100.4	41.42	19.01	60.43			
2%	46.8	0.25%	0.50%	1.83	49.5	1.642	3.141	15.96	2.995	8.27	90.4	29.12	15.10	44.22			
3%	42.7	0.50%	1.00%	3.65	44.7	1.483	2.471	11.34	2.393	6.61	163.3	41.39	24.13	65.52			
4%	37.8	0.50%	1.00%	3.65	40.2	1.333	1.929	7.96	1.894	5.23	146.8	29.06	19.10	48.16			
5%	33.4	0.50%	1.00%	3.65	35.6	1.181	1.455	5.32	1.448	4.00	130.0	19.41	14.60	34.01			
10%	20.9	2.50%	5.00%	18.25	27.1	0.900	0.787	2.19	0.793	2.19	495.5	40.00	39.99	79.99			
20%	7.5	5.00%	10.00%	36.50	14.2	0.470	0.215	0.31	0.183	0.50	518.0	11.44	18.42	29.86			
30%	3.9	5.00%	10.00%	36.50	5.7	0.190	0.081	0.05	0.015	0.04	209.1	1.73	1.54	3.27			
40%	2.7	5.00%	10.00%	36.50	3.3	0.110	0.068	0.02	0.000	0.00	121.1	0.85	0.00	0.85			
50%	2.1	5.00%	10.00%	36.50	2.4	0.079	0.066	0.02	0.000	0.00	87.0	0.59	0.00	0.59			
60%	1.6	5.00%	10.00%	36.50	1.8	0.061	0.065	0.01	0.000	0.00	66.7	0.44	0.00	0.44			
70%	1.3	5.00%	10.00%	36.50	1.4	0.047	0.064	0.01	0.000	0.00	52.2	0.34	0.00	0.34			
80%	1.1	5.00%	10.00%	36.50	1.2	0.039	0.064	0.01	0.000	0.00	43.5	0.29	0.00	0.29			
90%	0.8	5.00%	10.00%	36.50	1.0	0.032	0.064	0.01	0.000	0.00	34.8	0.23	0.00	0.23			
100%	0.2	5.00%	10.00%	36.50	0.5	0.016	0.064	0.00	0.000	0.00	17.4	0.11	0.00	0.11			
												2,537.4		438.28		660.35	
												(cfs)		(tons/yr)		(tons/yr)	
												5,032.9		222.07		660.35	
												(acre-ft)		(tons/yr)		(tons/yr)	
												Annual Totals:					

# POWERSED Model – Sediment Transport Capacity

**Worksheet 20a.** Sediment transport prediction representing the upstream supply up to bankfull for bedload and suspended sand sediment.

Stream: Trail Creek, Upstream Existing Sediment Supply		Location: Pike National Forest, Colorado (Used "GOOD-FAIR" Curves)			Gage Station #: Used Post-Fire Dimensionless F-D C.			Date: 08/14/10									
Observers: S=024, Q=30, 24, Bed.=0638 lb/s, S.Sand=19 mg/l		Stream Type: B4			Valley Type: VIII												
		Hydraulic geometry			Measure			Calculate									
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
Percentage of time	Daily mean discharge	Mid-ordinate stream-flow	Area	Width	Depth	Velocity	Slope	Shear stress	Stream power	Unit power	Time increment	Time increment	Daily mean bedload transport	Daily mean bedload transport	Time adjusted bedload transport	Time adjusted suspended sand transport	Time adjusted total transport
(%)	(cfs)	(cfs)	(ft <sup>2</sup> )	(ft)	(ft)	(ft/s)	(ft/ft)	(lb/ft <sup>2</sup> )	(lb/s)	(lb/ft/s)	(%)	(days)	(tons/day)	(tons/day)	(tons)	(tons)	(tons)
100.00%	0.16										0%			0.00	0.00	0.00	0.00
90.00%	0.79	0.48	0.42	4.50	0.09	0.99	0.0240	0.14	0.72	0.16	10%	36.50	0.00	0.00	0.00	0.00	0.00
80.00%	1.11	0.95	0.71	5.30	0.13	1.34	0.0240	0.20	1.42	0.27	10%	36.50	0.00	0.00	0.00	0.00	0.00
70.00%	1.27	1.19	0.81	5.46	0.15	1.42	0.0240	0.22	1.78	0.33	10%	36.50	0.00	0.00	0.00	0.00	0.00
60.00%	1.59	1.43	0.92	5.62	0.16	1.50	0.0240	0.24	2.14	0.38	10%	36.50	0.00	0.00	0.00	0.00	0.00
50.00%	2.07	1.83	1.09	5.88	0.19	1.63	0.0240	0.28	2.74	0.47	10%	36.50	0.00	0.01	0.00	0.36	0.36
40.00%	2.70	2.39	1.32	6.21	0.21	1.81	0.0240	0.32	3.58	0.58	10%	36.50	0.00	0.01	0.00	0.36	0.36
30.00%	3.94	3.32	1.62	6.45	0.25	2.01	0.0240	0.37	4.97	0.77	10%	36.50	0.00	0.01	0.00	0.36	0.36
20.00%	7.53	5.74	2.34	6.98	0.34	2.43	0.0240	0.49	8.60	1.23	10%	36.50	0.04	0.02	1.46	0.73	2.19
10.00%	20.87	14.20	4.32	8.22	0.53	3.27	0.0240	0.77	21.27	2.59	10%	36.50	0.52	0.16	18.98	5.84	24.82
5.00%	33.46	27.17	6.75	9.33	0.72	4.03	0.0240	1.05	40.69	4.36	5%	18.25	2.20	1.11	40.15	20.26	60.41
4.00%	37.82	35.64															
3.00%	42.69	40.26															
2.00%	46.82	44.76															
1.50%	52.29	49.56															
1.00%	57.76	55.03															
0.75%	63.43	60.60															
0.50%	70.63	67.03															
0.25%	78.39	74.51															
0.10%	87.25	82.82															
0.0060%	98.13	92.69															
Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr):															60.6	27.9	88.5

**Worksheet 20b.** Sediment transport prediction for the existing condition reach compared to the upstream sediment supply to assess bed stability.

Stream: Trail Creek, B4 Fair Riffle XS 2+74		Location: Pike National Forest, Colorado (Used "GOOD-FAIR" Curves)		Date: 08/14/10													
Observers: S=-024, Q=30, 24, Bed.=.0638 lb/s, S.Sand=19 mg/l		Stream Type: B4		Gage Station #: Used Post-Fire Dimensionless F-D C.													
Valley Type: VIII		Hydraulic geometry		Calculate													
Flow-duration curve		Measure		Calculate													
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
Percentage of time	Daily mean discharge	Mid-ordinate stream-flow	Area	Width	Depth	Velocity	Slope	Shear stress	Stream power	Unit power	Time increment	Time increment	Daily mean bedload transport	Daily suspended sand transport	Time adjusted bedload transport	Time adjusted suspended sand transport	Time adjusted total transport
(%)	(cfs)	(cfs)	(ft <sup>2</sup> )	(ft)	(ft)	(ft/s)	(ft/ft)	(lb/ft <sup>2</sup> )	(lb/s)	(lb/ft/s)	(%)	(days)	(tons/day)	(tons/day)	$[(13) \times (14)]$	$[(13) \times (15)]$	$[(16) + (17)]$
100.00%	0.16										0%				0.00	0.00	0.00
90.00%	0.79	0.48	0.33	3.03	0.11	1.37	0.0240	0.16	0.72	0.24	10%	36.50	0.00	0.00	0.00	0.00	0.00
80.00%	1.11	0.95	0.53	3.58	0.15	1.70	0.0240	0.22	1.42	0.40	10%	36.50	0.00	0.00	0.00	0.00	0.00
70.00%	1.27	1.19	0.63	3.79	0.17	1.83	0.0240	0.25	1.78	0.47	10%	36.50	0.00	0.00	0.00	0.00	0.00
60.00%	1.59	1.43	0.72	4.00	0.18	1.96	0.0240	0.27	2.14	0.54	10%	36.50	0.00	0.00	0.00	0.00	0.00
50.00%	2.07	1.83	0.86	4.28	0.20	2.09	0.0240	0.30	2.74	0.64	10%	36.50	0.00	0.01	0.00	0.36	0.36
40.00%	2.70	2.39	1.05	4.65	0.23	2.25	0.0240	0.33	3.58	0.77	10%	36.50	0.00	0.01	0.00	0.36	0.36
30.00%	3.94	3.32	1.32	5.06	0.26	2.49	0.0240	0.38	4.97	0.98	10%	36.50	0.00	0.01	0.00	0.36	0.36
20.00%	7.53	5.74	1.91	5.54	0.34	2.98	0.0240	0.50	8.60	1.55	10%	36.50	0.17	0.03	6.21	1.09	7.30
10.00%	20.87	14.20	4.31	10.87	0.40	3.28	0.0240	0.57	21.27	1.96	10%	36.50	0.30	0.11	10.95	4.01	14.96
5.00%	33.46	27.17	6.72	12.44	0.54	4.02	0.0240	0.78	40.69	3.27	5%	18.25	1.17	0.61	21.35	11.13	32.48
4.00%	37.82	35.64															
3.00%	42.69	40.26															
2.00%	46.82	44.76															
1.50%	52.29	49.56															
1.00%	57.76	55.03															
0.75%	63.43	60.60															
0.50%	70.63	67.03															
0.25%	78.39	74.51															
0.10%	87.25	82.82															
0.0060%	98.13	92.69															

Notes:	
Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr):	38.5
Upstream total annual sediment supply (tons/yr) (Worksheet 5-20a):	60.6
Difference in sediment transport capacity (tons/yr) (+ or -):	-22.1
Stability evaluation: Aggradation, Degradation or Stable:	Aggradation, = 37% Reduction in Transport

## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>Trail Creek, B4 Fair, XS 2+74</b>		Stream Type: <b>B4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>Chavez, Kasun, Wright et al.</b>		Date: <b>9/1/2010</b>			
<b>Enter Required Information for Existing Condition</b>					
18.8	$D_{50}$	Riffle bed material $D_{50}$ (mm)			
45.1	$\hat{D}_{50}$	Bar sample $D_{50}$ (mm)			
0.34	$D_{max}$	Largest particle from bar sample (ft)	105	(mm)	304.8 mm/ft
0.0240	$S$	Existing bankfull water surface slope (ft/ft)			
0.57	$d$	Existing bankfull mean depth (ft)			
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment			
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>					
0.42	$D_{50}/\hat{D}_{50}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 ( D_{50}/\hat{D}_{50} )^{-0.872}$		
5.60	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 ( D_{max}/D_{50} )^{-0.887}$		
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED:		
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	$d$	Required bankfull mean depth (ft)	$d = \frac{\tau^*(\gamma_s - 1)D_{max}}{S}$ (use $D_{max}$ in ft)		
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	$S$	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^*(\gamma_s - 1)D_{max}}{d}$ (use $D_{max}$ in ft)		
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					
<b>Sediment Competence Using Dimensional Shear Stress</b>					
0.854	Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d ) $\gamma = 62.4$ , $d =$ existing depth, $S =$ existing slope				
Shields	CO	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ (Figure 5-49)			
60	140				
Shields	CO	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) (Figure 5-49)			
1.4	0.6				
Shields	CO	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm)		$d = \frac{\tau}{\gamma S}$	
0.93	0.40	$\tau =$ predicted shear stress, $\gamma = 62.4$ , $S =$ existing slope			
Shields	CO	Predicted slope required to initiate movement of measured $D_{max}$ (mm)		$S = \frac{\tau}{\gamma d}$	
0.0394	0.0169	$\tau =$ predicted shear stress, $\gamma = 62.4$ , $d =$ existing depth			
Check: <input checked="" type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					

## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>Trail Creek, B4 Fair Reach</b>		Stream Type: <b>B4</b>
Location: <b>Pike National Forest, CO</b>		Valley Type: <b>VIII</b>
Observers: <b>Rosgen, et al.</b>		Date: <b>8/20/2010</b>
<b>Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)</b>		<b>Stability Rating (Check Appropriate Rating)</b>
Stream Type at potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)		<input checked="" type="checkbox"/> Stable
(E→C), (C→High W/d C)		<input type="checkbox"/> Moderately Unstable
(G→F), (F→D), (C→F)		<input type="checkbox"/> Unstable
(C→D), (B→G), (D→G), (C→G), (E→G)		<input type="checkbox"/> Highly Unstable

**Worksheet 5-25.** Lateral stability.

Stream: <b>Trail Creek, B4 Fair Reach</b>		Stream Type: <b>B4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/20/2010</b>			
Lateral stability criteria (choose one stability category for each criterion 1-5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	8
	(2)	(4)	(6)	1.75 (8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	<b>B4, B8</b>	B3	B5, B6, B7	2
	(1)	<b>B4, B8 (2)</b>	(3)	(4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		1
	<b>M1 (1)</b>		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	4
	(2)	<b>M/M (4)</b>	(6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	> 0.8	0.3 – 0.79	0.1 – 0.29	< 0.1	1
	<b>1.2 (1)</b>	(2)	(3)	(4)	
<b>Total Points</b>					<b>16</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input type="checkbox"/>	<i>Unstable</i> 13 – 21 <input checked="" type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	



**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>Trail Creek, B4 Fair Reach</b>		Stream Type: <b>B4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/20/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
1 <b>Sediment competence</b> (Worksheet 5-22)	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope—slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	2
	(2)	(4)	(6)	(8)	
2 <b>Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	8
	(2)	(4)	(6)	(8)	
3 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	8
	(2)	(4)	(6)	1.75 (8)	
4 <b>Stream Succession States</b> (Worksheet 5-24)	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	2
	(2)	(4)	(6)	(8)	
5 <b>Depositional Patterns</b> (Worksheet 5-10)	B1	B2, B4	B3, B5	B6, B7, B8	4
	(1)	(2)	(3)	B4, B8 (4)	
6 <b>Debris / Blockages</b> (Worksheet 5-11)	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	1
	D2 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>25</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
<b>Vertical Stability for Excess Deposition / Aggradation</b> (use total points and check stability rating)	<i>No Deposition</i> 10 – 14 <input type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input checked="" type="checkbox"/>	<i>Aggradation</i> > 30 <input type="checkbox"/>	

**Worksheet 5-27.** Vertical stability – degradation.

Stream: <b>Trail Creek, B4 Fair Reach</b>		Stream Type: <b>B4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/20/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>1 Sediment Competence</b> (Worksheet 5-22)	Does not indicate excess competence	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed	$D_{100}$ of bed moved	Particles much larger than $D_{100}$ of bed moved	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>2 Sediment Capacity</b> (POWERSED) (Worksheet 5-20)	Does not indicate excess capacity	Slight excess energy: up to 10% increase above reference	Excess energy sufficient to increase load up to 50% of annual load	Excess energy transporting more than 50% of annual load	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>3 Degree of Channel Incision (BHR)</b> (Worksheet 5-12)	1.00 – 1.10	1.11 – 1.30	1.31 – 1.50	> 1.50	<b>2</b>
	1.00 (2)	(4)	(6)	(8)	
<b>4 Stream Succession States</b> (Worksheets 5-12 and 5-24)	Does not indicate incision or degradation	If BHR > 1.1 and stream type has W/d between 5–10	If BHR > 1.1 and stream type has W/d less than 5	(B→G), (C→G), (E→G), (D→G)	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>5 Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	> 0.80	0.30 – 0.79	0.10 – 0.29	< 0.10	<b>1</b>
	1.10 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>9</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation</b> (use total points and check stability rating)	<i>Not Incised</i> 9 – 11 <input checked="" type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input type="checkbox"/>	<i>Degradation</i> > 27 <input type="checkbox"/>	

Worksheet 5-28. Channel enlargement.

Stream: <b>Trail Creek, B4 Fair Reach</b>		Stream Type: <b>B4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/20/2010</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1-4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	2
	(2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	6
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	6
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	2
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>16</b>
<b>Category Point Range</b>					
<b>Channel Enlargement Prediction (use total points and check stability rating)</b>	<i>No Increase</i> 8 – 10 <input type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input checked="" type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input type="checkbox"/>	<i>Extensive</i> > 24 <input type="checkbox"/>	

Worksheet 5-29. Overall sediment supply.

Stream: <b>Trail Creek, B4 Fair Reach</b>		Stream Type: <b>B4</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>		
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/20/2010</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1-5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	3	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	3	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	1	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	2	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	2	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>11</b>	
<b>Category Point Range</b>				
<b>Overall Sediment Supply Rating (use total points and check stability rating)</b>	<i>Low</i> 5 <input type="checkbox"/>	<i>Moderate</i> 6 – 10 <input type="checkbox"/>	<i>High</i> 11 – 15 <input checked="" type="checkbox"/>	<i>Very High</i> 16 – 20 <input type="checkbox"/>

Worksheet 5-32. Summary of stability condition categories.

Stream: <b>Trail Creek, B4 Fair Reach</b>		Location: <b>Pike National Forest, Colorado</b>	
Observers: <b>K. Wright &amp; B. Kasun</b>		Stream Type: <b>B4</b> Valley Type: <b>VIII</b>	
Date: <b>8/20/2010</b>		Date: <b>8/20/2010</b>	
<b>Channel Dimension (XS 2+74)</b>	Mean Bankfull Depth (ft): <b>0.57</b>	Bankfull Width (ft): <b>12.59</b>	Cross-Sectional Area (ft <sup>2</sup> ): <b>7.19</b>
<b>Channel Pattern</b>	λ <sub>r</sub> /W <sub>bktf</sub> : <b>7.16</b>	L <sub>tr</sub> /W <sub>bktf</sub> : <b>N/A</b>	R <sub>c</sub> /W <sub>bktf</sub> : <b>N/A</b>
	Mean: <b>7.16</b>	MWR: <b>2.97</b>	Sinuosity: <b>1.2</b>
<b>River Profile &amp; Bed Features</b>	Check: <input type="checkbox"/> Riffle/Pool <input checked="" type="checkbox"/> Step/Pool <input type="checkbox"/> Plane Bed <input type="checkbox"/> Convergence/Divergence <input type="checkbox"/> Dunes/Antidunes/Smooth Bed	Pool	Ratio
	Max Bankfull Depth (ft): <b>1.23</b>	Riffle	Pool
<b>Level III Stream Stability Indices</b>	Depth Ratio (max to mean): <b>1.67</b>	Pool Spacing: <b>1.85</b>	Valley: <b>3.62</b>
	Water Surface: <b>0.024</b>	Remarks: Condition, Vigor & Usage of Existing Reach:	
<b>Bank Erosion Summary</b>	Riparian Vegetation: <b>Willow, Aspen, Grass</b>	Potential Composition/Density: <b>Same w/o invasives</b>	Invasive species control needed
	Flow Regime: <b>P1, P2, P8 &amp; Order: S-3(3)</b>	Meanander Patterns: <b>M1</b>	Debris/Channel Blockages: <b>B4, B8</b>
<b>Sediment Capacity (POWERSED)</b>	Degree of Incision (Bank-Height Ratio): <b>1.0</b>	Degree of Incision Stability Rating: <b>Stable</b>	Modified Pfankuch Stability Rating (Numeric & Adjective Rating): <b>70 (Fair)</b>
	Width/depth Ratio (W/d): <b>22.1</b>	Reference W/d Ratio (W/d <sub>ref</sub> ): <b>12.6</b>	W/d Ratio State Stability Rating: <b>Highly Unstable</b>
<b>Entrainment/Competence</b>	Meander Width Ratio (MWR): <b>2.97</b>	Reference MWR <sub>ref</sub> : <b>2.7</b>	MWR / MWR <sub>ref</sub> Stability Rating: <b>Unconfined</b>
	Length of Reach Studied (ft): <b>340</b>	Annual Streambank Erosion Rate: <b>33.08</b> (tons/yr)	Curve Used: <b>Colorado</b>
<b>Successional Stage Shift</b>	<input type="checkbox"/> Sufficient Capacity <input checked="" type="checkbox"/> Insufficient Capacity <input type="checkbox"/> Excess Capacity	Remarks: <b>≈ 37% Reduction in Transport Capacity</b>	
	Largest Particle from Bar Sample (mm): <b>105</b>	τ = <b>1.363</b>	τ* = <b>N/A</b>
<b>Lateral Stability</b>	B → G → Fb → B → B	Existing Depth: <b>0.57</b>	Required Depth: <b>.4-.93</b>
	<input type="checkbox"/> Stable <input type="checkbox"/> Mod. Unstable <input checked="" type="checkbox"/> Unstable	Existing Stream State (Type): <b>B4</b>	Potential Stream State (Type): <b>B4</b>
<b>Vertical Stability (Aggradation)</b>	<input type="checkbox"/> No Deposition <input type="checkbox"/> Mod. Deposition <input checked="" type="checkbox"/> Ex. Deposition <input type="checkbox"/> Aggradation	Remarks/causes: <b>Bank Erosion, W/d, &amp; Depositional Patterns</b>	
	<input checked="" type="checkbox"/> Not Incised <input type="checkbox"/> Slightly Incised <input type="checkbox"/> Mod. Incised <input type="checkbox"/> Degradation	Remarks/causes: <b>POWERSED, W/d, Depositional Patterns</b>	
<b>Channel Enlargement</b>	<input type="checkbox"/> No Increase <input checked="" type="checkbox"/> Slight Increase <input type="checkbox"/> Mod. Increase <input type="checkbox"/> Extensive	Remarks/causes: <b>Trend toward Aggradation</b>	
	<input type="checkbox"/> Low <input type="checkbox"/> Moderate <input checked="" type="checkbox"/> High <input type="checkbox"/> Very High	Remarks/causes:	
<b>Sediment Supply (Channel Source)</b>	Remarks/causes:		



## *Appendix C6*

# **C4 Stream Type**

## *Fair Stability Reach*





# Table of Contents

## *Appendix C6: C4 Fair Reach*

<b>Reach Location &amp; Overview.....</b>	<b>C6-2</b>
<b>Survey Summary.....</b>	<b>C6-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C6-9</b>
<b><i>Velocity, Classification &amp; Morphological Relations.....</i></b>	<b>C6-9</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b><i>Stability Indices.....</i></b>	<b>C6-13</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b><i>BANCS Model – Streambank Erosion.....</i></b>	<b>C6-23</b>
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b><i>FLOWSED Model – Total Annual Sediment Yield.....</i></b>	<b>C6-25</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b><i>POWERSED Model– Sediment Transport Capacity to Assess Bed Stability.....</i></b>	<b>C6-27</b>
Worksheet 5-20a. Sediment transport prediction for the upstream condition.	
Worksheet 5-20b. Sediment transport prediction for the existing condition.	
<b><i>Sediment Competence/Entrainment.....</i></b>	<b>C6-29</b>
Worksheet 5-22. Sediment competence calculations.	
<b><i>Channel Stability Ratings.....</i></b>	<b>C6-30</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b><i>Summary.....</i></b>	<b>C6-36</b>
Worksheet 5-32. Summary of stability condition categories.	

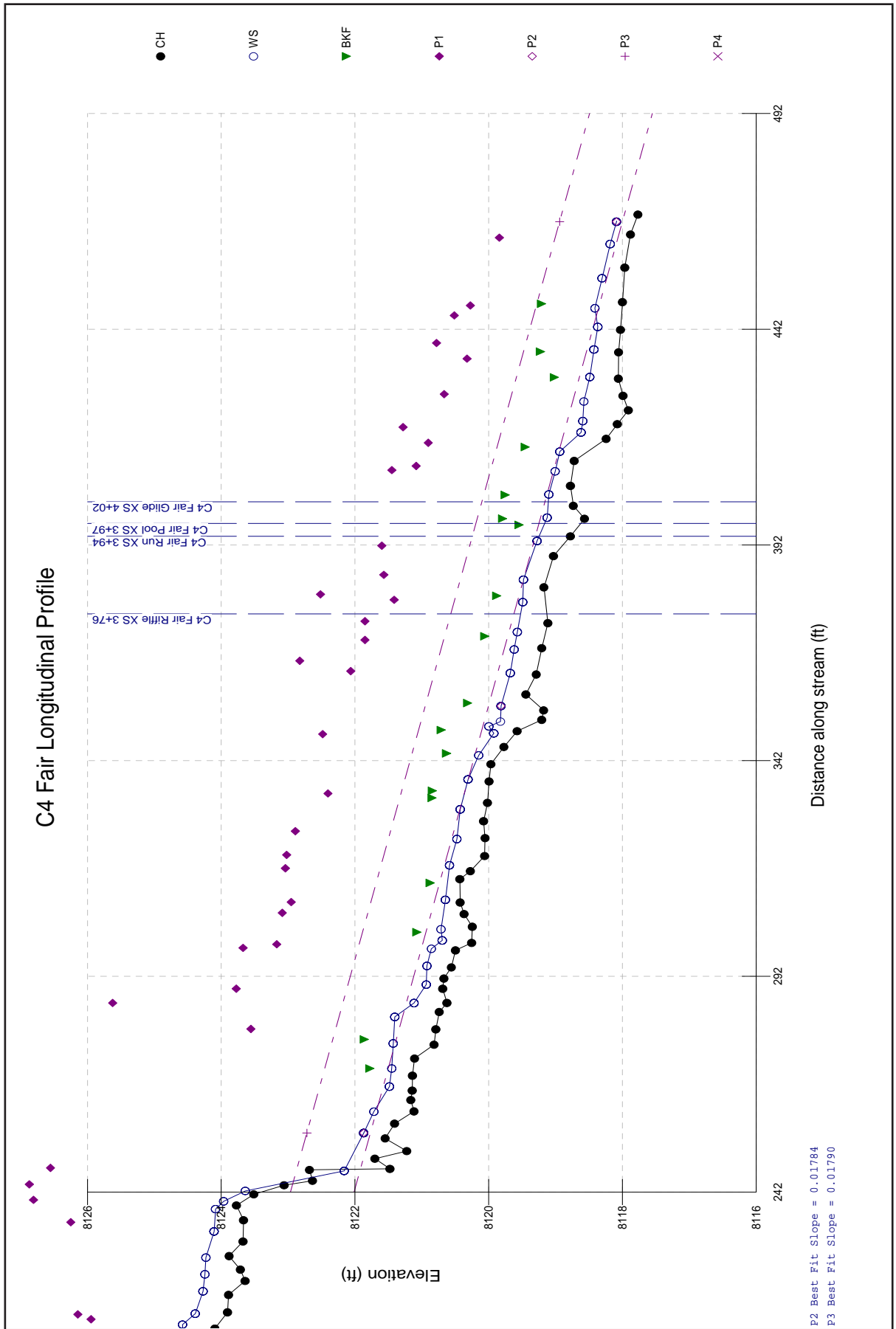
## C4 Fair Reach Location & Overview

The C4 Fair representative reach is a 4<sup>th</sup> order, perennial stream located in main Trail Creek (**Figure C-2**). The photograph depicts high eroding banks, although the riparian vegetation is slowly reoccupying this reach that has gradually evolved from an F4 to a C4 stream type. However, the higher width/depth ratio than the reference condition has led to excess sediment deposition in the channel as the sediment transport capacity model (POWERSED) indicates aggradation. The stability rating is “Fair” due to a “Fair” Pfankuch stability rating and the relatively high streambank erosion rate of  $0.0217 \text{ tons/yr/ft}$  compared to the C4 reference rate of  $0.0063 \text{ tons/yr/ft}$ . The sediment supply rating is *Moderate* due primarily to the streambank erosion source and increase in stored sediment in the channel bed. This rating indicates a potential accelerated increase in flow-related sediment based on increased post-fire streamflow peak flows compared to the reference C4 condition. The WRENSS model indicated a water yield increase due to the fire of  $1,745 \text{ acre-ft}$ . The bedload was consequently increased from  $39 \text{ tons/yr}$  to  $249 \text{ tons/yr}$ , and the suspended sediment increased from  $55 \text{ tons/yr}$  to  $455 \text{ tons/yr}$ , representing a total increase in sediment of  $610 \text{ tons/yr}$ . These are high values for a C4 stream type of this size, which reflect the accelerated sediment yield due to flow related sediment.

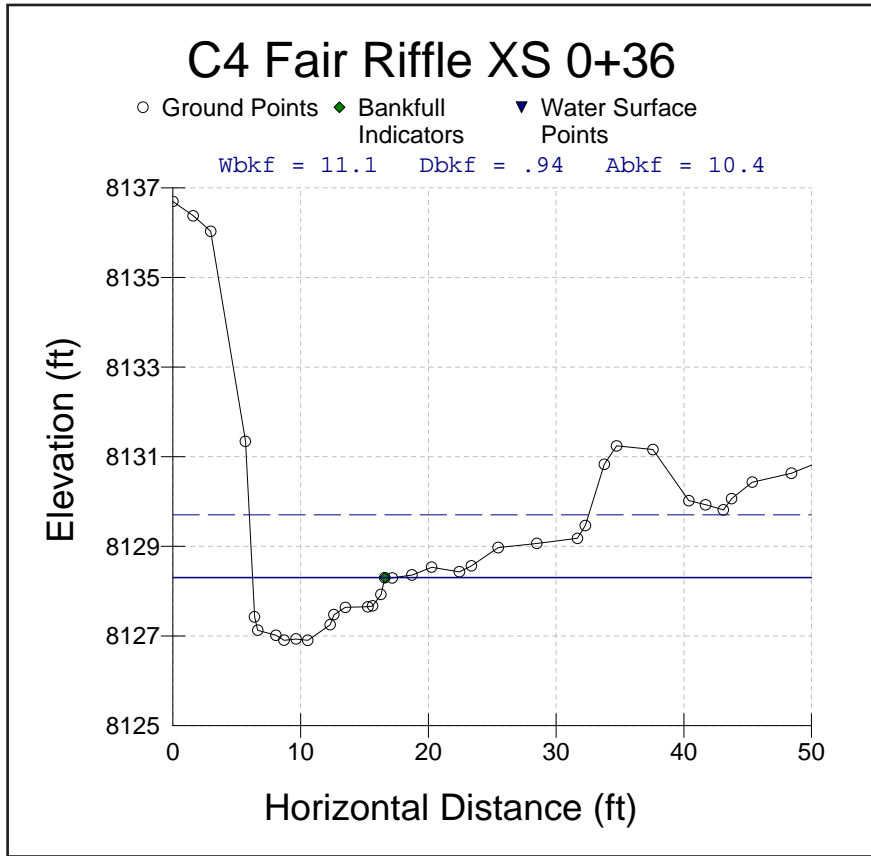
The following graphs and summary worksheets provide the detail of the morphology, hydraulics, streambank erosion rates, and stability conditions responsible for the overall “Fair” rating.



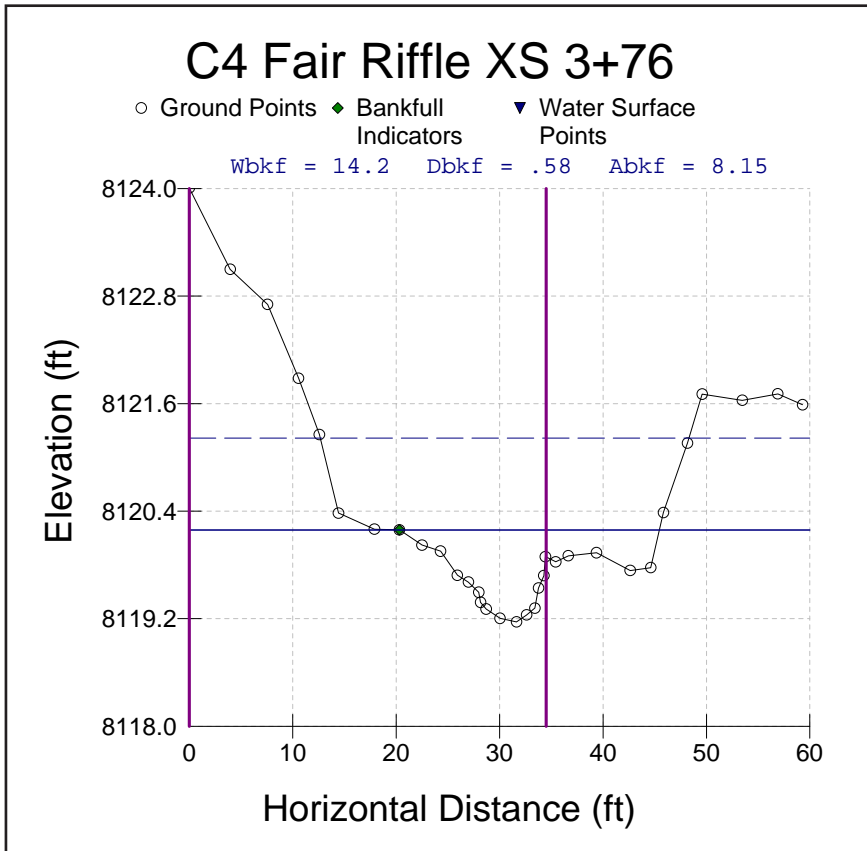
# Survey Summary



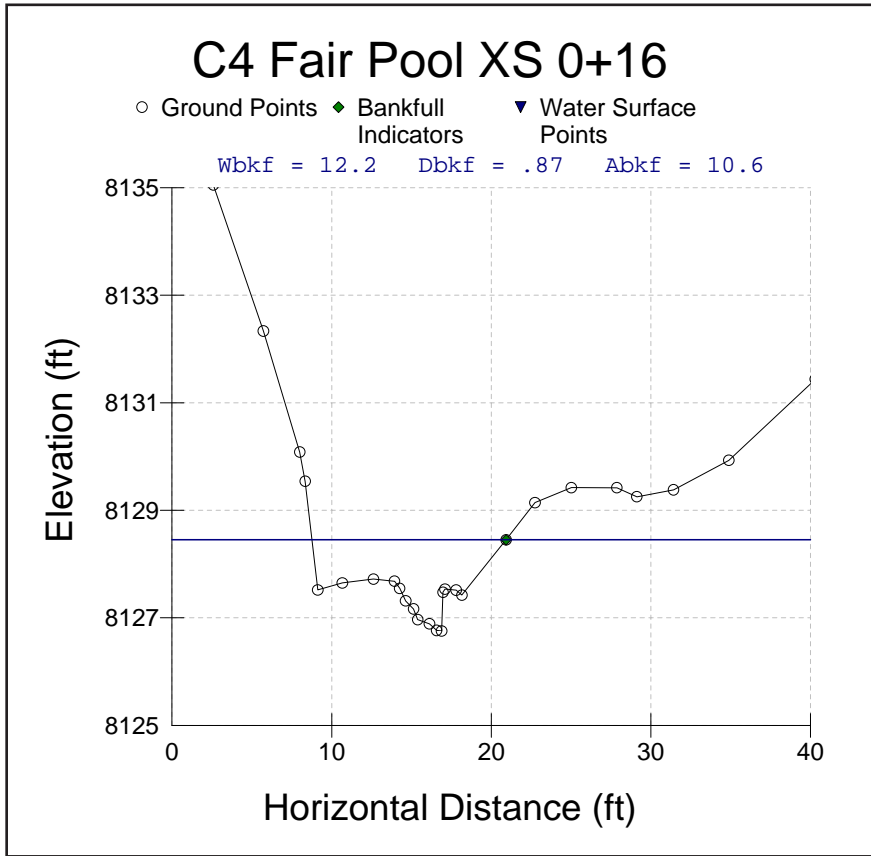
Longitudinal Profile (graph generated from RIVERMorph™)



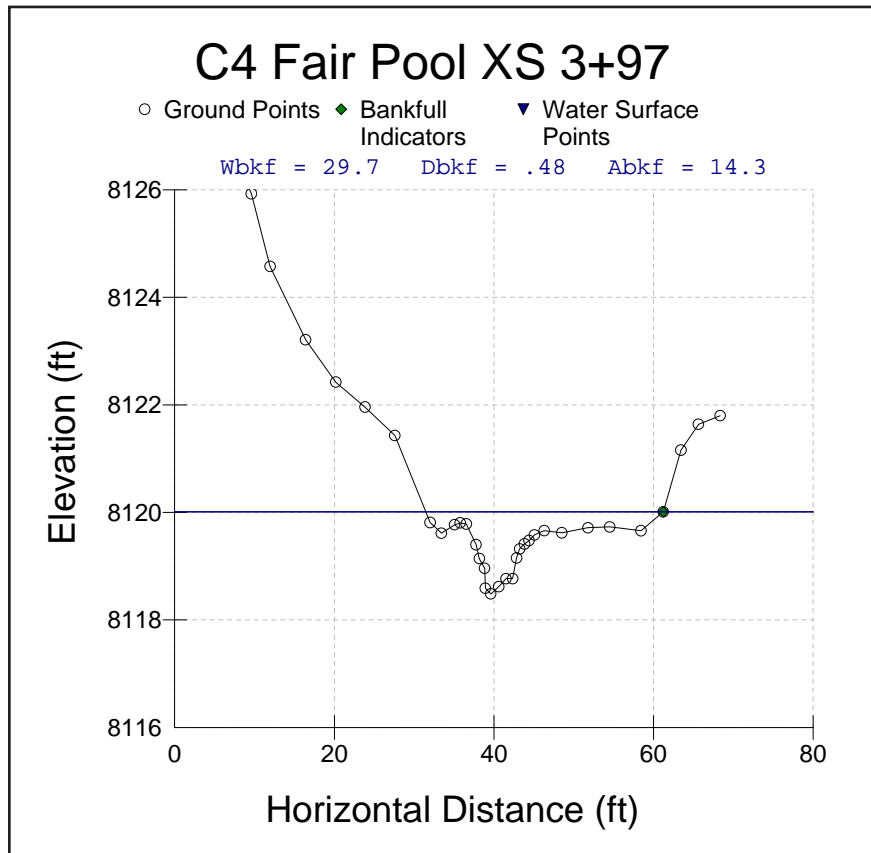
Riffle Cross-section 0+36 (graph generated from RIVERMorph™)



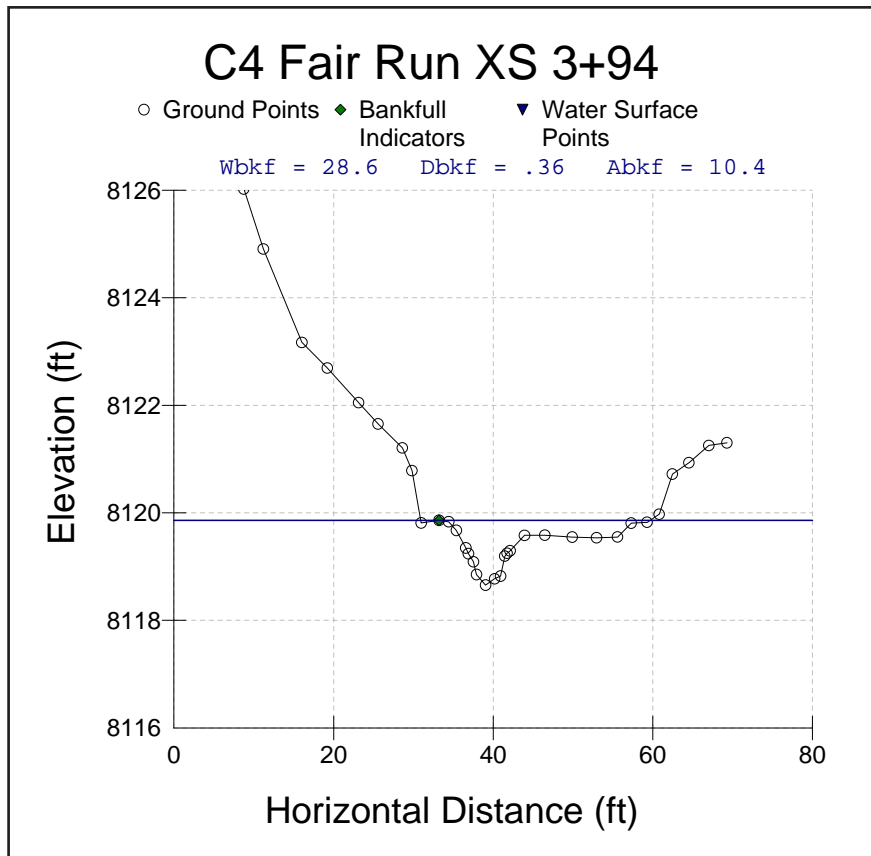
Representative Riffle Cross-section 3+76 (graph generated from RIVERMorph™)



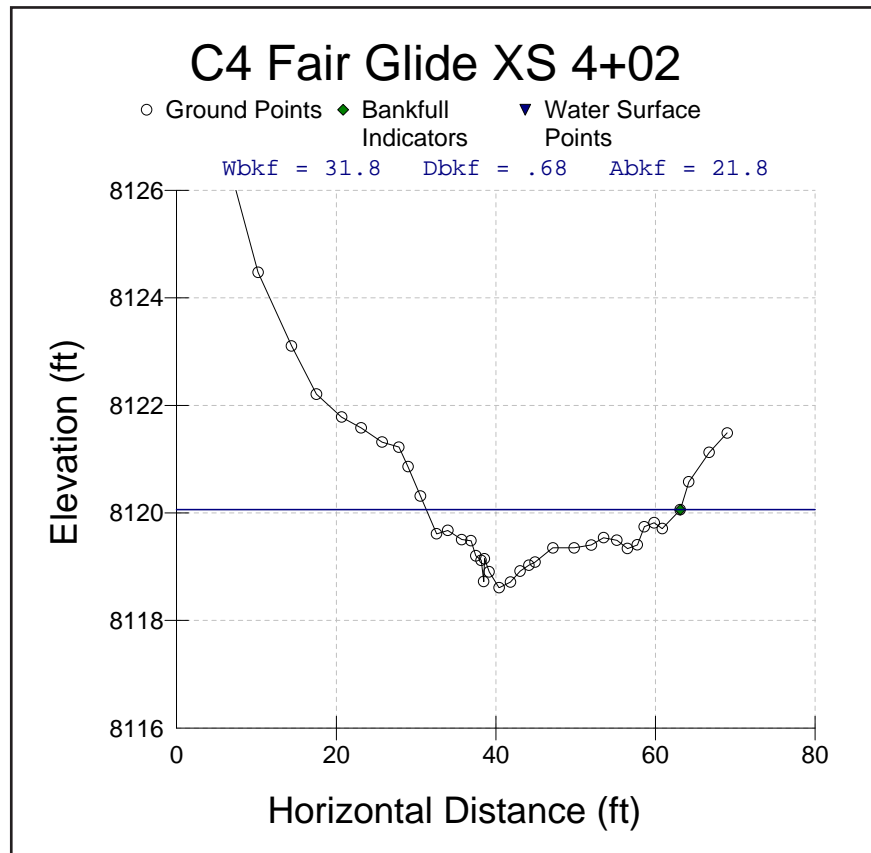
Pool Cross-section 0+16 (graph generated from RIVERMorph™)



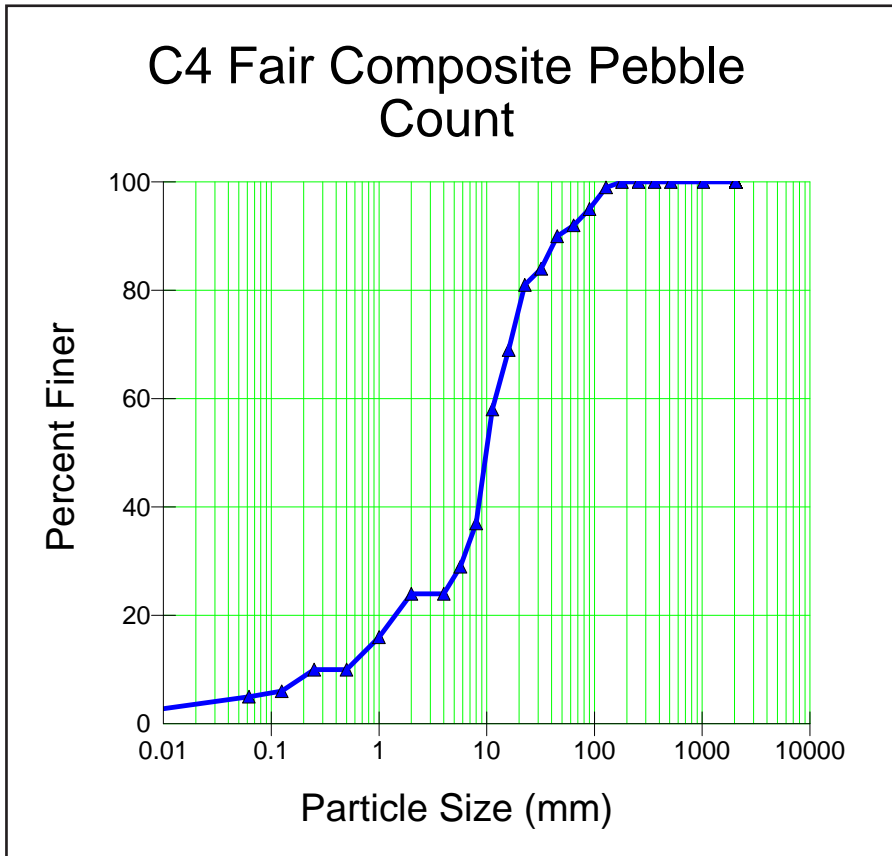
Pool Cross-section 3+97 (graph generated from RIVERMorph™)



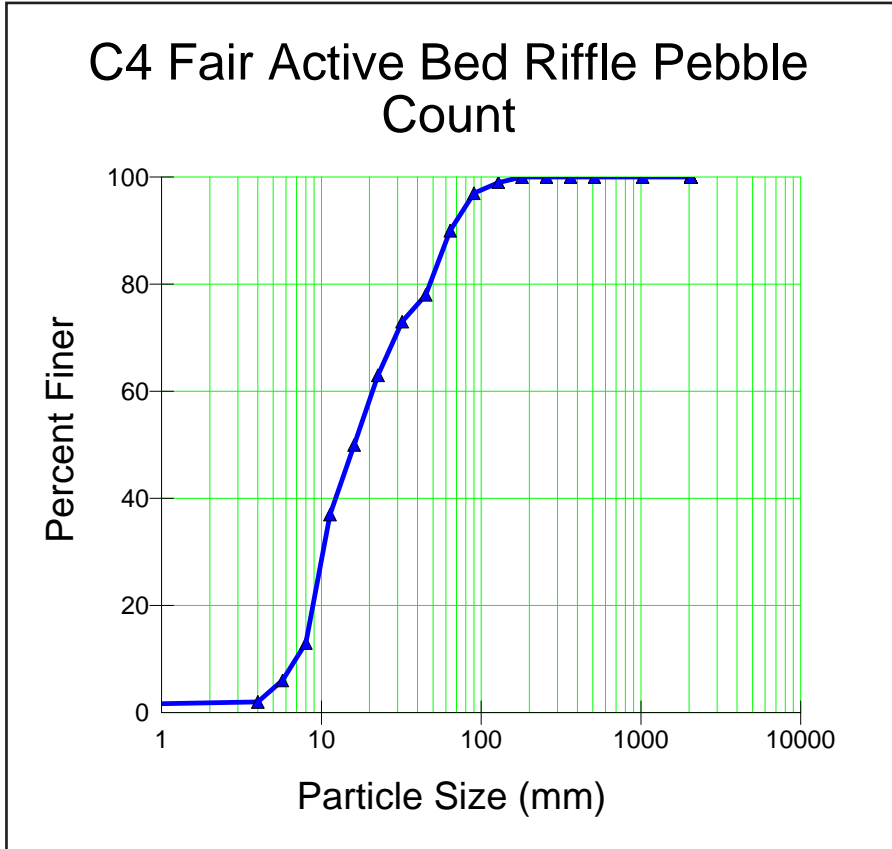
Run Cross-section 3+94 (graph generated from RIVERMorph™)



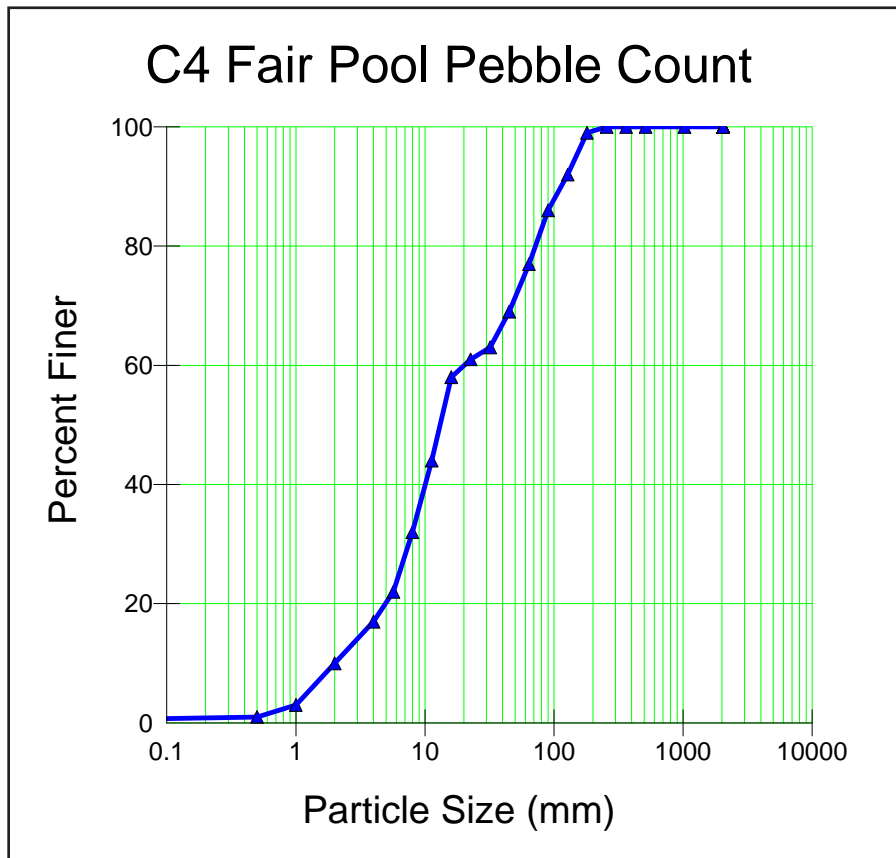
Glide Cross-section 4+02 (graph generated from RIVERMorph™)



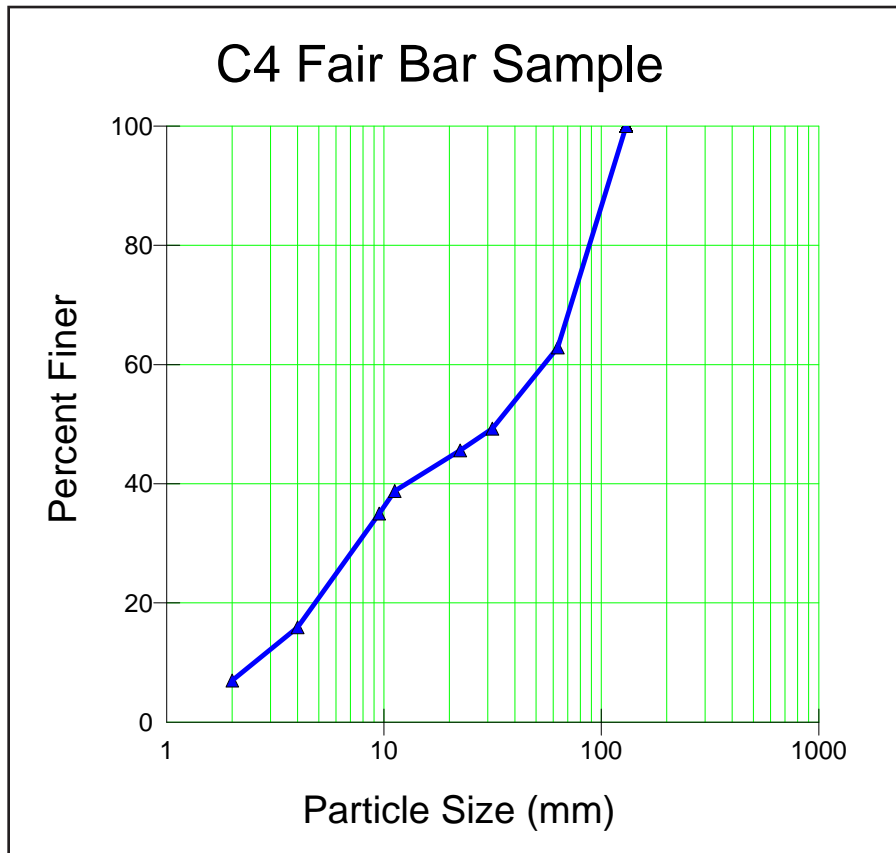
Composite Pebble Count (graph generated from RIVERMorph™)



Active Bed Riffle Pebble Count (graph generated from RIVERMorph™)



Pool Pebble Count (graph generated from RIVERMorph™)



Bar Sample (graph generated from RIVERMorph™)



# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates						
Stream:	Trail Creek, C4 Fair Reach			Location:	X-Sec 3+76, Pike N.F., Colorado	
Date:	8/22/2010	Stream Type:	C4	Valley Type:	VIII	
Observers:	K. Wright & B. Kasun			HUC:	_ _ _ _ _	
INPUT VARIABLES			OUTPUT VARIABLES			
Bankfull Riffle Cross-Sectional AREA	8.15	$A_{b_{kf}}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.58	$d_{b_{kf}}$ (ft)	
Bankfull Riffle WIDTH	14.2	$W_{b_{kf}}$ (ft)	Wetted PERIMETER ~ (2 * $d_{b_{kf}}$ ) + $W_{b_{kf}}$	15.31	$W_p$ (ft)	
$D_{84}$ at Riffle	54.5	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.18	$D_{84}$ (ft)	
Bankfull SLOPE	0.018	$S_{b_{kf}}$ (ft / ft)	Hydraulic RADIUS $A_{b_{kf}} / W_p$	0.53	R (ft)	
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R(ft) / $D_{84}$ (ft)	2.98	R / $D_{84}$	
Drainage Area	10.15	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.555	$u^*$ (ft/sec)	
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE	
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$			3.06	ft / sec	24.95	cfs
2. Roughness Coefficient: a) Manning's n from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.055$			2.39	ft / sec	19.46	cfs
2. Roughness Coefficient: b) Manning's n from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.04$			3.28	ft / sec	26.75	cfs
2. Roughness Coefficient: c) Manning's n from Jarrett (USGS): Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for Stream Types A1, A2, A3, B1, B2, B3, C2 & E3 $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ $n = 0.031$			4.24	ft / sec	34.56	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Limerinos			3.27	ft / sec	26.8	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)				ft / sec		cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q =$ <input type="text"/> year $u = Q / A$				ft / sec		cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$				ft / sec		cfs
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation (R/ $D_{84}$ ) – Estimation Method 1						
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.						
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.						
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.						
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.						

**Worksheet 5-3.** Level II stream classification.

Stream: <b>Trail Creek, C4 Fair Reach, Riffle XS 3+76</b>	
Basin:	Drainage Area: <b>10.15</b> acres mi <sup>2</sup>
Location: <b>Pike National Forest, Colorado</b>	
Twp.&Rge:	Sec.&Qtr.:
Cross-Section Monuments (Lat./Long.): <b>39.10042 Lat / 105.19497 Long</b> Date: <b>08/21/10</b>	
Observers: <b>K. Wright &amp; B. Kasun</b> Valley Type: <b>VIII</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>14.2</b> ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>0.58</b> ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>8.15</b> ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>24.41</b> ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>1.03</b> ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>35.67</b> ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>2.52</b> ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>10.04</b> mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.018</b> ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>1.05</b>

<b>Stream Type</b>	<b>C4</b>	(See Figure 2-14)
--------------------	-----------	-------------------

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, C4 Fair Reach</b>				Location: <b>Pike National Forest, Colorado</b>				
Observers: <b>K. Wright &amp; B. Kasun</b>			Date: <b>8/25/2010</b>		Valley Type: <b>VIII</b>		Stream Type: <b>C4</b>	
<b>River Reach Dimension Summary Data.....1</b>								
<b>Riffle Dimensions* ** ***</b>	<b>Riffle Dimensions* ** ***</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Width ( $W_{bkt}$ )	12.6	11.1	14.2	ft Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	9.3	8.2	10.4
	Mean Riffle Depth ( $d_{bkt}$ )	0.76	0.58	0.94	ft Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	18.1	11.8	24.4
	Maximum Riffle Depth ( $d_{max}$ )	1.22	1.03	1.40	ft Max Riffle Depth to Mean Riffle Depth ( $d_{max}/d_{bkt}$ )	1.633	1.489	1.776
	Width of Flood-Prone Area ( $W_{fpa}$ )	31.1	26.6	35.7	ft Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )	2.46	2.40	2.52
	Riffle Inner Berm Width ( $W_{ib}$ )	6.0	5.8	6.2	ft Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )	0.474	0.457	0.491
	Riffle Inner Berm Depth ( $d_{ib}$ )	0.42	0.25	0.34	ft Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )	0.553	0.329	0.441
	Riffle Inner Berm Area ( $A_{ib}$ )	2.0	1.4	2.6	ft <sup>2</sup> Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )	0.219	0.153	0.284
	Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )	18.9	14.8	23.0				
<b>Pool Dimensions* ** ***</b>	<b>Pool Dimensions* ** ***</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Pool Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Pool Width ( $W_{bkfp}$ )	21.0	12.2	29.8	ft Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )	1.661	0.964	2.361
	Mean Pool Depth ( $d_{bkfp}$ )	0.68	0.48	0.87	ft Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )	0.895	0.632	1.145
	Pool Cross-Sectional Area ( $A_{bkfp}$ )	12.5	10.6	14.4	ft Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )	1.349	1.148	1.550
	Maximum Pool Depth ( $d_{maxp}$ )	1.61	1.53	1.69	ft Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	2.118	2.013	2.224
	Pool Inner Berm Width ( $W_{ibp}$ )	3.8	3.6	4.0	ft Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )	0.180	0.169	0.191
	Pool Inner Berm Depth ( $d_{ibp}$ )	0.36	0.33	0.38	ft Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )	0.522	0.485	0.559
	Pool Inner Berm Area ( $A_{ibp}$ )	1.335	1.330	1.340	ft <sup>2</sup> Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )	0.107	0.106	0.107
	Point Bar Slope ( $S_{pb}$ )	0.300	0.260	0.340	ft/ft Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )	6.67	6.65	6.68
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Run Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Run Width ( $W_{bkfr}$ )	28.6			ft Run Width to Riffle Width ( $W_{bkfr} / W_{bkt}$ )	2.270		
	Mean Run Depth ( $d_{bkfr}$ )	0.36			ft Mean Run Depth to Mean Riffle Depth ( $d_{bkfr} / d_{bkt}$ )	0.474		
	Run Cross-Sectional Area ( $A_{bkfr}$ )	10.4			ft Run Area to Riffle Area ( $A_{bkfr} / A_{bkt}$ )	1.127		
	Maximum Run Depth ( $d_{maxr}$ )	1.20			ft Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )	1.579		
	Run Width/Depth Ratio ( $W_{bkfr} / d_{bkfr}$ )	79.5			ft			
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Glide Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Glide Width ( $W_{bkfg}$ )	29.6			ft Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )	2.346		
	Mean Glide Depth ( $d_{bkfg}$ )	0.49			ft Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )	0.645		
	Glide Cross-Sectional Area ( $A_{bkfg}$ )	14.4			ft Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )	1.557		
	Maximum Glide Depth ( $d_{maxg}$ )	1.21			ft Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )	1.592		
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )	60.4			ft/ft Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )	28.93		
	Glide Inner Berm Width ( $W_{ibg}$ )	8.4			ft Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )	0.284		
	Glide Inner Berm Depth ( $d_{ibg}$ )	0.29			ft Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )	0.592		
Glide Inner Berm Area ( $A_{ibg}$ )	2.5			ft <sup>2</sup> Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )	0.170			
<b>Step**</b>	<b>Step Dimensions**</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Step Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Step Width ( $W_{bkfs}$ )				ft Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )			
	Mean Step Depth ( $d_{bkfs}$ )				ft Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )			
	Step Cross-Sectional Area ( $A_{bkfs}$ )				ft Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )			
	Maximum Step Depth ( $d_{maxs}$ )				ft Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
	Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )							

**Worksheet 5-4b. Morphological relations (modified from Rosgen, 2006/2009).**

Stream: <b>Trail Creek, C4 Fair Reach</b>		Location: <b>Pike National Forest, Colorado</b>										
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/25/2010</b>		Valley Type: <b>VIII</b>		Stream Type: <b>C4</b>						
<b>Hydraulics</b>	<b>River Reach Summary Data.....2</b>											
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )		<b>3.27</b> ft/sec		Estimation Method		<b>Limerinos</b>					
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )		<b>26.8</b> cfs		Drainage Area		<b>10.2</b> mi <sup>2</sup>					
<b>Channel Pattern</b>	<b>Geometry</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Dimensionless Geometry Ratios</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>		
	Linear Wavelength ( $\lambda$ )		<b>94.4</b>	<b>51.0</b>	<b>124.8</b> ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )		<b>7.48</b>	<b>4.04</b>	<b>9.89</b>		
	Stream Meander Length ( $L_m$ )		<b>101.3</b>	<b>72.5</b>	<b>125.5</b> ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )		<b>8.03</b>	<b>5.75</b>	<b>9.95</b>		
	Radius of Curvature ( $R_c$ )		<b>43.9</b>	<b>21.6</b>	<b>66.5</b> ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )		<b>3.48</b>	<b>1.71</b>	<b>5.27</b>		
	Belt Width ( $W_{bit}$ )		<b>18.3</b>	<b>17.2</b>	<b>19.8</b> ft	Meander Width Ratio ( $W_{bit} / W_{bkt}$ )		<b>1.45</b>	<b>1.37</b>	<b>1.57</b>		
	Arc Length ( $L_a$ )		<b>33.1</b>	<b>19.3</b>	<b>50.9</b> ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )		<b>2.62</b>	<b>1.53</b>	<b>4.03</b>		
	Riffle Length ( $L_r$ )		<b>31.4</b>	<b>22.9</b>	<b>38.2</b> ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )		<b>2.49</b>	<b>1.82</b>	<b>3.03</b>		
	Individual Pool Length ( $L_p$ )		<b>8.0</b>	<b>7.1</b>	<b>8.6</b> ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )		<b>0.64</b>	<b>0.57</b>	<b>0.68</b>		
Pool to Pool Spacing ( $P_s$ )		<b>41.6</b>	<b>26.0</b>	<b>53.6</b> ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )		<b>3.30</b>	<b>2.06</b>	<b>4.25</b>			
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )		<b>0.0189</b> ft/ft		Average Water Surface Slope (S)		<b>0.0180</b> ft/ft		Sinuosity ( $S_{val} / S$ )		<b>1.05</b>	
	Stream Length (SL)		<b>474.6</b> ft		Valley Length (VL)		<b>454.6</b> ft		Sinuosity (SL / VL)		<b>1.04</b>	
	Low Bank Height (LBH)		start	<b>1.40</b> ft	Max Bankfull Depth ( $d_{max}$ )		start	<b>1.40</b> ft	Bank-Height Ratio (BHR) (LBH / $d_{max}$ )		start	<b>1.0</b>
			end	<b>1.03</b> ft			end	<b>1.03</b> ft			end	<b>1.0</b>
	<b>Facet Slopes</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Dimensionless Facet Slope Ratios</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>		
	Riffle Slope ( $S_{rif}$ )		<b>0.0910</b>	<b>0.0140</b>	<b>0.0240</b> ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rif} / S$ )		<b>5.0556</b>	<b>0.7778</b>	<b>1.3333</b>		
	Run Slope ( $S_{run}$ )		<b>0.0600</b>	<b>0.0390</b>	<b>0.0770</b> ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )		<b>3.3333</b>	<b>2.1667</b>	<b>4.2778</b>		
	Pool Slope ( $S_p$ )		<b>0.0040</b>	<b>0.0001</b>	<b>0.0070</b> ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )		<b>0.2222</b>	<b>0.0056</b>	<b>0.3889</b>		
	Glide Slope ( $S_g$ )		<b>0.0100</b>	<b>0.0060</b>	<b>0.0140</b> ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )		<b>0.5556</b>	<b>0.3333</b>	<b>0.7778</b>		
	Step Slope ( $S_s$ )				ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )						
	<b>Max Depths<sup>a</sup></b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Dimensionless Depth Ratios</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>		
	Max Riffle Depth ( $d_{max}$ )		<b>1.42</b>	<b>1.24</b>	<b>1.49</b> ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )		<b>1.868</b>	<b>1.632</b>	<b>1.961</b>		
	Max Run Depth ( $d_{maxr}$ )		<b>1.22</b>	<b>1.18</b>	<b>1.26</b> ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )		<b>1.605</b>	<b>1.553</b>	<b>1.658</b>		
Max Pool Depth ( $d_{maxp}$ )		<b>1.79</b>	<b>1.69</b>	<b>1.89</b> ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )		<b>2.355</b>	<b>2.224</b>	<b>2.487</b>			
Max Glide Depth ( $d_{maxg}$ )		<b>1.38</b>	<b>1.35</b>	<b>1.43</b> ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )		<b>1.816</b>	<b>1.776</b>	<b>1.882</b>			
Max Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )							
<b>Channel Materials</b>			<b>Reach<sup>b</sup></b>	<b>Riffle<sup>c</sup></b>	<b>Bar</b>	<b>Reach<sup>b</sup></b>	<b>Riffle<sup>c</sup></b>	<b>Bar</b>	<b>Protrusion Height<sup>d</sup></b>			
	% Silt/Clay		<b>5</b>	<b>0</b>	<b>0</b>	$D_{16}$	<b>1.00</b>	<b>8.41</b>	<b>4.03</b>	mm		
	% Sand		<b>19</b>	<b>0</b>	<b>7</b>	$D_{35}$	<b>7.42</b>	<b>11.03</b>	<b>9.50</b>	mm		
	% Gravel		<b>68</b>	<b>90</b>	<b>57</b>	$D_{50}$	<b>10.04</b>	<b>16.00</b>	<b>33.25</b>	mm		
	% Cobble		<b>8</b>	<b>10</b>	<b>36</b>	$D_{84}$	<b>32.00</b>	<b>54.50</b>	<b>101.12</b>	mm		
	% Boulder					$D_{95}$	<b>90.00</b>	<b>82.57</b>	<b>120.98</b>	mm		
	% Bedrock					$D_{100}$	<b>179.99</b>	<b>179.99</b>	<b>130.00</b>	mm		

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

## Stability Indices

**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation					
Stream: <b>Trail Creek, C4 Fair Reach</b>			Location: <b>Pike National Forest, Colorado</b>		
Observers: <b>K. Wright &amp; B. Kasun</b>		Reference reach <input type="checkbox"/>	Disturbed (impacted reach) <input checked="" type="checkbox"/>	Date: <b>8/21/10</b>	
Existing species composition: <b>Willow, Pine, Spruce, Carex</b>			Potential species composition: <b>Same but without invasives</b>		
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition
<b>1. Overstory</b>	Canopy layer	5%	25%	<b>Willow</b>	90%
				<b>P. Pine</b>	5%
				<b>Spruce</b>	5%
					100%
<b>2. Understory</b>	Shrub layer	5%	40%	<b>Willow</b>	75%
				<b>Raspberry</b>	5%
				<b>Thistle</b>	5%
				<b>Mullen</b>	10%
				<b>Nettles</b>	5%
					100%
<b>3. Ground level</b>	Herbaceous	5%	31%	<b>Forbs</b>	13%
				<b>Annual Grasses</b>	50%
				<b>Thistle</b>	12%
				<b>Carex/Juncus</b>	25%
					100%
<b>3. Ground level</b>	Leaf or needle litter	5%	4%	<b>Remarks:</b> Condition, vigor and/or usage of existing reach: <b>Eradication of invasives</b>	
*Based on crown closure. **Based on basal area to surface area.			<b>Column total = 100%</b>		

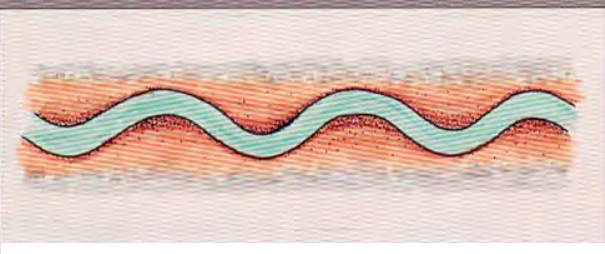





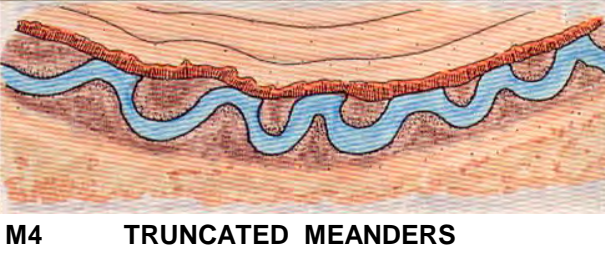
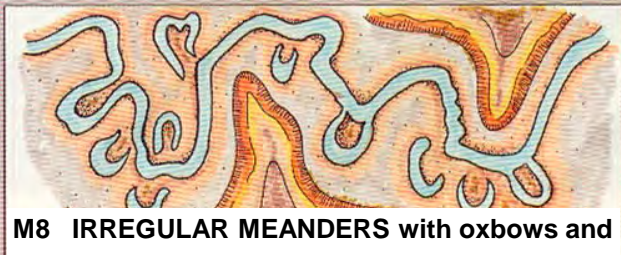
**Worksheet 5-7.** Flow regime.

<b>FLOW REGIME</b>								
Stream: <b>Trail Creek, C4 Fair Reach</b>			Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>K. Wright &amp; B. Kasun</b>						Date: <b>8/21/2010</b>		
<b>List ALL COMBINATIONS that APPLY.....</b>			<b>P1</b>	<b>P2</b>	<b>P8</b>			
<b>General Category</b>								
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation							
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
<b>P</b>	Perennial stream channels: Surface water persists yearlong.							
<b>Specific Category</b>								
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
<b>4</b>	Streamflow regulated by glacial melt.							
<b>5</b>	Ice flows/ice torrents from ice dam breaches.							
<b>6</b>	Alternating flow/backwater due to tidal influence.							
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.							
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
<b>9</b>	Rain-on-snow generated runoff.							

**Worksheet 5-8.** Stream order & stream size.

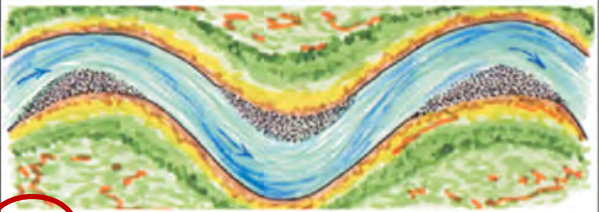


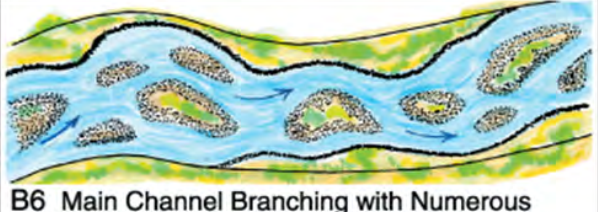
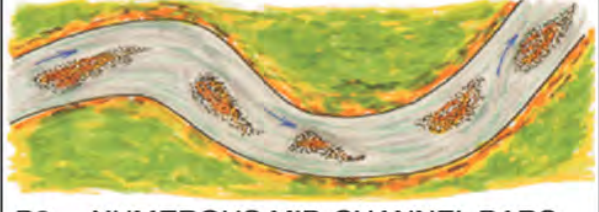
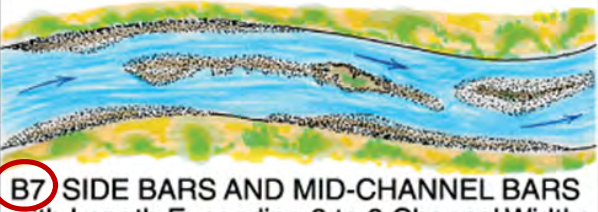


<b>Stream Size and Order</b>			
Stream:	<b>Trail Creek, C4 Fair Reach</b>		
Location:	<b>Pike National Forest, Colorado</b>		
Observers:	<b>K. Wright &amp; B. Kasun</b>		
Date:	<b>8/21/2010</b>		
<b>Stream Size Category and Order</b> ↗			<b>S-3(4)</b>
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0.305	<1	<input type="checkbox"/>
S-2	0.3 – 1.5	1 – 5	<input type="checkbox"/>
<b>S-3</b>	<b>1.5 – 4.6</b>	<b>5 – 15</b>	<input checked="" type="checkbox"/>
S-4	4.6 – 9	15 – 30	<input type="checkbox"/>
S-5	9 – 15	30 – 50	<input type="checkbox"/>
S-6	15 – 22.8	50 – 75	<input type="checkbox"/>
S-7	22.8 – 30.5	75 – 100	<input type="checkbox"/>
S-8	30.5 – 46	100 – 150	<input type="checkbox"/>
S-9	46 – 76	150 – 250	<input type="checkbox"/>
S-10	76 – 107	250 – 350	<input type="checkbox"/>
S-11	107 – 150	350 – 500	<input type="checkbox"/>
S-12	150 – 305	500 – 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
<b>Stream Order</b>			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			

Worksheet 5-9. Meander patterns.

<b>Meander Patterns</b>					
Stream: <b>Trail Creek, C4 Fair Reach</b>			Location: <b>Pike National Forest, CO</b>		
Observers: <b>K. Wright &amp; B. Kasun</b>			Date: <b>8/21/2010</b>		
List ALL CATEGORIES that APPLY	<b>M3</b>				
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>					
 <b>M1</b> <b>REGULAR MEANDERS</b>	 <b>M5</b> <b>UNCONFINED MEANDER SCROLLS</b>				
 <b>M2</b> <b>TORTUOUS MEANDERS</b>	 <b>M6</b> <b>CONFINED MEANDER SCROLLS</b>				
 <span style="border: 1px solid red; border-radius: 50%; padding: 2px;"><b>M3</b></span> <b>IRREGULAR MEANDERS</b>	 <b>M7</b> <b>DISTORTED MEANDER LOOPS</b>				
 <b>M4</b> <b>TRUNCATED MEANDERS</b>	 <b>M8</b> <b>IRREGULAR MEANDERS with oxbows and</b>				



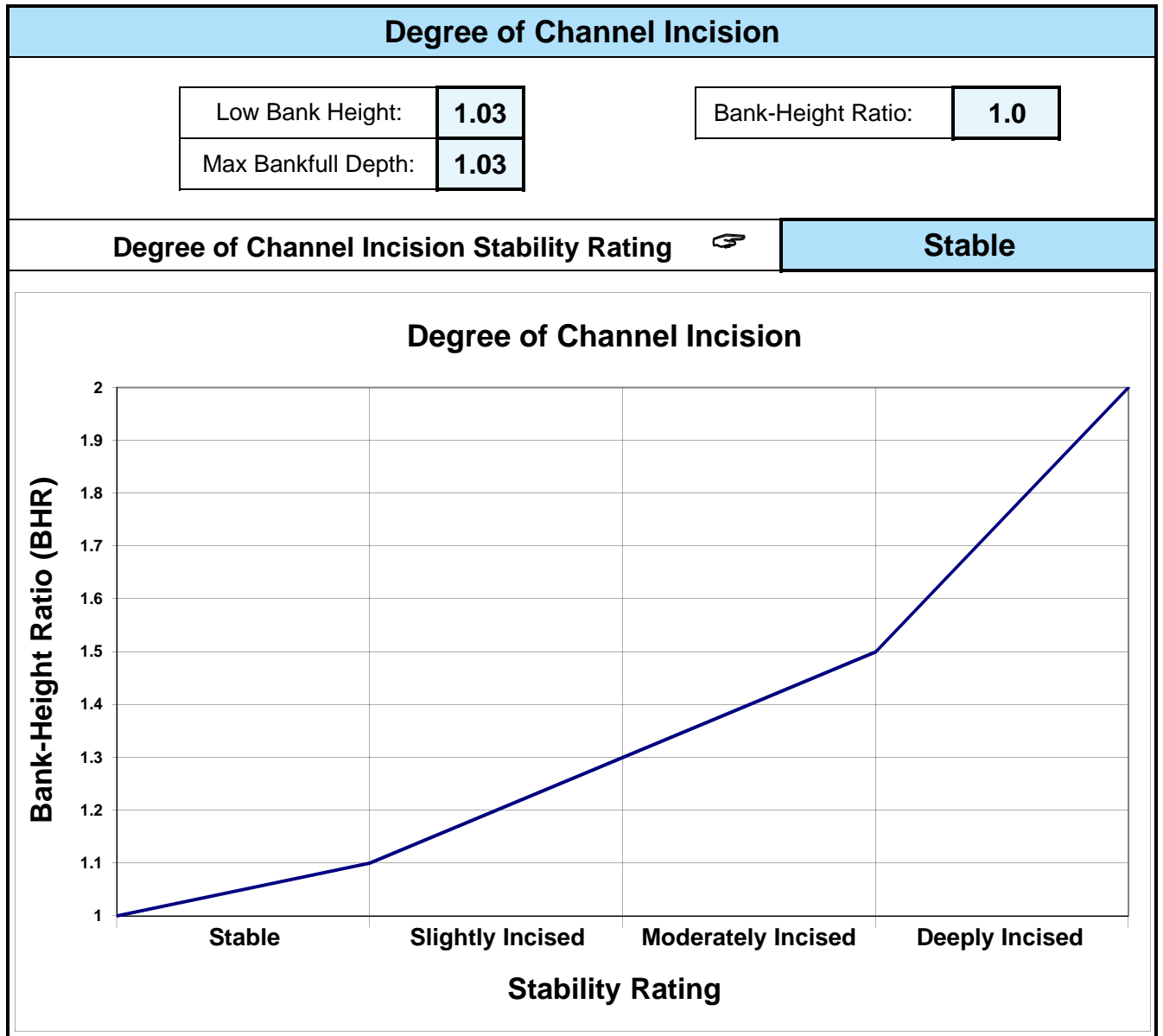
Worksheet 5-10. Depositional patterns.

<b>Depositional Patterns</b>				
Stream: <b>Trail Creek, C4 Fair Reach</b>	Location: <b>Pike National Forest, Colorado</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>	Date: <b>8/21/2010</b>			
List ALL CATEGORIES that APPLY	<b>B1</b>	<b>B4</b>	<b>B7</b>	
<i>Various Depositional Features modified from Galay et al. (1973)</i>				
 <b>B1</b> POINT BARS	 <b>B5</b> DIAGONAL BARS			
 <b>B2</b> POINT BARS with Few MID-CHANNEL BARS	 <b>B6</b> Main Channel Branching with Numerous MID-CHANNEL BARS and Islands			
 <b>B3</b> NUMEROUS MID-CHANNEL BARS	 <b>B7</b> SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths			
 <b>B4</b> SIDE BARS	 <b>B8</b> DELTA BARS			

**Worksheet 5-11.** Channel blockages.

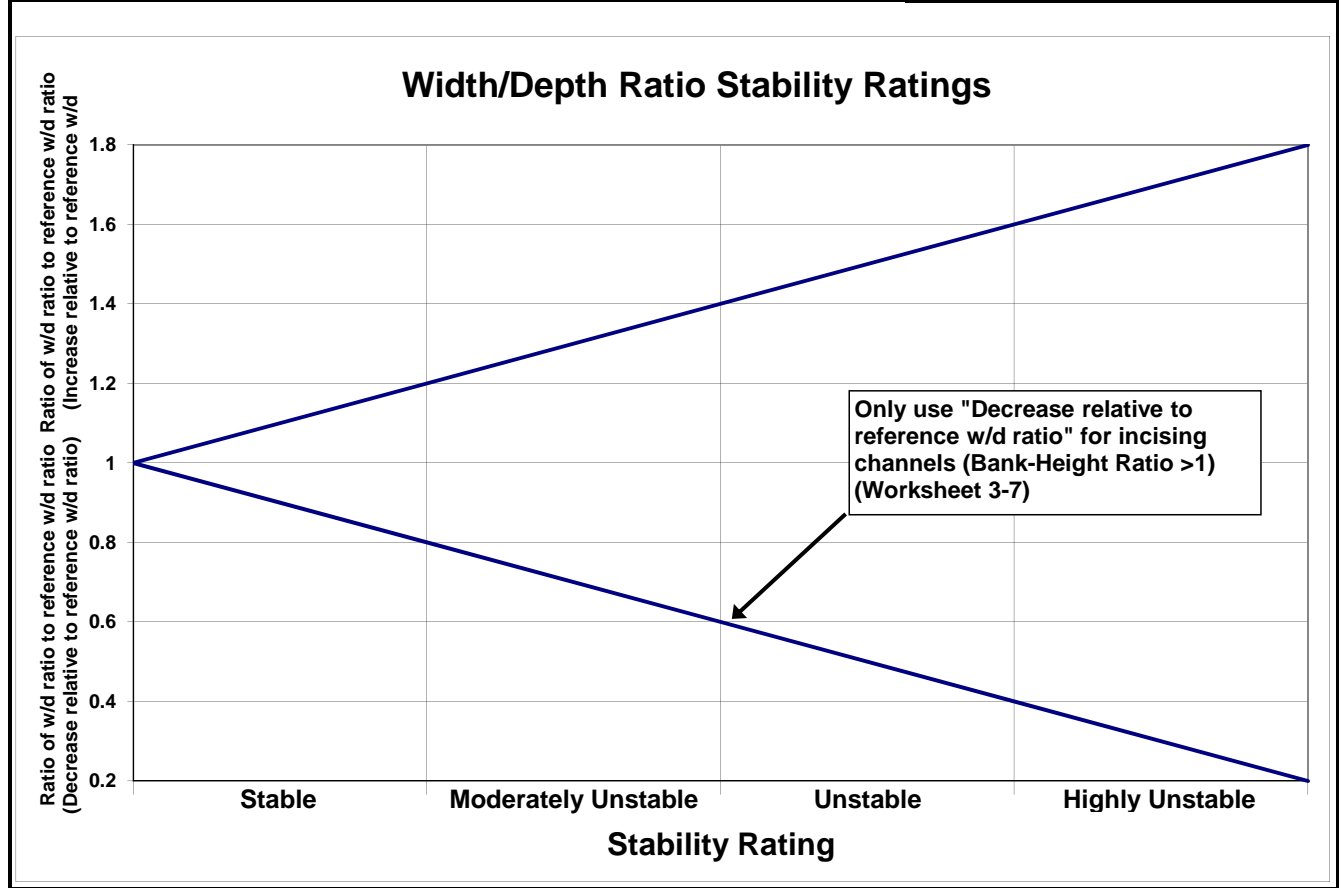
Channel Blockages		
Stream: <b>Trail Creek, C4 Fair Reach</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/21/2010</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input checked="" type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input type="checkbox"/>
<b>D4</b> Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

Worksheet 5-12. Degree of channel incision.

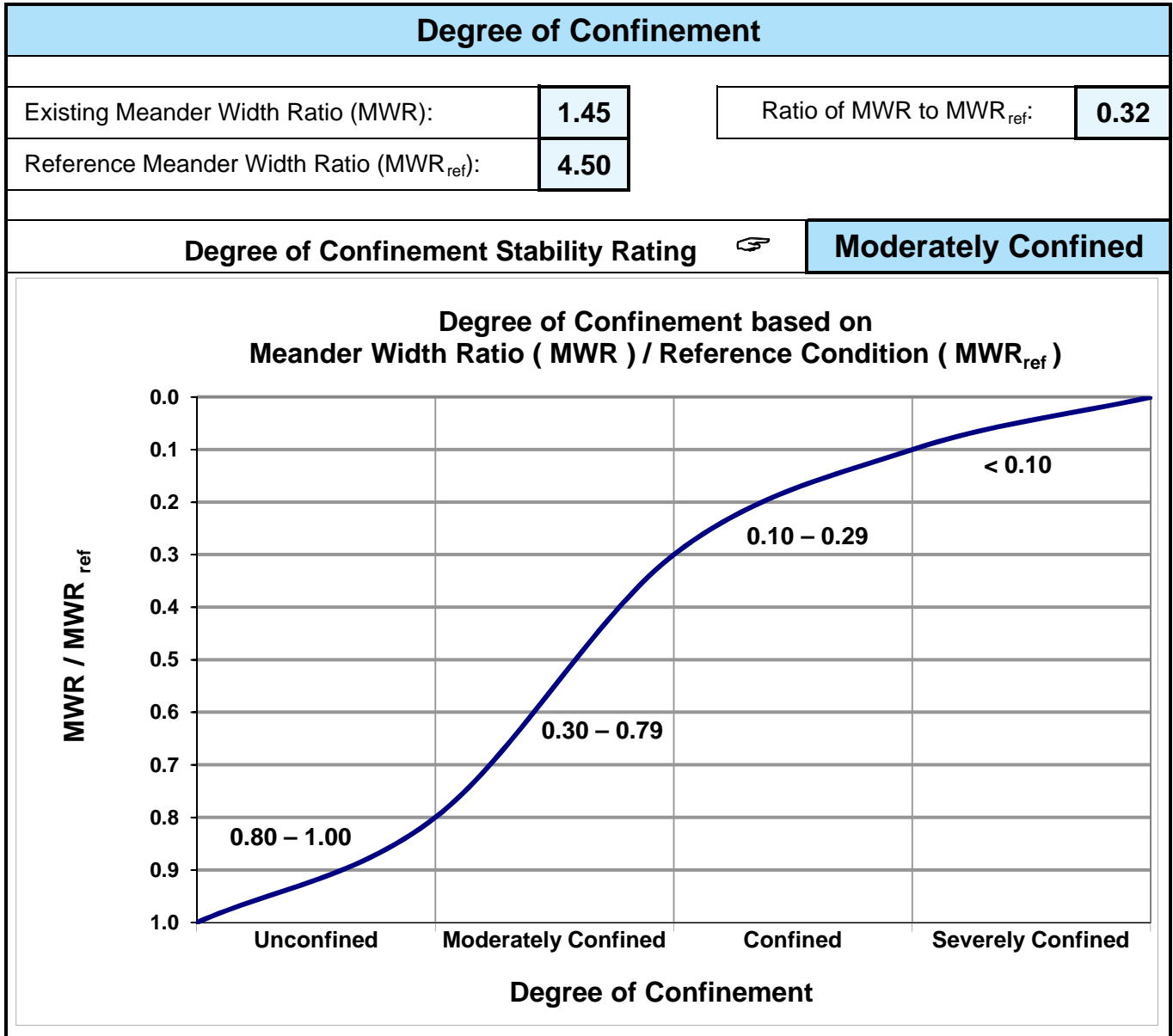


**Worksheet 5-13.** Width/depth ratio state.

Width/Depth Ratio State			
Existing Width/Depth Ratio:	<b>24.41</b>	Ratio of existing W/d to reference W/d:	<b>1.28</b>
Reference Width/Depth Ratio:	13.7-19		
<b>Width/Depth Ratio State Stability Rating</b>			<b>Moderately Unstable</b>



**Worksheet 5-14.** Degree of channel confinement (lateral containment).



Worksheet 5-15. Pfankuch channel stability rating.

Stream: Trail Creek, C4 Fair Reach		Location: Pike National Forest			Valley Type: VIII			Observers: K. Wright & B. Kasun			Date: 8/21/2010															
Loca- tion	Key Category	Excellent Description	Rating	Good Description	Rating	Fair Description	Rating	Poor Description	Rating																	
Upper banks	1	Landform slope	2	Bank slope gradient 30-40%.	5	Bank slope gradient 40-60%.	6	Bank slope gradient > 60%.	8																	
	2	Mass erosion	3	No evidence of past or future mass erosion.	6	Frequent or large, causing sediment nearly yearlong.	9	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.	12																	
	3	Debris jam potential	2	Essentially absent from immediate channel area.	4	Present, but mostly small twigs and limbs.	6	Moderate to heavy amounts, predominantly larger sizes.	8																	
	4	Vegetative bank protection	3	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	6	70-90% density. Fewer species or less vigor suggest less dense or deep root mass.	9	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.	12																	
Lower banks	5	Channel capacity	1	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0.	2	Bankfull stage is contained within banks. Width/depth ratio departure from reference width/depth ratio = 1.0-1.2. Bank-Height Ratio (BHR) = 1.0-1.3.	3	Bankfull stage is not contained; over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.	4																	
	6	Bank rock content	2	> 65% with large angular boulders. 12" + common.	4	40-65%. Mostly boulders and small cobbles 6-12".	7	20-40%. Most in the 3-6" diameter class.	8																	
	7	Obstructions to flow	2	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	4	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	6	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	8	Frequent obstructions and deflectors cause bank erosion yearlong. Sediment traps full, channel migration occurring.																
	8	Cutting	4	Little or none. Infrequent raw banks	7	Some, intermittently at outcurves and constrictions. Raw banks may be up to 12".	12	Significant. Cuts 12-24" high. Root mat overhangs and sloughing frequent.	16	Almost continuous cuts, some over 24" high. Failure of overhangs frequent.																
	9	Deposition	4	Little or no enlargement of channel or point bars.	8	Some new bar increase, mostly from coarse gravel.	12	Moderate deposition of new gravel and coarse sand on old and some new bars.	16	Extensive deposit of predominantly fine particles. Accelerated bar development.																
Bottom	10	Rock angularity	1	Sharp edges and corners. Plane surfaces rough.	2	Rounded corners and edges. Surfaces smooth and flat.	3	Corners and edges well rounded in 2 dimensions.	4	Well rounded in all dimensions, surfaces smooth.																
	11	Brightness	1	Surfaces dull, dark or stained. Generally not bright.	2	Mostly dull, but may have <35% bright surfaces.	3	Mixture dull and bright, i.e., 35-65% mixture range.	4	Predominantly bright, > 65%, exposed or scoured surfaces.																
	12	Consolidation of particles	2	Assigned sizes tightly packed or overlapping.	5	Moderately packed with some overlapping.	6	Mostly loose assortment with no apparent overlap.	8	No packing evident. Loose assortment, easily moved.																
	13	Bottom size distribution	4	No size change evident. Stable material 80-100%.	8	Distribution shift light. Stable material 50-80%.	12	Moderate change in sizes. Stable materials 20-50%.	16	Marked distribution change. Stable materials 0-20%.																
	14	Scouring and deposition	6	<5% of bottom affected by scour or deposition.	12	5-30% affected. Scour at constrictions and where grades steepen. Some deposition in pools.	18	30-50% affected. Deposits and scour at obstructions, constrictions and bends. Some filling of pools.	24	More than 50% of the bottom in a state of flux or change nearly yearlong.																
	15	Aquatic vegetation	1	Abundant growth moss-like, dark green perennial. In swift water too.	2	Common. Algae forms in low velocity and pool areas. Moss here too.	3	Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick.	4	Perennial types scarce or absent. Yellow-green, short-term bloom may be present.																
			Excellent total = 4	Good total = 39			Fair total = 31			Poor total = 20																
Stream type	A1	A2	A3	A4	A5	A6	B1	B2	B3	B4	B5	B6	C1	C2	C3	C4	C5	C6	D3	D4	D5	D6	Grand total = 94			
Good (Stable)	38-43	38-43	54-90	60-95	60-95	50-80	38-45	38-45	40-60	40-64	48-68	40-60	38-50	38-50	60-85	70-90	70-90	60-85	85-107	85-107	85-107	85-107	85-107	87-98	Existing stream type = C4	
Fair (Mod. unstable)	44-47	44-47	91-129	96-132	96-142	81-110	46-58	46-58	61-78	65-84	69-88	61-78	51-61	51-61	86-105	91-110	91-110	86-105	108-132	108-132	108-132	108-132	108-132	99-125	*Potential stream type = C4	
Poor (Unstable)	48+	48+	130+	133+	143+	111+	59+	59+	79+	85+	89+	79+	62+	62+	106+	111+	111+	106+	133+	133+	133+	133+	126+	Modified channel stability rating = Fair		
Stream type	DA3	DA4	DA5	DA6	E3	E4	E5	E6	F1	F2	F3	F4	F5	F6	G1	G2	G3	G4	G5	G6						
Good (Stable)	40-63	40-63	40-63	40-63	40-63	50-75	50-75	40-63	60-85	85-110	85-110	90-115	80-95	80-95	40-60	40-60	85-107	85-107	90-112	90-112	85-107	85-107	85-107			
Fair (Mod. unstable)	64-86	64-86	64-86	64-86	64-86	76-96	76-96	64-86	86-105	86-105	111-125	111-125	116-130	96-110	61-78	61-78	108-120	108-120	113-125	113-125	108-120	108-120	108-120			
Poor (Unstable)	87+	87+	87+	87+	87+	97+	97+	87+	106+	106+	126+	126+	131+	111+	79+	79+	121+	121+	126+	126+	121+	121+	121+			

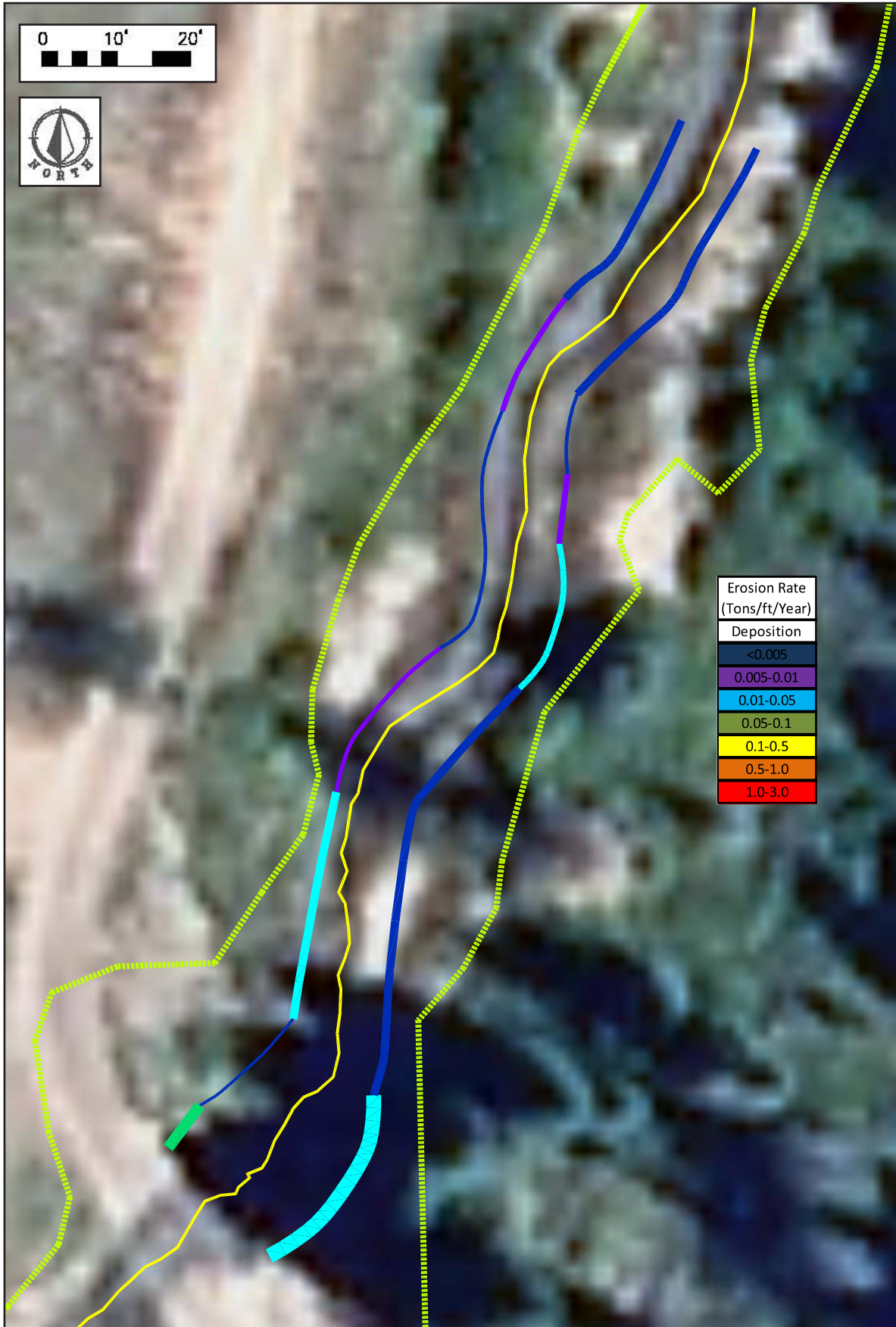
\*Rating is adjusted to potential stream type, not existing.

## BANCS Model – Streambank Erosion

**Worksheet 5-18.** Annual streambank erosion estimates.

Stream: <b>Trail Creek, C4 Fair Reach</b>		Location: <b>Pike National Forest, Colorado</b>					
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>215</b>				Date: <b>8/21/2010</b>	
Observers: <b>K. Wright &amp; B. Kasun</b>		Valley Type: <b>VIII</b>			Stream Type: <b>C4</b>		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 5-16) (adjective)	NBS rating (Worksheet 5-17) (adjective)	Bank erosion rate (Figure 5-34 or 5-35) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [(4)×(5)×(6)] (ft <sup>3</sup> /yr)	Erosion Rate (tons/yr/ft) {[ (7)/27 ] × 1.3 / (5)}
1. BR 0+00 to 0+20 Right	Very High	Moderate	0.37957	20.0	2.5	18.98	0.04569
2. BR 0+00 to 0+07 Left	High	High	0.57533	7.0	1.9	7.65	0.05263
3. BR 0+07 to 0+45 Left	Very Low	Low	0.00386	38.0	0.5	0.07	0.00009
4. BR 0+20 to 0+86 Right	Low	High	0.15505	66.0	1.4	14.33	0.01045
5. BR 0+45 to 0+65 Left	Moderate	High	0.42031	20.0	1.4	11.77	0.02833
6. BR 0+65 to 1+11 Left	Low	High	0.15505	46.0	0.7	4.99	0.00523
7. BR 0+86 to 1+00 Right	Moderate	High	0.42031	14.0	1.0	5.88	0.02024
8. BR 1+00 to 1+16 Right	Low	High	0.15505	16.0	1.0	2.48	0.00747
9. BR 1+16 to 1+39 Right	Low	Low	0.03566	23.0	0.6	0.49	0.00103
10. BR 1+39 to 2+15 Right	Moderate	Moderate	0.25348	76.0	1.1	21.19	0.01343
11. BR 1+11 to 1+39 Left	Low	Low	0.03566	28.0	0.7	0.65	0.00112
12. BR 1+39 to 1+66 Left	Low	High	0.15505	27.0	0.9	3.77	0.00672
13. BR 1+66 to 2+15 Left	Low	Moderate	0.07435	49.0	1.3	4.74	0.00465
14							
15							
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					Total Erosion (ft <sup>3</sup> /yr)	<b>96.99</b>	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					Total Erosion (yds <sup>3</sup> /yr)	<b>3.59</b>	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					Total Erosion (tons/yr)	<b>4.67</b>	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					Total Erosion (tons/yr/ft)	<b>0.0217</b>	

### Streambank Erosion Map





## FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Equation Type		Equation Source			Equation		Bankfull Discharge (cfs)		Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)			
1. Bedload Sediment		"Good/Fair" Pagosa			$y = -0.0113x + 1.0139x^{2.1929}$		26.8		0.0160		21.55			
2. Suspended Sediment		"Good/Fair" Pagosa			$y = 0.0636 + 0.9326x^{2.4085}$									
From Dimensional Flow-Duration Curve														
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	Calculate			
Percentage of Time	Daily Mean Discharge	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Suspended Sediment Discharge	Suspended Sediment Discharge	Dimensionless Bedload Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow [(5)×(9)]	Bedload Sediment [(5)×(11)]	Suspended + Bedload Sediment [(13)+(14)]	
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>50</sub> )	(S/S <sub>50</sub> )	(tons/day)	(b <sub>d</sub> /b <sub>50d</sub> )	(tons/day)	(cfs)	(tons)	(tons)	
0%	68.2													
0.10%	58.5	0.05%	0.09%	0.34	63.3	2.363	7.461	27.50	6.670	10.18	21.7	9.43	12.93	
0.25%	50.6	0.08%	0.15%	0.55	54.6	2.036	5.232	16.61	4.809	7.34	29.9	9.10	13.11	
0.50%	43.7	0.13%	0.25%	0.91	47.2	1.761	3.706	10.18	3.494	5.33	43.1	9.29	14.15	
0.75%	37.4	0.13%	0.25%	0.91	40.5	1.513	2.592	6.12	2.502	3.82	37.0	5.58	9.06	
1%	32.3	0.13%	0.25%	0.91	34.8	1.300	1.817	3.68	1.790	2.73	31.8	3.36	5.85	
1.5%	27.7	0.25%	0.50%	1.83	30.0	1.120	1.289	2.25	1.289	1.97	54.8	4.11	7.70	
2%	23.1	0.25%	0.50%	1.83	25.4	0.949	0.886	1.31	0.893	1.36	46.4	2.39	4.88	
3%	19.5	0.50%	1.00%	3.65	21.3	0.795	0.600	0.74	0.602	0.92	77.8	2.72	6.07	
4%	16.6	0.50%	1.00%	3.65	18.1	0.674	0.424	0.45	0.415	0.63	65.9	1.63	3.94	
5%	14.8	0.50%	1.00%	3.65	15.7	0.587	0.322	0.29	0.304	0.46	57.4	1.08	2.77	
10%	9.3	2.50%	5.00%	18.25	12.1	0.450	0.200	0.14	0.165	0.25	220.2	2.56	7.15	
20%	5.1	5.00%	10.00%	36.50	7.2	0.269	0.103	0.04	0.045	0.07	262.7	1.57	4.10	
30%	3.4	5.00%	10.00%	36.50	4.2	0.158	0.075	0.02	0.006	0.01	154.5	0.67	1.03	
40%	2.4	5.00%	10.00%	36.50	2.9	0.108	0.068	0.01	0.000	0.00	105.6	0.42	0.42	
50%	1.8	5.00%	10.00%	36.50	2.1	0.079	0.066	0.01	0.000	0.00	77.3	0.30	0.30	
60%	1.4	5.00%	10.00%	36.50	1.6	0.061	0.065	0.01	0.000	0.00	59.2	0.22	0.22	
70%	1.1	5.00%	10.00%	36.50	1.3	0.047	0.064	0.00	0.000	0.00	46.4	0.17	0.17	
80%	1.0	5.00%	10.00%	36.50	1.1	0.039	0.064	0.00	0.000	0.00	38.6	0.14	0.14	
90%	0.7	5.00%	10.00%	36.50	0.8	0.032	0.064	0.00	0.000	0.00	30.9	0.11	0.11	
100%	0.1	5.00%	10.00%	36.50	0.4	0.016	0.064	0.00	0.000	0.00	15.5	0.06	0.06	
<b>Annual Totals:</b>											<b>1,476.5</b> (cfs)		<b>94.2</b> (tons/yr)	
											<b>2,928.6</b> (acre-ft)		<b>39.3</b> (tons/yr)	

**Worksheet 19b.** Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Equation Type		Equation Source			Equation		Bankfull Discharge (cfs)			Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)		
1. Bedload Sediment		"Good/Fair" Pagosa			$y = -0.0113x + 1.0139x^{2.1929}$		26.8			0.0290		38.00		
2. Suspended Sediment		"Good/Fair" Pagosa			$y = 0.0636 + 0.9326x^{2.4085}$									
From Dimensional Flow-Duration Curve														
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	Calculate		(15)	
Percentage of Time	Daily Mean Discharge	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Suspended Sediment Discharge	Suspended Sediment Discharge	Dimensionless Bedload Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow	Suspended Sediment	Bedload Sediment	Suspended + Bedload Sediment
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>med</sub> )	(S/S <sub>med</sub> )	(tons/day)	(b <sub>d</sub> /b <sub>bed</sub> )	(tons/day)	[(5)×(6)]	(tons)	[(5)×(11)]	[(13)+(14)]
0%	89.6													
0.10%	79.9	0.05%	0.09%	0.34	84.8	3.163	15.000	130.47	12.657	34.97	29.1	44.76	12.00	56.76
0.25%	72.1	0.08%	0.15%	0.55	76.0	2.836	11.549	90.07	9.962	27.52	41.6	49.31	15.07	64.38
0.50%	65.2	0.13%	0.25%	0.91	68.6	2.561	9.046	63.70	7.962	22.00	62.6	58.13	20.07	78.20
0.75%	58.8	0.13%	0.25%	0.91	62.0	2.313	7.094	45.12	6.368	17.59	56.6	41.18	16.05	57.23
1%	53.8	0.13%	0.25%	0.91	56.3	2.100	5.633	32.53	5.149	14.22	51.4	29.68	12.98	42.66
1.5%	48.9	0.25%	0.50%	1.83	51.3	1.915	4.523	23.81	4.203	11.61	93.7	43.46	21.19	64.65
2%	44.0	0.25%	0.50%	1.83	46.4	1.732	3.567	16.99	3.372	9.32	84.7	31.01	17.00	48.02
3%	40.3	0.50%	1.00%	3.65	42.2	1.573	2.839	12.28	2.726	7.53	153.9	44.82	27.49	72.31
4%	35.8	0.50%	1.00%	3.65	38.1	1.420	2.234	8.72	2.176	6.01	138.9	31.84	21.95	53.79
5%	31.7	0.50%	1.00%	3.65	33.7	1.259	1.686	5.84	1.668	4.61	123.1	21.30	16.82	38.12
10%	19.7	2.50%	5.00%	18.25	25.7	0.959	0.907	2.39	0.913	2.52	469.0	43.62	46.06	89.68
20%	6.9	5.00%	10.00%	36.50	13.3	0.497	0.237	0.32	0.207	0.57	486.0	11.80	20.92	32.72
30%	3.5	5.00%	10.00%	36.50	5.2	0.194	0.082	0.04	0.017	0.05	189.9	1.59	1.67	3.26
40%	2.4	5.00%	10.00%	36.50	3.0	0.110	0.068	0.02	0.000	0.00	107.8	0.75	0.00	0.75
50%	1.8	5.00%	10.00%	36.50	2.1	0.079	0.066	0.01	0.000	0.00	77.3	0.52	0.00	0.52
60%	1.4	5.00%	10.00%	36.50	1.6	0.061	0.065	0.01	0.000	0.00	59.2	0.39	0.00	0.39
70%	1.1	5.00%	10.00%	36.50	1.3	0.047	0.064	0.01	0.000	0.00	46.4	0.31	0.00	0.31
80%	1.0	5.00%	10.00%	36.50	1.1	0.039	0.064	0.01	0.000	0.00	38.6	0.25	0.00	0.25
90%	0.7	5.00%	10.00%	36.50	0.8	0.032	0.064	0.01	0.000	0.00	30.9	0.20	0.00	0.20
100%	0.1	5.00%	10.00%	36.50	0.4	0.016	0.064	0.00	0.000	0.00	15.5	0.10	0.00	0.10
<b>Annual Totals:</b>											2,356.1 (cfs)	455.0 (tons/yr)	249.3 (tons/yr)	704.3 (tons/yr)
											4,673.3 (acre-ft)			

# POWERSED Model – Sediment Transport Capacity

**Worksheet 20a.** Sediment transport prediction representing the upstream supply up to bankfull for bedload and suspended sand sediment.

Stream: Trail Creek, Upstream Existing Sediment Supply		Location: Pike National Forest, Colorado (Used "GOOD-FAIR" Curves)		Date: 08/27/10														
Observers: S=0.189, Q=27, 21.3, Bed.=0638, S.Sand=19		Stream Type: C4	Valley Type: VIII	Gage Station #: Used Post-Fire Dimensionless F-D C.														
Flow-duration curve		Calculate																
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	
Percentage of time	Daily mean discharge	Mid-ordinate stream-flow	Area	Width	Depth	Velocity	Slope	Shear stress	Stream power	Unit power	Time increment	Time increment	Daily mean bedload transport	Daily mean bedload transport	Time adjusted bedload transport	Time adjusted suspended sand transport	Time adjusted total transport	
(%)	(cfs)	(cfs)	(ft <sup>2</sup> )	(ft)	(ft)	(ft/s)	(ft/ft)	(lb/ft <sup>2</sup> )	(lb/s)	(lb/ft/s)	(%)	(days)	(tons/day)	(tons/day)	(tons)	(tons)	(tons)	
100.00%	0.14										0%				0.00	0.00	0.00	
90.00%	0.71	0.43	0.44	3.86	0.11	0.93	0.0189	0.13	0.51	0.13	10%	36.50	0.00	0.00	0.00	0.00	0.00	
80.00%	0.99	0.85	0.73	4.75	0.15	1.16	0.0189	0.18	1.00	0.21	10%	36.50	0.00	0.00	0.00	0.00	0.00	
70.00%	1.13	1.06	0.85	5.02	0.17	1.23	0.0189	0.20	1.25	0.25	10%	36.50	0.00	0.00	0.00	0.00	0.00	
60.00%	1.41	1.27	0.96	5.25	0.18	1.29	0.0189	0.21	1.50	0.29	10%	36.50	0.00	0.00	0.00	0.00	0.00	
50.00%	1.83	1.62	1.14	5.63	0.20	1.39	0.0189	0.24	1.91	0.34	10%	36.50	0.00	0.01	0.00	0.36	0.36	
40.00%	2.40	2.12	1.39	6.09	0.23	1.51	0.0189	0.27	2.50	0.41	10%	36.50	0.00	0.01	0.00	0.36	0.36	
30.00%	3.51	2.96	1.76	6.67	0.26	1.66	0.0189	0.31	3.49	0.52	10%	36.50	0.00	0.01	0.00	0.36	0.36	
20.00%	6.90	5.21	2.67	7.99	0.33	1.95	0.0189	0.39	6.14	0.77	10%	36.50	0.04	0.02	1.46	0.73	2.19	
10.00%	19.73	13.32	4.98	9.19	0.54	2.66	0.0189	0.62	15.71	1.71	10%	36.50	0.56	0.16	20.44	5.84	26.28	
5.00%	31.65	25.69	8.17	11.63	0.70	3.15	0.0189	0.80	30.30	2.61	5%	18.25	2.46	1.17	44.89	21.35	66.24	
4.00%	35.79	33.72																
3.00%	40.31	38.05																
2.00%	43.97	42.14																
1.50%	48.86	46.42																
1.00%	53.75	51.31																
0.75%	58.79	56.27																
0.50%	65.17	61.98																
0.25%	72.06	68.62																
0.10%	79.92	75.99																
0.0060%	89.58	84.75																
														Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr):		66.8	29.0	95.8

**Worksheet 20b.** Sediment transport prediction for the existing condition reach compared to the upstream sediment supply to assess bed stability.

Stream: Trail Creek, C4 Fair Riffle XS 3+76															Location: Pike National Forest, Colorado (Used "GOOD-FAIR" Curves)			Date: 08/27/10	
Observers: S=0.189, Q=27, 21.3, Bed.=.0638, S.Sand=19															Gage Station #: Used Post-Fire Dimensionless F-D C.				
Stream Type: C4															Valley Type: VIII				
Flow-duration curve					Hydraulic geometry					Measure					Calculate				
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)		
Percentage of time	Daily mean discharge	Mid-ordinate stream-flow	Area	Width	Depth	Velocity	Slope	Shear stress	Stream power	Unit power	Time increment	Time increment	Daily mean bedload transport	Daily mean suspended sand transport	Time adjusted bedload transport	Time adjusted suspended sand transport	Time adjusted total transport		
(%)	(cfs)	(cfs)	(ft <sup>2</sup> )	(ft)	(ft)	(ft/s)	(ft/ft)	(lb/ft <sup>2</sup> )	(lb/s)	(lb/ft/s)	(%)	(days)	(tons/day)	(tons/day)	(tons)	(tons)	(tons)		
100.00%	0.14										0%				0.00	0.00	0.00		
90.00%	0.71	0.43	0.47	4.50	0.10	0.81	0.0189	0.12	0.51	0.11	10%	36.50	0.00	0.00	0.00	0.00	0.00		
80.00%	0.99	0.85	0.77	5.27	0.15	1.06	0.0189	0.17	1.00	0.19	10%	36.50	0.00	0.00	0.00	0.00	0.00		
70.00%	1.13	1.06	0.89	5.35	0.17	1.14	0.0189	0.19	1.25	0.23	10%	36.50	0.00	0.00	0.00	0.00	0.00		
60.00%	1.41	1.27	1.00	5.44	0.18	1.22	0.0189	0.21	1.50	0.28	10%	36.50	0.00	0.00	0.00	0.00	0.00		
50.00%	1.83	1.62	1.19	5.59	0.21	1.36	0.0189	0.25	1.91	0.34	10%	36.50	0.00	0.01	0.00	0.36	0.36		
40.00%	2.40	2.12	1.42	5.92	0.24	1.46	0.0189	0.28	2.50	0.42	10%	36.50	0.00	0.01	0.00	0.36	0.36		
30.00%	3.51	2.96	1.82	6.49	0.28	1.63	0.0189	0.32	3.49	0.54	10%	36.50	0.00	0.01	0.00	0.36	0.36		
20.00%	6.90	5.21	2.97	9.49	0.31	1.76	0.0189	0.36	6.14	0.65	10%	36.50	0.04	0.02	1.46	0.73	2.19		
10.00%	19.73	13.32	7.23	21.73	0.33	1.83	0.0189	0.39	15.71	0.72	10%	36.50	0.04	0.05	1.46	1.83	3.29		
5.00%	31.65	25.69	11.40	25.15	0.45	2.25	0.0189	0.53	30.30	1.20	5%	18.25	0.26	0.20	4.75	3.65	8.40		
4.00%	35.79	33.72																	
3.00%	40.31	38.05																	
2.00%	43.97	42.14																	
1.50%	48.86	46.42																	
1.00%	53.75	51.31																	
0.75%	58.79	56.27																	
0.50%	65.17	61.98																	
0.25%	72.06	68.62																	
0.10%	79.92	75.99																	
0.0060%	89.58	84.75																	
Notes:															Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr):			7.7	
															Upstream total annual sediment supply (tons/yr) (Worksheet 5-20a):			66.8	
															Difference in sediment transport capacity (tons/yr) (+ or -):			-59.1	
Stability evaluation: Aggradation, Degradation or Stable:															Aggradation, = 84%			Reduction in Transport	

## Sediment Competence/Entrainment

Worksheet 5-22. Sediment competence calculations.

Stream: <b>Trail Creek, C4 Fair Reach</b>		Stream Type: <b>C4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/21/10</b>			
<b>Enter Required Information for Existing Condition</b>					
16.0	$D_{50}$	Riffle bed material $D_{50}$ (mm)			
33.3	$\hat{D}_{50}$	Bar sample $D_{50}$ (mm)			
0.43	$D_{max}$	Largest particle from bar sample (ft)	130	(mm)	304.8 mm/ft
0.018	S	Existing bankfull water surface slope (ft/ft)			
0.58	d	Existing bankfull mean depth (ft)			
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment			
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>					
0.48	$D_{50}/\hat{D}_{50}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 ( D_{50}/\hat{D}_{50} )^{-0.872}$		
8.13	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 ( D_{max}/D_{50} )^{-0.887}$		
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED:		
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	d	Required bankfull mean depth (ft)	$d = \frac{\tau^*(\gamma_s - 1)D_{max}}{S}$ (use $D_{max}$ in ft)		
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	S	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^*(\gamma_s - 1)D_{max}}{d}$ (use $D_{max}$ in ft)		
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					
<b>Sediment Competence Using Dimensional Shear Stress</b>					
0.651	Bankfull shear stress $\tau = \gamma ds$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d) $\gamma = 62.4$ , d = existing depth, S = existing slope				
Shields	CO	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ (Figure 5-49)			
46	120				
Shields	CO	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) (Figure 5-49)			
1.7	0.7				
Shields	CO	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm)			
1.51	0.62	$d = \frac{\tau}{\gamma S}$ $\tau$ = predicted shear stress, $\gamma = 62.4$ , S = existing slope			
Shields	CO	Predicted slope required to initiate movement of measured $D_{max}$ (mm)			
0.0470	0.0193	$S = \frac{\tau}{\gamma d}$ $\tau$ = predicted shear stress, $\gamma = 62.4$ , d = existing depth			
Check: <input checked="" type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					

## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>Trail Creek, C4 Fair Reach</b>	Stream Type: <b>C4</b>
Location: <b>Pike National Forest, CO</b>	Valley Type: <b>VIII</b>
Observers: <b>K. Wright &amp; B. Kasun</b>	Date: <b>8/21/10</b>
<b>Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)</b>	<b>Stability Rating (Check Appropriate Rating)</b>
Stream Type at potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	<input type="checkbox"/> Stable
(E→C), ( <b>C→High W/d C</b> )	<input checked="" type="checkbox"/> Moderately Unstable
(G→F), (F→D), (C→F)	<input type="checkbox"/> Unstable
(C→D), (B→G), (D→G), (C→G), (E→G)	<input type="checkbox"/> Highly Unstable

Worksheet 5-25. Lateral stability.

Stream: <b>Trail Creek, C4 Fair Reach</b>		Stream Type: <b>C4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/21/10</b>			
Lateral stability criteria (choose one stability category for each criterion 1–5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	4
	(2)	1.3 (4)	(6)	(8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	3
	B1 (1)	B4 (2)	(3)	B7 (4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		1
	M3 (1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	2
	(2)	(4)	(5)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	2
	(1)	0.32 (2)	(3)	(4)	
<b>Total Points</b>					<b>12</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input checked="" type="checkbox"/>	<i>Unstable</i> 13 – 21 <input type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	

**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>Trail Creek, C4 Fair Reach</b>		Stream Type: <b>C4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/21/10</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
1 <b>Sediment competence</b> (Worksheet 5-22)	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope—slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	4
	(2)	(4)	(6)	(8)	
2 <b>Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	8
	(2)	(4)	(6)	(8)	
3 <b>W/d Ratio State</b> (Worksheet 5-13)	1.0 – 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	4
	(2)	1.3 (4)	(6)	(8)	
4 <b>Stream Succession States</b> (Worksheet 5-24)	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	6
	(2)	(4)	(6)	(8)	
5 <b>Depositional Patterns</b> (Worksheet 5-10)	B1	B2, B4	B3, B5	B6, B7, B8	3
	B1 (1)	B4 (2)	(3)	B7 (4)	
6 <b>Debris / Blockages</b> (Worksheet 5-11)	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	1
	D1 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>26</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
Vertical Stability for Excess Deposition / Aggradation (use total points and check stability rating)	<i>No Deposition</i> 10 – 14 <input type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input checked="" type="checkbox"/>	<i>Aggradation</i> > 30 <input type="checkbox"/>	



Worksheet 5-27. Vertical stability – degradation.

Stream: <b>Trail Creek, C4 Fair Reach</b>		Stream Type: <b>C4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/21/10</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>Sediment Competence</b> (Worksheet 5-22)	Does not indicate excess competence	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed	$D_{100}$ of bed moved	Particles much larger than $D_{100}$ of bed moved	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>Sediment Capacity</b> (POWERSED) (Worksheet 5-20)	Does not indicate excess capacity	Slight excess energy: up to 10% increase above reference	Excess energy sufficient to increase load up to 50% of annual load	Excess energy transporting more than 50% of annual load	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>Degree of Channel Incision (BHR)</b> (Worksheet 5-12)	1.00 – 1.10	1.11 – 1.30	1.31 – 1.50	> 1.50	<b>2</b>
	1.00 (2)	(4)	(6)	(8)	
<b>Stream Succession States</b> (Worksheets 5-12 and 5-24)	Does not indicate incision or degradation	If BHR > 1.1 and stream type has W/d between 5–10	If BHR > 1.1 and stream type has W/d less than 5	(B→G), (C→G), (E→G), (D→G)	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.80 – 1.00	0.30 – 0.79	0.10 – 0.29	< 0.10	<b>2</b>
	(1)	0.32 (2)	(3)	(4)	
<b>Total Points</b>					<b>10</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation</b> (use total points and check stability rating)	<i>Not Incised</i> 9 – 11 <input checked="" type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input type="checkbox"/>	<i>Degradation</i> > 27 <input type="checkbox"/>	

**Worksheet 5-28.** Channel enlargement.

Stream: <b>Trail Creek, C4 Fair Reach</b>		Stream Type: <b>C4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/21/10</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1-4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	4
	(2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	4
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	6
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	2
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>16</b>
<b>Category Point Range</b>					
<b>Channel Enlargement Prediction (use total points and check stability rating)</b>	<i>No Increase</i> 8 – 10 <input type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input checked="" type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input type="checkbox"/>	<i>Extensive</i> > 24 <input type="checkbox"/>	

Worksheet 5-29. Overall sediment supply.

Stream: <b>Trail Creek, C4 Fair Reach</b>		Stream Type: <b>C4</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>		
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/21/10</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1-5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	2	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	3	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	1	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	2	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	2	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>10</b>	
<b>Category Point Range</b>				
Overall Sediment Supply Rating (use total points and check stability rating)	<i>Low</i> 5 <input type="checkbox"/>	<i>Moderate</i> 6 – 10 <input checked="" type="checkbox"/>	<i>High</i> 11 – 15 <input type="checkbox"/>	<i>Very High</i> 16 – 20 <input type="checkbox"/>

Worksheet 5-32. Summary of stability condition categories.

Stream: <b>Trail Creek, C4 Fair Reach</b>		Location: <b>Pike National Forest, Colorado</b>	
Observers: <b>K. Wright &amp; B. Kasun</b>		Stream Type: <b>C4</b> Valley Type: <b>VIII</b>	
Channel Dimension (Rifle XS 3+76)	Mean Bankfull Depth (ft): <b>0.58</b>	Bankfull Width (ft): <b>14.2</b>	Cross-Sectional Area (ft <sup>2</sup> ): <b>8.15</b>
	Width of Flood-Prone Area (ft): <b>35.67</b>	Entrenchment Ratio: <b>2.52</b>	
Channel Pattern	Mean: $\lambda/W_{b,skf}$ : <b>7.48</b>	$R_c/W_{b,skf}$ : <b>8.03</b>	$MWR$ : <b>1.45</b>
	Range: $L_m/W_{b,skf}$ : <b>4.04-9.89</b>	$R_c/W_{b,skf}$ : <b>5.75-9.95</b>	$MWR$ : <b>1.37-1.57</b>
River Profile & Bed Features	Check: <input checked="" type="checkbox"/> Riffle/Pool <input type="checkbox"/> Step/Pool <input type="checkbox"/> Plane Bed <input type="checkbox"/> Convergence/Divergence <input type="checkbox"/> Dunes/Antidunes/Smooth Bed		Slope
	Max Bankfull Depth (ft): <b>1.42</b>	Riffle	Ratio
Level III Stream Stability Indices	Depth Ratio (max to mean): <b>1.79</b>	Pool	Pool-to-Pool Spacing: <b>3.3</b>
	Reference W/d Ratio (W/d <sub>ref</sub> ): <b>24.4</b>	Riffle	Valley: <b>0.0189</b>
Bank Erosion Summary	Meaner Width Ratio (MWR): <b>1.45</b>	Reference MWR <sub>ref</sub> : <b>4.5</b>	Water Surface: <b>0.018</b>
	Length of Reach Studied (ft): <b>215</b>	Annual Streambank Erosion Rate: (tons/yr) <b>4.67</b>	Remarks: <b>0.0217</b>
Sediment Capacity (POWERSED)	<input type="checkbox"/> Sufficient Capacity <input checked="" type="checkbox"/> Insufficient Capacity <input type="checkbox"/> Excess Capacity	Remarks: <b>≈ 84% Reduction in Transport Capacity</b>	
	Curve Used: <b>Colorado</b>		
Entrainment/Competence	Annual Streambank Erosion Rate: (tons/yr/ft) <b>0.0217</b>		
	Curve Used: <b>Colorado</b>		
Successional Stage Shift	W/d Ratio State Stability Rating: <b>1.28</b>	W/d Ratio State Stability Rating: <b>1.28</b>	W/d Ratio State Stability Rating: <b>1.28</b>
	MWR / MWR <sub>ref</sub> Stability Rating: <b>Moderately Confined</b>	MWR / MWR <sub>ref</sub> Stability Rating: <b>0.32</b>	MWR / MWR <sub>ref</sub> Stability Rating: <b>0.32</b>
Lateral Stability	Reference W/d Ratio (W/d <sub>ref</sub> ): <b>13.7-19</b>	Width/Depth Ratio State (W/d) / (W/d <sub>ref</sub> ): <b>1.28</b>	W/d Ratio State Stability Rating: <b>Moderately Unstable</b>
	Degree of Incision Stability Rating: <b>1.0</b>	Degree of Incision Stability Rating: <b>Stable</b>	Modified Pfankuch Stability Rating (Numeric & Adjective Rating): <b>94 (Fair)</b>
Vertical Stability (Aggradation)	Reference W/d Ratio (W/d <sub>ref</sub> ): <b>13.7-19</b>	Width/Depth Ratio State (W/d) / (W/d <sub>ref</sub> ): <b>1.28</b>	W/d Ratio State Stability Rating: <b>Moderately Unstable</b>
	Degree of Incision Stability Rating: <b>1.0</b>	Degree of Incision Stability Rating: <b>Stable</b>	Modified Pfankuch Stability Rating (Numeric & Adjective Rating): <b>94 (Fair)</b>
Vertical Stability (Degradation)	Reference W/d Ratio (W/d <sub>ref</sub> ): <b>13.7-19</b>	Width/Depth Ratio State (W/d) / (W/d <sub>ref</sub> ): <b>1.28</b>	W/d Ratio State Stability Rating: <b>Moderately Unstable</b>
	Degree of Incision Stability Rating: <b>1.0</b>	Degree of Incision Stability Rating: <b>Stable</b>	Modified Pfankuch Stability Rating (Numeric & Adjective Rating): <b>94 (Fair)</b>
Channel Enlargement	Reference W/d Ratio (W/d <sub>ref</sub> ): <b>13.7-19</b>	Width/Depth Ratio State (W/d) / (W/d <sub>ref</sub> ): <b>1.28</b>	W/d Ratio State Stability Rating: <b>Moderately Unstable</b>
	Degree of Incision Stability Rating: <b>1.0</b>	Degree of Incision Stability Rating: <b>Stable</b>	Modified Pfankuch Stability Rating (Numeric & Adjective Rating): <b>94 (Fair)</b>
Sediment Supply (Channel Source)	Reference W/d Ratio (W/d <sub>ref</sub> ): <b>13.7-19</b>	Width/Depth Ratio State (W/d) / (W/d <sub>ref</sub> ): <b>1.28</b>	W/d Ratio State Stability Rating: <b>Moderately Unstable</b>
	Degree of Incision Stability Rating: <b>1.0</b>	Degree of Incision Stability Rating: <b>Stable</b>	Modified Pfankuch Stability Rating (Numeric & Adjective Rating): <b>94 (Fair)</b>

## *Appendix C7*

# **C4 Stream Type** *Poor Stability Reach*



# Table of Contents

## *Appendix C7: C4 Poor Reach*

<b>Reach Location &amp; Overview.....</b>	<b>C7-2</b>
<b>Survey Summary.....</b>	<b>C7-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C7-7</b>
<b><i>Velocity, Classification &amp; Morphological Relations.....</i></b>	<b>C7-7</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b><i>Stability Indices.....</i></b>	<b>C7-11</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b><i>BANCS Model – Streambank Erosion.....</i></b>	<b>C7-21</b>
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b><i>FLOWSED Model – Total Annual Sediment Yield.....</i></b>	<b>C7-23</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b><i>POWERSED Model– Sediment Transport Capacity to Assess Bed Stability.....</i></b>	<b>C7-25</b>
Worksheet 5-20a. Sediment transport prediction for the upstream condition.	
Worksheet 5-20b. Sediment transport prediction for the existing condition.	
<b><i>Sediment Competence/Entrainment.....</i></b>	<b>C7-27</b>
Worksheet 5-22. Sediment competence calculations.	
<b><i>Channel Stability Ratings.....</i></b>	<b>C7-28</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b><i>Summary.....</i></b>	<b>C7-34</b>
Worksheet 5-32. Summary of stability condition categories.	

## C4 Poor Reach Location & Overview

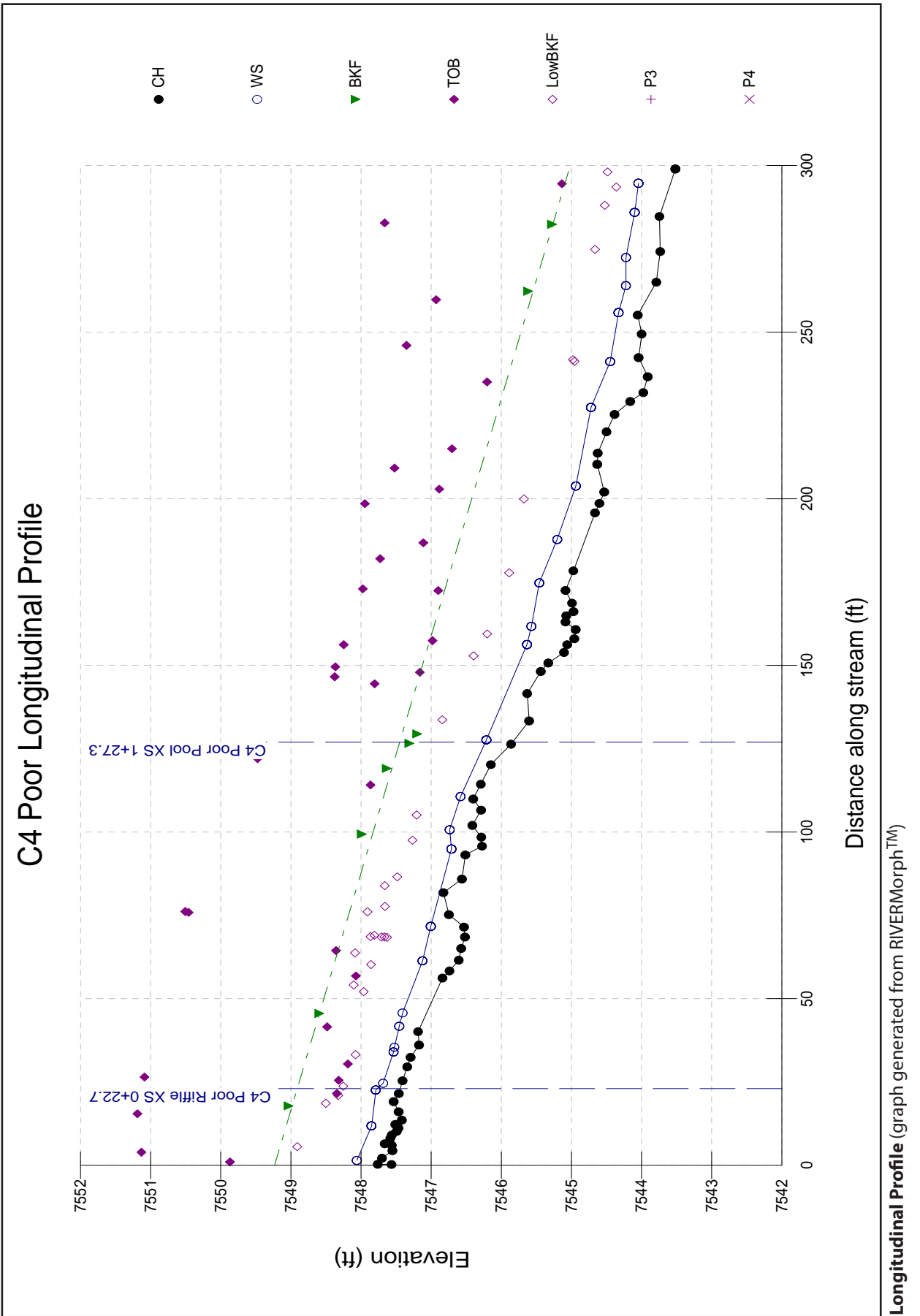
The C4 Poor representative reach is a 4<sup>th</sup> order, perennial stream located in main Trail Creek (**Figure C-2**). The higher width/depth ratio than the reference condition has led to excess sediment deposition in the channel as the POWERSED sediment transport capacity model and the sediment competency calculations both indicate aggradation. The stability rating is “Poor” due to a “Poor” Pfankuch stability rating and the relatively high streambank erosion rate of  $0.0472 \text{ tons/yr/ft}$  compared to the C4 reference rate of  $0.0063 \text{ tons/yr/ft}$ . The sediment supply rating is *High* due primarily to the streambank erosion source and increase in stored sediment in the channel bed. This rating indicates a potential accelerated increase in flow-related sediment based on increased post-fire streamflow peak flows compared to the reference C4 condition. The WRENSS model indicates a water yield increase due to the fire of  $2,733 \text{ acre-ft}$ . As a result, bedload increased from  $45 \text{ tons/yr}$  to  $5,117 \text{ tons/yr}$ , and suspended sediment increased from  $144 \text{ tons/yr}$  to  $9,512 \text{ tons/yr}$ , representing a total increase in sediment of  $14,441 \text{ tons/yr}$ . These are extremely high values for a C4 stream type of this size (48 cfs), which reflect the accelerated sediment yield due to flow related sediment.

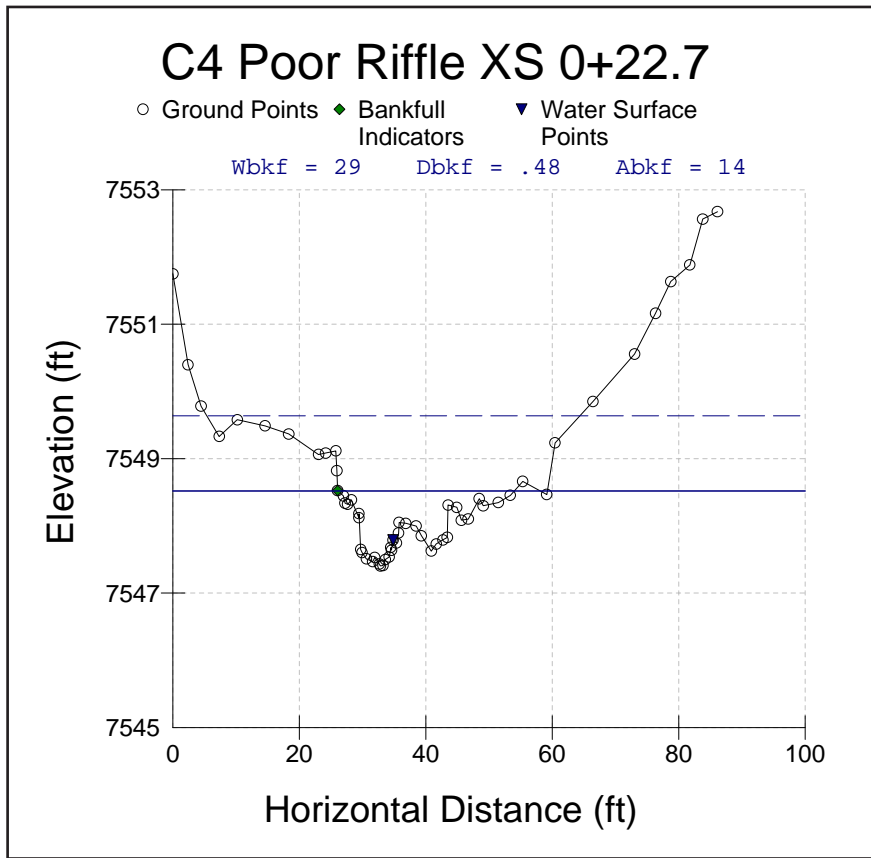
The photograph depicts the typical character of this representative C4 Poor stream type with minimum vegetative influence. The following graphs and summary worksheets provide the detail of the morphology, hydraulics, streambank erosion rates, and stability conditions responsible for the overall “Poor” rating.



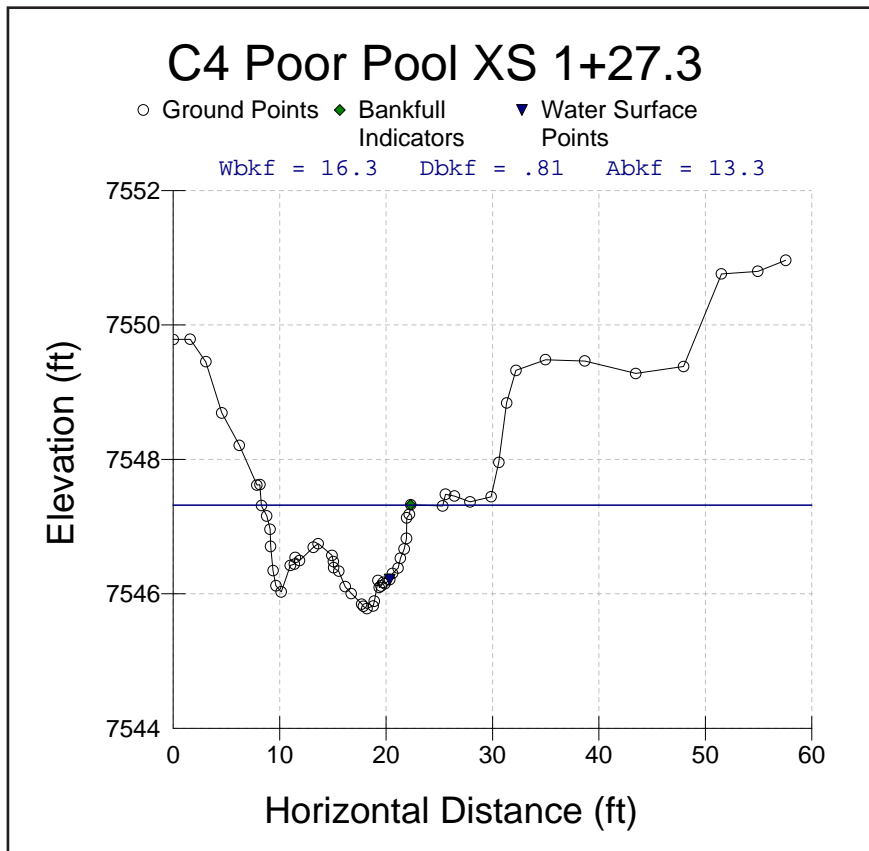


# Survey Summary

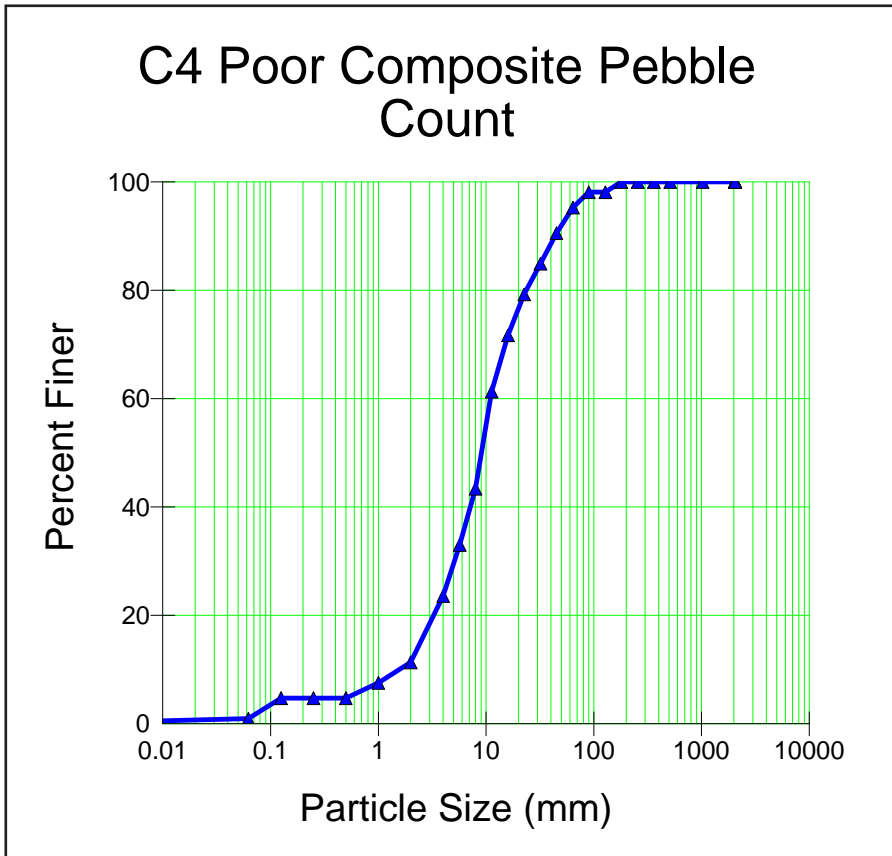




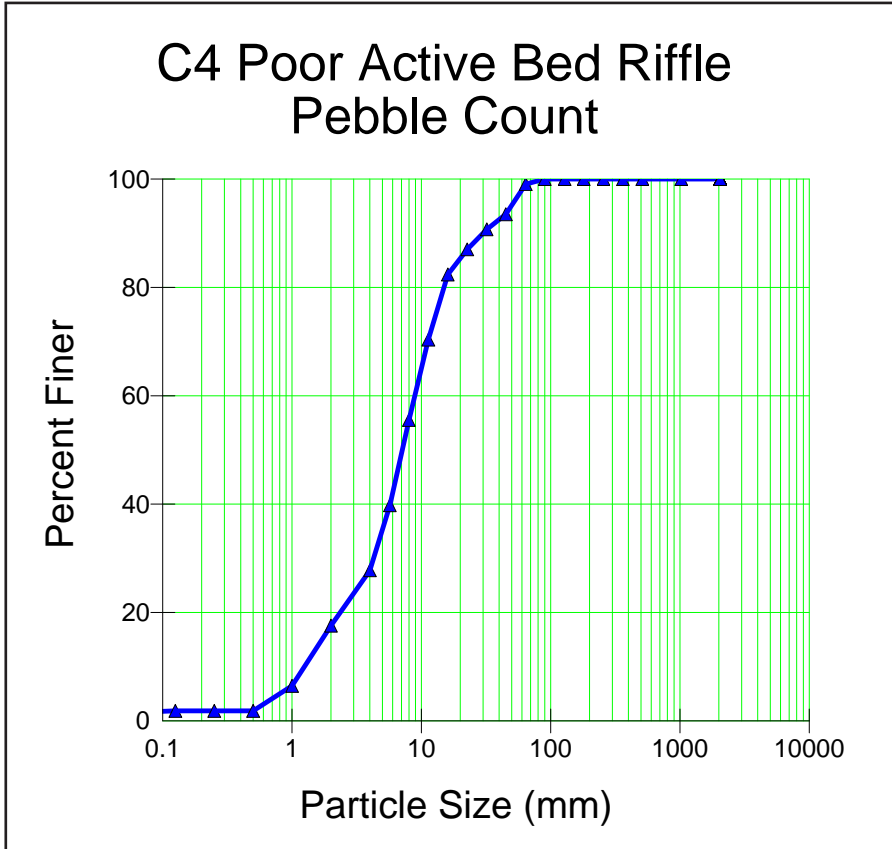
**Representative Riffle Cross-section 0+22.7** (graph generated from RIVERMorph™)



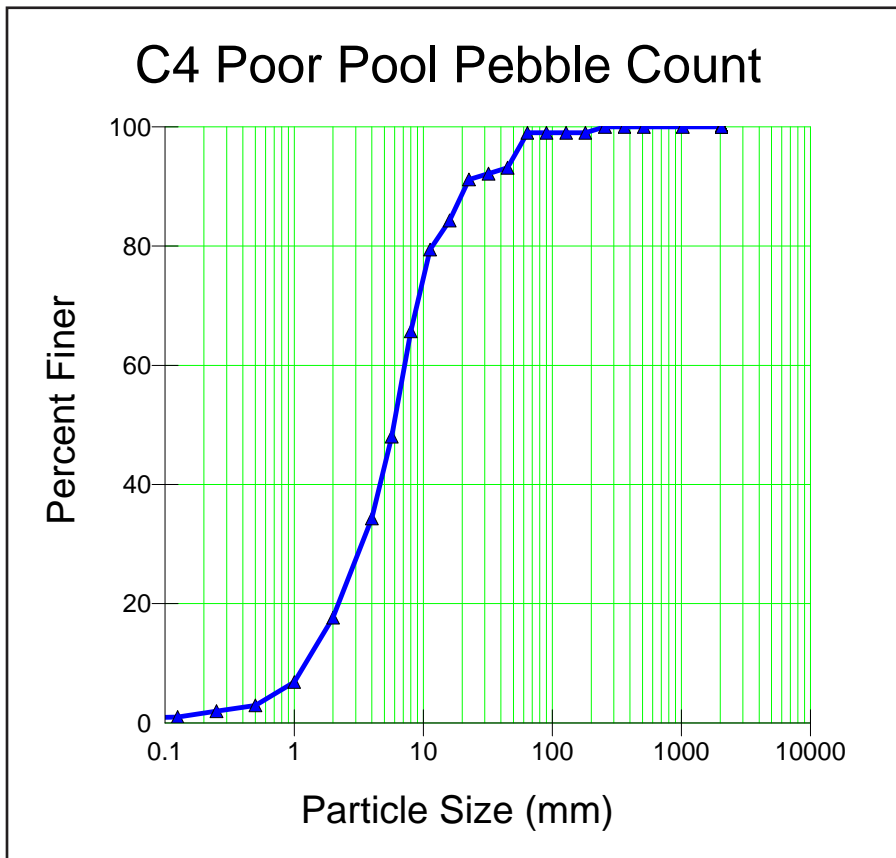
**Pool Cross-section 1+27.3** (graph generated from RIVERMorph™)



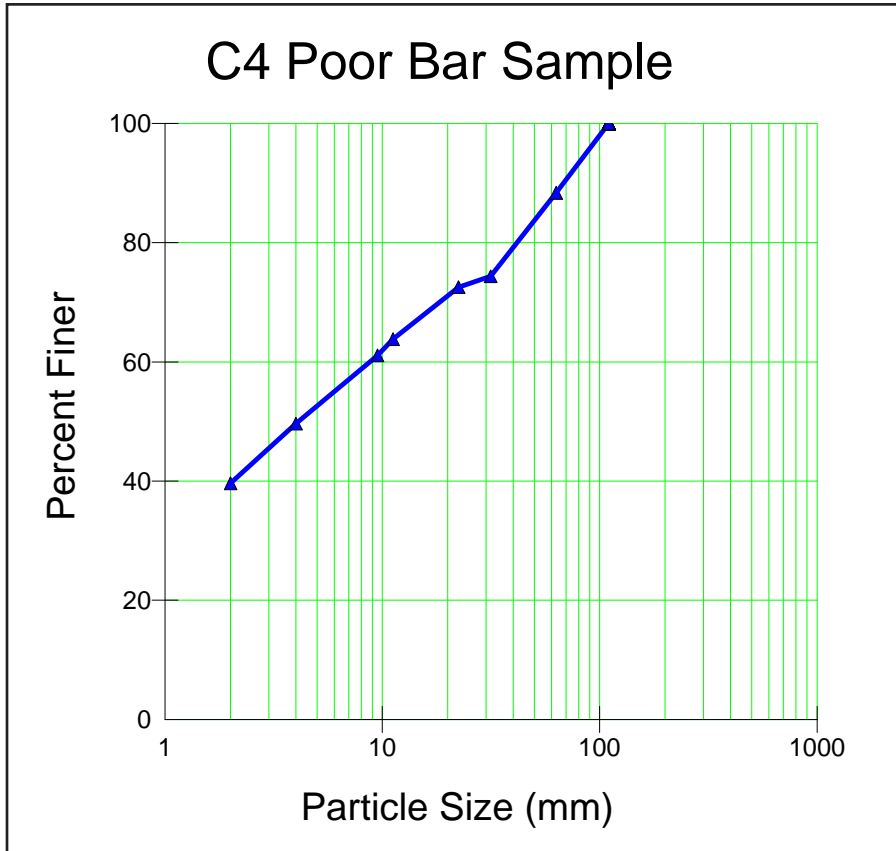
Composite Pebble Count (graph generated from RIVERMorph™)



Active Bed Riffle Pebble Count (graph generated from RIVERMorph™)



Pool Pebble Count (graph generated from RIVERMorph™)



Bar Sample (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates							
Stream:	Trail Creek, C4 Poor Reach			Location:	XS 0+22.7, Pike N.F., Colorado		
Date:	8/18/2010	Stream Type:	C4	Valley Type:	VIII		
Observers:	L. Chavez et al.			HUC:	_ _ _ _ _		
INPUT VARIABLES				OUTPUT VARIABLES			
Bankfull Riffle Cross-Sectional AREA	14.0	$A_{b_{kf}}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.48	$d_{b_{kf}}$ (ft)		
Bankfull Riffle WIDTH	29.0	$W_{b_{kf}}$ (ft)	Wetted PERIMETER $\sim (2 * d_{b_{kf}}) + W_{b_{kf}}$	29.98	$W_p$ (ft)		
$D_{84}$ at Riffle	18.3	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.06	$D_{84}$ (ft)		
Bankfull SLOPE	0.0140	$S_{b_{kf}}$ (ft / ft)	Hydraulic RADIUS $A_{b_{kf}} / W_p$	0.47	R (ft)		
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness $R(ft) / D_{84} (ft)$	7.76	$R / D_{84}$		
Drainage Area	15.9	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.458	$u^*$ (ft/sec)		
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE	
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$				3.60	ft / sec	50.26	cfs
2. Roughness Coefficient: a) Manning's n from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.0253$				4.18	ft / sec	58.37	cfs
2. Roughness Coefficient: b) Manning's n from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.031$				3.41	ft / sec	47.64	cfs
2. Roughness Coefficient: c) Manning's n from Jarrett (USGS): Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for Stream Types A1, A2, A3, B1, B2, B3, C2 & E3 $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ $n = 0.087$				1.22	ft / sec	16.96	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Limerinos				3.81	ft / sec	53.1	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)					ft / sec		cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q =$ <input type="text"/> year $u = Q / A$					ft / sec		cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation ( $R/D_{84}$ ) – Estimation Method 1							
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.							
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.							
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.							
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.							

**Worksheet 5-3.** Level II stream classification.

Stream: <b>Trail Creek, C4 Poor Reach</b>	
Basin: <b>South Platte</b>	Drainage Area: <b>10176</b> acres <b>15.9</b> mi <sup>2</sup>
Location: <b>Pike National Forest, Colorado</b>	
Twp.&Rge:	Sec.&Qtr.:
Cross-Section Monuments (Lat./Long.): <b>Riffle XS 0+22.7</b>	
Date: <b>08/19/10</b>	
Observers: <b>L. Chavez et al.</b>	
Valley Type: <b>VIII</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>29.02</b> ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>0.48</b> ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>13.95</b> ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>60.46</b> ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>1.12</b> ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>59</b> ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>2.03</b> ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>9.22</b> mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.014</b> ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length ( $SL / VL$ ); or estimated from a ratio of valley slope divided by channel slope ( $VS / S$ ).	<b>1.08</b>

<b>Stream Type</b>	<b>C4</b>	(See Figure 2-14)
--------------------	-----------	-------------------

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, C4 Poor Reach</b>				Location: <b>Pike National Forest, Colorado</b>							
Observers: <b>L. Chavez et al.</b>			Date: <b>8/18/2010</b>		Valley Type: <b>VIII</b>		Stream Type: <b>C4</b>				
<b>River Reach Dimension Summary Data.....1</b>											
<b>Riffle Dimensions* ** ** *</b>	<b>Riffle Dimensions* ** ** *</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Width (W <sub>bkf</sub> )			<b>29.0</b>		ft	Riffle Cross-Sectional Area (A <sub>bkf</sub> ) (ft <sup>2</sup> )	<b>14.0</b>			
	Mean Riffle Depth (d <sub>bkf</sub> )			<b>0.48</b>		ft	Riffle Width/Depth Ratio (W <sub>bkf</sub> / d <sub>bkf</sub> )	<b>60.5</b>			
	Maximum Riffle Depth (d <sub>max</sub> )			<b>1.12</b>		ft	Max Riffle Depth to Mean Riffle Depth (d <sub>max</sub> /d <sub>bkf</sub> )	<b>2.333</b>			
	Width of Flood-Prone Area (W <sub>fpa</sub> )			<b>59.0</b>		ft	Entrenchment Ratio (W <sub>fpa</sub> / W <sub>bkf</sub> )	<b>2.0</b>			
	Riffle Inner Berm Width (W <sub>ib</sub> )			<b>14.4</b>		ft	Riffle Inner Berm Width to Riffle Width (W <sub>ib</sub> / W <sub>bkf</sub> )	<b>0.496</b>			
	Riffle Inner Berm Depth (d <sub>ib</sub> )			<b>0.35</b>		ft	Riffle Inner Berm Depth to Mean Depth (d <sub>ib</sub> / d <sub>bkf</sub> )	<b>0.729</b>			
	Riffle Inner Berm Area (A <sub>ib</sub> )			<b>5.0</b>		ft <sup>2</sup>	Riffle Inner Berm Area to Riffle Area (A <sub>ib</sub> / A <sub>bkf</sub> )	<b>0.358</b>			
	Riffle Inner Berm W/D Ratio (W <sub>ib</sub> / d <sub>ib</sub> )			<b>41.1</b>							
<b>Pool Dimensions* ** ** *</b>	<b>Pool Dimensions* ** ** *</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Pool Dimensions &amp; Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Pool Width (W <sub>bkfp</sub> )			<b>16.3</b>		ft	Pool Width to Riffle Width (W <sub>bkfp</sub> / W <sub>bkf</sub> )	<b>0.563</b>			
	Mean Pool Depth (d <sub>bkfp</sub> )			<b>0.81</b>		ft	Mean Pool Depth to Mean Riffle Depth (d <sub>bkfp</sub> / d <sub>bkf</sub> )	<b>1.688</b>			
	Pool Cross-Sectional Area (A <sub>bkfp</sub> )			<b>13.3</b>		ft	Pool Area to Riffle Area (A <sub>bkfp</sub> / A <sub>bkf</sub> )	<b>0.951</b>			
	Maximum Pool Depth (d <sub>maxp</sub> )			<b>1.54</b>		ft	Max Pool Depth to Mean Riffle Depth (d <sub>maxp</sub> / d <sub>bkf</sub> )	<b>3.208</b>			
	Pool Inner Berm Width (W <sub>ibp</sub> )			<b>12.7</b>		ft	Pool Inner Berm Width to Pool Width (W <sub>ibp</sub> / W <sub>bkfp</sub> )	<b>0.778</b>			
	Pool Inner Berm Depth (d <sub>ibp</sub> )			<b>0.50</b>		ft	Pool Inner Berm Depth to Pool Depth (d <sub>ibp</sub> / d <sub>bkfp</sub> )	<b>0.617</b>			
	Pool Inner Berm Area (A <sub>ibp</sub> )			<b>6.4</b>		ft <sup>2</sup>	Pool Inner Berm Area to Pool Area (A <sub>ibp</sub> / A <sub>bkfp</sub> )	<b>0.483</b>			
	Point Bar Slope (S <sub>pb</sub> )			<b>0.220</b>		ft/ft	Pool Inner Berm Width/Depth Ratio (W <sub>ibp</sub> / d <sub>ibp</sub> )	<b>25.4</b>			
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Run Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Run Width (W <sub>bkfr</sub> )					ft	Run Width to Riffle Width (W <sub>bkfr</sub> / W <sub>bkf</sub> )				
	Mean Run Depth (d <sub>bkfr</sub> )					ft	Mean Run Depth to Mean Riffle Depth (d <sub>bkfr</sub> / d <sub>bkf</sub> )				
	Run Cross-Sectional Area (A <sub>bkfr</sub> )					ft	Run Area to Riffle Area (A <sub>bkfr</sub> / A <sub>bkf</sub> )				
	Maximum Run Depth (d <sub>maxr</sub> )					ft	Max Run Depth to Mean Riffle Depth (d <sub>maxr</sub> / d <sub>bkf</sub> )				
Run Width/Depth Ratio (W <sub>bkfr</sub> / d <sub>bkfr</sub> )					ft						
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Glide Dimensions &amp; Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Glide Width (W <sub>bktg</sub> )					ft	Glide Width to Riffle Width (W <sub>bktg</sub> / W <sub>bkf</sub> )				
	Mean Glide Depth (d <sub>bktg</sub> )					ft	Mean Glide Depth to Mean Riffle Depth (d <sub>bktg</sub> / d <sub>bkf</sub> )				
	Glide Cross-Sectional Area (A <sub>bktg</sub> )					ft	Glide Area to Riffle Area (A <sub>bktg</sub> / A <sub>bkf</sub> )				
	Maximum Glide Depth (d <sub>maxg</sub> )					ft	Max Glide Depth to Mean Riffle Depth (d <sub>maxg</sub> / d <sub>bkf</sub> )				
	Glide Width/Depth Ratio (W <sub>bktg</sub> / d <sub>bktg</sub> )					ft/ft	Glide Inner Berm Width/Depth Ratio (W <sub>ibg</sub> / d <sub>ibg</sub> )				
	Glide Inner Berm Width (W <sub>ibg</sub> )					ft	Glide Inner Berm Width to Glide Width (W <sub>ibg</sub> / W <sub>bktg</sub> )				
	Glide Inner Berm Depth (d <sub>ibg</sub> )					ft	Glide Inner Berm Depth to Glide Depth (d <sub>ibg</sub> / d <sub>bktg</sub> )				
Glide Inner Berm Area (A <sub>ibg</sub> )					ft <sup>2</sup>	Glide Inner Berm Area to Glide Area (A <sub>ibg</sub> / A <sub>bktg</sub> )					
<b>Step**</b>	<b>Step Dimensions**</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Step Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Step Width (W <sub>bkfs</sub> )					ft	Step Width to Riffle Width (W <sub>bkfs</sub> / W <sub>bkf</sub> )				
	Mean Step Depth (d <sub>bkfs</sub> )					ft	Mean Step Depth to Riffle Depth (d <sub>bkfs</sub> / d <sub>bkf</sub> )				
	Step Cross-Sectional Area (A <sub>bkfs</sub> )					ft	Step Area to Riffle Area (A <sub>bkfs</sub> / A <sub>bkf</sub> )				
	Maximum Step Depth (d <sub>maxs</sub> )					ft	Max Step Depth to Mean Riffle Depth (d <sub>maxs</sub> / d <sub>bkf</sub> )				
Step Width/Depth Ratio (W <sub>bkfs</sub> / d <sub>bkfs</sub> )											

**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, C4 Poor Reach</b>		Location: <b>Pike National Forest, Colorado</b>						
Observers: <b>L. Chavez et al.</b>		Date: <b>8/18/2010</b>		Valley Type: <b>VIII</b>		Stream Type: <b>C4</b>		
<b>River Reach Summary Data.....2</b>								
<b>Hydraulics</b>	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )		<b>3.41</b>	ft/sec	Estimation Method		<b>"n" by Stream Type</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )		<b>47.6</b>	cfs	Drainage Area		<b>15.9</b> mi <sup>2</sup>	
<b>Channel Pattern</b>	<b>Geometry</b>			<b>Dimensionless Geometry Ratios</b>				
	Linear Wavelength ( $\lambda$ )			ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )			
	Stream Meander Length ( $L_m$ )	<b>123.0</b>		ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )	<b>4.24</b>		
	Radius of Curvature ( $R_c$ )	<b>34.2</b>	<b>19.5</b>	<b>55.3</b> ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )	<b>1.18</b>	<b>0.67</b> <b>1.91</b>	
	Belt Width ( $W_{bit}$ )	<b>40.1</b>	<b>24.1</b>	<b>48.2</b> ft	Meander Width Ratio ( $W_{bit} / W_{bkt}$ )	<b>1.38</b>	<b>0.83</b> <b>1.66</b>	
	Arc Length ( $L_a$ )			ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )			
	Riffle Length ( $L_r$ )	<b>18.8</b>	<b>16.1</b>	<b>23.2</b> ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )	<b>0.65</b>	<b>0.55</b> <b>0.80</b>	
	Individual Pool Length ( $L_p$ )	<b>6.7</b>	<b>2.0</b>	<b>12.0</b> ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )	<b>0.23</b>	<b>0.07</b> <b>0.41</b>	
Pool to Pool Spacing ( $P_s$ )	<b>33.4</b>	<b>8.8</b>	<b>131.0</b> ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )	<b>1.15</b>	<b>0.30</b> <b>4.51</b>		
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )	<b>0.0148</b>	ft/ft	Average Water Surface Slope (S)	<b>0.014</b>	ft/ft	Sinuosity ( $S_{val} / S$ )	<b>1.08</b>
	Stream Length (SL)	<b>168.1</b>	ft	Valley Length (VL)	<b>158.2</b>	ft	Sinuosity (SL / VL)	<b>1.06</b>
	Low Bank Height (LBH)	start: <b>1.12</b> ft end: <b>1.54</b> ft		Max Bankfull Depth ( $d_{max}$ )	start: <b>1.12</b> ft end: <b>1.54</b> ft		Bank-Height Ratio (BHR) (LBH / $d_{max}$ )	start: <b>1.0</b> end: <b>1.0</b>
	<b>Facet Slopes</b>			<b>Dimensionless Facet Slope Ratios</b>				
	Riffle Slope ( $S_{rif}$ )	<b>0.0160</b>		ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.1679</b>		
	Run Slope ( $S_{run}$ )	<b>0.0240</b>		ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )	<b>1.7518</b>		
	Pool Slope ( $S_p$ )	<b>0.0110</b>		ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )	<b>0.8029</b>		
	Glide Slope ( $S_g$ )	<b>0.0170</b>		ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )	<b>1.2409</b>		
	Step Slope ( $S_s$ )			ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )			
	<b>Max Depths<sup>a</sup></b>			<b>Dimensionless Depth Ratios</b>				
	Max Riffle Depth ( $d_{max}$ )	<b>1.56</b>	<b>1.34</b>	<b>1.71</b> ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>3.250</b>	<b>2.792</b>	<b>3.563</b>
	Max Run Depth ( $d_{maxr}$ )	<b>1.50</b>	<b>1.35</b>	<b>1.65</b> ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )	<b>3.125</b>	<b>2.813</b>	<b>3.438</b>
	Max Pool Depth ( $d_{maxp}$ )	<b>1.77</b>	<b>1.60</b>	<b>1.99</b> ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	<b>3.688</b>	<b>3.333</b>	<b>4.146</b>
	Max Glide Depth ( $d_{maxg}$ )	<b>1.66</b>	<b>1.59</b>	<b>1.82</b> ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )	<b>3.458</b>	<b>3.313</b>	<b>3.792</b>
Max Step Depth ( $d_{maxs}$ )			ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )				
<b>Channel Materials</b>	<b>Reach<sup>b</sup></b>			<b>Reach<sup>b</sup></b>			<b>Protrusion Height<sup>d</sup></b>	
	% Silt/Clay	<b>0.9</b>	<b>0.0</b>	<b>0.0</b>	$D_{16}$	<b>2.8</b>	<b>1.9</b>	<b>0.0</b> mm
	% Sand	<b>10.4</b>	<b>17.6</b>	<b>39.6</b>	$D_{35}$	<b>6.1</b>	<b>5.0</b>	<b>0.0</b> mm
	% Gravel	<b>84.0</b>	<b>81.5</b>	<b>49.1</b>	$D_{50}$	<b>9.2</b>	<b>7.2</b>	<b>4.2</b> mm
	% Cobble	<b>4.7</b>	<b>0.9</b>	<b>11.3</b>	$D_{84}$	<b>30.5</b>	<b>18.3</b>	<b>53.2</b> mm
	% Boulder				$D_{95}$	<b>62.9</b>	<b>50.1</b>	<b>89.8</b> mm
	% Bedrock				$D_{100}$	<b>180.0</b>	<b>90.0</b>	<b>110.0</b> mm

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.  
<sup>b</sup> Composite sample of riffles and pools within the designated reach.      <sup>c</sup> Active bed of a riffle.      <sup>d</sup> Height of roughness feature above bed.



## Stability Indices

**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation					
Stream: <b>Trail Creek, C4 Poor Reach</b>		Location: <b>Pike National Forest, Colorado</b>			
Observers: <b>L. Chavez et al.</b>		Reference reach <input type="checkbox"/>	Disturbed (impacted reach) <input checked="" type="checkbox"/>	Date: <b>8/18/10</b>	
Existing species composition: <b>Spruce, Willow, Shrubs, Grasses</b>		Potential species composition: <b>Higher density of existing species without invasives</b>			
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition
<b>1. Overstory</b>	Canopy layer	<b>15%</b>	<b>20%</b>	<b>Spruce</b>	<b>60%</b>
				<b>Willow</b>	<b>40%</b>
				<b>100%</b>	
<b>2. Understory</b>	Shrub layer	<b>28%</b>	<b>28%</b>	<b>Willow</b>	<b>98%</b>
				<b>River Birch</b>	<b>1%</b>
				<b>Raspberry</b>	<b>1%</b>
				<b>100%</b>	
<b>3. Ground level</b>	Herbaceous	<b>10%</b>	<b>10%</b>	<b>Horseweed</b>	<b>10%</b>
				<b>Grasses</b>	<b>30%</b>
				<b>Fireweed &amp; Unc forbs</b>	<b>30%</b>
				<b>Invasives</b>	<b>27%</b>
				<b>Carex</b>	<b>1%</b>
	<b>Rushes, Phacelix</b>	<b>2%</b>			
				<b>100%</b>	
	Leaf or needle litter	<b>2%</b>	<b>2%</b>	<b>Remarks:</b> Condition, vigor and/or usage of existing reach: <b>Grasses, Fescue - Streambank; Invasives: Cheatgrass, Mullen, Canada Thistle, Yellow sweet clover</b>	
	Bare ground	<b>40%</b>	<b>40%</b>		
			<b>Column total = 100%</b>		

\*Based on crown closure.

\*\*Based on basal area to surface area.

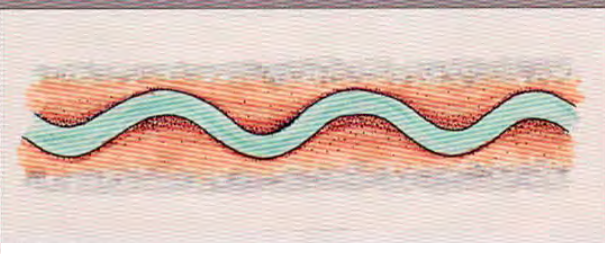


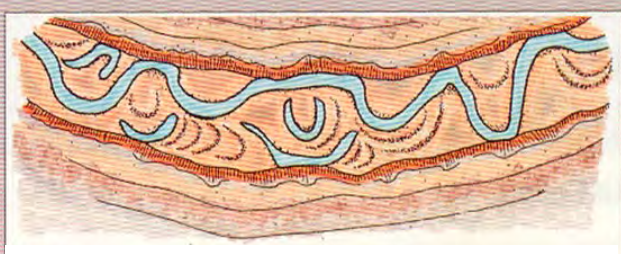

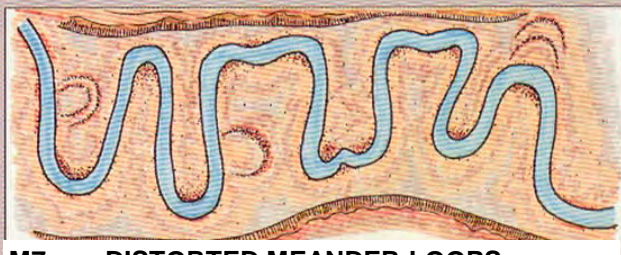
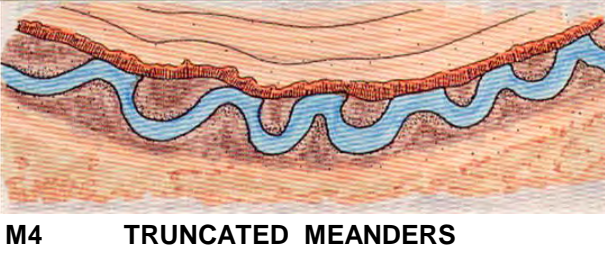
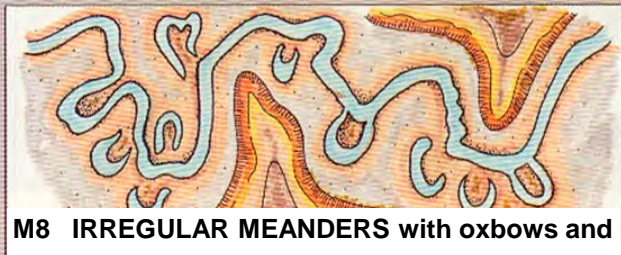
**Worksheet 5-7.** Flow regime.

FLOW REGIME							
Stream: <b>Trail Creek, C4 Poor Reach</b>				Location: <b>Pike National Forest, Colorado</b>			
Observers: <b>L. Chavez et al.</b>				Date: <b>8/18/2010</b>			
<b>List ALL COMBINATIONS that APPLY.....</b>		<b>P2</b>	<b>P8</b>				
General Category							
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation						
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.						
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.						
<b>P</b>	Perennial stream channels: Surface water persists yearlong.						
Specific Category							
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.						
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.						
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.						
<b>4</b>	Streamflow regulated by glacial melt.						
<b>5</b>	Ice flows/ice torrents from ice dam breaches.						
<b>6</b>	Alternating flow/backwater due to tidal influence.						
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.						
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.						
<b>9</b>	Rain-on-snow generated runoff.						

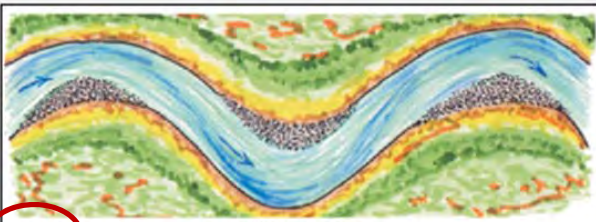

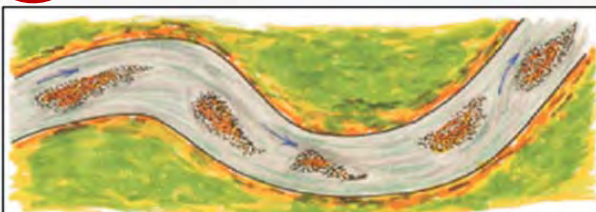

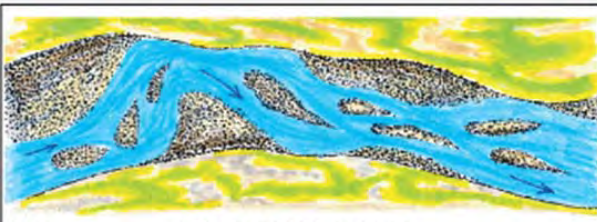

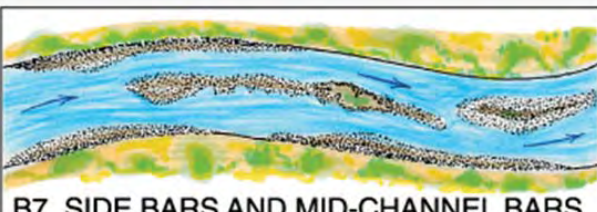

**Worksheet 5-8.** Stream order & stream size.

<b>Stream Size and Order</b>			
Stream:	<b>Trail Creek, C4 Poor Reach</b>		
Location:	<b>Pike National Forest, Colorado</b>		
Observers:	<b>L. Chavez <i>et al.</i></b>		
Date:	<b>8/18/2010</b>		
<b>Stream Size Category and Order</b> ↗			<b>S-4(4)</b>
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0.305	<1	<input type="checkbox"/>
S-2	0.3 – 1.5	1 – 5	<input type="checkbox"/>
S-3	1.5 – 4.6	5 – 15	<input type="checkbox"/>
<b>S-4</b>	<b>4.6 – 9</b>	<b>15 – 30</b>	<input checked="" type="checkbox"/>
S-5	9 – 15	30 – 50	<input type="checkbox"/>
S-6	15 – 22.8	50 – 75	<input type="checkbox"/>
S-7	22.8 – 30.5	75 – 100	<input type="checkbox"/>
S-8	30.5 – 46	100 – 150	<input type="checkbox"/>
S-9	46 – 76	150 – 250	<input type="checkbox"/>
S-10	76 – 107	250 – 350	<input type="checkbox"/>
S-11	107 – 150	350 – 500	<input type="checkbox"/>
S-12	150 – 305	500 – 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
<b>Stream Order</b>			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			

Worksheet 5-9. Meander patterns.

<b>Meander Patterns</b>					
Stream: <b>Trail Creek, C4 Poor Reach</b>		Location: <b>Pike National Forest, CO</b>			
Observers: <b>L. Chavez et al.</b>		Date: <b>8/18/2010</b>			
List ALL CATEGORIES that APPLY	<b>M3</b>				
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>					
 <b>M1</b> <b>REGULAR MEANDERS</b>	 <b>M5</b> <b>UNCONFINED MEANDER SCROLLS</b>				
 <b>M2</b> <b>TORTUOUS MEANDERS</b>	 <b>M6</b> <b>CONFINED MEANDER SCROLLS</b>				
 <b>M3</b> <b>IRREGULAR MEANDERS</b>	 <b>M7</b> <b>DISTORTED MEANDER LOOPS</b>				
 <b>M4</b> <b>TRUNCATED MEANDERS</b>	 <b>M8</b> <b>IRREGULAR MEANDERS with oxbows and</b>				

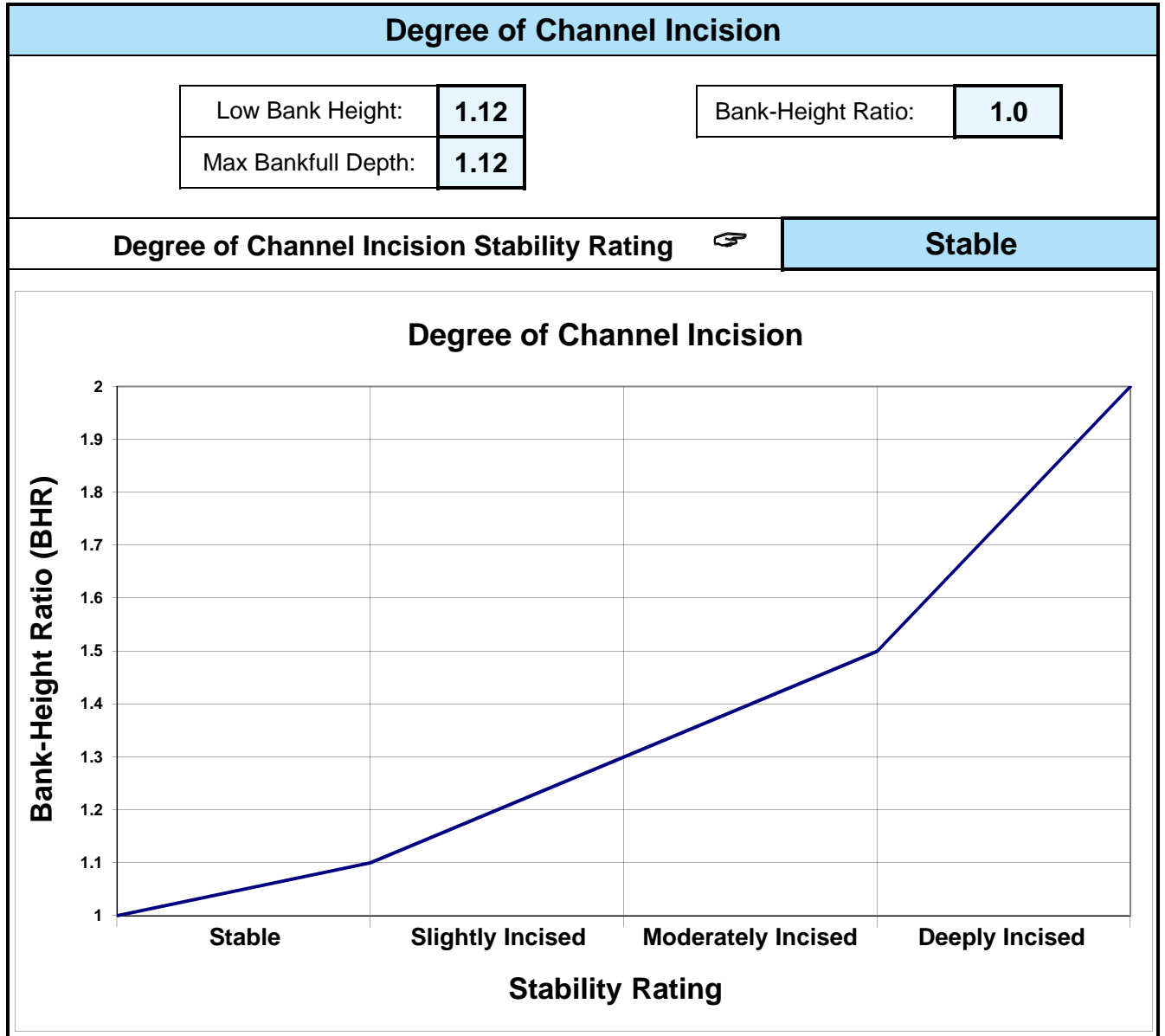
Worksheet 5-10. Depositional patterns.

<b>Depositional Patterns</b>				
Stream: <b>Trail Creek, C4 Poor Reach</b>	Location: <b>Pike National Forest, Colorado</b>			
Observers: <b>L. Chavez et al.</b>	Date: <b>8/18/2010</b>			
List ALL CATEGORIES that APPLY	<b>B1</b>	<b>B2</b>	<b>B4</b>	
<i>Various Depositional Features modified from Galay et al. (1973)</i>				
<div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B1</b> POINT BARS</p> </div> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B2</b> POINT BARS with Few MID-CHANNEL BARS</p> </div> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B3</b> NUMEROUS MID-CHANNEL BARS</p> </div> <div style="border: 1px solid black; padding: 5px;">  <p><b>B4</b> SIDE BARS</p> </div>	<div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B5</b> DIAGONAL BARS</p> </div> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B6</b> Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</p> </div> <div style="border: 1px solid black; padding: 5px; margin-bottom: 5px;">  <p><b>B7</b> SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</p> </div> <div style="border: 1px solid black; padding: 5px;">  <p><b>B8</b> DELTA BARS</p> </div>			

**Worksheet 5-11.** Channel blockages.

Channel Blockages		
Stream: <b>Trail Creek, C4 Poor Reach</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>L. Chavez et al.</b>		Date: <b>8/18/2010</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input checked="" type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input type="checkbox"/>
<b>D4</b> Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

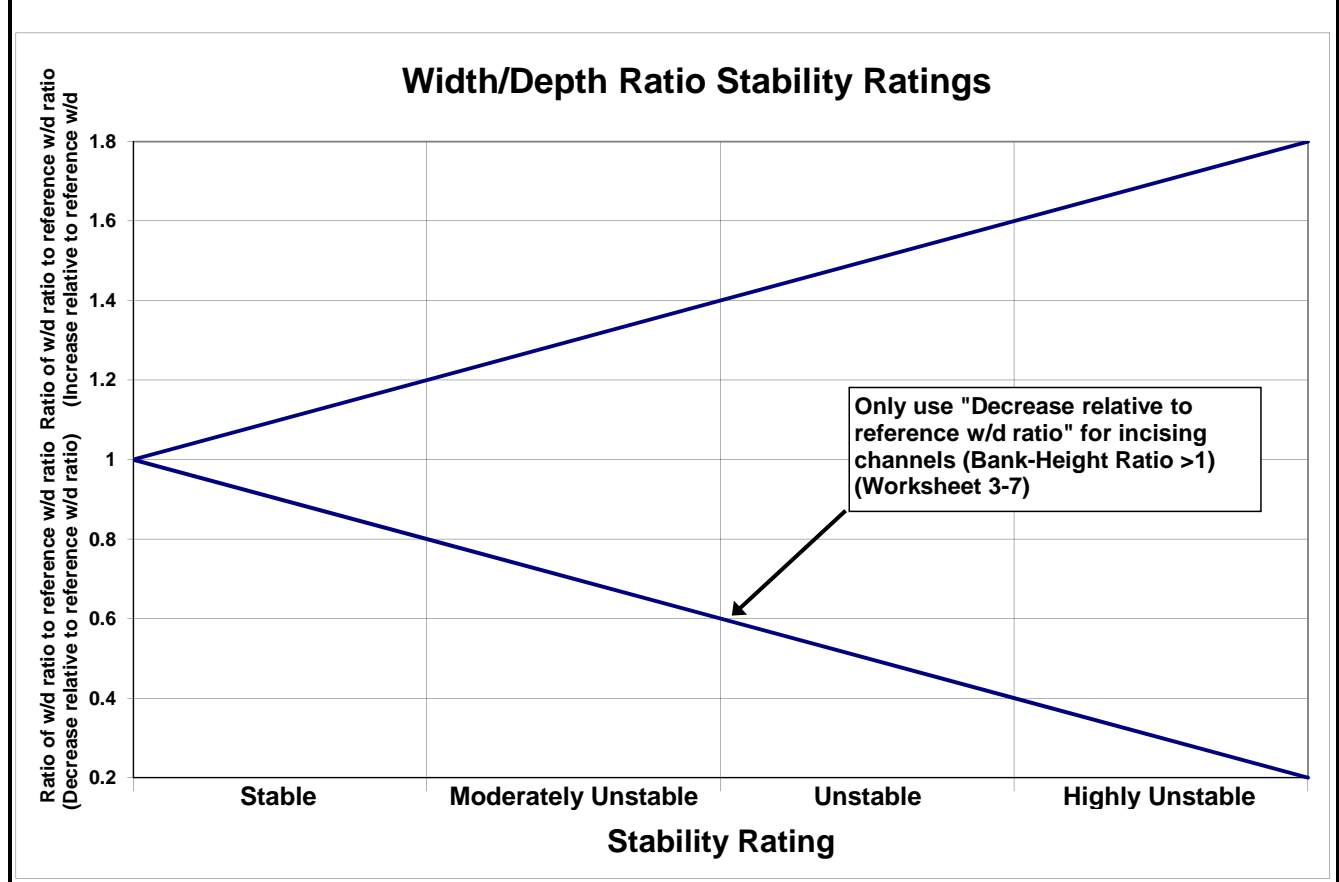
Worksheet 5-12. Degree of channel incision.



**Worksheet 5-13.** Width/depth ratio state.

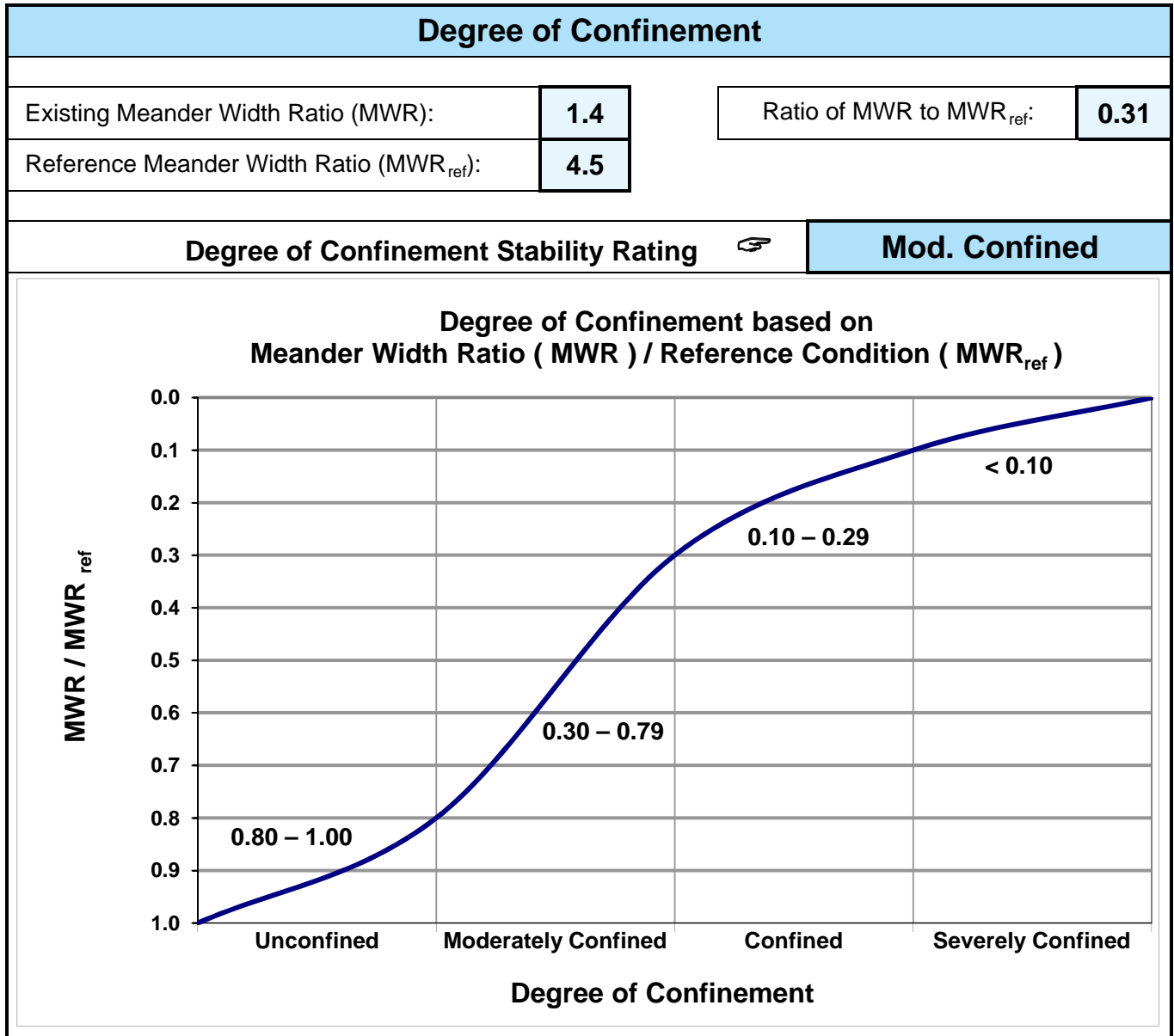
Width/Depth Ratio State			
Existing Width/Depth Ratio:	<b>60</b>	Ratio of existing W/d to reference W/d:	<b>4.38</b>
Reference Width/Depth Ratio:	<b>13.7</b>		

<b>Width/Depth Ratio State Stability Rating</b>	<b>Highly Unstable</b>
---	------------------------





**Worksheet 5-14.** Degree of channel confinement (lateral containment).



Worksheet 5-15. Pfankuch channel stability rating.

Stream: Trail Creek, C4 Poor Reach		Location: Pike National Forest, CO		Valley Type: VIII		Observers: L. Chavez et al.		Date: 8/18/2010																	
Local- tion	Key Category	Excellent Description	Rating	Good Description	Rating	Fair Description	Rating	Poor Description	Rating																
Upper banks	1	Landform slope	2	Bank slope gradient 30-40%.	4	Bank slope gradient 40-60%.	6	Bank slope gradient > 60%.	8																
	2	Mass erosion	3	No evidence of past or future mass erosion.	6	Frequent or large, causing sediment nearly yearlong.	9	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.	12																
	3	Debris jam potential	2	Essentially absent from immediate channel area.	4	Moderate to heavy amounts, mostly larger sizes.	6	Moderate to heavy amounts, predominantly larger sizes.	8																
	4	Vegetative bank protection	3	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	6	70-90% density. Fewer species or less vigor suggest less dense or deep root mass.	9	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.	12																
Lower banks	5	Channel capacity	1	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0.	2	Bankfull stage is contained within banks. Width/depth ratio departure from reference width/depth ratio = 1.0-1.2. Bank-Height Ratio (BHR) = 1.1-1.3.	3	Bankfull stage is not contained; over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.	4																
	6	Bank rock content	2	> 65% with large angular boulders. 12" + common.	4	40-65%. Mostly boulders and small cobbles 6-12".	6	20-40%. Most in the 3-6" diameter class.	8																
	7	Obstructions to flow	2	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	5	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	6	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	8																
	8	Cutting	4	Little or none. Infrequent raw banks <6".	6	Some, intermittently at outcaves and constrictions. Raw banks may be up to 12".	12	Significant. Cuts 12-24" high. Root mat overhangs and sloughing evident.	16																
	9	Deposition	4	Little or no enlargement of channel or point bars.	8	Some new bar increase, mostly from coarse gravel.	12	Moderate deposition of new gravel and coarse sand on old and some new bars.	16																
Bottom	10	Rock angularity	1	Sharp edges and corners. Plane surfaces rough.	2	Rounded corners and edges. Surfaces smooth and flat.	3	Corners and edges well rounded in 2 dimensions.	4																
	11	Brightness	1	Surfaces dull, dark or stained. Generally not bright.	2	Mostly dull, but may have <35% bright surfaces.	3	Mixture dull and bright, i.e., 35-65% mixture range.	4																
	12	Consolidation of particles	2	Assorted sizes tightly packed or overlapping.	4	Moderately packed with some overlapping.	6	Mostly loose assortment with no apparent overlap.	8																
	13	Bottom size distribution	4	No size change evident. Stable material 80-100%.	8	Distribution shift light. Stable material 50-80%.	12	Moderate change in sizes. Stable materials 20-50%.	16																
	14	Scouring and deposition	6	<5% of bottom affected by scour or deposition.	12	5-30% affected. Scour at constrictions and where grades steepen. Some deposition in pools.	18	30-50% affected. Deposits and scour at obstructions, constrictions and bends. Some filling of pools.	24																
	15	Aquatic vegetation	1	Abundant growth moss-like, dark green perennial. In swift water too.	2	Common. Algae forms in low velocity and pool areas. Moss here too.	3	Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick.	4																
			Excellent total = 0	Good total = 19			Fair total = 6			Poor total = 108															
Stream type	A1	A2	A3	A4	A5	A6	B1	B2	B3	B4	B5	B6	C1	C2	C3	C4	C5	C6	D3	D4	D5	D6	Grand total =	133	
Good (Stable)	38-43	38-43	54-90	60-95	60-95	50-80	38-45	38-45	40-60	48-68	40-60	38-50	38-50	60-85	70-90	70-90	60-85	85-107	85-107	85-107	85-107	85-107	85-107	67-98	
Fair (Mod. unstable)	44-47	44-47	91-129	96-132	96-142	81-110	46-58	46-58	61-78	65-84	69-88	61-78	51-61	51-61	86-105	91-110	91-110	86-105	108-132	108-132	108-132	108-132	108-132	99-125	C4
Poor (Unstable)	48+	48+	130+	133+	143+	111+	59+	59+	79+	85+	89+	79+	62+	62+	106+	111+	111+	106+	133+	133+	133+	133+	133+	126+	*Potential stream type =
Stream type	DA3	DA4	DA5	DA6	E3	E4	E5	E6	F1	F2	F3	F4	F5	F6	G1	G2	G3	G4	G5	G6	G6	G6	G6	G6	C4
Good (Stable)	40-63	40-63	40-63	40-63	40-63	50-75	50-75	40-63	60-85	60-85	85-110	85-110	90-115	80-95	40-60	40-60	85-107	85-107	90-112	90-112	85-107	85-107	85-107	85-107	
Fair (Mod. unstable)	64-86	64-86	64-86	64-86	64-86	76-96	76-96	64-86	86-105	86-105	111-125	111-125	116-130	96-110	61-78	61-78	108-120	108-120	113-125	113-125	108-120	108-120	108-120	108-120	Modified channel stability rating =
Poor (Unstable)	87+	87+	87+	87+	87+	97+	97+	87+	106+	106+	126+	126+	131+	111+	79+	79+	121+	121+	126+	126+	121+	121+	121+	121+	POOR

\*Rating is adjusted to potential stream type, not existing.

## BANCS Model – Streambank Erosion

Worksheet 5-18. Annual streambank erosion estimates.

Stream: <b>Trail Creek, C4 Poor Reach</b>		Location: <b>Pike National Forest, Colorado</b>					
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>160</b>				Date: <b>8/19/2010</b>	
Observers: <b>L. Chavez et al.</b>		Valley Type: <b>VIII</b>			Stream Type: <b>C4</b>		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 5-16) (adjective)	NBS rating (Worksheet 5-17) (adjective)	Bank erosion rate (Figure 5- 34 or 5-35) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [[4]×(5)×(6)] (ft <sup>3</sup> /yr)	Erosion Rate {[(7)/27] × 1.3 / (5)}
0+00 - 0+16							
1. LB	High	Low	0.25042	16.0	1.5	6.01	0.01809
0+00 - 0+16							
2. RB	Very High	Very Low	0.16522	16.0	1.8	4.76	0.01432
0+16 - 0+30							
3. LB	Very High	Moderate	0.37957	14.0	1.5	7.97	0.02741
0+16 -							
4. 0+110 RB	Very High	Low	0.25042	94.0	1.0	23.54	0.01206
0+30 - 0+95							
5. LB	High	Moderate	0.37957	65.0	1.5	37.01	0.02741
110 - 160							
6. RB	Very High	High	0.57533	50.0	1.2	34.52	0.03324
0+95 - 117							
7. LB	Moderate	Low	0.15287	22.0	1.5	5.04	0.01104
8 117-140 LB	High	High	0.57533	23.0	1.3	17.20	0.03601
9 140 - 160 LB	Very High	High	0.57533	20.0	1.8	20.71	0.04986
10							
11							
12							
13							
14							
15							
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					Total Erosion (ft <sup>3</sup> /yr)	156.77	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					Total Erosion (yds <sup>3</sup> /yr)	5.81	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					Total Erosion (tons/yr)	7.55	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					Total Erosion (tons/yr/ft)	0.0472	

Streambank Erosion Map



## FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Equation Type		Equation Source		Equation		Bankfull Discharge (cfs)		Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)				
1. Bedload Sediment		"Good/Fair" Pagosa		$y = -0.0113x + 1.0139x^{2.1929}$		47.64		0.0182		31.70				
2. Suspended Sediment		"Good/Fair" Pagosa		$y = 0.0636 + 0.9326x^{2.4085}$										
From Dimensional Flow-Duration Curve														
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)			
Percentage of Time	Daily Mean Discharge (cfs)	Mid-Ordinate (percent)	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow (cfs)	Dimensionless Streamflow ( $Q/Q_{b,d}$ )	Dimensionless Suspended Sediment Discharge ( $S/S_{b,d}$ )	Suspended Sediment Discharge (tons/day)	Dimensionless Bedload Discharge ( $b_j/b_{b,d}$ )	Bedload Sediment Discharge (tons/day)	Time Adjusted Streamflow [(5)×(6)] (cfs)			
(%)	(cfs)	(%)	(%)	(days)	(cfs)	( $Q/Q_{b,d}$ )	( $S/S_{b,d}$ )	(tons/day)	( $b_j/b_{b,d}$ )	(tons/day)	(cfs)			
0%	121.1													
0.10%	104.0	0.05%	0.09%	0.34	112.6	2.363	7.461	71.89	6.670	11.59	38.6			
0.25%	90.0	0.08%	0.15%	0.55	97.0	2.036	5.232	43.43	4.809	8.35	53.1			
0.50%	77.8	0.13%	0.25%	0.91	83.9	1.761	3.706	26.61	3.494	6.07	76.5			
0.75%	66.4	0.13%	0.25%	0.91	72.1	1.513	2.592	15.99	2.502	4.35	65.8			
1%	57.4	0.13%	0.25%	0.91	61.9	1.300	1.817	9.63	1.790	3.11	56.5			
1.5%	49.3	0.25%	0.50%	1.83	53.4	1.120	1.289	5.89	1.289	2.24	97.4			
2%	41.1	0.25%	0.50%	1.83	45.2	0.949	0.886	3.43	0.893	1.55	82.5			
3%	34.6	0.50%	1.00%	3.65	37.9	0.795	0.600	1.95	0.602	1.05	138.2			
4%	29.6	0.50%	1.00%	3.65	32.1	0.674	0.424	1.17	0.415	0.72	117.2			
5%	26.3	0.50%	1.00%	3.65	28.0	0.587	0.322	0.77	0.304	0.53	102.1			
10%	16.6	2.50%	5.00%	18.25	21.4	0.450	0.200	0.37	0.165	0.29	391.4			
20%	9.0	5.00%	10.00%	36.50	12.8	0.269	0.103	0.11	0.045	0.08	466.9			
30%	6.0	5.00%	10.00%	36.50	7.5	0.158	0.075	0.05	0.006	0.01	274.6			
40%	4.3	5.00%	10.00%	36.50	5.1	0.108	0.068	0.03	0.000	0.00	187.7			
50%	3.3	5.00%	10.00%	36.50	3.8	0.079	0.066	0.02	0.000	0.00	137.3			
60%	2.5	5.00%	10.00%	36.50	2.9	0.061	0.065	0.02	0.000	0.00	105.3			
70%	2.0	5.00%	10.00%	36.50	2.3	0.047	0.064	0.01	0.000	0.00	82.4			
80%	1.8	5.00%	10.00%	36.50	1.9	0.039	0.064	0.01	0.000	0.00	68.7			
90%	1.3	5.00%	10.00%	36.50	1.5	0.032	0.064	0.01	0.000	0.00	54.9			
100%	0.3	5.00%	10.00%	36.50	0.8	0.016	0.064	0.00	0.000	0.00	27.5			
<b>Annual Totals:</b>											2,624.6 (cfs)	143.6 (tons/yr)	44.7 (tons/yr)	188.3 (tons/yr)
<b>Annual Totals:</b>											5,205.8 (acre-ft)			

Worksheet 19b. Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Equation Type		Equation Source				Equation		Bankfull Discharge (cfs)			Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)	
1. Bedload Sediment		"Poor" Pagosa				$y = 0.07176 + 1.02176x^{2.3772}$		47.64			0.4699		223.46	
2. Suspended Sediment		"Poor" Pagosa				$y = 0.0989 + 0.9213x^{3.659}$								
		From Dimensional Flow-Duration Curve				From Sediment Rating Curves				Calculate		Calculate Sediment Yield		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Percentage of Time	Daily Mean Discharge	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimension-less Streamflow	Dimension-less Suspended Sediment Discharge	Suspended Sediment Discharge	Dimension-less Bedload Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow	Suspended Sediment	Bedload Sediment	Suspended + Bedload Sediment
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>50</sub> )	(S/S <sub>50</sub> )	(tons/day)	(b <sub>y</sub> /b <sub>50</sub> )	(tons/day)	(cfs)	(tons)	(tons)	(tons)
0%	154.7													
0.10%	137.6	0.05%	0.09%	0.34	146.2	3.068	55.803	4921.27	14.753	660.40	50.1	1688.49	226.58	1915.07
0.25%	123.6	0.08%	0.15%	0.55	130.6	2.741	36.984	2914.12	11.303	505.99	71.5	1595.48	277.03	1872.51
0.50%	111.4	0.13%	0.25%	0.91	117.5	2.466	25.143	1782.14	8.805	394.17	107.2	1626.21	359.68	1985.88
0.75%	100.0	0.13%	0.25%	0.91	105.7	2.218	17.100	1090.35	6.862	307.19	96.4	994.95	280.31	1275.26
1%	91.0	0.13%	0.25%	0.91	95.5	2.005	11.845	682.66	5.412	242.27	87.2	622.93	221.07	844.00
1.5%	82.4	0.25%	0.50%	1.83	86.7	1.820	8.349	436.86	4.317	193.24	158.3	797.27	352.65	1149.92
2%	73.8	0.25%	0.50%	1.83	78.1	1.639	5.722	269.63	3.381	151.34	142.5	492.07	276.20	768.27
3%	67.3	0.50%	1.00%	3.65	70.5	1.480	3.970	168.95	2.668	119.45	257.4	616.66	435.98	1052.64
4%	59.6	0.50%	1.00%	3.65	63.4	1.331	2.725	104.29	2.090	93.54	231.5	380.65	341.43	722.08
5%	52.7	0.50%	1.00%	3.65	56.2	1.179	1.781	60.35	1.583	70.84	205.0	220.26	258.57	478.83
10%	32.9	2.50%	5.00%	18.25	42.8	0.898	0.722	18.64	0.864	38.67	781.2	340.10	705.80	1045.90
20%	11.9	5.00%	10.00%	36.50	22.4	0.470	0.157	2.12	0.241	10.80	816.8	77.35	394.30	471.65
30%	6.2	5.00%	10.00%	36.50	9.0	0.190	0.101	0.55	0.091	4.09	330.1	20.12	149.39	169.51
40%	4.3	5.00%	10.00%	36.50	5.2	0.110	0.099	0.31	0.077	3.45	191.1	11.44	126.02	137.46
50%	3.3	5.00%	10.00%	36.50	3.8	0.079	0.099	0.22	0.074	3.32	137.3	8.20	121.25	129.45
60%	2.5	5.00%	10.00%	36.50	2.9	0.061	0.099	0.17	0.073	3.27	105.3	6.28	119.37	125.66
70%	2.0	5.00%	10.00%	36.50	2.3	0.047	0.099	0.13	0.072	3.24	82.4	4.92	118.44	123.35
80%	1.8	5.00%	10.00%	36.50	1.9	0.039	0.099	0.11	0.072	3.23	68.7	4.10	118.02	122.12
90%	1.3	5.00%	10.00%	36.50	1.5	0.032	0.099	0.09	0.072	3.22	54.9	3.28	117.70	120.98
100%	0.3	5.00%	10.00%	36.50	0.8	0.016	0.099	0.04	0.072	3.21	27.5	1.64	117.34	118.98
<b>Annual Totals:</b>											4,002.5 (cfs)	9,512.4 (tons/yr)	5,117.1 (tons/yr)	14,629.5 (tons/yr)

# POWERSED Model – Sediment Transport Capacity

**Worksheet 20a.** Sediment transport prediction representing the upstream supply up to bankfull for bedload and suspended sand sediment.

Stream: Trail Creek, Upstream Existing Sediment Supply		Location: Pike National Forest, Colorado (Used "POOR" Curves)		Gage Station #: Used Post-Fire Dimensionless F-D C.		Date: 08/27/10												
Observers: S=0.14, Q=48, 38, Bed.=1.0337, S.Sand=111.73		Stream Type: C4		Valley Type: VIII		Used Post-Fire Dimensionless F-D C.												
Hydraulic geometry				Calculate														
Calculate		Measure																
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	
Percentage of time	Daily mean discharge	Mic-ordinate stream-flow	Area	Width	Depth	Velocity	Slope	Shear stress	Stream power	Unit power	Time increment	Time increment	Daily mean bedload transport	Daily mean suspended sand transport	Time adjusted bedload transport	Time adjusted suspended sand transport	Time adjusted total transport	Time adjusted total transport
(%)	(cfs)	(cfs)	(ft <sup>2</sup> )	(ft)	(ft)	(ft/s)	(ft/ft)	(lb/ft <sup>2</sup> )	(lb/s)	(lb/ft/s)	(%)	(days)	(tons/day)	(tons/day)	(tons)	(tons)	(tons)	(tons)
100.00%	0.25										0%				0.00	0.00	0.00	0.00
90.00%	1.26	0.76	0.77	5.15	0.15	0.98	0.0140	0.13	0.66	0.13	10%	36.50	3.20	0.02	116.80	0.73	117.53	117.53
80.00%	1.76	1.51	1.25	6.17	0.20	1.19	0.0140	0.18	1.32	0.21	10%	36.50	3.20	0.05	116.80	1.83	118.63	118.63
70.00%	2.01	1.89	1.47	6.55	0.22	1.27	0.0140	0.19	1.65	0.25	10%	36.50	3.24	0.06	118.26	2.19	120.45	120.45
60.00%	2.52	2.27	1.67	6.88	0.24	1.34	0.0140	0.21	1.98	0.29	10%	36.50	3.24	0.07	118.26	2.56	120.82	120.82
50.00%	3.27	2.90	2.00	7.41	0.27	1.45	0.0140	0.23	2.53	0.34	10%	36.50	3.28	0.09	119.72	3.28	123.00	123.00
40.00%	4.28	3.78	2.41	7.93	0.30	1.55	0.0140	0.26	3.30	0.42	10%	36.50	3.33	0.11	121.55	4.01	125.56	125.56
30.00%	6.23	5.26	3.05	8.72	0.35	1.71	0.0140	0.30	4.60	0.53	10%	36.50	3.46	0.16	126.29	5.84	132.13	132.13
20.00%	11.91	9.07	4.54	10.32	0.44	1.99	0.0140	0.38	7.92	0.77	10%	36.50	4.06	0.28	148.19	10.22	158.41	158.41
10.00%	32.94	22.43	8.32	11.88	0.70	2.69	0.0140	0.59	19.59	1.65	10%	36.50	10.67	1.05	389.45	38.33	427.78	427.78
5.00%	52.81	42.88	12.90	13.23	0.98	3.32	0.0140	0.82	37.46	2.83	5%	18.25	38.10	9.17	695.33	167.35	862.68	862.68
4.00%	59.69	56.25																
3.00%	67.38	63.54																
2.00%	73.93	70.66																
1.50%	82.58	78.26																
1.00%	91.23	86.91																
0.75%	100.22	95.73																
0.50%	111.62	105.92																
0.25%	123.90	117.76																
0.10%	137.93	130.92																
0.0060%	155.15	146.54																
Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr):														2070.7	236.3	2307.0		

**Worksheet 20b.** Sediment transport prediction for the existing condition reach compared to the upstream sediment supply to assess bed stability.

Stream: Trail Creek, C4 Poor, Riffle XS 0+22.7		Location: Pike National Forest, Colorado (Used "POOR" Curves)		Date: 08/27/10													
Observers: S=.014, Q=48, 38, Bed.=1.0337, S.Sand=111.73		Stream Type: C4		Gage Station #: Used Post-Fire Dimensionless F-D C.													
Valley Type: VIII		Stream Type: C4		Gage Station #: Used Post-Fire Dimensionless F-D C.													
Flow-duration curve			Hydraulic geometry			Measure			Calculate								
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
Percentage of time	Daily mean discharge	Mid-ordinate stream-flow	Area	Width	Depth	Velocity	Slope	Shear stress	Stream power	Unit power	Time increment	Time increment	Daily mean bedload transport	Daily mean suspended sand transport	Time adjusted bedload transport	Time adjusted suspended sand transport	Time adjusted total transport
(%)	(cfs)	(cfs)	(ft <sup>2</sup> )	(ft)	(ft)	(ft/s)	(ft/ft)	(lb/ft <sup>2</sup> )	(lb/s)	(lb/ft/s)	(%)	(days)	(tons/day)	(tons/day)	(tons)	(tons)	(tons)
100.00%	0.25										0%				0.00	0.00	0.00
90.00%	1.26	0.76	0.54	4.60	0.12	1.36	0.0140	0.10	0.66	0.14	10%	36.50	3.20	0.02	116.80	0.73	117.53
80.00%	1.76	1.51	0.91	5.79	0.16	1.63	0.0140	0.13	1.32	0.23	10%	36.50	3.20	0.05	116.80	1.83	118.63
70.00%	2.01	1.89	1.09	6.45	0.17	1.73	0.0140	0.14	1.65	0.26	10%	36.50	3.24	0.06	118.26	2.19	120.45
60.00%	2.52	2.27	1.27	7.18	0.18	1.77	0.0140	0.15	1.98	0.28	10%	36.50	3.24	0.07	118.26	2.56	120.82
50.00%	3.27	2.90	1.57	8.39	0.19	1.84	0.0140	0.16	2.53	0.30	10%	36.50	3.24	0.09	118.26	3.28	121.54
40.00%	4.28	3.78	1.91	9.38	0.20	1.95	0.0140	0.17	3.30	0.35	10%	36.50	3.28	0.11	119.72	4.01	123.73
30.00%	6.23	5.26	2.40	10.04	0.24	2.15	0.0140	0.20	4.60	0.46	10%	36.50	3.37	0.16	123.01	5.84	128.85
20.00%	11.91	9.07	3.49	11.13	0.31	2.57	0.0140	0.26	7.92	0.71	10%	36.50	3.89	0.28	141.99	10.22	152.21
10.00%	32.94	22.43	7.22	17.24	0.42	3.10	0.0140	0.35	19.59	1.14	10%	36.50	6.83	0.84	249.30	30.66	279.96
5.00%	52.81	42.88	12.75	27.51	0.46	3.35	0.0140	0.39	37.46	1.36	5%	18.25	8.51	1.78	155.31	32.48	187.79
4.00%	59.69	56.25															
3.00%	67.38	63.54															
2.00%	73.93	70.66															
1.50%	82.58	78.26															
1.00%	91.23	86.91															
0.75%	100.22	95.73															
0.50%	111.62	105.92															
0.25%	123.90	117.76															
0.10%	137.93	130.92															
0.0060%	155.15	146.54															

Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr):		1377.7
Upstream total annual sediment supply (tons/yr) (Worksheet 5-20a):		2070.7
Difference in sediment transport capacity (tons/yr) (+ or -):		-693.0
Stability evaluation: Aggradation, Degradation or Stable:		Aggradation, > 35% Reduction in Transport

Notes:



## Sediment Competence/Entrainment

Worksheet 5-22. Sediment competence calculations.

Stream: <b>Trail Creek, C4 Poor Reach</b>		Stream Type: <b>C4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>L. Chavez et al.</b>		Date: <b>8/18/2010</b>			
<b>Enter Required Information for Existing Condition</b>					
7.2	$D_{50}$	Riffle bed material $D_{50}$ (mm)			
4.2	$\hat{D}_{50}$	Bar sample $D_{50}$ (mm)			
0.36	$D_{max}$	Largest particle from bar sample (ft)	110	(mm)	304.8 mm/ft
0.014	S	Existing bankfull water surface slope (ft/ft)			
0.48	d	Existing bankfull mean depth (ft)			
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment			
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>					
1.71	$D_{50}/\hat{D}_{50}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 ( D_{50}/\hat{D}_{50} )^{-0.872}$		
15.28	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 ( D_{max}/D_{50} )^{-0.887}$		
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED:		
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	d	Required bankfull mean depth (ft)	$d = \frac{\tau^*(\gamma_s - 1)D_{max}}{S}$ (use $D_{max}$ in ft)		
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	S	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^*(\gamma_s - 1)D_{max}}{d}$ (use $D_{max}$ in ft)		
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					
<b>Sediment Competence Using Dimensional Shear Stress</b>					
0.419	Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d) $\gamma = 62.4$ , d = existing depth, S = existing slope				
Shields	CO	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ (Figure 5-49)			
30	80				
Shields	CO	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) (Figure 5-49)			
1.6	0.66				
Shields	CO	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm)			
1.83	0.76	$d = \frac{\tau}{\gamma S}$ $\tau$ = predicted shear stress, $\gamma = 62.4$ , S = existing slope			
Shields	CO	Predicted slope required to initiate movement of measured $D_{max}$ (mm)			
0.0534	0.0220	$S = \frac{\tau}{\gamma d}$ $\tau$ = predicted shear stress, $\gamma = 62.4$ , d = existing depth			
Check: <input type="checkbox"/> Stable <input checked="" type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					

## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>Trail Creek, C4 Poor Reach</b>	Stream Type: <b>C4</b>
Location: <b>Pike National Forest, CO</b>	Valley Type: <b>VIII</b>
Observers: <b>L. Chavez et al.</b>	Date: <b>8/18/2010</b>
<b>Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)</b>	<b>Stability Rating (Check Appropriate Rating)</b>
Stream Type at potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	<input type="checkbox"/> Stable
(E→C), ( <b>C→High W/d C</b> )	<input checked="" type="checkbox"/> Moderately Unstable
(G→F), (F→D), (C→F)	<input type="checkbox"/> Unstable
(C→D), (B→G), (D→G), (C→G), (E→G)	<input type="checkbox"/> Highly Unstable

Worksheet 5-25. Lateral stability.

Stream: <b>Trail Creek, C4 Poor Reach</b>		Stream Type: <b>C4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>L. Chavez et al.</b>		Date: <b>8/18/2010</b>			
Lateral stability criteria (choose one stability category for each criterion 1–5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	8
	(2)	(4)	(6)	4.4 (8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	2
	(1)	B1, B2, B4 (2)	(3)	(4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		1
	M3 (1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	6
	(2)	(4)	VH/M, VH/H (6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	2
	(1)	0.31 (2)	(3)	(4)	
<b>Total Points</b>					<b>19</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input type="checkbox"/>	<i>Unstable</i> 13 – 21 <input checked="" type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	

**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>Trail Creek, C4 Poor Reach</b>		Stream Type: <b>C4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>L. Chavez et al.</b>		Date: <b>8/18/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
1 <b>Sediment competence</b> (Worksheet 5-22)	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope—slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	6
	(2)	(4)	(6)	(8)	
2 <b>Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	8
	(2)	(4)	(6)	(8)	
3 <b>W/d Ratio State</b> (Worksheet 5-13)	1.0 – 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	8
	(2)	(4)	(6)	4.4 (8)	
4 <b>Stream Succession States</b> (Worksheet 5-24)	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	6
	(2)	(4)	(6)	(8)	
5 <b>Depositional Patterns</b> (Worksheet 5-10)	B1	B2, B4	B3, B5	B6, B7, B8	2
	(1)	B1, B2, B4 (2)	(3)	(4)	
6 <b>Debris / Blockages</b> (Worksheet 5-11)	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	1
	D2 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>31</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
Vertical Stability for Excess Deposition / Aggradation (use total points and check stability rating)	<i>No Deposition</i> 10 – 14 <input type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input type="checkbox"/>	<i>Aggradation</i> > 30 <input checked="" type="checkbox"/>	

Worksheet 5-27. Vertical stability – degradation.

Stream: <b>Trail Creek, C4 Poor Reach</b>		Stream Type: <b>C4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>L. Chavez et al.</b>		Date: <b>8/18/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>1 Sediment Competence (Worksheet 5-22)</b>	Does not indicate excess competence	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed	$D_{100}$ of bed moved	Particles much larger than $D_{100}$ of bed moved	<b>2</b>
	<b>Insufficient (2)</b>	<b>(4)</b>	<b>(6)</b>	<b>(8)</b>	
<b>2 Sediment Capacity (POWERSED) (Worksheet 5-20)</b>	Does not indicate excess capacity	Slight excess energy: up to 10% increase above reference	Excess energy sufficient to increase load up to 50% of annual load	Excess energy transporting more than 50% of annual load	<b>2</b>
	<b>Insufficient (2)</b>	<b>(4)</b>	<b>(6)</b>	<b>(8)</b>	
<b>3 Degree of Channel Incision (BHR) (Worksheet 5-12)</b>	1.00 – 1.10	1.11 – 1.30	1.31 – 1.50	> 1.50	<b>2</b>
	<b>1.00 (2)</b>	<b>(4)</b>	<b>(6)</b>	<b>(8)</b>	
<b>4 Stream Succession States (Worksheets 5-12 and 5-24)</b>	Does not indicate incision or degradation	If BHR > 1.1 and stream type has W/d between 5–10	If BHR > 1.1 and stream type has W/d less than 5	(B→G), (C→G), (E→G), (D→G)	<b>2</b>
	<b>(2)</b>	<b>(4)</b>	<b>(6)</b>	<b>(8)</b>	
<b>5 Confinement (MWR / MWR<sub>ref</sub>) (Worksheet 5-14)</b>	0.80 – 1.00	0.30 – 0.79	0.10 – 0.29	< 0.10	<b>2</b>
	<b>(1)</b>	<b>0.32 (2)</b>	<b>(3)</b>	<b>(4)</b>	
<b>Total Points</b>					<b>10</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation (use total points and check stability rating)</b>	<b>Not Incised</b> 9 – 11 <input checked="" type="checkbox"/>	<b>Slightly Incised</b> 12 – 18 <input type="checkbox"/>	<b>Moderately Incised</b> 19 – 27 <input type="checkbox"/>	<b>Degradation</b> > 27 <input type="checkbox"/>	

**Worksheet 5-28.** Channel enlargement.

Stream: <b>Trail Creek, C4 Poor Reach</b>		Stream Type: <b>C4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>L. Chavez et al.</b>		Date: <b>8/18/2010</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1-4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	4
	(2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	6
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	8
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	2
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>20</b>
<b>Category Point Range</b>					
<b>Channel Enlargement Prediction (use total points and check stability rating)</b>	<b>No Increase</b> 8 – 10 <input type="checkbox"/>	<b>Slight Increase</b> 11 – 16 <input type="checkbox"/>	<b>Moderate Increase</b> 17 – 24 <input checked="" type="checkbox"/>	<b>Extensive</b> > 24 <input type="checkbox"/>	

Worksheet 5-29. Overall sediment supply.

Stream: <b>Trail Creek, C4 Poor Reach</b>		Stream Type: <b>C4</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>		
Observers: <b>L. Chavez et al.</b>		Date: <b>8/18/2010</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1-5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	3	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	4	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	1	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	3	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	4	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>15</b>	
<b>Category Point Range</b>				
Overall Sediment Supply Rating (use total points and check stability rating)	<b>Low</b> 5 <input type="checkbox"/>	<b>Moderate</b> 6 – 10 <input type="checkbox"/>	<b>High</b> 11 – 15 <input checked="" type="checkbox"/>	<b>Very High</b> 16 – 20 <input type="checkbox"/>

Worksheet 5-32. Summary of stability condition categories.

Stream: <b>Trail Creek, C4 Poor Reach</b>		Location: <b>Pike National Forest, Colorado</b>	
Observers: <b>L. Chavez et al.</b>		Date: <b>8/18/2010</b>	Stream Type: <b>C4</b> Valley Type: <b>VIII</b>
<b>Channel Dimension (Riffle XS 0+22.7)</b>	Mean Bankfull Depth (ft): <b>0.48</b>	Bankfull Width (ft): <b>29.02</b>	Cross-Sectional Area (ft <sup>2</sup> ): <b>13.95</b> Width of Flood-Prone Area (ft): <b>59</b> Entrenchment Ratio: <b>2.03</b>
<b>Channel Pattern</b>	Mean: $\lambda W_{bkr}$ Range: $\lambda W_{bkr}$	$L_m W_{bkr}$ : <b>1.18</b> $R_c W_{bkr}$ : <b>0.67-1.91</b>	MWR: <b>1.38</b> Sinuosity: <b>1.08</b>
<b>River Profile &amp; Bed Features</b>	<input checked="" type="checkbox"/> Riffle/Pool <input type="checkbox"/> Step/Pool <input type="checkbox"/> Plane Bed <input type="checkbox"/> Convergence/Divergence <input type="checkbox"/> Dunes/Antidunes/Smooth Bed Max Bankfull Depth (ft): <b>1.56</b> Riffle Pool Depth Ratio (max to mean): <b>1.77</b> Riffle Pool Spacing: <b>3.25</b> Pool Spacing: <b>3.69</b> Pool Ratio: <b>1.15</b> Valley: <b>0.0148</b> Water Surface: <b>0.014</b>	Remarks: Condition, Vigor & Usage of Existing Reach:	
<b>Level III Stream Stability Indices</b>	Riparian Vegetation: <b>Spruce, Willow, Shrubs, Grass</b> Potential Composition/Density: <b>Higher Density w/o Invasives</b> <b>Banks - grasses/fescue; eradicate invasives</b> Flow Regime: <b>P2, P8</b> Stream Size & Order: <b>S-4(4)</b> Meander Patterns: <b>M3</b> Depositional Patterns: <b>B1, B2, B4</b> Debris/Channel Blockages: <b>D2</b> Degree of Incision (Bank-Height Ratio): <b>1.0</b> Degree of Incision Stability Rating: <b>Stable</b> Modified Pfankuch Stability Rating (Numeric & Adjective Rating): <b>133 (Poor)</b>	Remarks: <b>&gt; 30% Reduction in Transport</b>	
<b>Bank Erosion Summary</b>	Width/depth Ratio (W/d): <b>60</b> Reference W/d Ratio (W/d <sub>ref</sub> ): <b>13.7</b> Width/Depth Ratio State (W/d) / (W/d <sub>ref</sub> ): <b>4.38</b> W/d Ratio State Stability Rating: <b>Highly Unstable</b> Meander Width Ratio (MWR): <b>1.4</b> Reference MWR <sub>ref</sub> : <b>4.5</b> Degree of confinement (MWR / MWR <sub>ref</sub> ): <b>0.31</b> MWR / MWR <sub>ref</sub> Stability Rating: <b>Moderately Confined</b> Length of Reach Studied (ft): <b>160</b> Annual Streambank Erosion Rate: <b>7.55</b> (tons/yr) Curve Used: <b>Colorado</b> Remarks: <b>Not fully recovered, see NBS - unveg banks</b>	Remarks: <b>&gt; 30% Reduction in Transport</b>	
<b>Sediment Capacity (POWERSED)</b>	<input type="checkbox"/> Sufficient Capacity <input checked="" type="checkbox"/> Insufficient Capacity <input type="checkbox"/> Excess Capacity	Remarks: <b>&gt; 30% Reduction in Transport</b>	
<b>Entrainment/Competence</b>	Largest Particle from Bar Sample (mm): <b>110</b> $\tau =$ <b>0.419</b> $\tau^* =$ <b>N/A</b> Existing Depth: <b>0.48</b> Required Depth: <b>0.76</b> Existing Slope: <b>0.014</b> Required Slope: <b>0.022</b>	Remarks: <b>&gt; 30% Reduction in Transport</b>	
<b>Successional Stage Shift</b>	<b>C</b> → <b>D</b> → <b>G</b> → <b>F</b> → <b>C</b> → <b>C4</b> Existing Stream State (Type): <b>C4</b> Potential Stream State (Type): <b>C4</b>	Remarks: <b>&gt; 30% Reduction in Transport</b>	
<b>Lateral Stability</b>	<input type="checkbox"/> Stable <input type="checkbox"/> Mod. Unstable <input checked="" type="checkbox"/> Unstable <input type="checkbox"/> Highly Unstable	Remarks/causes: <b>Hayman Fire - unveg banks</b>	
<b>Vertical Stability (Aggradation)</b>	<input type="checkbox"/> No Deposition <input type="checkbox"/> Mod. Deposition <input type="checkbox"/> Ex. Deposition <input checked="" type="checkbox"/> Aggradation	Remarks/causes: <b>Pikes Peak granitics, not fully recovered</b>	
<b>Vertical Stability (Degradation)</b>	<input checked="" type="checkbox"/> Not Incised <input type="checkbox"/> Slightly Incised <input type="checkbox"/> Mod. Incised <input type="checkbox"/> Degradation	Remarks/causes: <b>Pikes Peak granitics, not fully recovered</b>	
<b>Channel Enlargement</b>	<input type="checkbox"/> No Increase <input type="checkbox"/> Slight Increase <input checked="" type="checkbox"/> Mod. Increase <input type="checkbox"/> Extensive	Remarks/causes: <b>Pikes Peak granitics, not fully recovered</b>	
<b>Sediment Supply (Channel Source)</b>	<input type="checkbox"/> Low <input type="checkbox"/> Moderate <input checked="" type="checkbox"/> High <input type="checkbox"/> Very High	Remarks/causes: <b>Pikes Peak granitics, not fully recovered</b>	



## *Appendix C8*

# **D4a+ Stream Type** *Poor Stability Reach*



# Table of Contents

## *Appendix C8: D4a+ Reach*

<b>Reach Location &amp; Overview.....</b>	<b>C5-2</b>
<b>Survey Summary.....</b>	<b>C5-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C5-6</b>
<b><i>Velocity, Classification &amp; Morphological Relations.....</i></b>	<b>C5-6</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b><i>Stability Indices.....</i></b>	<b>C5-10</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b><i>BANCS Model – Streambank Erosion.....</i></b>	<b>C5-20</b>
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b><i>FLOWSED Model – Total Annual Sediment Yield.....</i></b>	<b>C5-22</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b><i>POWERSED Model– Sediment Transport Capacity to Assess Bed Stability.....</i></b>	<b>C5-24</b>
Worksheet 5-20a. Sediment transport prediction for the upstream condition.	
Worksheet 5-20b. Sediment transport prediction for the existing condition.	
<b><i>Sediment Competence/Entrainment.....</i></b>	<b>C5-26</b>
Worksheet 5-22. Sediment competence calculations.	
<b><i>Channel Stability Ratings.....</i></b>	<b>C5-27</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b><i>Summary.....</i></b>	<b>C5-33</b>
Worksheet 5-32. Summary of stability condition categories.	

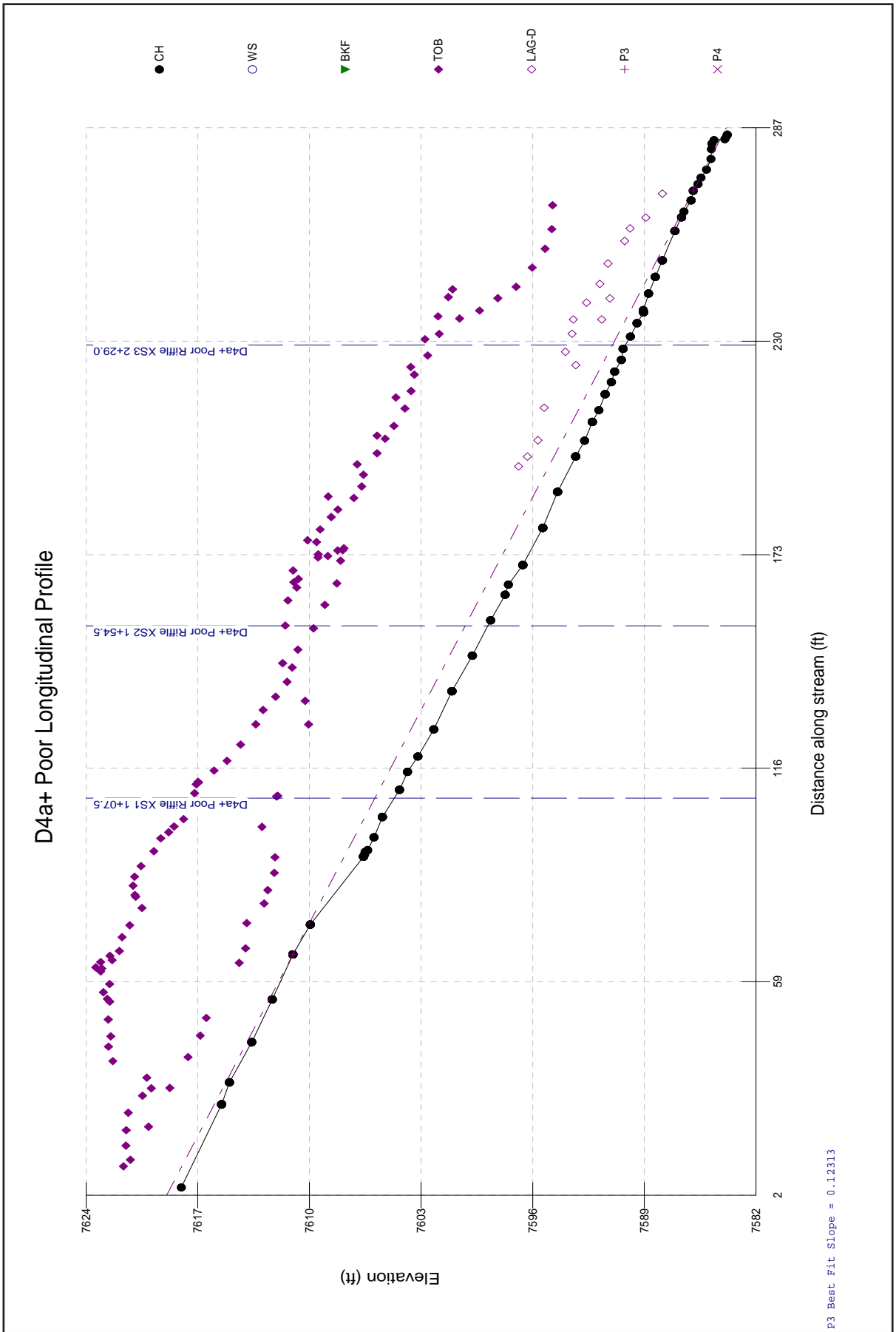
## D4a+ Poor Reach Location & Overview

The D4a+ Poor reach is an ephemeral, 2<sup>nd</sup> order, steep, braided stream located as a main tributary to Trail Creek (see location map **Figure C-2**). The stream is widening and aggrading as the extreme width/depth ratio has led to excess sediment deposition in the channel. The potential stable stream type in this valley fill (Valley Type VIII) is a B4a stream type. The stability rating is “Poor” due to a “Poor” Pfankuch stability rating and the extremely high streambank erosion rate of  $0.7183 \text{ tons/yr/ft}$ . This rate is more than two orders of magnitude higher than the B4 reference rate of  $0.0048 \text{ tons/yr/ft}$ . The POWERSED sediment transport capacity model indicates aggradation. The sediment supply rating is *High* due primarily to the streambank erosion source and increase in stored sediment in the channel bed. This rating indicates a potential accelerated increase in flow-related sediment based on increased post-fire streamflow peak flows compared to the reference B4 condition. The WRENSS model indicates a water yield increase due to the fire of  $59 \text{ acre-ft}$ . Consequently, bedload increased from  $13 \text{ tons/yr}$  to  $144 \text{ tons/yr}$ , and suspended sediment increased from  $0.3 \text{ tons/yr}$  to  $119 \text{ tons/yr}$ , representing a total increase in sediment of  $250 \text{ tons/yr}$ . These are extremely high values for a very small (4 cfs) D4a+ stream type, which reflect the accelerated sediment yield due to flow-related sediment and very high contributions from streambank erosion.

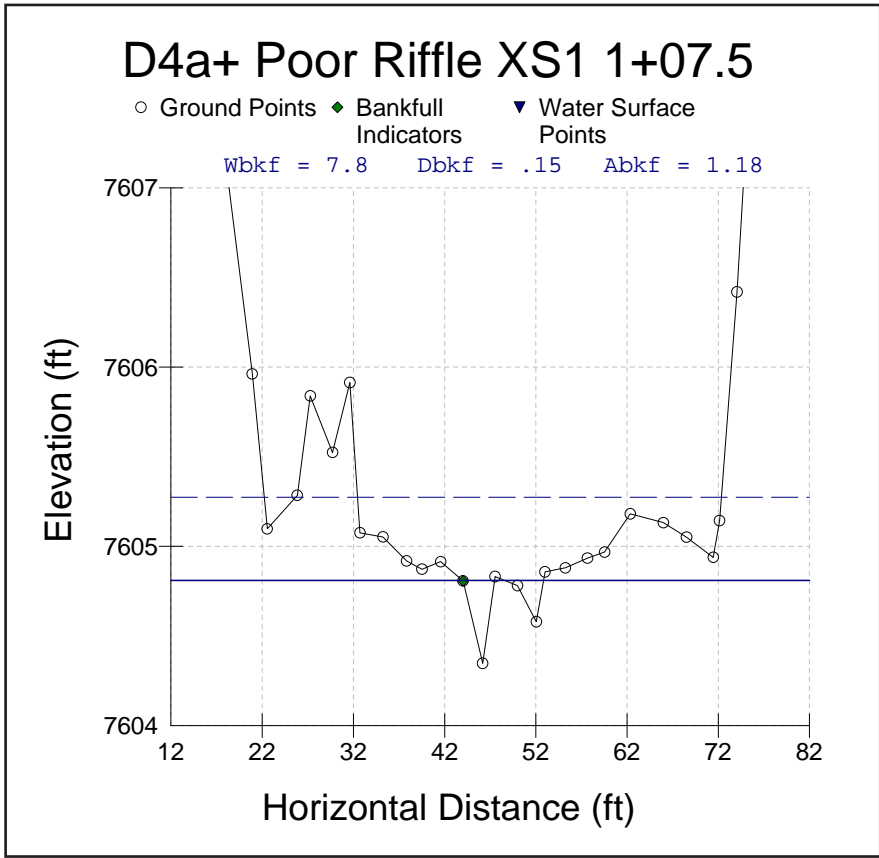
The photograph depicts the typical character of this representative D4a+ Poor stream type. The following graphs and summary worksheets provide the detail of the morphology, hydraulics, streambank erosion rates, and stability conditions responsible for the overall “Poor” rating.



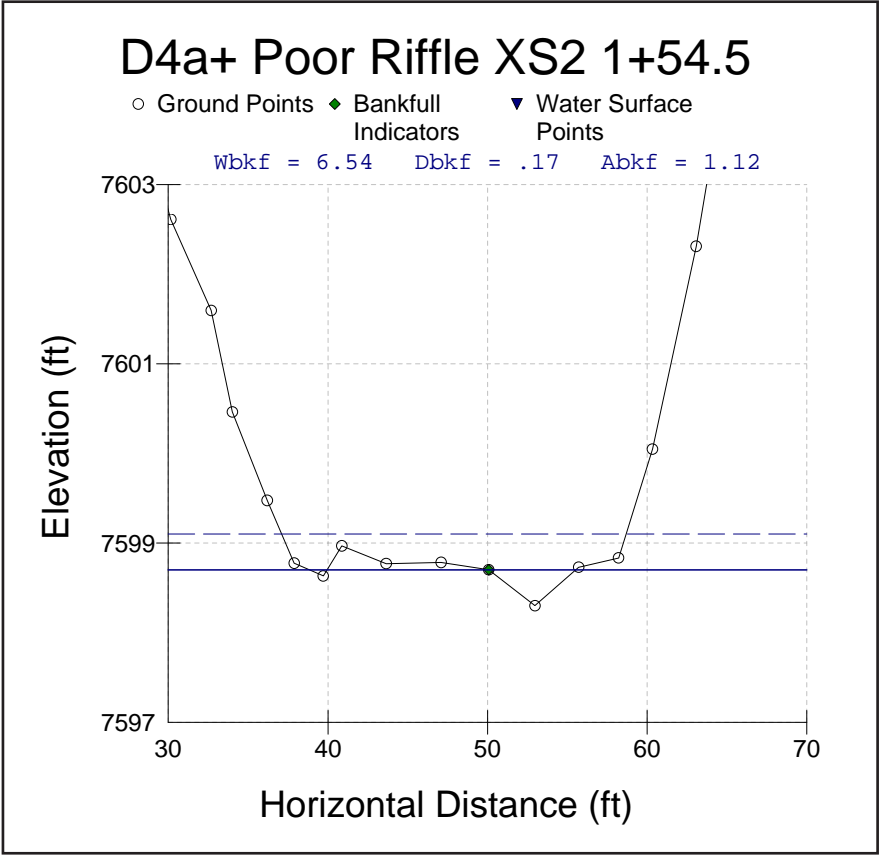
# Survey Summary



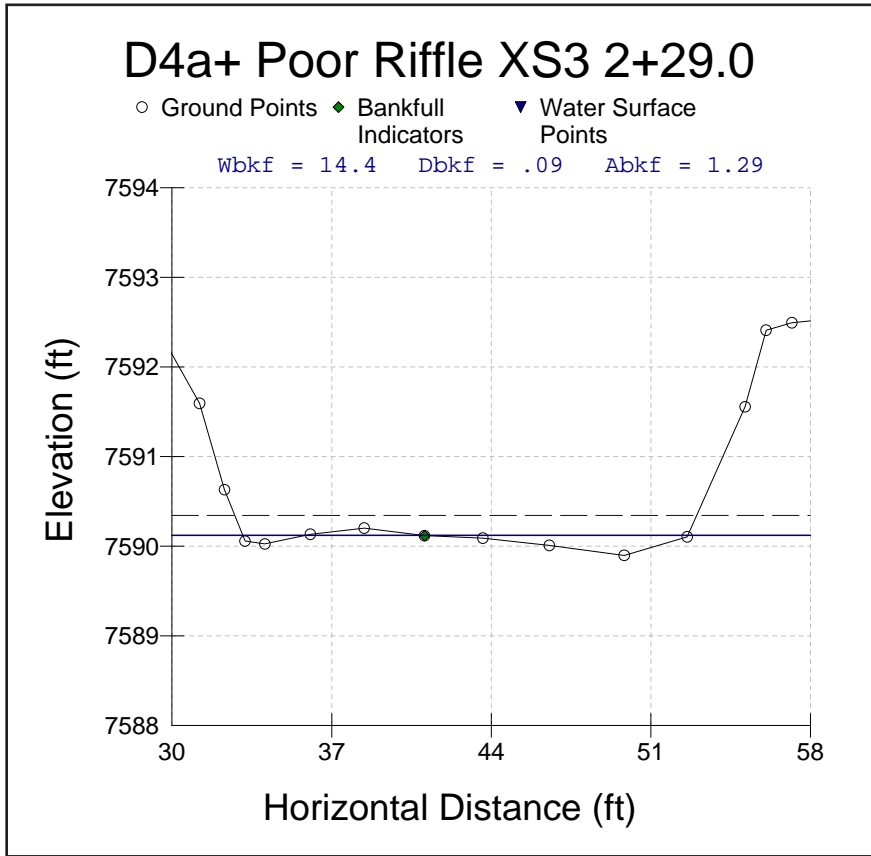
Longitudinal Profile (graph generated from RIVERMorph™)



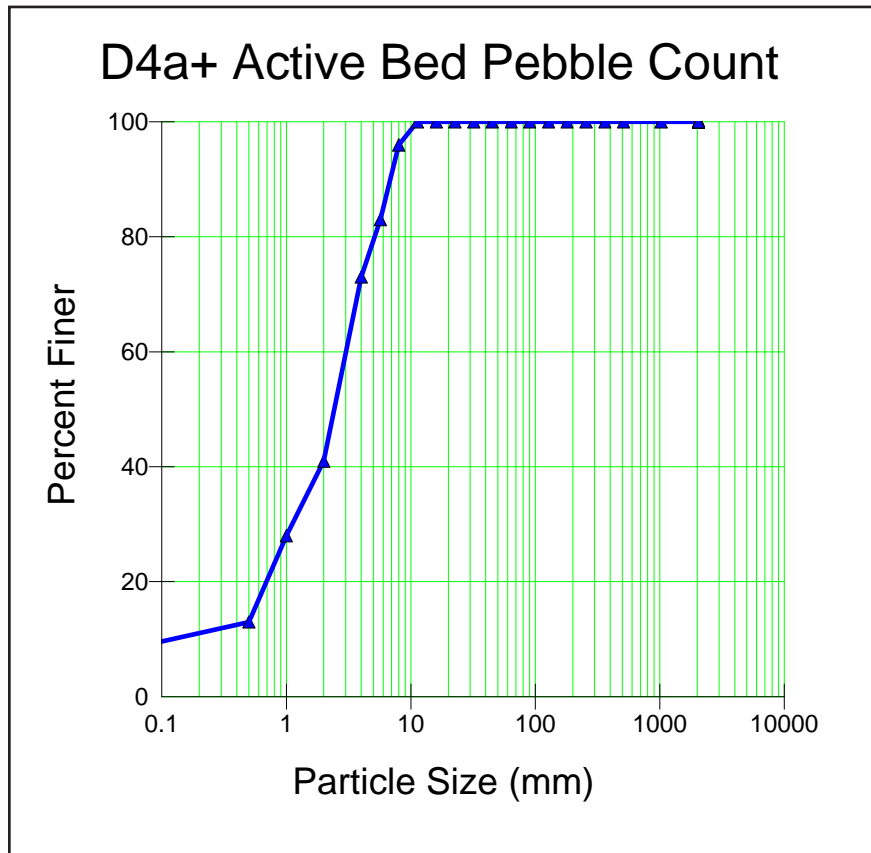
Representative Cross-section 1+07.5 (graph generated from RIVERMorph™)



Cross-section 1+54.5 (graph generated from RIVERMorph™)



Cross-section 2+29 (graph generated from RIVERMorph™)



Active Bed Riffle Pebble Count (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates							
Stream:	Trail Creek Trib., D4a+ Poor			Location:	Riffle XS 1+07.5, Pike N.F., Colorado		
Date:	8/15/2010	Stream Type:	D4a	Valley Type:	VIII		
Observers:	Rosgen et al.			HUC:	-- -- -- -- -- -- -- -- -- --		
INPUT VARIABLES				OUTPUT VARIABLES			
Bankfull Riffle Cross-Sectional AREA	1.18	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.15	$d_{bkf}$ (ft)		
Bankfull Riffle WIDTH	7.8	$W_{bkf}$ (ft)	Wetted PERIMETER ~ (2 * $d_{bkf}$ ) + $W_{bkf}$	8.10	$W_p$ (ft)		
$D_{84}$ at Riffle	5.9	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.02	$D_{84}$ (ft)		
Bankfull SLOPE	0.12	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	0.15	R (ft)		
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R(ft) / $D_{84}$ (ft)	7.53	R / $D_{84}$		
Drainage Area	0.2	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.750	$u^*$ (ft/sec)		
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE	
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$				3.87	ft / sec	4.57	cfs
2. Roughness Coefficient: a) Manning's n from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.043$				3.32	ft / sec	3.92	cfs
2. Roughness Coefficient: b) Manning's n from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n =$ <input type="text"/>					ft / sec		cfs
2. Roughness Coefficient: c) Manning's n from Jarrett (USGS): $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for $n = 0.237$				0.60	ft / sec	0.71	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Limerinos n				4.15	ft / sec	4.9	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Darcy-Weisbach				3.93	ft / sec	4.6	cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q =$ <input type="text"/> year $u = Q / A$					ft / sec		cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation (R/ $D_{84}$ ) – Estimation Method 1							
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.							
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.							
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.							
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.							



Worksheet 5-3. Level II stream classification.

Stream: <b>Trail Creek Trib., D4a+ Poor Reach</b>	
Basin:	Drainage Area: acres <b>0.2</b> mi <sup>2</sup>
Location: <b>Pike National Forest, Colorado</b>	
Twp.&Rge:	Sec.&Qtr.:
Cross-Section Monuments (Lat./Long.): <b>Riffle XS 1+07.5</b>	Date: <b>8/15/2010</b>
Observers: <b>Rosgen et al.</b>	Valley Type: <b>VIII</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>7.8</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A_{bkf} / W_{bkf}$ ).	<b>0.15</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>1.18</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>52</b>	ft/ft
<b>Maximum DEPTH (<math>d_{max}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>0.46</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>43.31</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>5.55</b>	ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the median or dominant diameter of channel materials, as sampled proportionately from the channel surface, between the bankfull stage and Thalweg elevations.	<b>2.56</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.123</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope ( $S_{val} / S$ ).	<b>1.03</b>	

<div style="border: 1px solid black; padding: 5px; display: inline-block;">Stream Type</div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: #e0f0ff;"><b>D4a+</b></div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;">See Classification Key (Figure 2-14)</div>
--	---	---

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek D4a+ Poor Reach</b>				Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>Rosgen et al.</b>		Date: <b>8/15/2010</b>		Valley Type: <b>VIII</b>		Stream Type: <b>D4a</b>			
River Reach Dimension Summary Data.....1									
Riffle Dimensions*, **, ***	Riffle Dimensions***, ***, ***	Mean	Min	Max	Riffle Dimensions & Dimensionless Ratios****	Mean	Min	Max	
	Riffle Width ( $W_{bkt}$ )	9.6	6.5	14.4	ft	Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	1.2	1.1	1.3
	Mean Riffle Depth ( $d_{bkt}$ )	0.14	0.09	0.17	ft	Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	83.5	38.5	159.9
	Maximum Riffle Depth ( $d_{max}$ )	0.36	0.22	0.46	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	2.571	1.571	3.286
	Width of Flood-Prone Area ( $W_{fpa}$ )	28.4	20.3	43.3	ft	Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )	3.4	1.4	5.6
	Riffle Inner Berm Width ( $W_{ib}$ )				ft	Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )			
	Riffle Inner Berm Depth ( $d_{ib}$ )				ft	Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )			
	Riffle Inner Berm Area ( $A_{ib}$ )				ft <sup>2</sup>	Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )			
	Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )								
Pool Dimensions*, **, ***	Pool Dimensions***, ***, ***	Mean	Min	Max	Pool Dimensions & Dimensionless Ratios****	Mean	Min	Max	
	Pool Width ( $W_{bkfp}$ )				ft	Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )			
	Mean Pool Depth ( $d_{bkfp}$ )				ft	Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )			
	Pool Cross-Sectional Area ( $A_{bkfp}$ )				ft	Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )			
	Maximum Pool Depth ( $d_{maxp}$ )				ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )			
	Pool Inner Berm Width ( $W_{ibp}$ )				ft	Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )			
	Pool Inner Berm Depth ( $d_{ibp}$ )				ft	Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )			
	Pool Inner Berm Area ( $A_{ibp}$ )				ft <sup>2</sup>	Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )			
	Point Bar Slope ( $S_{pb}$ )				ft/ft	Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )			
Run Dimensions*	Run Dimensions*	Mean	Min	Max	Run Dimensionless Ratios****	Mean	Min	Max	
	Run Width ( $W_{bkfr}$ )				ft	Run Width to Riffle Width ( $W_{bkfr} / W_{bkt}$ )			
	Mean Run Depth ( $d_{bkfr}$ )				ft	Mean Run Depth to Mean Riffle Depth ( $d_{bkfr} / d_{bkt}$ )			
	Run Cross-Sectional Area ( $A_{bkfr}$ )				ft	Run Area to Riffle Area ( $A_{bkfr} / A_{bkt}$ )			
	Maximum Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )			
Run Width/Depth Ratio ( $W_{bkfr} / d_{bkfr}$ )				ft					
Glide Dimensions*	Glide Dimensions*	Mean	Min	Max	Glide Dimensions & Dimensionless Ratios****	Mean	Min	Max	
	Glide Width ( $W_{bkfg}$ )				ft	Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )			
	Mean Glide Depth ( $d_{bkfg}$ )				ft	Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )			
	Glide Cross-Sectional Area ( $A_{bkfg}$ )				ft	Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )			
	Maximum Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )			
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )				ft/ft	Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )			
	Glide Inner Berm Width ( $W_{ibg}$ )				ft	Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )			
	Glide Inner Berm Depth ( $d_{ibg}$ )				ft	Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )			
Glide Inner Berm Area ( $A_{ibg}$ )				ft <sup>2</sup>	Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )				
Step**	Step Dimensions**	Mean	Min	Max	Step Dimensionless Ratios****	Mean	Min	Max	
	Step Width ( $W_{bkfs}$ )				ft	Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )			
	Mean Step Depth ( $d_{bkfs}$ )				ft	Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )			
	Step Cross-Sectional Area ( $A_{bkfs}$ )				ft	Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )			
	Maximum Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )									

**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek Trib., D4a+ Poor Reach</b>		Location: <b>Pike National Forest, Colorado</b>						
Observers: <b>Rosgen et al.</b>		Date: <b>8/15/2010</b>	Valley Type: <b>VIII</b>					
		Stream Type: <b>D4a</b>						
<b>River Reach Summary Data.....2</b>								
<b>Hydraulics</b>	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )	<b>3.32</b>	ft/sec	Estimation Method	<b>"n" from FF/RR</b>			
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )	<b>3.92</b>	cfs	Drainage Area	<b>0.2</b> mi <sup>2</sup>			
<b>Channel Pattern</b>	<b>Geometry</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Dimensionless Geometry Ratios</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Linear Wavelength ( $\lambda$ )			ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )			
	Stream Meander Length ( $L_m$ )			ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )			
	Radius of Curvature ( $R_c$ )			ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )			
	Belt Width ( $W_{bit}$ )			ft	Meander Width Ratio ( $W_{bit} / W_{bkt}$ )			
	Arc Length ( $L_a$ )			ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )			
	Riffle Length ( $L_r$ )			ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )			
	Individual Pool Length ( $L_p$ )			ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )			
Pool to Pool Spacing ( $P_s$ )			ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )				
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )	<b>0.1267</b>	ft/ft	Average Water Surface Slope (S)	<b>0.1230</b>	ft/ft	Sinuosity ( $S_{val} / S$ )	<b>1.03</b>
	Stream Length (SL)		ft	Valley Length (VL)		ft	Sinuosity (SL / VL)	
	Low Bank Height (LBH)	start: <b>0.46</b> ft end: <b>0.22</b> ft		Max Bankfull Depth ( $d_{max}$ )	start: <b>0.46</b> ft end: <b>0.22</b> ft		Bank-Height Ratio (BHR) (LBH / $d_{max}$ )	start: <b>1.0</b> end: <b>1.0</b>
	<b>Facet Slopes</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Dimensionless Facet Slope Ratios</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Slope ( $S_{rit}$ )			ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rit} / S$ )			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )			
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )			
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )			
	Step Slope ( $S_s$ )			ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )			
	<b>Max Depths<sup>a</sup></b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Dimensionless Depth Ratios</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Max Riffle Depth ( $d_{max}$ )			ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )			
	Max Run Depth ( $d_{maxr}$ )			ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )			
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )			
	Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )			
	Max Step Depth ( $d_{maxs}$ )			ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
<b>Channel Materials</b>		<b>Reach<sup>b</sup></b>	<b>Riffle<sup>c</sup></b>	<b>Bar</b>	<b>Reach<sup>b</sup></b>	<b>Riffle<sup>c</sup></b>	<b>Bar</b>	<b>Protrusion Height<sup>d</sup></b>
	% Silt/Clay		<b>0</b>		$D_{16}$	<b>0.60</b>		mm
	% Sand		<b>41</b>		$D_{35}$	<b>1.54</b>		mm
	% Gravel		<b>59</b>		$D_{50}$	<b>2.56</b>		mm
	% Cobble		<b>0</b>		$D_{84}$	<b>5.88</b>		mm
	% Boulder		<b>0</b>		$D_{95}$	<b>7.83</b>		mm
	% Bedrock		<b>0</b>		$D_{100}$	<b>11.30</b>		mm

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

## Stability Indices


**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation					
Stream: <b>Trail Creek Trib., D4a+ Poor Reach</b>		Location: <b>Pike National Forest, Colorado</b>			
Observers: <b>Rosgen et al.</b>	Reference reach: <input type="checkbox"/>	Disturbed (impacted reach): <input checked="" type="checkbox"/>	Date: <b>8/16/2010</b>		
Existing species composition: <b>Ponderosa Pine - 5% Burnt, Annual Grass/Forb, Cheatgrass</b>		Potential species composition: <b>Willow, Alder, Grass, Aspen</b>			
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition
<b>1. Overstory</b>	Canopy layer	5%	<1%	<b>Ponderosa Pine</b>	100%
					100%
<b>2. Understory</b>	Shrub layer		0%		
					100%
<b>3. Ground level</b>	Herbaceous		5%	<b>Mullan Cheatgrass</b> <b>Ag Spic</b> <b>Annual grass</b> <b>Forbs</b>	
	Leaf or needle litter		5%	<b>Remarks:</b> Condition, vigor and/or usage of existing reach:	100%
	Bare ground		90%		
*Based on crown closure. **Based on basal area to surface area.			<b>Column total = 100%</b>		

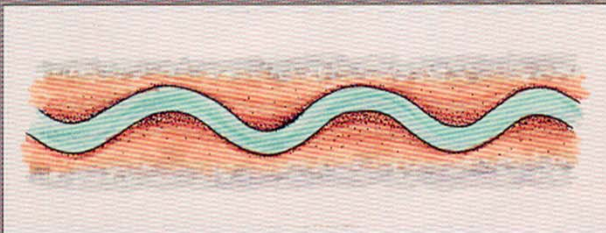



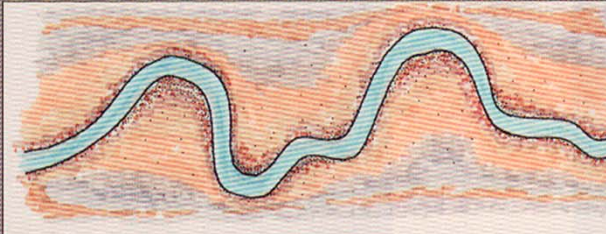
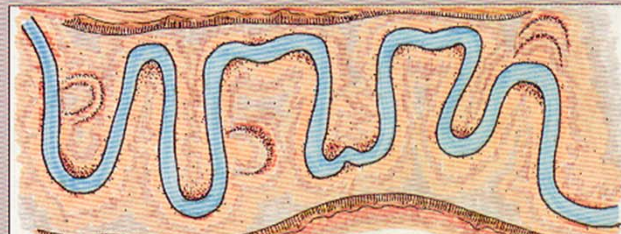
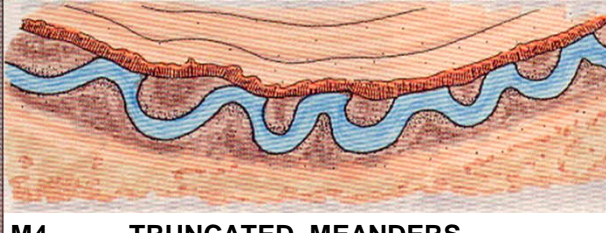
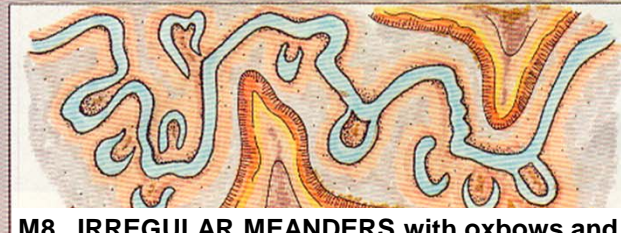
**Worksheet 5-7.** Flow regime.

<b>FLOW REGIME</b>								
Stream: <b>Trail Creek Trib., D4a+ Poor</b>			Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>Rosgen <i>et al.</i></b>						Date: <b>8/16/2010</b>		
<b>List ALL COMBINATIONS that APPLY.....</b>	<b>E2</b>	<b>E8</b>	<b>S2</b>	<b>S8</b>				
<b>General Category</b>								
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation							
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
<b>P</b>	Perennial stream channels: Surface water persists yearlong.							
<b>Specific Category</b>								
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
<b>4</b>	Streamflow regulated by glacial melt.							
<b>5</b>	Ice flows/ice torrents from ice dam breaches.							
<b>6</b>	Alternating flow/backwater due to tidal influence.							
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.							
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
<b>9</b>	Rain-on-snow generated runoff.							

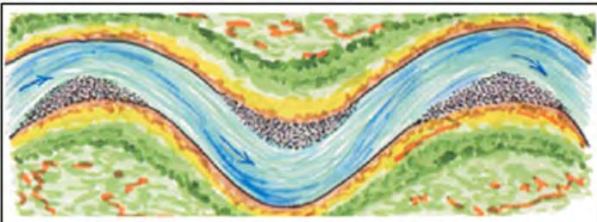


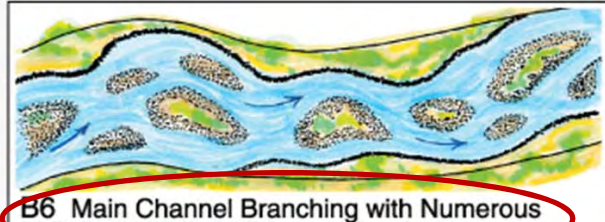
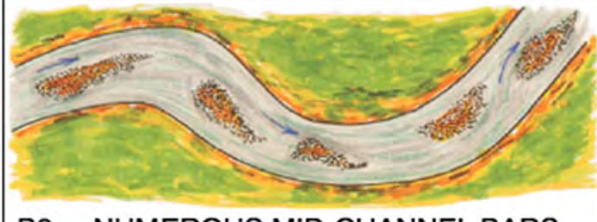



**Worksheet 5-8.** Stream order & stream size.

Stream Size and Order			
Stream:	Trail Creek Trib., D4a+ Poor Reach		
Location:	Pike National Forest, Colorado		
Observers:	Rosgen <i>et al.</i>		
Date:	8/16/2010		
Stream Size Category and Order 			S-3(2)
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0.305	<1	<input type="checkbox"/>
S-2	0.3 – 1.5	1 – 5	<input type="checkbox"/>
<b>S-3</b>	<b>1.5 – 4.6</b>	<b>5 – 15</b>	<input checked="" type="checkbox"/>
S-4	4.6 – 9	15 – 30	<input type="checkbox"/>
S-5	9 – 15	30 – 50	<input type="checkbox"/>
S-6	15 – 22.8	50 – 75	<input type="checkbox"/>
S-7	22.8 – 30.5	75 – 100	<input type="checkbox"/>
S-8	30.5 – 46	100 – 150	<input type="checkbox"/>
S-9	46 – 76	150 – 250	<input type="checkbox"/>
S-10	76 – 107	250 – 350	<input type="checkbox"/>
S-11	107 – 150	350 – 500	<input type="checkbox"/>
S-12	150 – 305	500 – 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
Stream Order			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			

Worksheet 5-9. Meander patterns.

<b>Meander Patterns</b>					
Stream: <b>Trail Creek Trib., D4a+ Poor Reach</b>			Location: <b>Pike National Forest, CO</b>		
Observers: <b>Rosgen et al.</b>			Date: <b>8/16/2010</b>		
List ALL CATEGORIES that APPLY	N/A				
<b>Various Meander Pattern variables modified from Galay et al. (1973)</b>					
 <p><b>M1 REGULAR MEANDERS</b></p>			 <p><b>M5 UNCONFINED MEANDER SCROLLS</b></p>		
 <p><b>M2 TORTUOUS MEANDERS</b></p>			 <p><b>M6 CONFINED MEANDER SCROLLS</b></p>		
 <p><b>M3 IRREGULAR MEANDERS</b></p>			 <p><b>M7 DISTORTED MEANDER LOOPS</b></p>		
 <p><b>M4 TRUNCATED MEANDERS</b></p>			 <p><b>M8 IRREGULAR MEANDERS with oxbows and</b></p>		

**Worksheet 5-10.** Depositional patterns.

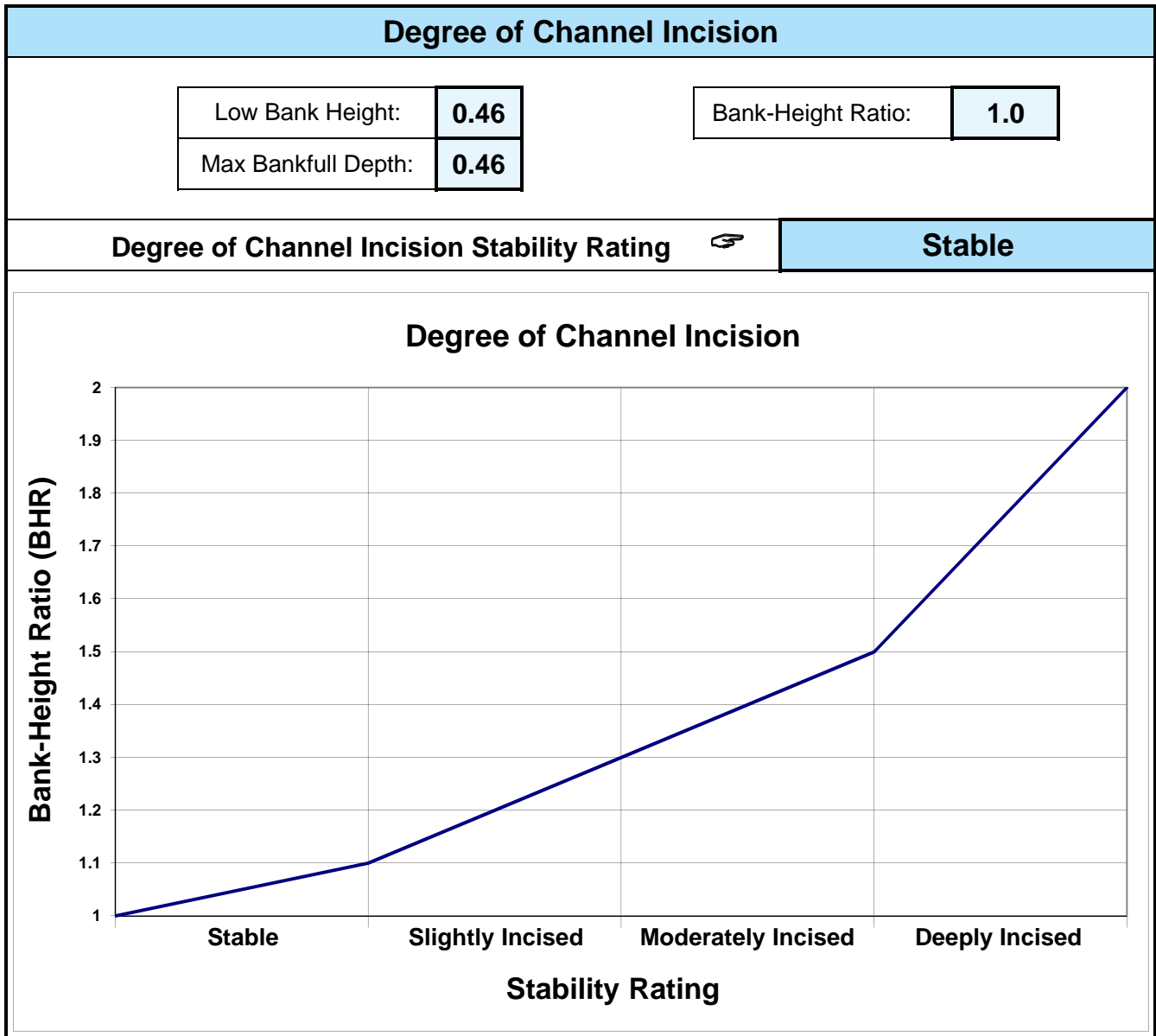
<b>Depositional Patterns</b>					
Stream: <b>Trail Creek Trib., D4a+ Poor Reach</b>		Location: <b>Pike National Forest, Colorado</b>			
Observers: <b>Rosgen et al.</b>		Date: <b>8/16/2010</b>			
List ALL CATEGORIES that APPLY	B5	B6	B7		
<i>Various Depositional Features modified from Galay et al. (1973)</i>					
 <b>B1</b> <b>POINT BARS</b>	 <span style="border: 1px solid red; border-radius: 50%; padding: 2px;"><b>B5</b></span> <b>DIAGONAL BARS</b>				
 <b>B2</b> <b>POINT BARS with Few MID-CHANNEL BARS</b>	 <span style="border: 1px solid red; border-radius: 50%; padding: 2px;"><b>B6</b></span> <b>Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</b>				
 <b>B3</b> <b>NUMEROUS MID-CHANNEL BARS</b>	 <span style="border: 1px solid red; border-radius: 50%; padding: 2px;"><b>B7</b></span> <b>SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</b>				
 <b>B4</b> <b>SIDE BARS</b>	 <b>B8</b> <b>DELTA BARS</b>				



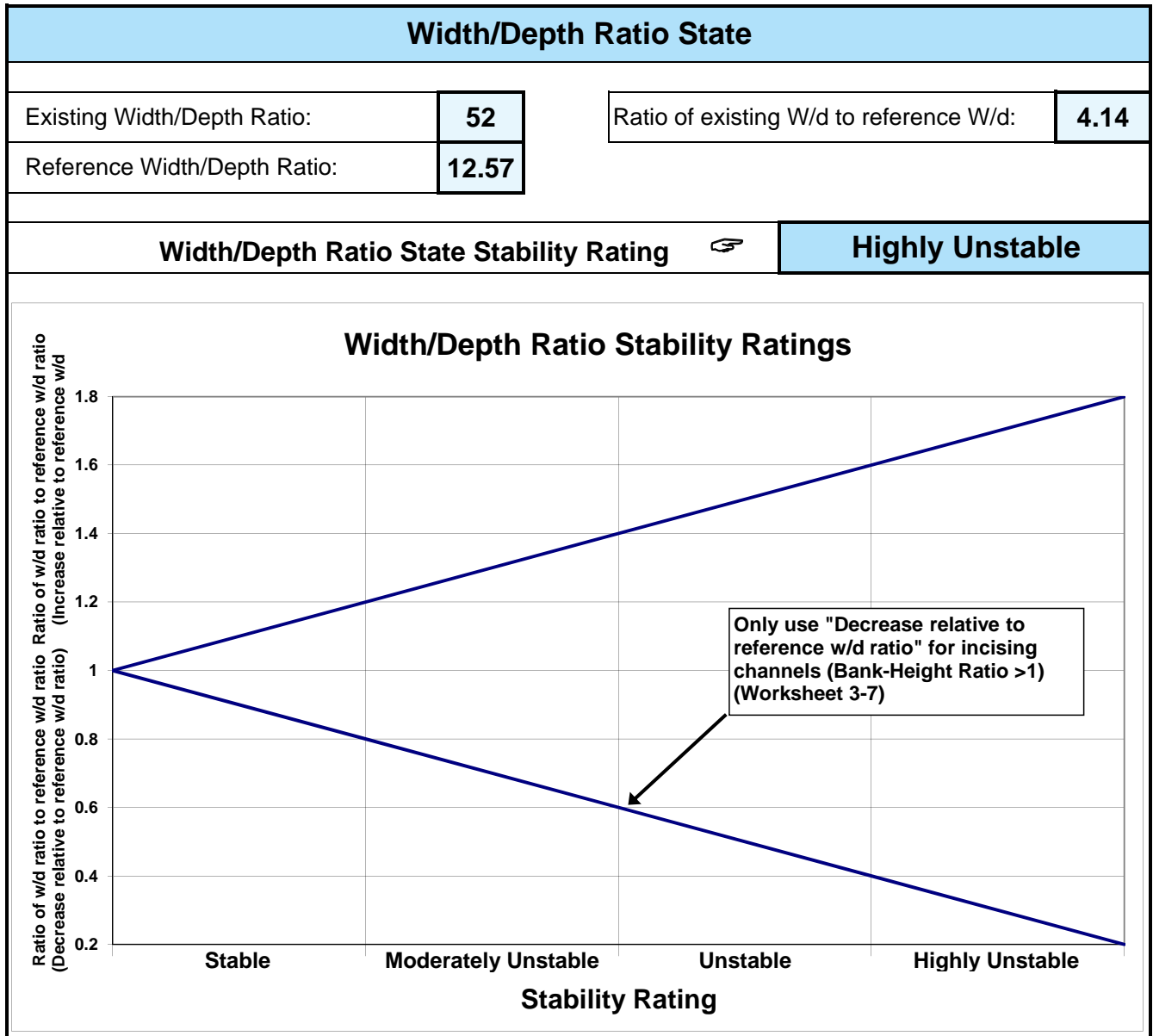
## Worksheet 5-11. Channel blockages.

Channel Blockages		
Stream: <b>Trail Creek Trib., D4a+ Poor Reach</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>Rosgen et al.</b>		Date: <b>8/16/2010</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input type="checkbox"/>
<b>D4</b> Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input checked="" type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

**Worksheet 5-12.** Degree of channel incision.



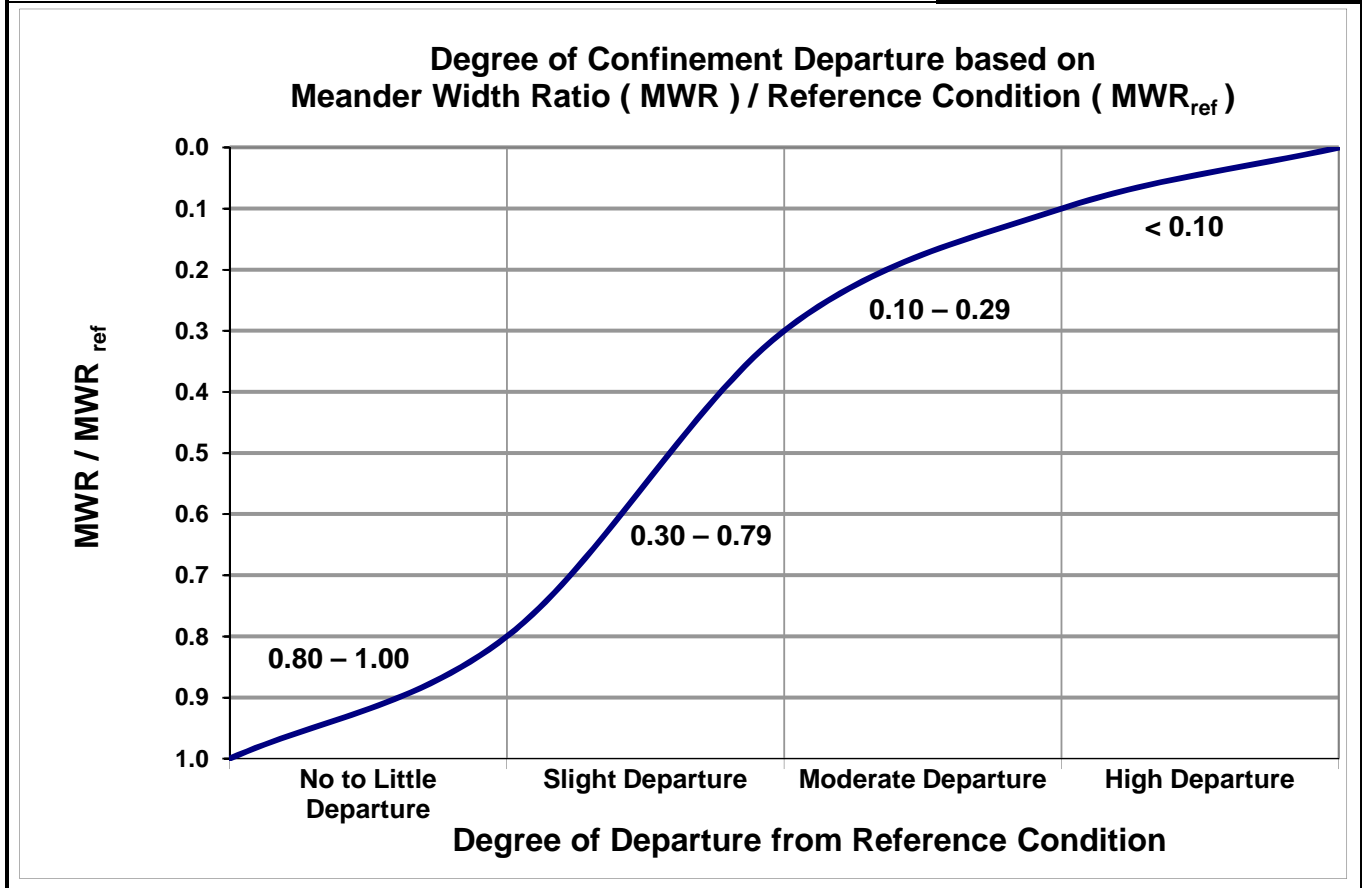
Worksheet 5-13. Width/depth ratio state.



**Worksheet 5-14.** Degree of channel confinement (lateral containment).

Degree of Confinement			
Existing Meander Width Ratio (MWR):	<b>2.04</b>	Ratio of MWR to $MWR_{ref}$ :	<b>0.76</b>
Reference Meander Width Ratio ( $MWR_{ref}$ ):	<b>2.7</b>		

<b>Degree of Confinement Stability Rating</b>	<b>Slight Departure</b>
---	-------------------------



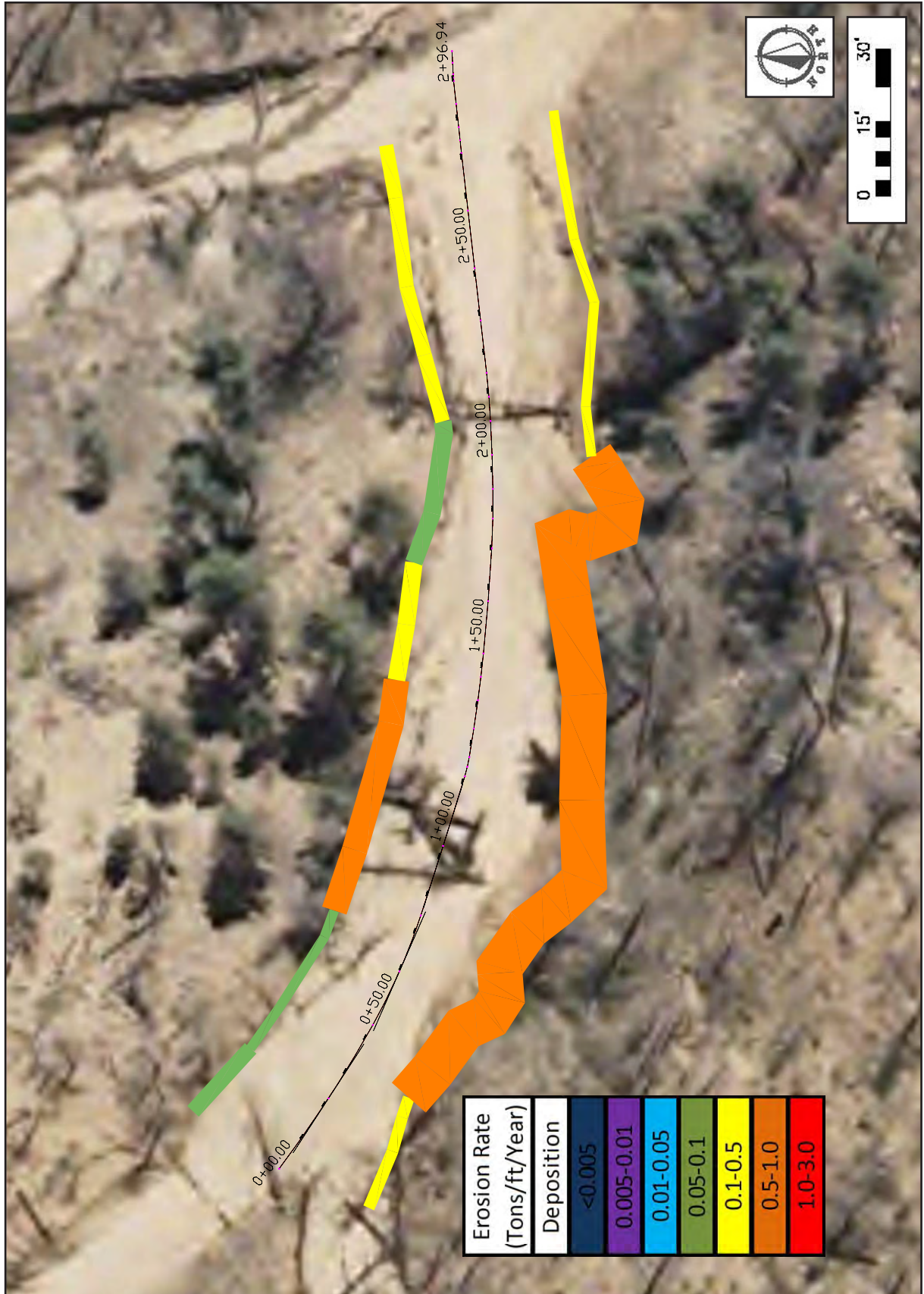


## BANCS Model – Streambank Erosion

**Worksheet 5-18.** Annual streambank erosion estimates.

Stream: <b>Trail Creek Trib., D4a+ Poor Reach</b>		Location: <b>Pike National Forest, Colorado</b>					
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>300</b>				Date: <b>8/15/2010</b>	
Observers: <b>Rosgen et al.</b>		Valley Type: <b>VIII</b>			Stream Type: <b>D4a</b>		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 5-16) (adjective)	NBS rating (Worksheet 5-17) (adjective)	Bank erosion rate (Figure 5-34 or 5-35) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [(4)×(5)×(6)] (ft <sup>3</sup> /yr)	Erosion Rate (tons/yr/ft) {[ (7)/27 ] × 1.3 / (5)}
1. 0+00 - 0+20 R	Extreme	Moderate	1.07417	20.0	3.0	64.45	0.15516
2. 0+00 - 0+33 L	Extreme	Low	0.41998	33.0	4.0	55.44	0.08088
3. 0+20 - 0+215 R	Extreme	Moderate	1.07417	195.0	11.5	2408.83	0.59477
4. 0+33 - 0+76 L	Extreme	Low	0.41998	43.0	2.5	45.15	0.05055
5. 0+76 - 0+145 L	Extreme	Extreme	2.76027	69.0	6.5	1237.98	0.86386
6. 0+145 - 0+203 L	Extreme	Moderate	1.07417	25.0	4.5	120.84	0.23274
7. 0+203 - 0+228 L	High	Low	0.25042	25.0	4.5	28.17	0.05426
8. 0+215 - 0+300 R	Extreme	Moderate	1.07417	85.0	2.5	228.26	0.12930
9. 0+228 - 0+300 L	Extreme	Moderate	1.07417	72.0	3.7	286.16	0.19136
10							
11							
12							
13							
14							
15							
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					Total Erosion (ft <sup>3</sup> /yr)	<b>4475.28</b>	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					Total Erosion (yds <sup>3</sup> /yr)	<b>165.75</b>	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					Total Erosion (tons/yr)	<b>215.48</b>	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					Total Erosion (tons/yr/ft)	<b>0.7183</b>	

Streambank Erosion Map



## FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Equation Type		Equation Source		Equation		Bankfull Discharge (cfs)		Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)				
1. Bedload Sediment		"Good/Fair" Pagosa		$y = -0.0113x + 1.0139x^{2.1929}$		3.92		0.0052		0.7368				
2. Suspended Sediment		"Good/Fair" Pagosa		$y = 0.06336 + 0.9326x^{2.4085}$										
		From Dimensional Flow-Duration Curve				From Sediment Rating Curves				Calculate		Calculate Sediment Yield		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Percentage of Time	Daily Mean Discharge (cfs)	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Suspended Sediment Discharge	Suspended Sediment Discharge (tons/day)	Dimensionless Bedload Discharge	Bedload Sediment Discharge (tons/day)	Time Adjusted Streamflow [(5)×(6)]	Suspended Sediment [(5)×(9)]	Bedload Sediment [(5)×(11)]	Suspended + Bedload Sediment [(13)+(14)]
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>bed</sub> )	(S/S <sub>bed</sub> )	(tons/day)	(b <sub>y</sub> /b <sub>bed</sub> )	(tons/day)	(cfs)	(tons)	(tons)	(tons)
0%	10.0													
0.10%	8.6	0.05%	0.09%	0.34	9.3	2.363	7.461	0.14	6.670	3.27	3.2	0.05	1.12	1.17
0.25%	7.4	0.08%	0.15%	0.55	8.0	2.036	5.232	0.08	4.809	2.36	4.4	0.05	1.29	1.34
0.50%	6.4	0.13%	0.25%	0.91	6.9	1.761	3.706	0.05	3.494	1.71	6.3	0.05	1.56	1.61
0.75%	5.5	0.13%	0.25%	0.91	5.9	1.513	2.592	0.03	2.502	1.23	5.4	0.03	1.12	1.15
1%	4.7	0.13%	0.25%	0.91	5.1	1.300	1.817	0.02	1.790	0.88	4.6	0.02	0.80	0.82
1.5%	4.1	0.25%	0.50%	1.83	4.4	1.120	1.289	0.01	1.289	0.63	8.0	0.02	1.15	1.17
2%	3.4	0.25%	0.50%	1.83	3.7	0.949	0.886	0.01	0.893	0.44	6.8	0.01	0.80	0.81
3%	2.8	0.50%	1.00%	3.65	3.1	0.795	0.600	0.00	0.602	0.30	11.4	0.01	1.08	1.09
4%	2.4	0.50%	1.00%	3.65	2.6	0.674	0.424	0.00	0.415	0.20	9.6	0.01	0.74	0.75
5%	2.2	0.50%	1.00%	3.65	2.3	0.587	0.322	0.00	0.304	0.15	8.4	0.01	0.54	0.55
10%	1.4	2.50%	5.00%	18.25	1.8	0.450	0.200	0.00	0.165	0.08	32.2	0.01	1.48	1.49
20%	0.7	5.00%	10.00%	36.50	1.1	0.269	0.103	0.00	0.045	0.02	38.4	0.01	0.81	0.82
30%	0.5	5.00%	10.00%	36.50	0.6	0.158	0.075	0.00	0.006	0.00	22.6	0.00	0.11	0.12
40%	0.4	5.00%	10.00%	36.50	0.4	0.108	0.068	0.00	0.000	0.00	15.4	0.00	0.00	0.00
50%	0.3	5.00%	10.00%	36.50	0.3	0.079	0.066	0.00	0.000	0.00	11.3	0.00	0.00	0.00
60%	0.2	5.00%	10.00%	36.50	0.2	0.061	0.065	0.00	0.000	0.00	8.7	0.00	0.00	0.00
70%	0.2	5.00%	10.00%	36.50	0.2	0.047	0.064	0.00	0.000	0.00	6.8	0.00	0.00	0.00
80%	0.1	5.00%	10.00%	36.50	0.2	0.039	0.064	0.00	0.000	0.00	5.6	0.00	0.00	0.00
90%	0.1	5.00%	10.00%	36.50	0.1	0.032	0.064	0.00	0.000	0.00	4.5	0.00	0.00	0.00
100%	0.0	5.00%	10.00%	36.50	0.1	0.016	0.064	0.00	0.000	0.00	2.3	0.00	0.00	0.00
<b>Annual Totals:</b>											216.0 (cfs)	0.3 (tons/yr)	12.6 (tons/yr)	12.9 (tons/yr)
											428.4 (acre-ft)			



Worksheet 19b. Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Equation Type		Equation Source				Equation		Bankfull Discharge (cfs)			Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)	
1. Bedload Sediment		"Poor" Pagosa				$Y = 0.07176x + 1.02176x^{2.3772}$		3.92			0.0230		111.69	
2. Suspended Sediment		"Poor" Pagosa				$Y = 0.0989 + 0.9213x^{3.659}$								
		From Dimensional Flow-Duration Curve				From Sediment Rating Curves				Calculate		Calculate Sediment Yield		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Percentage of Time	Daily Mean Discharge	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Suspended Sediment Discharge	Suspended Sediment Discharge	Dimensionless Bedload Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow [(5)x(6)]	Suspended Sediment [(5)x(9)]	Bedload Sediment [(5)x(11)]	Suspended Sediment + Bedload Sediment [(13)+(14)]
(%)	(cfs)	(%)	(%)	(days)	(cfs)	( $Q/Q_{bed}$ )	( $S/S_{bed}$ )	(tons/day)	( $b_b/b_{bed}$ )	(tons/day)	(cfs)	(tons)	(tons)	(tons)
0%	10.7													
0.10%	9.3	0.05%	0.09%	0.34	10.0	2.548	28.319	85.29	9.510	20.85	3.4	29.26	7.15	36.42
0.25%	8.1	0.08%	0.15%	0.55	8.7	2.221	17.173	45.08	6.881	15.09	4.8	24.68	8.26	32.94
0.50%	7.1	0.13%	0.25%	0.91	7.6	1.946	10.620	24.42	5.043	11.06	7.0	22.29	10.09	32.38
0.75%	6.2	0.13%	0.25%	0.91	6.7	1.698	6.491	13.03	3.669	8.04	6.1	11.89	7.34	19.23
1%	5.5	0.13%	0.25%	0.91	5.8	1.485	4.011	7.04	2.686	5.89	5.3	6.42	5.37	11.80
1.5%	4.8	0.25%	0.50%	1.83	5.1	1.304	2.531	3.90	1.991	4.37	9.3	7.12	7.97	15.09
2%	4.1	0.25%	0.50%	1.83	4.4	1.130	1.540	2.06	1.438	3.15	8.1	3.75	5.76	9.51
3%	3.6	0.50%	1.00%	3.65	3.8	0.975	0.938	1.08	1.033	2.27	13.9	3.94	8.27	12.22
4%	3.1	0.50%	1.00%	3.65	3.3	0.846	0.599	0.60	0.759	1.66	12.1	2.19	6.08	8.26
5%	2.7	0.50%	1.00%	3.65	2.9	0.742	0.408	0.36	0.575	1.26	10.6	1.31	4.60	5.91
10%	1.7	2.50%	5.00%	18.25	2.2	0.568	0.215	0.14	0.338	0.74	40.6	2.63	13.52	16.15
20%	0.8	5.00%	10.00%	36.50	1.3	0.321	0.113	0.04	0.140	0.31	46.0	1.57	11.24	12.82
30%	0.5	5.00%	10.00%	36.50	0.7	0.166	0.100	0.02	0.086	0.19	23.8	0.72	6.89	7.61
40%	0.4	5.00%	10.00%	36.50	0.4	0.108	0.099	0.01	0.077	0.17	15.5	0.46	6.16	6.62
50%	0.3	5.00%	10.00%	36.50	0.3	0.079	0.099	0.01	0.074	0.16	11.3	0.34	5.94	6.28
60%	0.2	5.00%	10.00%	36.50	0.2	0.061	0.099	0.01	0.073	0.16	8.7	0.26	5.85	6.11
70%	0.2	5.00%	10.00%	36.50	0.2	0.047	0.099	0.01	0.072	0.16	6.8	0.20	5.80	6.00
80%	0.1	5.00%	10.00%	36.50	0.2	0.039	0.099	0.00	0.072	0.16	5.6	0.17	5.78	5.95
90%	0.1	5.00%	10.00%	36.50	0.1	0.032	0.099	0.00	0.072	0.16	4.5	0.13	5.77	5.90
100%	0.0	5.00%	10.00%	36.50	0.1	0.016	0.099	0.00	0.072	0.16	2.3	0.07	5.75	5.82
<b>Annual Totals:</b>											245.7 (cfs)	119.4 (tons/yr)	143.6 (tons/yr)	263.0 (tons/yr)
											487.3 (acre-ft)			

# POWERSED Model – Sediment Transport Capacity

**Worksheet 20a.** Sediment transport prediction representing the upstream supply up to bankfull for bedload and suspended sand sediment.

Stream: Trail Creek, Upstream Existing Sediment Supply		Location: Pike National Forest, Colorado (Used "POOR" Curves)		Date: 08/20/10													
Observers: S=-.123, Q=4, 3.1, Bed.=.0506, S.Sand=55.84		Stream Type: D4a+		Gage Station #: Used Post-Fire Dimensionless F-D C.													
Valley Type: III		Calculate		Calculate													
Flow-duration curve		Hydraulic geometry		Measure													
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
Percentage of time	Daily mean discharge	Mid-ordinate stream-flow	Area	Width	Depth	Velocity	Slope	Shear stress	Stream power	Unit power	Time increment	Time increment	Daily mean bedload transport	Daily mean bedload transport	Time adjusted bedload transport	Time adjusted suspended sand transport	Time adjusted total transport
(%)	(cfs)	(cfs)	(ft <sup>2</sup> )	(ft)	(ft)	(ft/s)	(ft/ft)	(lb/ft <sup>2</sup> )	(lb/s)	(lb/ft/s)	(%)	(days)	(tons/day)	(tons/day)	(tons)	(tons)	(tons)
100.00%	0.02										0%			0.00	0.00	0.00	0.00
90.00%	0.10	0.06	0.10	2.22	0.05	1.23	0.1230	0.35	0.46	0.21	10%	36.50	0.17	0.00	6.21	0.00	6.21
80.00%	0.14	0.12	0.12	2.26	0.05	1.31	0.1230	0.41	0.92	0.41	10%	36.50	0.17	0.00	6.21	0.00	6.21
70.00%	0.17	0.16	0.14	2.29	0.06	1.36	0.1230	0.47	1.23	0.54	10%	36.50	0.17	0.00	6.21	0.00	6.21
60.00%	0.21	0.19	0.15	2.31	0.06	1.39	0.1230	0.50	1.46	0.63	10%	36.50	0.17	0.00	6.21	0.00	6.21
50.00%	0.27	0.24	0.16	2.35	0.07	1.45	0.1230	0.52	1.84	0.78	10%	36.50	0.17	0.00	6.21	0.00	6.21
40.00%	0.35	0.31	0.19	2.40	0.08	1.54	0.1230	0.60	2.38	0.99	10%	36.50	0.17	0.00	6.21	0.00	6.21
30.00%	0.50	0.43	0.23	2.49	0.09	1.68	0.1230	0.70	3.30	1.33	10%	36.50	0.17	0.01	6.21	0.36	6.57
20.00%	0.78	0.64	0.30	2.64	0.11	1.93	0.1230	0.86	4.91	1.86	10%	36.50	0.17	0.01	6.21	0.36	6.57
10.00%	1.57	1.18	0.47	2.98	0.16	2.47	0.1230	1.19	9.06	3.04	10%	36.50	0.26	0.02	9.49	0.73	10.22
5.00%	2.50	2.04	0.68	3.29	0.21	2.96	0.1230	1.55	15.66	4.76	5%	18.25	0.60	0.05	10.95	0.91	11.86
4.00%	2.82	2.66	0.81	3.47	0.23	3.22	0.1230	1.74	20.42	5.88	1%	3.65	0.99	0.12	3.61	0.44	4.05
3.00%	3.26	3.04	0.89	3.56	0.25	3.35	0.1230	1.86	23.33	6.55	1%	3.65	1.34	0.20	4.89	0.73	5.62
2.00%	3.80	3.53	0.99	3.68	0.27	3.52	0.1230	2.00	27.09	7.36	1%	3.65	1.81	0.36	6.61	1.31	7.92
1.50%	4.48	4.14	1.11	3.84	0.29	3.72	0.1230	2.14	31.78	8.28	1%	1.83	2.59	0.71	4.73	1.30	6.03
1.00%	5.15	4.82															
0.75%	5.89	5.52															
0.50%	6.83	6.36															
0.25%	7.84	7.34															
0.10%	8.99	8.42															
0.0060%	10.40	9.70															
Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr):															90.0	6.1	96.1

**Worksheet 20b.** Sediment transport prediction for the existing condition reach compared to the upstream sediment supply to assess bed stability.

Stream: Trail Creek, D4a+ Poor, Riffle XS 1+07.5		Location: Pike National Forest, Colorado (Used "POOR" Curves)		Date: 08/20/10													
Observers: S=, 123, Q=4, 3.1, Bed.=, 0506, S.Sand=55.84		Stream Type: D4a+		Gage Station #: Used Post-Fire Dimensionless F-D C.													
		Valley Type: III															
Flow-duration curve			Calculate														
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
Percentage of time	Daily mean discharge	Mid-ordinate stream-flow	Area	Width	Depth	Velocity	Slope	Shear stress	Stream power	Unit power	Time increment	Time increment	Daily mean bedload transport	Daily mean suspended sand transport	Time adjusted bedload transport	Time adjusted suspended sand transport	Time adjusted total transport
(%)	(cfs)	(cfs)	(ft <sup>2</sup> )	(ft)	(ft)	(ft/s)	(ft/ft)	(lb/ft <sup>2</sup> )	(lb/s)	(lb/ft/s)	(%)	(days)	(tons/day)	(tons/day)	[(13)×(14)]	[(13)×(15)]	[(16)+(17)]
100.00%	0.02										0%			0.00	0.00	0.00	0.00
90.00%	0.10	0.06	0.04	0.75	0.05	1.54	0.1230	0.39	0.46	0.61	10%	36.50	0.17	0.00	6.21	0.00	6.21
80.00%	0.14	0.12	0.06	0.90	0.07	1.72	0.1230	0.49	0.92	1.02	10%	36.50	0.17	0.00	6.21	0.00	6.21
70.00%	0.17	0.16	0.07	1.00	0.07	1.84	0.1230	0.52	1.23	1.23	10%	36.50	0.17	0.00	6.21	0.00	6.21
60.00%	0.21	0.19	0.09	1.07	0.08	1.92	0.1230	0.62	1.46	1.36	10%	36.50	0.17	0.00	6.21	0.00	6.21
50.00%	0.27	0.24	0.10	1.19	0.08	2.07	0.1230	0.62	1.84	1.55	10%	36.50	0.17	0.00	6.21	0.00	6.21
40.00%	0.35	0.31	0.13	1.36	0.10	2.28	0.1230	0.71	2.38	1.75	10%	36.50	0.17	0.00	6.21	0.00	6.21
30.00%	0.50	0.43	0.17	1.67	0.10	2.46	0.1230	0.75	3.30	1.98	10%	36.50	0.17	0.01	6.21	0.36	6.57
20.00%	0.78	0.64	0.25	2.23	0.11	2.55	0.1230	0.83	4.91	2.20	10%	36.50	0.22	0.01	8.03	0.36	8.39
10.00%	1.57	1.18	0.42	3.42	0.12	2.76	0.1230	0.91	9.06	2.65	10%	36.50	0.22	0.02	8.03	0.73	8.76
5.00%	2.50	2.04	0.65	4.60	0.14	3.05	0.1230	1.05	15.66	3.40	5%	18.25	0.35	0.04	6.39	0.73	7.12
4.00%	2.82	2.66	0.83	5.51	0.15	3.21	0.1230	1.13	20.42	3.71	1%	3.65	0.39	0.05	1.42	0.18	1.60
3.00%	3.26	3.04	0.94	6.22	0.15	3.22	0.1230	1.13	23.33	3.75	1%	3.65	0.39	0.06	1.42	0.22	1.64
2.00%	3.80	3.53	1.09	7.14	0.15	3.24	0.1230	1.15	27.09	3.79	1%	3.65	0.39	0.07	1.42	0.26	1.68
1.50%	4.48	4.14	1.27	8.28	0.15	3.26	0.1230	1.15	31.78	3.84	1%	1.83	0.43	0.09	0.78	0.16	0.94
1.00%	5.15	4.82															
0.75%	5.89	5.52															
0.50%	6.83	6.36															
0.25%	7.84	7.34															
0.10%	8.99	8.42															
0.0060%	10.40	9.70															

Notes:  
 Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr): 71.0  
 Upstream total annual sediment supply (tons/yr) (Worksheet 5-20a): 90.0  
 Difference in sediment transport capacity (tons/yr) (+ or - ): -19.0  
 Stability evaluation: Aggradation, Degradation or Stable: Aggradation, > 23% Reduction in Transport

## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>Trail Creek Trib., D4a+ Poor Reach</b>		Stream Type: <b>D4a Poor</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>Rosgen et al.</b>		Date: <b>8/16/2010</b>			
<b>Enter Required Information for Existing Condition</b>					
2.6	$D_{50}$	Riffle bed material $D_{50}$ (mm)			
	$\hat{D}_{50}$	Bar sample $D_{50}$ (mm)			
0.04	$D_{max}$	Largest particle from <b>Bed Material</b> (ft)	11.3	(mm)	304.8 mm/ft
0.123	$S$	Existing bankfull water surface slope (ft/ft)			
0.15	$d$	Existing bankfull mean depth (ft)			
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment			
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>					
N/A	$D_{50}/\hat{D}_{50}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 ( D_{50}/\hat{D}_{50} )^{-0.872}$		
N/A	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 ( D_{max}/D_{50} )^{-0.887}$		
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED:		
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	$d$	Required bankfull mean depth (ft)	$d = \frac{\tau^*(\gamma_s - 1)D_{max}}{S}$ (use $D_{max}$ in ft)		
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	$S$	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^*(\gamma_s - 1)D_{max}}{d}$ (use $D_{max}$ in ft)		
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					
<b>Sediment Competence Using Dimensional Shear Stress</b>					
1.151	Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d ) $\gamma = 62.4$ , $d =$ existing depth, $S =$ existing slope				
Shields <b>88</b>	CO <b>180</b>	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ ( <b>Figure 5-49</b> )			
Shields <b>0.18</b>	CO <b>0.03</b>	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) ( <b>Figure 5-49</b> )			
Shields <b>0.02</b>	CO <b>0.004</b>	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm)		$d = \frac{\tau}{\gamma S}$	
		$\tau =$ predicted shear stress, $\gamma = 62.4$ , $S =$ existing slope			
Shields <b>0.0192</b>	CO <b>0.0032</b>	Predicted slope required to initiate movement of measured $D_{max}$ (mm)		$S = \frac{\tau}{\gamma d}$	
		$\tau =$ predicted shear stress, $\gamma = 62.4$ , $d =$ existing depth			
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input checked="" type="checkbox"/> Degrading					

## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>Trail Creek Trib., D4a+ Poor</b>		Stream Type: <b>D4a</b>
Location: <b>Pike National Forest, CO</b>		Valley Type: <b>VIII</b>
Observers: <b>Rosgen et al.</b>		Date: <b>8/16/2010</b>
Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)	Stability Rating (Check Appropriate Rating)	
Stream Type at potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	<input type="checkbox"/> Stable	
(E→C), (C→High W/d C)	<input type="checkbox"/> Moderately Unstable	
(G→F), (F→D), (C→F)	<input type="checkbox"/> Unstable	
(C→D), (B→G), (D→G), (C→G), (E→G)	<input checked="" type="checkbox"/> Highly Unstable	

**Worksheet 5-25.** Lateral stability.

Stream: <b>Trail Creek Trib., D4a+ Poor Reach</b>		Stream Type: <b>D4a</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>Rosgen et al.</b>		Date: <b>8/16/2010</b>			
Lateral stability criteria (choose one stability category for each criterion 1-5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	8
	(2)	(4)	(6)	4.1 (8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	4
	(1)	(2)	(3)	B5, B6, B7 (4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		1
	N/A (1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	8
	(2)	(4)	(6)	Ex/M (8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	2
	(1)	0.8 (2)	(3)	(4)	
<b>Total Points</b>					<b>23</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input type="checkbox"/>	<i>Unstable</i> 13 – 21 <input type="checkbox"/>	<i>Highly Unstable</i> > 21 <input checked="" type="checkbox"/>	

**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>Trail Creek Trib., D4a+ Poor Reach</b>		Stream Type: <b>D4a</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>Rosgen et al.</b>		Date: <b>8/16/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
<b>1 Sediment competence (Worksheet 5-22)</b>	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope—slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	<b>2</b>
	<b>Excess (2)</b>	<b>(4)</b>	<b>(6)</b>	<b>(8)</b>	
<b>2 Sediment Capacity (POWERSED) (Worksheet 5-20)</b>	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	<b>7</b>
	<b>(2)</b>	<b>(4)</b>	<b>(6)</b>	<b>&gt; 21% (7)</b>	
<b>3 W/d Ratio State (Worksheet 5-13)</b>	1.0 – 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	<b>8</b>
	<b>(2)</b>	<b>(4)</b>	<b>(6)</b>	<b>4.1 (8)</b>	
<b>4 Stream Succession States (Worksheet 5-24)</b>	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	<b>8</b>
	<b>(2)</b>	<b>(4)</b>	<b>(6)</b>	<b>(8)</b>	
<b>5 Depositional Patterns (Worksheet 5-10)</b>	B1	B2, B4	B3, B5	B6, B7, B8	<b>4</b>
	<b>(1)</b>	<b>(2)</b>	<b>(3)</b>	<b>B5, B6, B7 (4)</b>	
<b>6 Debris / Blockages (Worksheet 5-11)</b>	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	<b>2</b>
	<b>(1)</b>	<b>D4 (2)</b>	<b>(3)</b>	<b>(4)</b>	
<b>Total Points</b>					<b>31</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
<b>Vertical Stability for Excess Deposition / Aggradation (use total points and check stability rating)</b>	<i>No Deposition</i> 10 – 14 <input type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input type="checkbox"/>	<i>Aggradation</i> > 30 <input checked="" type="checkbox"/>	

**Worksheet 5-27.** Vertical stability – degradation.

Stream: <b>Trail Creek Trib., D4a+ Poor Reach</b>		Stream Type: <b>D4a</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>Rosgen et al.</b>		Date: <b>8/16/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>1 Sediment Competence</b> (Worksheet 5-22)	Does not indicate excess competence	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed	$D_{100}$ of bed moved	Particles much larger than $D_{100}$ of bed moved	<b>8</b>
	(2)	(4)	(6)	(8)	
<b>2 Sediment Capacity</b> (POWERSED) (Worksheet 5-20)	Does not indicate excess capacity	Slight excess energy: up to 10% increase above reference	Excess energy sufficient to increase load up to 50% of annual load	Excess energy transporting more than 50% of annual load	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>3 Degree of Channel Incision (BHR)</b> (Worksheet 5-12)	1.00 – 1.10	1.11 – 1.30	1.31 – 1.50	> 1.50	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>4 Stream Succession States</b> (Worksheets 5-12 and 5-24)	Does not indicate incision or degradation	If BHR > 1.1 and stream type has W/d between 5–10	If BHR > 1.1 and stream type has W/d less than 5	(B→G), (C→G), (E→G), (D→G)	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>5 Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.80 – 1.00	0.30 – 0.79	0.10 – 0.29	< 0.10	<b>2</b>
	(1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>16</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation</b> (use total points and check stability rating)	<i>Not Incised</i> 9 – 11 <input type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input checked="" type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input type="checkbox"/>	<i>Degradation</i> > 27 <input type="checkbox"/>	



Worksheet 5-28. Channel enlargement.

Stream: <b>Trail Creek Trib., D4a+ Poor Reach</b>		Stream Type: <b>D4a</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>Rosgen et al.</b>		Date: <b>8/16/2010</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1–4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	8
	(2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	8
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	8
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	4
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>28</b>
<b>Category Point Range</b>					
Channel Enlargement Prediction (use total points and check stability rating)	<i>No Increase</i> 8 – 10 <input type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input type="checkbox"/>	<i>Extensive</i> > 24 <input checked="" type="checkbox"/>	

Worksheet 5-29. Overall sediment supply.

Stream: <b>Trail Creek Trib., D4a+ Poor Reach</b>		Stream Type: <b>D4a</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>		
Observers: <b>Rosgen et al.</b>		Date: <b>8/16/2010</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1-5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	4	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	4	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	2	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	4	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	4	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>18</b>	
<b>Category Point Range</b>				
<b>Overall Sediment Supply Rating</b> (use total points and check stability rating)	<b>Low</b> 5 <input type="checkbox"/>	<b>Moderate</b> 6 – 10 <input type="checkbox"/>	<b>High</b> 11 – 15 <input type="checkbox"/>	<b>Very High</b> 16 – 20 <input checked="" type="checkbox"/>





## *Appendix C9*

# **E4 Stream Type**

***Good Stability HWD Reach***



# Table of Contents

## *Appendix C9: E4 Good HWD Reach*

<b>Reach Location &amp; Overview.....</b>	<b>C9-2</b>
<b>Survey Summary.....</b>	<b>C9-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C9-9</b>
<b><i>Velocity, Classification &amp; Morphological Relations.....</i></b>	<b>C9-9</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b><i>Stability Indices.....</i></b>	<b>C9-13</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b><i>BANCS Model – Streambank Erosion.....</i></b>	<b>C9-23</b>
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b><i>FLOWSED Model – Total Annual Sediment Yield.....</i></b>	<b>C9-25</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b><i>Sediment Competence/Entrainment.....</i></b>	<b>C9-27</b>
Worksheet 5-22. Sediment competence calculations.	
<b><i>Channel Stability Ratings.....</i></b>	<b>C9-28</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b><i>Summary.....</i></b>	<b>C9-34</b>
Worksheet 5-32. Summary of stability condition categories.	

## E4 Good HWD Reach Location & Overview

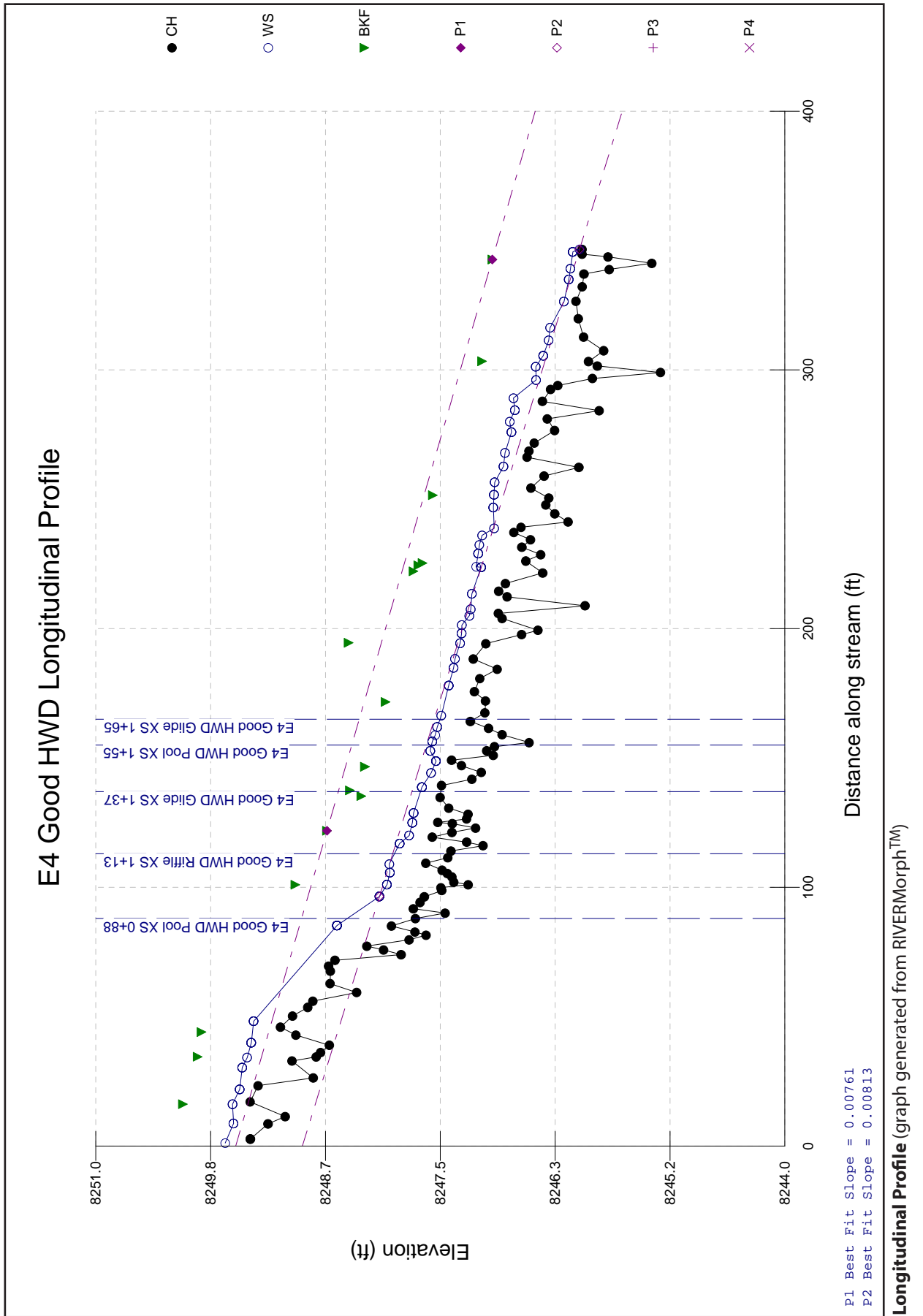
The E4 Good HWD representative reach is a 3<sup>rd</sup> order, perennial, low gradient, meandering stream located in upper Trail Creek (see location map **Figure C-2**). The photograph depicts excellent riparian vegetation, although the stream is recovering from past impacts. The width/depth ratio of 9.72 is at the upper end of the range of values for an E4 stream type, but the reach has a very high recovery potential in the lacustrine, beaver meadow, Valley Type X. The stream is narrowing and deepening as it is becoming more stable and has fishery potential. The potential stable stream type in this valley type is E4; thus no POWERSED run was made as the stream has not departed from the reference stream type, shows no incision, and its width/depth ratio indicates no excess deposition. The stability rating is “Good” due to a Pfankuch stability rating of “Good” and the relatively low streambank erosion rate of *0.007 tons/yr/ft*. However, according to the WRENSS model, the water yield due to the fire increased from *1,377 acre-ft* to *2,700 acre-ft*, representing an increase of *1,324 acre-ft*, which is double the pre-fire condition. The FLOWSED model showed that bedload increased from *36 tons/yr* to *216 tons/yr* and the suspended sediment increased from *20 tons/yr* to *200 tons/yr*, representing a total increase in sediment of *350 tons/yr*. This sediment yield increase is the result of increased sediment transport capacity or efficient routing of sediment supplied from upstream sources due to the low width/depth ratio.

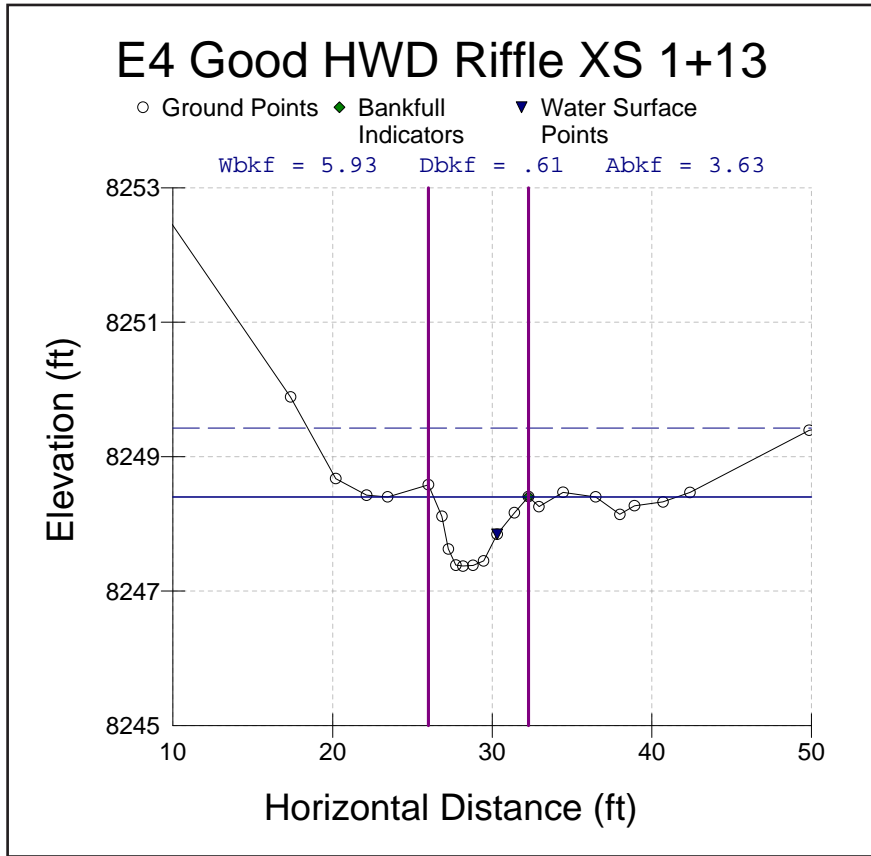
The photograph depicts the typical character of this representative E4 stream type. The following graphs and summary worksheets provide the detail of the morphology, hydraulics, streambank erosion rates, and stability conditions responsible for the overall “Good” rating.



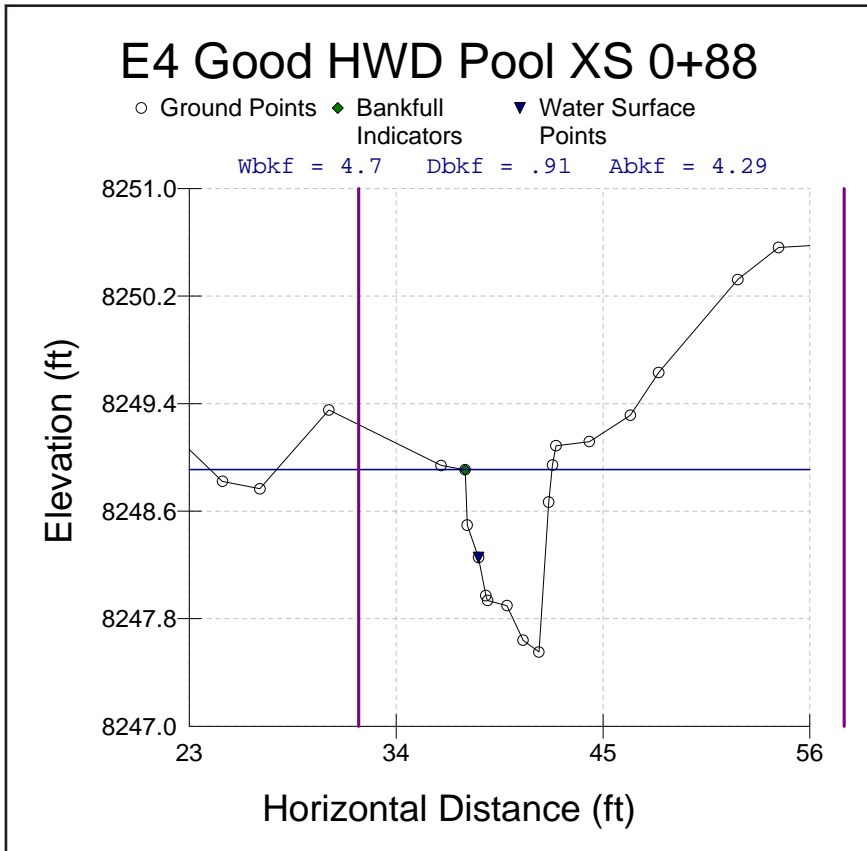


# Survey Summary

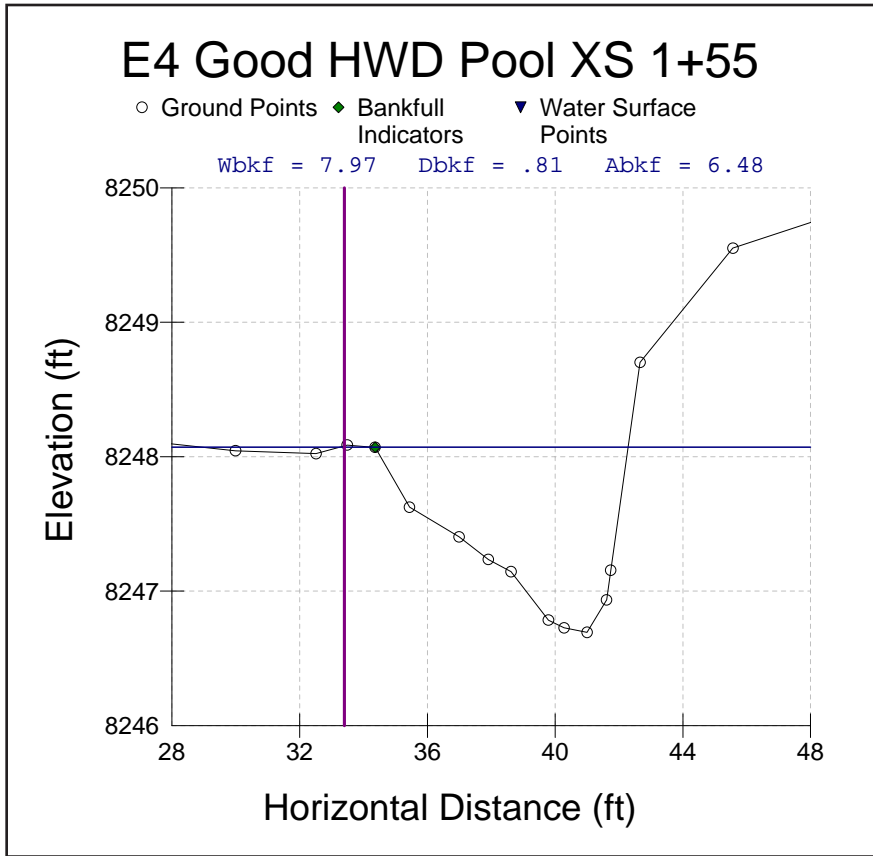




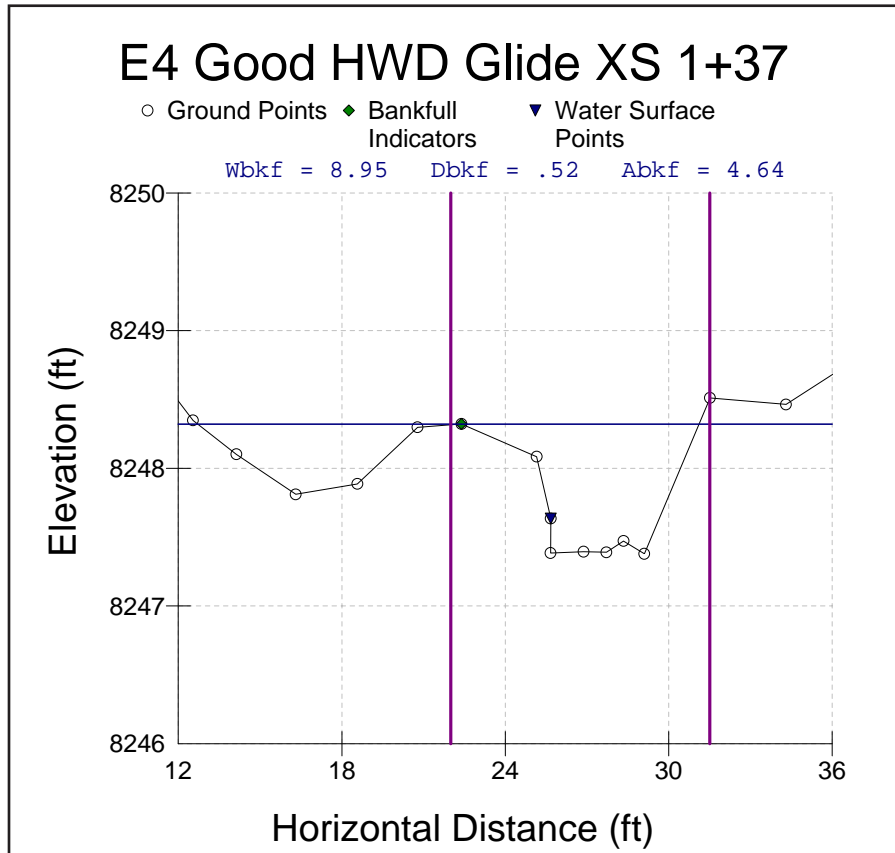
Representative Riffle Cross-section 1+13 (graph generated from RIVERMorph™)



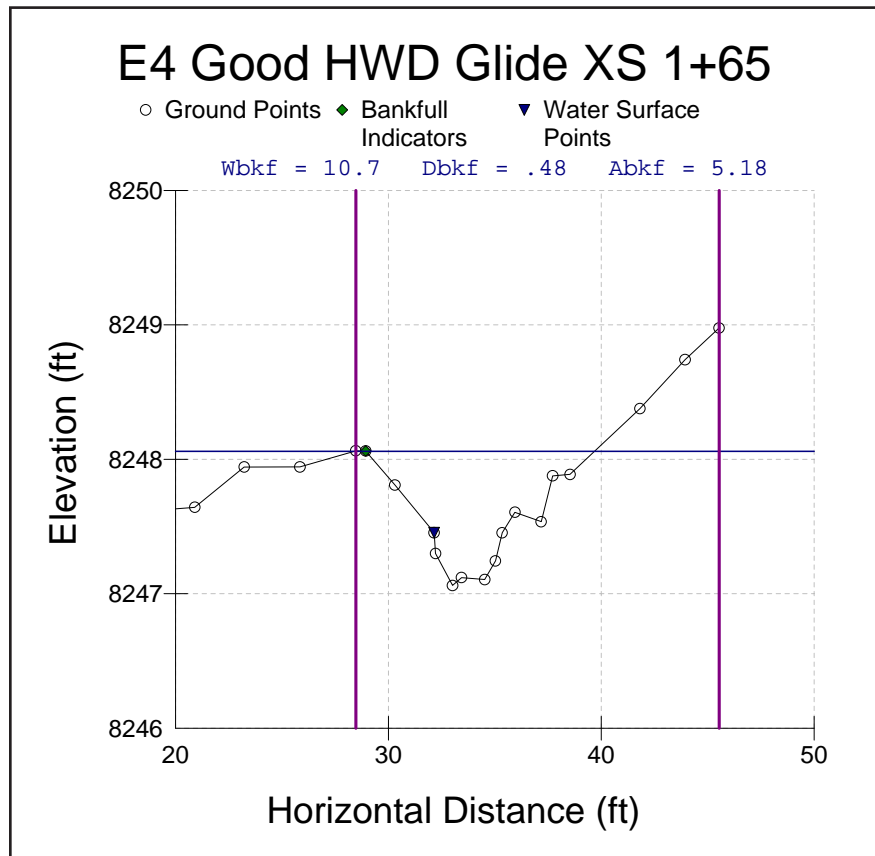
Pool Cross-section 0+88 (graph generated from RIVERMorph™)



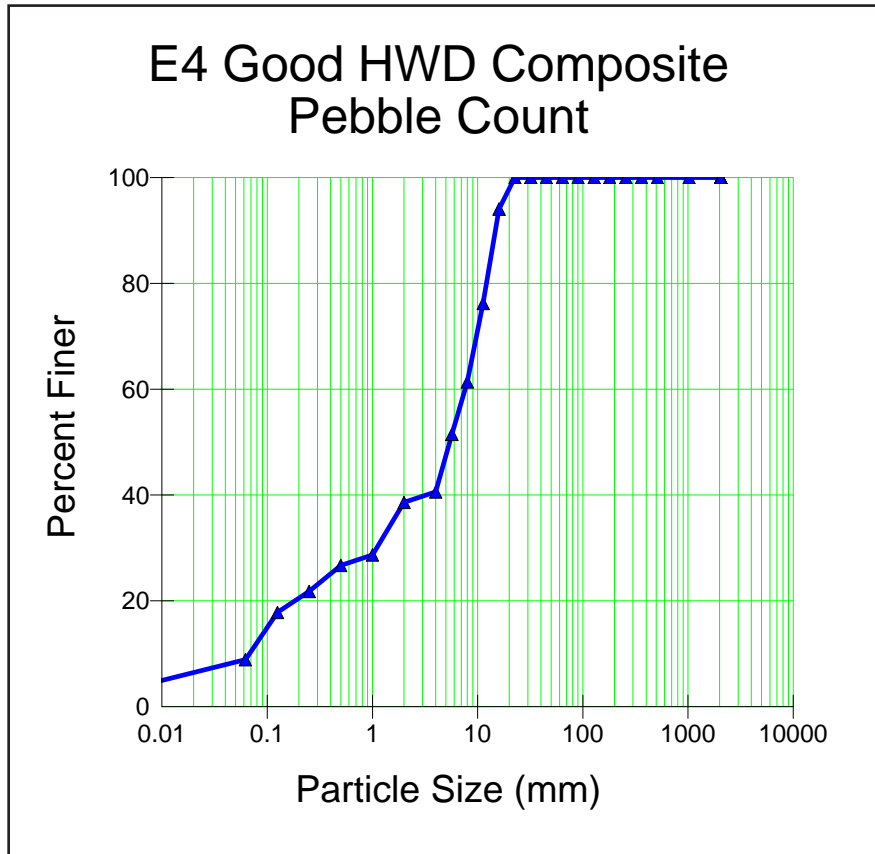
Pool Cross-section 0+50.8 (graph generated from RIVERMorph™)



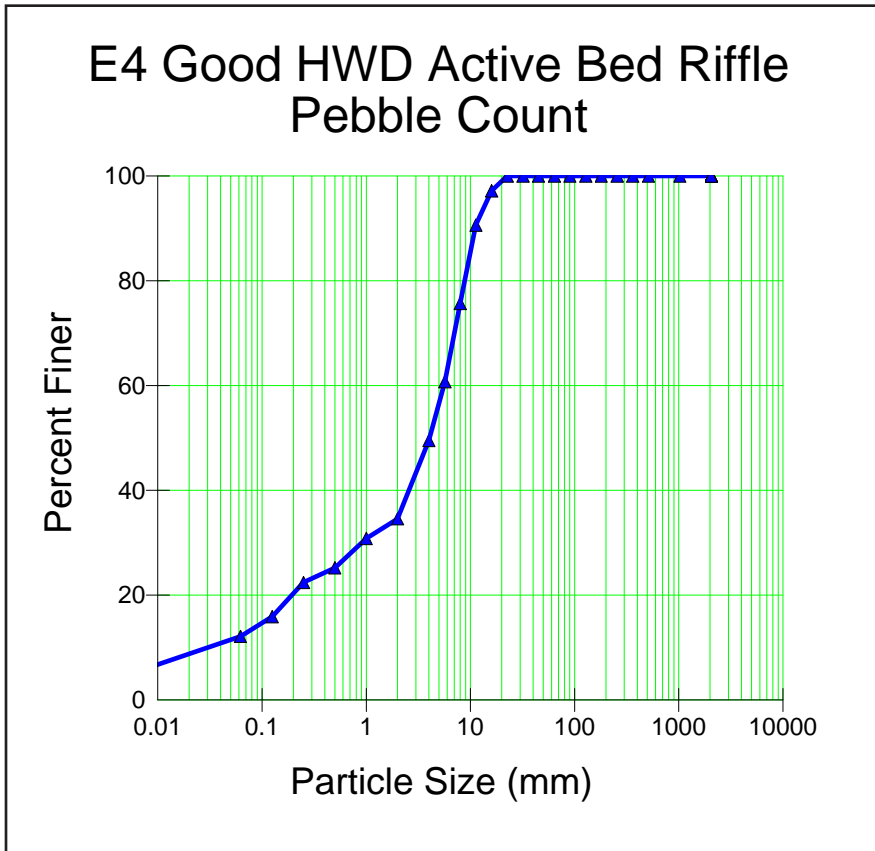
Glide Cross-section 1+37 (graph generated from RIVERMorph™)



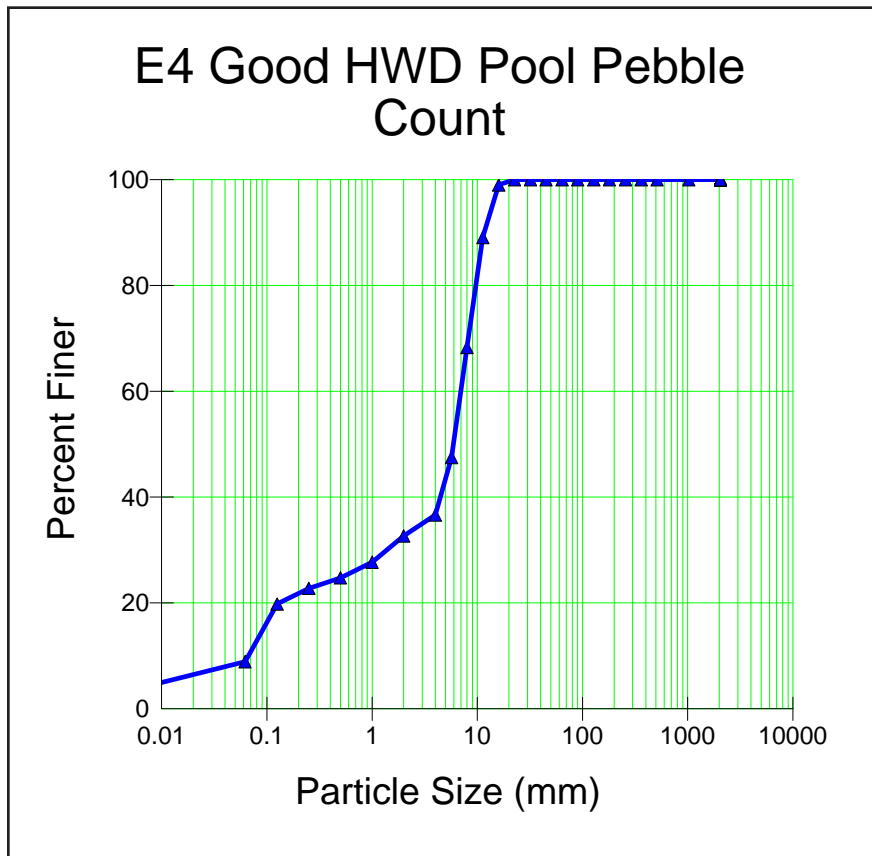
Glide Cross-section 1+65 (graph generated from RIVERMorph™)



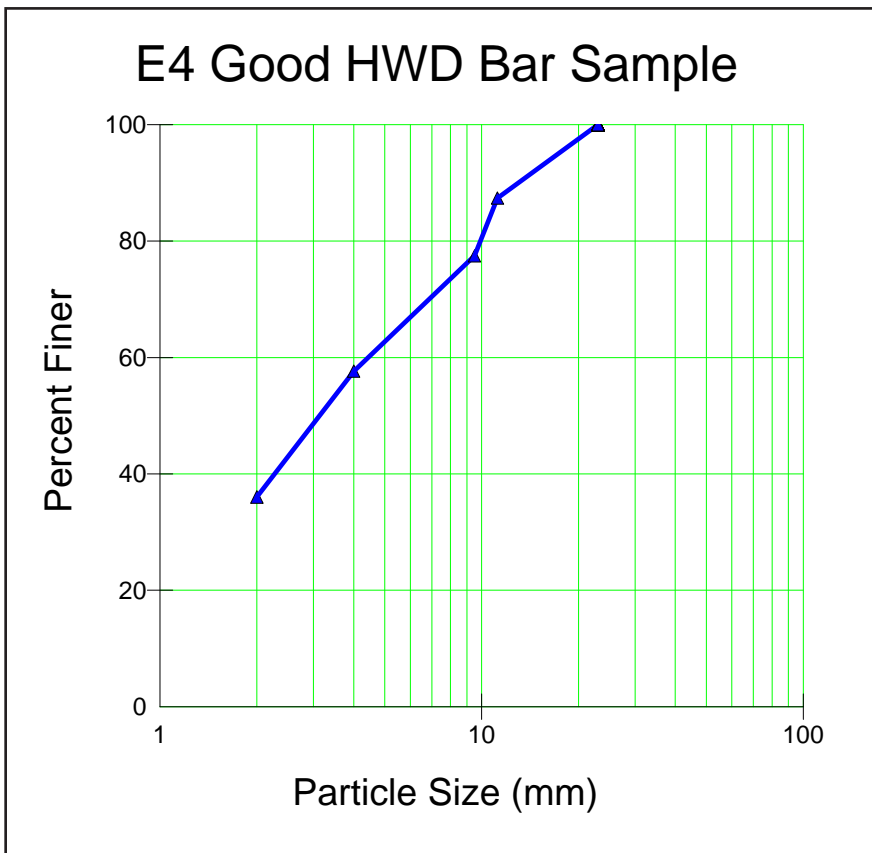
**Composite Pebble Count** (graph generated from RIVERMorph™)



**Active Bed Riffle Pebble Count** (graph generated from RIVERMorph™)



Pool Pebble Count (graph generated from RIVERMorph™)



Bar Sample (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates					
Stream:	Trail Creek, E4 Good HWD Reach		Location:	Riffle XS 1+13, Pike N.F., Colorado	
Date:	8/23/2010	Stream Type:	E4	Valley Type:	X
Observers:	K. Wright & B. Kasun		HUC:	_ _ _ _ _	
INPUT VARIABLES			OUTPUT VARIABLES		
Bankfull Riffle Cross-Sectional AREA	3.63	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.61	$d_{bkf}$ (ft)
Bankfull Riffle WIDTH	5.93	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim (2 * d_{bkf}) + W_{bkf}$	7.15	$W_p$ (ft)
$D_{84}$ at Riffle	9.8	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.03	$D_{84}$ (ft)
Bankfull SLOPE	0.008	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	0.51	R (ft)
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness $R(ft) / D_{84}(ft)$	15.73	$R / D_{84}$
Drainage Area	7.7	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.362	$u^*$ (ft/sec)
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$			3.47	ft / sec	12.60 cfs
2. Roughness Coefficient: a) Manning's n from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.027$			3.14	ft / sec	11.40 cfs
2. Roughness Coefficient: b) Manning's n from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.032$			2.65	ft / sec	9.62 cfs
2. Roughness Coefficient: c) Manning's n from Jarrett (USGS): $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ <small>Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for Stream Types A1, A2, A3, B1, B2, B3, C2 &amp; E3</small>			1.22	ft / sec	4.43 cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) $u/u^*$			3.48	ft / sec	12.6 cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)				ft / sec	cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q =$ <input type="text"/> year $u = Q / A$				ft / sec	cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$				ft / sec	cfs
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation ( $R/D_{84}$ ) – Estimation Method 1					
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.					
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.					
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.					
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.					

**Worksheet 5-3.** Level II stream classification.

Stream: <b>Trail Creek, E4 Good HWD Reach</b>	
Basin:	Drainage Area: acres <b>7.7</b> mi <sup>2</sup>
Location: <b>Pike National Forest, Colorado</b>	
Twp.&Rge:	Sec.&Qtr.:
Cross-Section Monuments (Lat./Long.): <b>Riffle XS 1+13</b> Date: <b>08/23/201</b>	
Observers: <b>K. Wright &amp; B. Kasun</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>5.93</b> ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>0.61</b> ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>3.63</b> ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>9.72</b> ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>1.03</b> ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>32.23</b> ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>5.44</b> ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>5.47</b> mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.008</b> ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length ( $SL / VL$ ); or estimated from a ratio of valley slope divided by channel slope ( $VS / S$ ).	<b>1.46</b>

Stream Type

E4

(See Figure 2-14)



Worksheet 5-4a. Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, E4 Good HWD Reach</b>		Location: <b>Pike National Forest, Colorado</b>							
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/23/2010</b>		Valley Type: <b>X</b>		Stream Type: <b>E4</b>			
<b>River Reach Dimension Summary Data.....1</b>									
<b>Riffle Dimensions*</b> , **, ***, ****	<b>Riffle Dimensions*</b> , **, ***, ****	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Width ( $W_{bkt}$ )	<b>5.93</b>			ft	Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	<b>3.63</b>		
	Mean Riffle Depth ( $d_{bkt}$ )	<b>0.61</b>			ft	Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	<b>9.72</b>		
	Maximum Riffle Depth ( $d_{max}$ )	<b>1.03</b>			ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>1.69</b>		
	Width of Flood-Prone Area ( $W_{fpa}$ )	<b>32.2</b>			ft	Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )	<b>5.44</b>		
	Riffle Inner Berm Width ( $W_{ib}$ )	<b>2.6</b>			ft	Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )	<b>0.438</b>		
	Riffle Inner Berm Depth ( $d_{ib}$ )	<b>0.19</b>			ft	Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )	<b>0.311</b>		
	Riffle Inner Berm Area ( $A_{ib}$ )	<b>0.51</b>			ft <sup>2</sup>	Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )	<b>0.140</b>		
	Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )	<b>14.2</b>							
<b>Pool Dimensions*</b> , **, ***, ****	<b>Pool Dimensions*</b> , **, ***, ****	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Pool Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Pool Width ( $W_{bkfp}$ )	<b>6.34</b>	<b>4.70</b>	<b>7.97</b>	ft	Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )	<b>1.07</b>	<b>0.79</b>	<b>1.34</b>
	Mean Pool Depth ( $d_{bkfp}$ )	<b>0.86</b>	<b>0.81</b>	<b>0.91</b>	ft	Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )	<b>1.41</b>	<b>1.33</b>	<b>1.49</b>
	Pool Cross-Sectional Area ( $A_{bkfp}$ )	<b>5.39</b>	<b>4.29</b>	<b>6.48</b>	ft	Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )	<b>1.48</b>	<b>1.18</b>	<b>1.79</b>
	Maximum Pool Depth ( $d_{maxp}$ )	<b>1.37</b>	<b>1.36</b>	<b>1.38</b>	ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	<b>2.25</b>	<b>2.23</b>	<b>2.26</b>
	Pool Inner Berm Width ( $W_{ibp}$ )	<b>3.16</b>	<b>3.07</b>	<b>3.24</b>	ft	Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )	<b>0.498</b>	<b>0.484</b>	<b>0.511</b>
	Pool Inner Berm Depth ( $d_{ibp}$ )	<b>0.26</b>	<b>0.22</b>	<b>0.3</b>	ft	Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )	<b>0.30</b>	<b>0.26</b>	<b>0.35</b>
	Pool Inner Berm Area ( $A_{ibp}$ )	<b>0.83</b>	<b>0.68</b>	<b>0.98</b>	ft <sup>2</sup>	Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )	<b>0.15</b>	<b>0.13</b>	<b>0.18</b>
	Point Bar Slope ( $S_{pb}$ )	<b>0.19</b>	<b>0.13</b>	<b>0.24</b>	ft/ft	Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )			
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Run Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Run Width ( $W_{bkfr}$ )				ft	Run Width to Riffle Width ( $W_{bkfr} / W_{bkt}$ )			
	Mean Run Depth ( $d_{bkfr}$ )				ft	Mean Run Depth to Mean Riffle Depth ( $d_{bkfr} / d_{bkt}$ )			
	Run Cross-Sectional Area ( $A_{bkfr}$ )				ft	Run Area to Riffle Area ( $A_{bkfr} / A_{bkt}$ )			
	Maximum Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )			
	Run Width/Depth Ratio ( $W_{bkfr} / d_{bkfr}$ )				ft				
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Glide Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Glide Width ( $W_{bkfg}$ )	<b>9.85</b>	<b>8.95</b>	<b>10.74</b>	ft	Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )	<b>1.66</b>	<b>1.51</b>	<b>1.81</b>
	Mean Glide Depth ( $d_{bkfg}$ )	<b>0.50</b>	<b>0.48</b>	<b>0.52</b>	ft	Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )	<b>0.82</b>	<b>0.79</b>	<b>0.85</b>
	Glide Cross-Sectional Area ( $A_{bkfg}$ )	<b>4.91</b>	<b>4.64</b>	<b>5.18</b>	ft	Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )	<b>1.35</b>	<b>1.28</b>	<b>1.43</b>
	Maximum Glide Depth ( $d_{maxg}$ )	<b>0.97</b>	<b>0.94</b>	<b>1.00</b>	ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )	<b>1.59</b>	<b>1.54</b>	<b>1.64</b>
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )	<b>19.80</b>	<b>17.21</b>	<b>22.38</b>	ft/ft	Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )	<b>14.36</b>	<b>11.24</b>	<b>17.48</b>
	Glide Inner Berm Width ( $W_{ibg}$ )	<b>3.64</b>	<b>3.26</b>	<b>4.02</b>	ft	Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )	<b>0.370</b>	<b>0.331</b>	<b>0.408</b>
	Glide Inner Berm Depth ( $d_{ibg}$ )	<b>0.26</b>	<b>0.23</b>	<b>0.29</b>	ft	Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )	<b>0.520</b>	<b>0.460</b>	<b>0.580</b>
Glide Inner Berm Area ( $A_{ibg}$ )	<b>0.93</b>	<b>0.92</b>	<b>0.94</b>	ft <sup>2</sup>	Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )	<b>0.189</b>	<b>0.187</b>	<b>0.191</b>	
<b>Step**</b>	<b>Step Dimensions**</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Step Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Step Width ( $W_{bkfs}$ )				ft	Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )			
	Mean Step Depth ( $d_{bkfs}$ )				ft	Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )			
	Step Cross-Sectional Area ( $A_{bkfs}$ )				ft	Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )			
	Maximum Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
	Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )								

**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, E4 Good HWD Reach</b>		Location: <b>Pike National Forest, Colorado</b>							
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/23/2010</b>	Valley Type: <b>X</b>						
		Stream Type: <b>E4</b>							
<b>River Reach Summary Data.....2</b>									
<b>Hydraulics</b>	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $U_{bkt}$ )	<b>3.47</b>	ft/sec	Estimation Method	<b>FF/RR</b>				
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )	<b>12.60</b>	cfs	Drainage Area	<b>7.7</b> mi <sup>2</sup>				
<b>Channel Pattern</b>	<b>Geometry</b>			<b>Dimensionless Geometry Ratios</b>					
	Linear Wavelength ( $\lambda$ )	<b>35.5</b>	<b>25.5</b>	<b>49</b>	ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )	<b>5.99</b>	<b>4.30</b>	<b>8.26</b>
	Stream Meander Length ( $L_m$ )	<b>47.6</b>	<b>30.5</b>	<b>66.4</b>	ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )	<b>8.03</b>	<b>5.15</b>	<b>11.20</b>
	Radius of Curvature ( $R_c$ )	<b>7.4</b>	<b>4.5</b>	<b>10.4</b>	ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )	<b>1.25</b>	<b>0.75</b>	<b>1.75</b>
	Belt Width ( $W_{bit}$ )	<b>22.9</b>	<b>16.3</b>	<b>31.6</b>	ft	Meander Width Ratio ( $W_{bit} / W_{bkt}$ )	<b>3.86</b>	<b>2.75</b>	<b>5.33</b>
	Arc Length ( $L_a$ )	<b>11.64</b>	<b>8.2</b>	<b>14.2</b>	ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )	<b>1.96</b>	<b>1.38</b>	<b>2.39</b>
	Riffle Length ( $L_r$ )	<b>19.2</b>	<b>8.4</b>	<b>29.5</b>	ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )	<b>3.24</b>	<b>1.41</b>	<b>4.97</b>
	Individual Pool Length ( $L_p$ )	<b>10.1</b>	<b>6.9</b>	<b>17.5</b>	ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )	<b>1.70</b>	<b>1.16</b>	<b>2.95</b>
Pool to Pool Spacing ( $P_s$ )	<b>21.1</b>	<b>7.0</b>	<b>43.2</b>	ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )	<b>3.56</b>	<b>1.19</b>	<b>7.28</b>	
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )	<b>0.0117</b>	ft/ft	Average Water Surface Slope ( $S$ )	<b>0.008</b>	ft/ft	Sinuosity ( $S_{val} / S$ )	<b>1.46</b>	
	Stream Length (SL)	<b>90.0</b>	ft	Valley Length (VL)	<b>61.6</b>	ft	Sinuosity (SL / VL)	<b>1.46</b>	
	Low Bank Height (LBH)	start: <b>0.89</b> ft end: <b>0.94</b> ft		Max Bankfull Depth ( $d_{max}$ )	start: <b>1.00</b> ft end: <b>1.00</b> ft		Bank-Height Ratio (BHR) (LBH / $d_{max}$ )	start: <b>1.0</b> end: <b>1.0</b>	
	<b>Facet Slopes</b>			<b>Dimensionless Facet Slope Ratios</b>					
	Riffle Slope ( $S_{rit}$ )	<b>0.0130</b>	<b>0.0110</b>	<b>0.0150</b>	ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rit} / S$ )	<b>1.6250</b>	<b>1.3750</b>	<b>1.8750</b>
	Run Slope ( $S_{run}$ )	<b>0.0320</b>	<b>0.0140</b>	<b>0.0480</b>	ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )	<b>4.0000</b>	<b>1.7500</b>	<b>6.0000</b>
	Pool Slope ( $S_p$ )	<b>0.0050</b>	<b>0.0030</b>	<b>0.0070</b>	ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )	<b>0.6250</b>	<b>0.3750</b>	<b>0.8750</b>
	Glide Slope ( $S_g$ )	<b>0.0060</b>	<b>0.0060</b>	<b>0.0080</b>	ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )	<b>0.7500</b>	<b>0.7500</b>	<b>1.0000</b>
	Step Slope ( $S_s$ )				ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )			
	<b>Max Depths<sup>a</sup></b>			<b>Dimensionless Depth Ratios</b>					
	Max Riffle Depth ( $d_{maxr}$ )	<b>1.100</b>			ft	Max Riffle Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )	<b>1.803</b>		
	Max Run Depth ( $d_{maxr}$ )	<b>1.100</b>			ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )	<b>1.803</b>		
	Max Pool Depth ( $d_{maxp}$ )	<b>1.490</b>			ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	<b>2.443</b>		
	Max Glide Depth ( $d_{maxg}$ )	<b>1.000</b>			ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )	<b>1.639</b>		
Max Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )				
<b>Channel Materials</b>	<b>Reach<sup>b</sup></b>			<b>Reach<sup>b</sup></b>			<b>Protrusion Height<sup>d</sup></b>		
	% Silt/Clay	<b>8.91</b>	<b>12.15</b>	<b>0</b>	$D_{16}$	<b>0.1</b>	<b>0.1</b>	<b>0.0</b>	mm
	% Sand	<b>29.7</b>	<b>22.43</b>	<b>36.04</b>	$D_{35}$	<b>1.6</b>	<b>2.1</b>	<b>0.0</b>	mm
	% Gravel	<b>61.39</b>	<b>65.42</b>	<b>63.96</b>	$D_{50}$	<b>5.5</b>	<b>4.1</b>	<b>3.3</b>	mm
	% Cobble				$D_{84}$	<b>13.4</b>	<b>9.8</b>	<b>10.6</b>	mm
	% Boulder				$D_{95}$	<b>17.0</b>	<b>14.4</b>	<b>18.3</b>	mm
	% Bedrock				$D_{100}$	<b>22.6</b>	<b>22.6</b>	<b>23.0</b>	mm

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.  
<sup>b</sup> Composite sample of riffles and pools within the designated reach.      <sup>c</sup> Active bed of a riffle.      <sup>d</sup> Height of roughness feature above bed.

## Stability Indices

**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation					
Stream: <b>Trail Creek, E4 Good HWD Reach</b>		Location: <b>Pike National Forest, Colorado</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Reference reach <input type="checkbox"/>	Disturbed (impacted reach) <input checked="" type="checkbox"/>	Date: <b>8/23/2010</b>	
Existing species composition: <b>Willow, Thistle, Carex Juncus, Toad Flax, Grasses</b>		Potential species composition: <b>Same as Existing Composition</b>			
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition
<b>1. Overstory</b>	Canopy layer	85%	30%	<b>Willow</b>	60%
				<b>Carex</b>	20%
				<b>Juncus</b>	20%
				100%	
<b>2. Understory</b>	Shrub layer		20%	<b>Willow</b>	60%
				<b>Carex</b>	18%
				<b>Juncus</b>	18%
				<b>Water Hemlock</b>	5%
100%					
<b>3. Ground level</b>	Herbaceous		45%	<b>Annual Grasses</b>	50%
				<b>Brome</b>	40%
				<b>Thistle</b>	10%
	100%				
<b>3. Ground level</b>	Leaf or needle litter		5%	<b>Remarks:</b> Condition, vigor and/or usage of existing reach: <b>Needs invasive weed control</b>	
	Bare ground		0%		
*Based on crown closure.		**Based on basal area to surface area.		<b>Column total = 100%</b>	

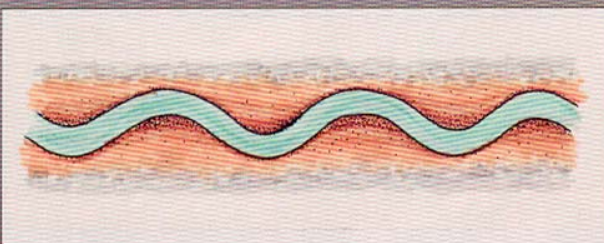



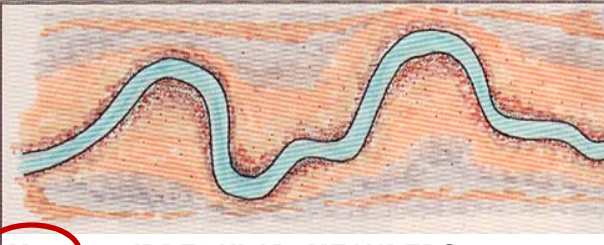
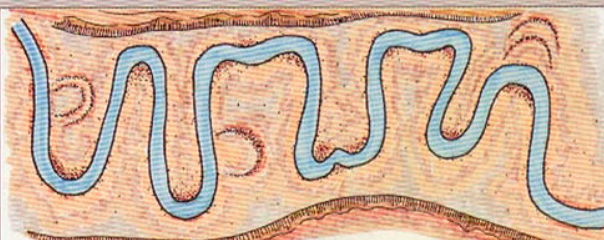
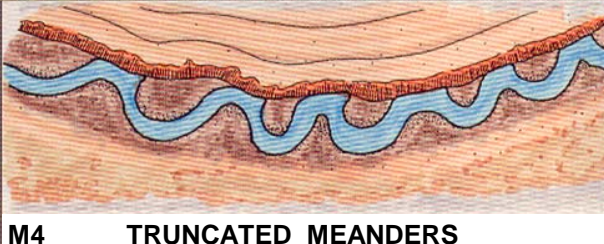
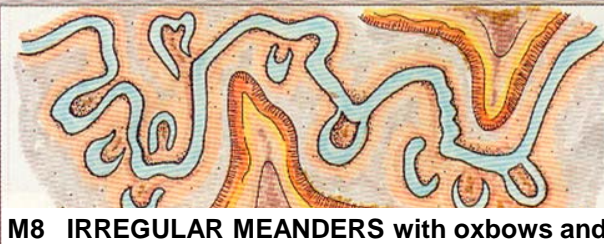
**Worksheet 5-7.** Flow regime.

<b>FLOW REGIME</b>								
Stream: <b>Trail Creek, E4 Good HWD</b>			Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>K. Wright &amp; B. Kasun</b>						Date: <b>8/23/2010</b>		
<b>List ALL COMBINATIONS that APPLY.....</b>			<b>P1</b>	<b>P2</b>	<b>P8</b>			
<b>General Category</b>								
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation							
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
<b>P</b>	Perennial stream channels: Surface water persists yearlong.							
<b>Specific Category</b>								
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
<b>4</b>	Streamflow regulated by glacial melt.							
<b>5</b>	Ice flows/ice torrents from ice dam breaches.							
<b>6</b>	Alternating flow/backwater due to tidal influence.							
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.							
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
<b>9</b>	Rain-on-snow generated runoff.							

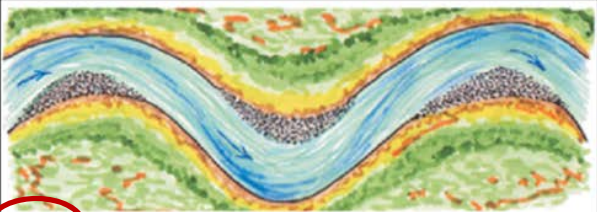


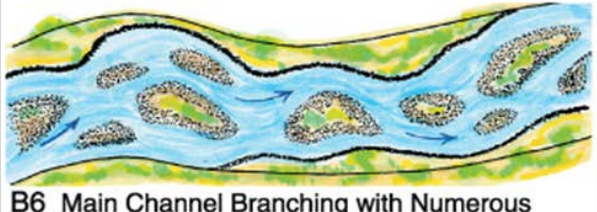

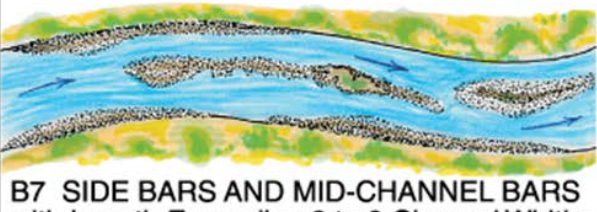

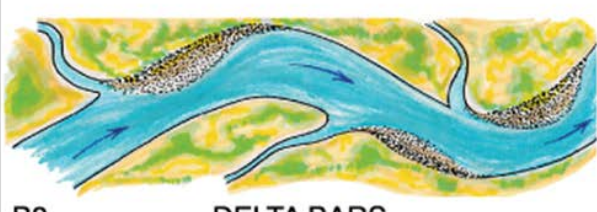
**Worksheet 5-8.** Stream order & stream size.

<b>Stream Size and Order</b>			
Stream:	<b>Trail Creek, E4 Good HWD Reach</b>		
Location:	<b>Pike National Forest, Colorado</b>		
Observers:	<b>K. Wright &amp; B. Kasun</b>		
Date:	<b>8/23/2010</b>		
<b>Stream Size Category and Order</b>			<b>S-3(3)</b>
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0.305	<1	<input type="checkbox"/>
S-2	0.3 – 1.5	1 – 5	<input type="checkbox"/>
<b>S-3</b>	<b>1.5 – 4.6</b>	<b>5 – 15</b>	<input checked="" type="checkbox"/>
S-4	4.6 – 9	15 – 30	<input type="checkbox"/>
S-5	9 – 15	30 – 50	<input type="checkbox"/>
S-6	15 – 22.8	50 – 75	<input type="checkbox"/>
S-7	22.8 – 30.5	75 – 100	<input type="checkbox"/>
S-8	30.5 – 46	100 – 150	<input type="checkbox"/>
S-9	46 – 76	150 – 250	<input type="checkbox"/>
S-10	76 – 107	250 – 350	<input type="checkbox"/>
S-11	107 – 150	350 – 500	<input type="checkbox"/>
S-12	150 – 305	500 – 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
<b>Stream Order</b>			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			

Worksheet 5-9. Meander patterns.

<b>Meander Patterns</b>					
Stream: <b>Trail Creek, E4 Good HWD Reach</b>			Location: <b>Pike National Forest, CO</b>		
Observers: <b>K. Wright &amp; B. Kasun</b>			Date: <b>8/23/2010</b>		
List ALL CATEGORIES that APPLY	<b>M3</b>				
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>					
					
<b>M1</b> <b>REGULAR MEANDERS</b>	<b>M5</b> <b>UNCONFINED MEANDER SCROLLS</b>				
					
<b>M2</b> <b>TORTUOUS MEANDERS</b>	<b>M6</b> <b>CONFINED MEANDER SCROLLS</b>				
					
<b>M3</b> <b>IRREGULAR MEANDERS</b>	<b>M7</b> <b>DISTORTED MEANDER LOOPS</b>				
					
<b>M4</b> <b>TRUNCATED MEANDERS</b>	<b>M8</b> <b>IRREGULAR MEANDERS with oxbows and</b>				

Worksheet 5-10. Depositional patterns.

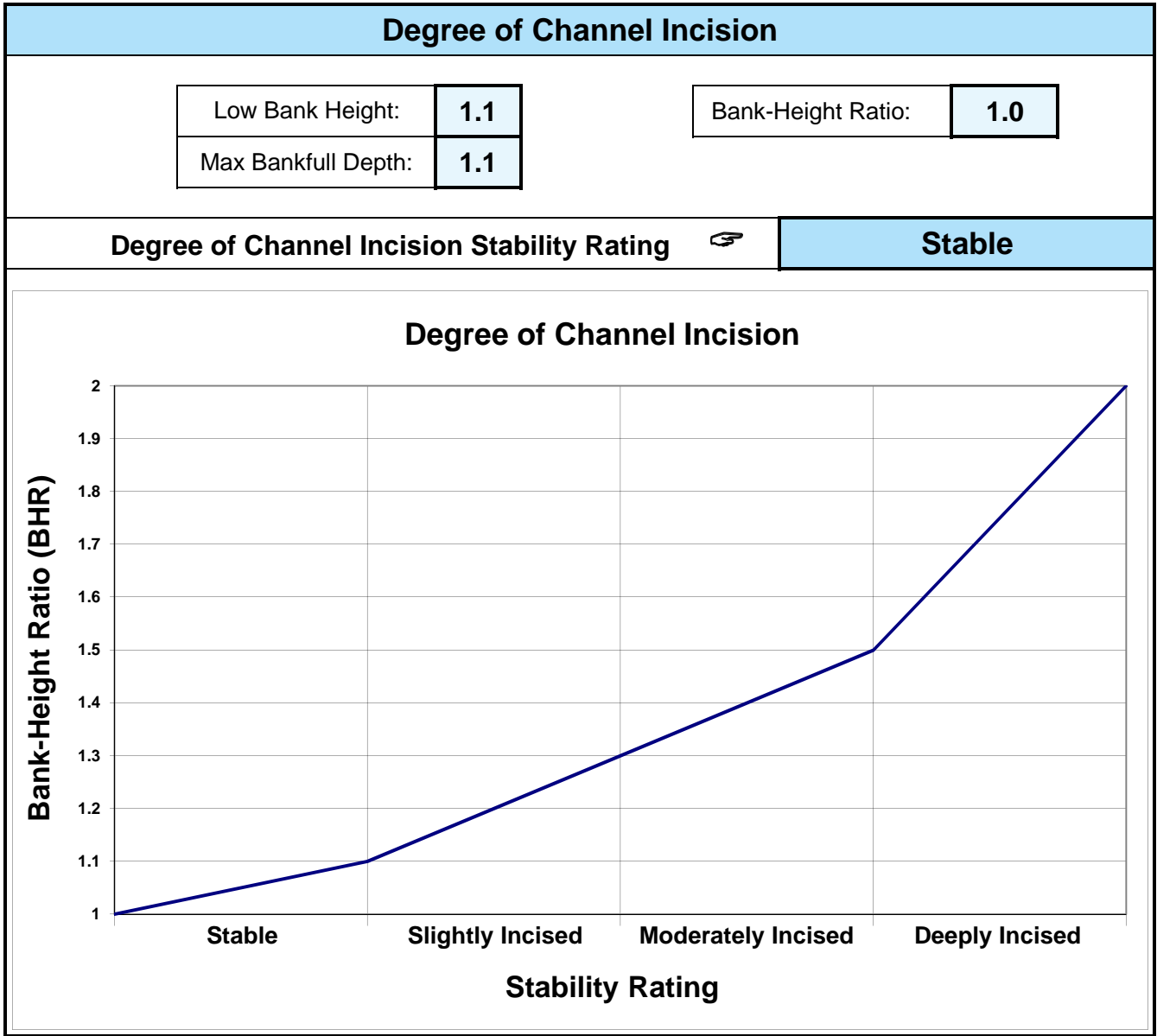
<b>Depositional Patterns</b>					
Stream: <b>Trail Creek, E4 Good HWD Reach</b>			Location: <b>Pike National Forest, Colorado</b>		
Observers: <b>K. Wright &amp; B. Kasun</b>			Date: <b>8/23/2010</b>		
List ALL CATEGORIES that APPLY		<b>B1</b>	<b>B4</b>		
<i>Various Depositional Features modified from Galay et al. (1973)</i>					
 <p style="margin-top: 5px;"><b>B1</b> POINT BARS</p>	 <p style="margin-top: 5px;"><b>B5</b> DIAGONAL BARS</p>				
 <p style="margin-top: 5px;"><b>B2</b> POINT BARS with Few MID-CHANNEL BARS</p>	 <p style="margin-top: 5px;"><b>B6</b> Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</p>				
 <p style="margin-top: 5px;"><b>B3</b> NUMEROUS MID-CHANNEL BARS</p>	 <p style="margin-top: 5px;"><b>B7</b> SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</p>				
 <p style="margin-top: 5px;"><b>B4</b> SIDE BARS</p>	 <p style="margin-top: 5px;"><b>B8</b> DELTA BARS</p>				

**Worksheet 5-11.** Channel blockages.

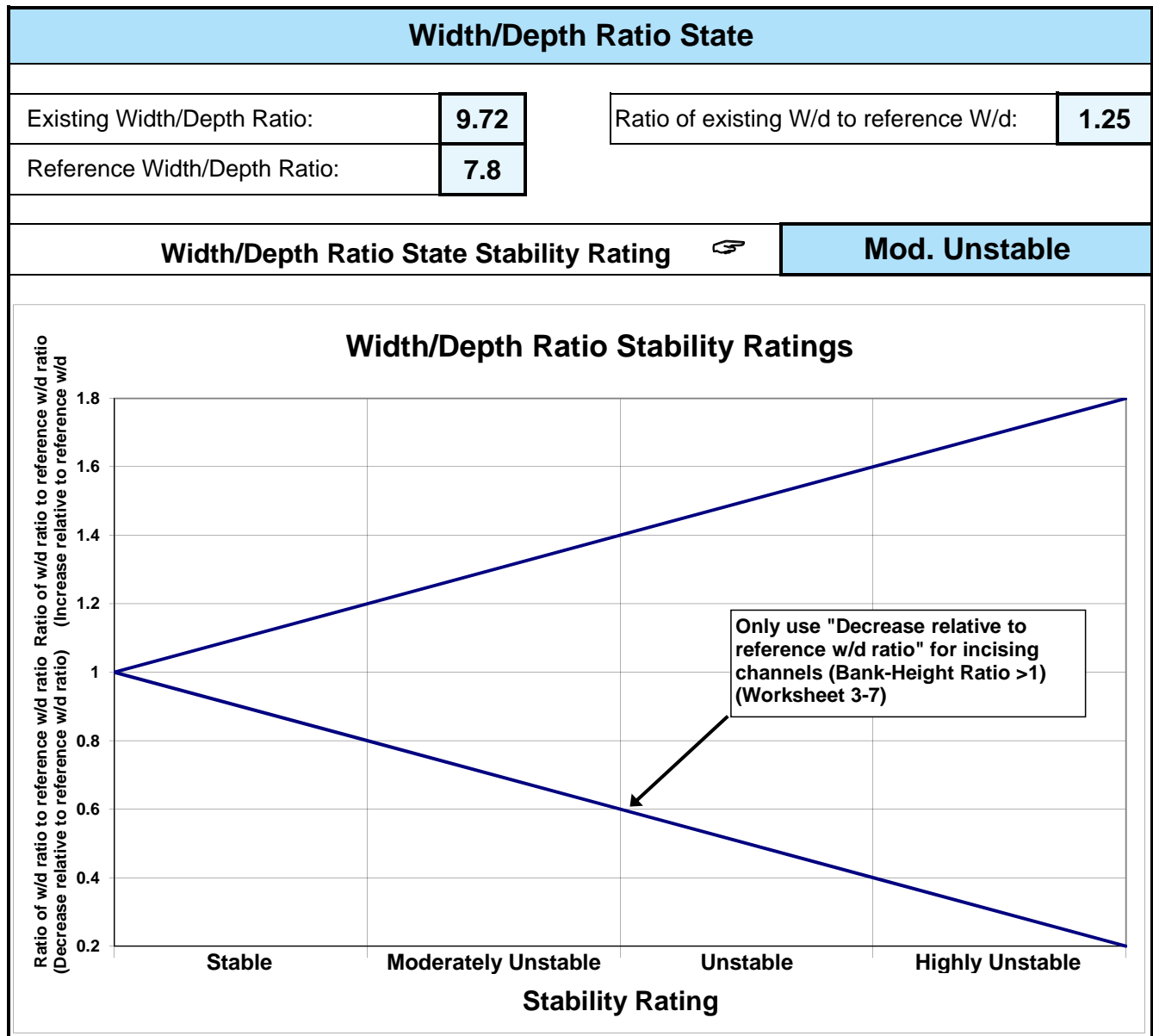
Channel Blockages		
Stream: <b>Trail Creek, E4 Good HWD Reach</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/23/2010</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input checked="" type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input type="checkbox"/>
<b>D4</b> Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>



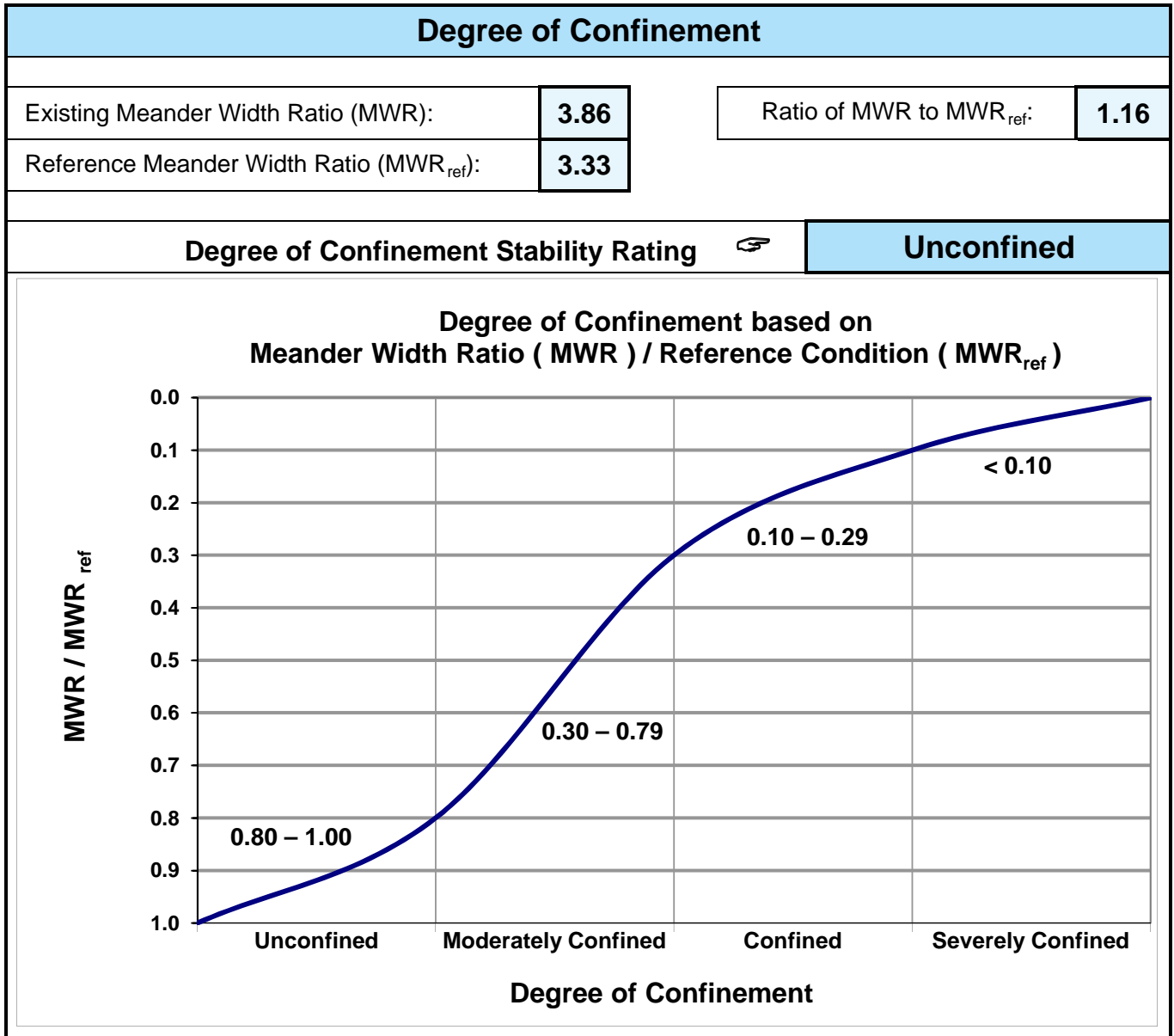
Worksheet 5-12. Degree of channel incision.



**Worksheet 5-13.** Width/depth ratio state.



**Worksheet 5-14.** Degree of channel confinement (lateral containment).



Worksheet 5-15. Pflankuch channel stability rating.

Stream: Trail Creek, E4 Good HWD Reach		Location: Pike National Forest, CO			Valley Type: X			Observers: K. Wright & B. Kasun			Date: 8/23/2010		
Loca- tion	Key Category	Excellent			Good			Fair			Poor		
		Description	Rating		Description	Rating		Description	Rating		Description	Rating	
Upper banks	1	Landform slope	Bank slope gradient <30%.	2	Bank slope gradient 30-40%.	4	Bank slope gradient 40-60%.	6	Bank slope gradient > 60%.	8			
	2	Mass erosion	No evidence of past or future mass erosion.	3	Infrequent. Mostly healed over. Low future potential.	6	Frequent or large, causing sediment nearly yearlong.	9	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.	12			
	3	Debris jam potential	Essentially absent from immediate channel area.	2	Present, but mostly small twigs and limbs.	4	Moderate to heavy amounts, mostly larger sizes.	6	Moderate to heavy amounts, predominantly larger sizes.	8			
	4	Vegetative bank protection	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	3	70-90% density. Fewer species or less vigor suggest less dense or deep root mass.	6	50-70% density. Lower vigor and fewer species from a shallow, discontinuous root mass.	9	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.	12			
Lower banks	5	Channel capacity	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0.	1	Bankfull stage is contained within banks. Width/depth ratio departure from reference width/depth ratio = 1.0-1.2. Bank-Height Ratio (BHR) = 1.0-1.1.	2	20-40%. Most in the 3-6" diameter class.	3	Bankfull stage is not contained; over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.	4			
	6	Bank rock content	> 65% with large angular boulders. 12"+ common.	2	40-65%. Mostly boulders and small cobbles 6-12".	4	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	6	<20% rock fragments of gravel sizes, 1-3" or less.	8			
	7	Obstructions to flow	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	2	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	4	Significant. Cuts 12-24" high. Root mat overhangs and sloughing evident.	12	Frequent obstructions and deflectors cause bank erosion yearlong. Sediment traps full, channel migration occurring.	16			
	8	Cutting	Little or none. Infrequent raw banks <6".	5	Some, intermittently at outcrops and to 12".	6	Moderate deposition of new gravel and coarse sand on old and some new bars.	12	Almost continuous cuts, some over 24" high. Failure of overhangs frequent.	16			
Bottom	9	Deposition	Little or no enlargement of channel or point bars.	4	Some new bar increase, mostly from coarse gravel.	8	Comers and edges well rounded in 2 dimensions.	3	Well rounded in all dimensions, surfaces smooth.	4			
	10	Rock angularity	Sharp edges and corners. Plane surfaces rough.	1	Rounded corners and edges. Surfaces smooth and flat.	2	Mixture dull and bright, i.e., 35-65% bright mixture range.	3	Predominantly bright, > 65% exposed or scored surfaces.	4			
	11	Brightness	Surfaces dull, dark or stained. Generally not bright.	1	Mostly dull, but may have <35% bright surfaces.	2	Mostly loose assortment with no apparent overlap.	7	No packing evident. Loose assortment, easily moved.	8			
	12	Consolidation of particles	Assorted sizes tightly packed or overlapping.	2	Moderately packed with some overlapping.	4	Moderate change in sizes. Stable materials 20-50%.	12	Marked distribution change. Stable materials 0-20%.	16			
Stream type	13	Bottom size distribution	No size change evident. Stable material 80-100%.	4	Distribution shift light. Stable material 50-80%.	8	30-50% affected. Deposits and scour at obstructions, constrictions and bends. Some filling of pools.	18	More than 50% of the bottom in a state of flux or change nearly yearlong.	24			
	14	Scouring and deposition	<5% of bottom affected by scour or deposition.	6	5-30% affected. Scour at constrictions and where grades steepen. Some deposition in pools.	12	Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick.	3	Perennial types scarce or absent. Yellow-green, short-term bloom may be present.	4			
	15	Aquatic vegetation	Abundant growth moss-like, dark green perennial. In swift water too.	1	Common. Algae forms in low velocity and pool areas. Moss here too.	2							
		<b>Excellent total = 32</b>			<b>Good total = 2</b>			<b>Fair total = 10</b>			<b>Poor total = 12</b>		
		<b>Grand total = 56</b>			<b>Existing stream type = E4</b>			<b>*Potential stream type = E4</b>			<b>Modified channel stability rating = Good</b>		

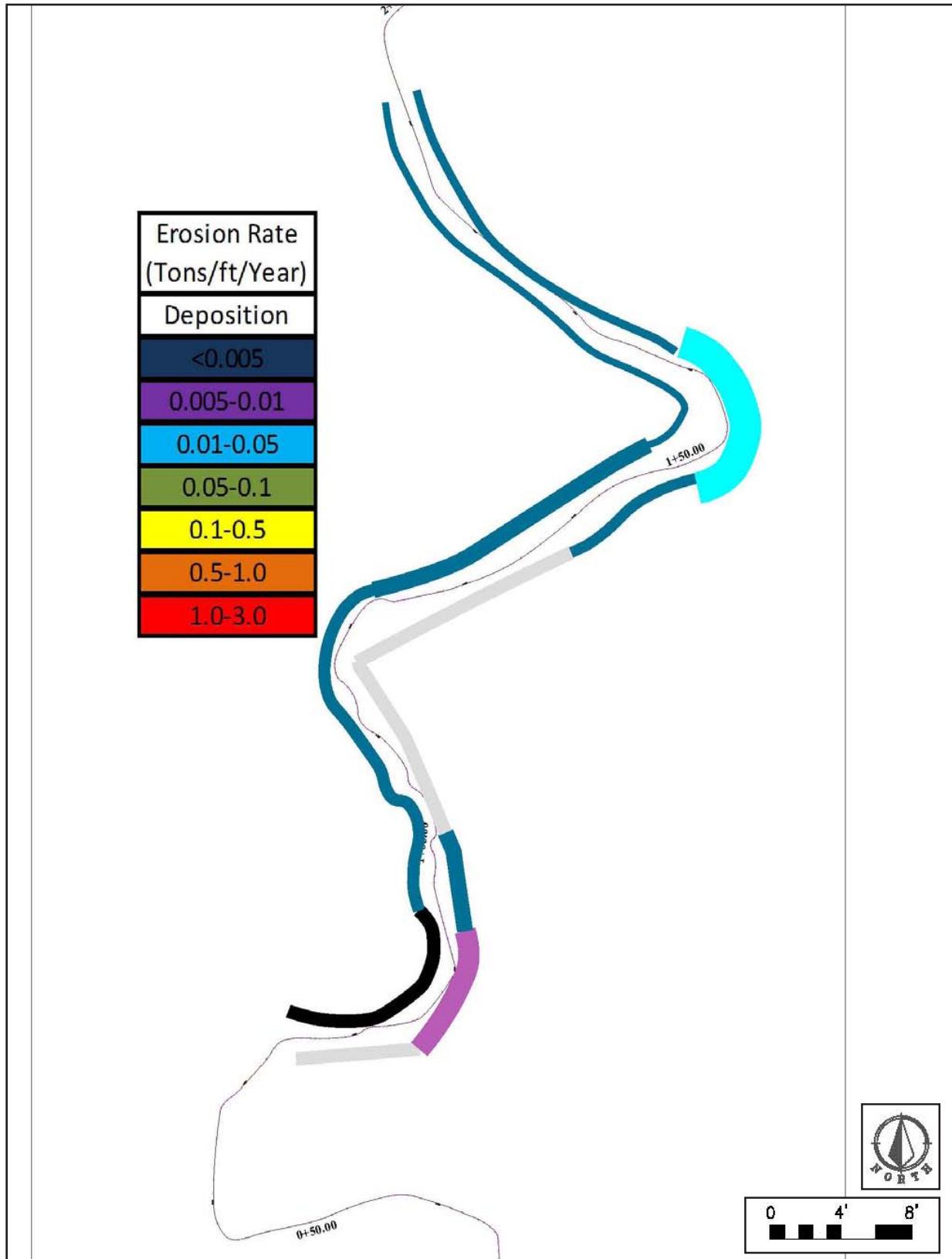
\*Rating is adjusted to potential stream type, not existing.

## BANCS Model – Streambank Erosion

Worksheet 5-18. Annual streambank erosion estimates.

Stream: <b>Trail Creek, E4 Good HWD Reach</b>		Location: <b>Pike National Forest, Colorado</b>					
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>90</b>				Date: <b>8/23/2010</b>	
Observers: <b>K. Wright &amp; B. Kasun</b>		Valley Type: <b>X</b>			Stream Type: <b>E4</b>		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 5-16) (adjective)	NBS rating (Worksheet 5-17) (adjective)	Bank erosion rate (Figure 5-34 or 5-35) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal $[(4) \times (5) \times (6)]$ (ft <sup>3</sup> /yr)	Erosion Rate $\{[(7)/27] \times 1.3 / (5)\}$ (tons/yr/ft)
1. <b>O+08 - 0+16</b> RB	Low	High	0.15505	8.0	1.6	1.98	0.01194
2. <b>0+16 - 0+26</b> RB	Low	Moderate	0.07435	10.0	1.2	0.89	0.00430
3. <b>0+17-0+35</b> LB	Low	Low	0.03566	18.0	0.9	0.58	0.00155
4. <b>0+35-0+45</b> LB	Low	Moderate	0.07435	10.0	0.9	0.67	0.00322
5. <b>0+62-0+69</b> RB	Low	Low	0.03566	7.0	0.8	0.20	0.00137
6. <b>0+45 - 0+69</b> LB	Very Low	High	0.02130	1.0	1.2	0.03	0.00123
7. <b>0+69 - 0+77</b> RB	Moderate	High	0.42031	8.0	2.4	8.07	0.04857
8. <b>0+69 - 0+90</b> LB	Low	Low	0.03566	21.0	0.5	0.37	0.00086
9. <b>0+77 - 0+90</b> RB	Low	Low	0.03566	13.0	0.6	0.28	0.00103
10							
11							
12							
13							
14							
15							
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					Total Erosion (ft <sup>3</sup> /yr)	13.07	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					Total Erosion (yds <sup>3</sup> /yr)	0.48	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					Total Erosion (tons/yr)	0.63	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					Total Erosion (tons/yr/ft)	0.0070	

**Streambank Erosion Map**



## FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Equation Type		Equation Source		Equation		Bankfull Discharge (cfs)		Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)				
1. Bedload Sediment		"Good/Fair" Pagosa		$y = -0.0113x + 1.0139x^{2.1929}$		12.6		0.0148		16.998				
2. Suspended Sediment		"Good/Fair" Pagosa		$y = 0.0636 + 0.9326x^{2.4085}$										
From Dimensional Flow-Duration Curve														
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Percentage of Time	Daily Mean Discharge (cfs)	Mid-Ordinate (%)	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow (cfs)	Dimensionless Streamflow	Dimensionless Suspended Sediment Discharge ( $S/S_{Bkt}$ )	Suspended Sediment Discharge (tons/day)	Dimensionless Bedload Discharge ( $b_b/b_{Bkt}$ )	Bedload Sediment Discharge (tons/day)	Time Adjusted Streamflow $[(5) \times (6)]$ (cfs)	Suspended Sediment $[(5) \times (9)]$ (tons)	Bedload Sediment $[(5) \times (11)]$ (tons)	Suspended Sediment + Bedload Sediment $[(13) + (14)]$ (tons)
0%	32.0													
0.10%	27.5	0.05%	0.09%	0.34	29.8	2.363	7.461	10.19	6.670	9.40	10.2	3.50	3.22	6.72
0.25%	23.8	0.08%	0.15%	0.55	25.7	2.036	5.232	6.16	4.809	6.78	14.0	3.37	3.71	7.08
0.50%	20.6	0.13%	0.25%	0.91	22.2	1.761	3.706	3.77	3.494	4.92	20.2	3.44	4.49	7.93
0.75%	17.6	0.13%	0.25%	0.91	19.1	1.513	2.592	2.27	2.502	3.53	17.4	2.07	3.22	5.29
1%	15.2	0.13%	0.25%	0.91	16.4	1.300	1.817	1.37	1.790	2.52	14.9	1.25	2.30	3.55
1.5%	13.0	0.25%	0.50%	1.83	14.1	1.120	1.289	0.84	1.289	1.82	25.8	1.52	3.31	4.84
2%	10.9	0.25%	0.50%	1.83	12.0	0.949	0.886	0.49	0.893	1.26	21.8	0.89	2.30	3.18
3%	9.2	0.50%	1.00%	3.65	10.0	0.795	0.600	0.28	0.602	0.85	36.6	1.01	3.09	4.10
4%	7.8	0.50%	1.00%	3.65	8.5	0.674	0.424	0.17	0.415	0.59	31.0	0.60	2.14	2.74
5%	7.0	0.50%	1.00%	3.65	7.4	0.587	0.322	0.11	0.304	0.43	27.0	0.40	1.56	1.96
10%	4.4	2.50%	5.00%	18.25	5.7	0.450	0.200	0.05	0.165	0.23	103.5	0.95	4.24	5.19
20%	2.4	5.00%	10.00%	36.50	3.4	0.269	0.103	0.02	0.045	0.06	123.5	0.58	2.34	2.92
30%	1.6	5.00%	10.00%	36.50	2.0	0.158	0.075	0.01	0.006	0.01	72.6	0.25	0.33	0.58
40%	1.1	5.00%	10.00%	36.50	1.4	0.108	0.068	0.00	0.000	0.00	49.6	0.15	0.00	0.15
50%	0.9	5.00%	10.00%	36.50	1.0	0.079	0.066	0.00	0.000	0.00	36.3	0.11	0.00	0.11
60%	0.7	5.00%	10.00%	36.50	0.8	0.061	0.065	0.00	0.000	0.00	27.8	0.08	0.00	0.08
70%	0.5	5.00%	10.00%	36.50	0.6	0.047	0.064	0.00	0.000	0.00	21.8	0.06	0.00	0.06
80%	0.5	5.00%	10.00%	36.50	0.5	0.039	0.064	0.00	0.000	0.00	18.2	0.05	0.00	0.05
90%	0.3	5.00%	10.00%	36.50	0.4	0.032	0.064	0.00	0.000	0.00	14.5	0.04	0.00	0.04
100%	0.1	5.00%	10.00%	36.50	0.2	0.016	0.064	0.00	0.000	0.00	7.3	0.02	0.00	0.02
<b>Annual Totals:</b>						694.2 (cfs)	1,376.9 (acre-ft)	20.4 (tons/yr)	36.3 (tons/yr)	56.6 (tons/yr)				

**Worksheet 19b.** Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Equation Type		Equation Source		Equation		Bankfull Discharge (cfs)		Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)					
1. Bedload Sediment		"Good/Fair" Pagosa		$y = -0.0113x + 1.0139x^{2.1929}$		12.6		0.0148		16.998					
2. Suspended Sediment		"Good/Fair" Pagosa		$y = 0.0636 + 0.9326x^{2.4085}$											
From Dimensional Flow-Duration Curve															
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)				
Percentage of Time	Daily Mean Discharge (cfs)	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Suspended Sediment Discharge	Suspended Sediment Discharge	Dimensionless Bedload Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow [(5)×(6)]				
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>bed</sub> )	(S/S <sub>bed</sub> )	(tons/day)	(b <sub>s</sub> /b <sub>bed</sub> )	(tons/day)	(cfs)				
(15)	(14)	(13)									(15)				
Suspended + Bedload Sediment [(13)×(14)]	Bedload Sediment [(5)×(11)]	Suspended Sediment [(5)×(9)]									(tons)				
0%	48.3														
0.10%	43.8	0.05%	0.09%	0.34	46.0	3.654	21.209	44.82	17.374	24.48	15.8	15.38	8.40	23.78	
0.25%	40.1	0.08%	0.15%	0.55	41.9	3.327	16.937	32.59	14.144	19.93	23.0	17.84	10.91	28.75	
0.50%	36.8	0.13%	0.25%	0.91	38.5	3.052	13.769	24.30	11.702	16.49	35.1	22.17	15.04	37.22	
0.75%	33.8	0.13%	0.25%	0.91	35.3	2.804	11.241	18.23	9.718	13.69	32.2	16.63	12.49	29.13	
1%	31.5	0.13%	0.25%	0.91	32.6	2.591	9.303	13.94	8.169	11.51	29.8	12.72	10.50	23.22	
1.5%	29.1	0.25%	0.50%	1.83	30.3	2.403	7.764	10.79	6.919	9.75	55.2	19.69	17.79	37.48	
2%	26.7	0.25%	0.50%	1.83	27.9	2.213	6.383	8.17	5.777	8.14	50.9	14.91	14.86	29.76	
3%	25.0	0.50%	1.00%	3.65	25.8	2.050	5.319	6.31	4.883	6.88	94.3	23.01	25.11	48.12	
4%	22.4	0.50%	1.00%	3.65	23.7	1.878	4.318	4.69	4.026	5.67	86.4	17.11	20.71	37.82	
5%	19.7	0.50%	1.00%	3.65	21.0	1.671	3.274	3.16	3.113	4.39	76.8	11.54	16.01	27.55	
10%	12.3	2.50%	5.00%	18.25	16.0	1.271	1.725	1.27	1.704	2.40	292.3	23.14	43.82	66.96	
20%	3.8	5.00%	10.00%	36.50	8.0	0.637	0.378	0.14	0.366	0.52	293.0	5.09	18.81	23.90	
30%	1.7	5.00%	10.00%	36.50	2.7	0.216	0.087	0.01	0.024	0.03	99.5	0.40	1.23	1.63	
40%	1.1	5.00%	10.00%	36.50	1.4	0.112	0.068	0.00	0.000	0.00	51.3	0.16	0.00	0.16	
50%	0.9	5.00%	10.00%	36.50	1.0	0.079	0.066	0.00	0.000	0.00	36.3	0.11	0.00	0.11	
60%	0.7	5.00%	10.00%	36.50	0.8	0.061	0.065	0.00	0.000	0.00	27.8	0.08	0.00	0.08	
70%	0.5	5.00%	10.00%	36.50	0.6	0.047	0.064	0.00	0.000	0.00	21.8	0.06	0.00	0.06	
80%	0.5	5.00%	10.00%	36.50	0.5	0.039	0.064	0.00	0.000	0.00	18.2	0.05	0.00	0.05	
90%	0.3	5.00%	10.00%	36.50	0.4	0.032	0.064	0.00	0.000	0.00	14.5	0.04	0.00	0.04	
100%	0.1	5.00%	10.00%	36.50	0.2	0.016	0.064	0.00	0.000	0.00	7.3	0.02	0.00	0.02	
<b>Annual Totals:</b>										1,361.4 (cfs)		200.2 (tons/yr)		415.9 (tons/yr)	
										2,700.4 (acre-ft)					



## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>Trail Creek, E4 Good HWD Reach</b>		Stream Type: <b>E4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>X</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8-23-2010</b>			
<b>Enter Required Information for Existing Condition</b>					
4.1	$D_{50}$	Riffle bed material $D_{50}$ (mm)			
3.3	$\hat{D}_{50}$	Bar sample $D_{50}$ (mm)			
0.08	$D_{max}$	Largest particle from bar sample (ft)	23	(mm)	304.8 mm/ft
0.008	S	Existing bankfull water surface slope (ft/ft)			
0.52	d	Existing bankfull mean depth (ft)			
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment			
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>					
1.24	$D_{50}/\hat{D}_{50}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 ( D_{50}/\hat{D}_{50} )^{-0.872}$		
5.65	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 ( D_{max}/D_{50} )^{-0.887}$		
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED:		
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	d	Required bankfull mean depth (ft)	$d = \frac{\tau^*(\gamma_s - 1)D_{max}}{S}$ (use $D_{max}$ in ft)		
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	S	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^*(\gamma_s - 1)D_{max}}{d}$ (use $D_{max}$ in ft)		
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					
<b>Sediment Competence Using Dimensional Shear Stress</b>					
0.260	Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d) $\gamma = 62.4$ , d = existing depth, S = existing slope				
Shields 18	CO 58	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ (Figure 5-49)			
Shields 0.32	CO 0.08	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) (Figure 5-49)			
Shields 0.64	CO 0.16	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm) $\tau =$ predicted shear stress, $\gamma = 62.4$ , S = existing slope	$d = \frac{\tau}{\gamma S}$		
Shields 0.0099	CO 0.0025	Predicted slope required to initiate movement of measured $D_{max}$ (mm) $\tau =$ predicted shear stress, $\gamma = 62.4$ , d = existing depth	$S = \frac{\tau}{\gamma d}$		
Check: <input checked="" type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					

## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>Trail Creek, E4 Good HWD</b>		Stream Type: <b>E4</b>
Location: <b>Pike National Forest, CO</b>		Valley Type: <b>X</b>
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/23/2010</b>
<b>Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)</b>	<b>Stability Rating (Check Appropriate Rating)</b>	
<b>Stream Type at Potential, (C→E)</b> E-C-Gc-F-C-E	<input checked="" type="checkbox"/> Stable	
(E→C), (C→High W/d C)	<input type="checkbox"/> Moderately Unstable	
(G→F), (F→D), (C→F)	<input type="checkbox"/> Unstable	
(C→D), (B→G), (D→G), (C→G), (E→G)	<input type="checkbox"/> Highly Unstable	

Worksheet 5-25. Lateral stability.

Stream: <b>Trail Creek, E4 Good HWD Reach</b>		Stream Type: <b>E4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>X</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/23/2010</b>			
Lateral stability criteria (choose one stability category for each criterion 1–5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	4
	(2)	1.25 (4)	(6)	(8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	2
	(1)	B1, B4 (2)	(3)	(4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		1
	M3 (1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	2
	L/L (2)	(4)	(6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	1
	0.88 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>10</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input checked="" type="checkbox"/>	<i>Unstable</i> 13 – 21 <input type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	

**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>Trail Creek, E4 Good HWD Reach</b>		Stream Type: <b>E4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>X</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/23/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
1 <b>Sediment competence</b> (Worksheet 5-22)	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope—slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	2
	(2)	(4)	(6)	(8)	
2 <b>Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	2
	(2)	(4)	(6)	(8)	
3 <b>W/d Ratio State</b> (Worksheet 5-13)	1.0 – 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	4
	(2)	1.3 (4)	(6)	(8)	
4 <b>Stream Succession States</b> (Worksheet 5-24)	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	2
	at potential (2)	(4)	(6)	(8)	
5 <b>Depositional Patterns</b> (Worksheet 5-10)	B1	B2, B4	B3, B5	B6, B7, B8	2
	(1)	B1, B4 (2)	(3)	(4)	
6 <b>Debris / Blockages</b> (Worksheet 5-11)	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	1
	D1 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>13</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
Vertical Stability for Excess Deposition / Aggradation (use total points and check stability rating)	<i>No Deposition</i> 10 – 14 <input checked="" type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input type="checkbox"/>	<i>Aggradation</i> > 30 <input type="checkbox"/>	

Worksheet 5-27. Vertical stability – degradation.

Stream: <b>Trail Creek, E4 Good HWD Reach</b>		Stream Type: <b>E4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>X</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/23/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>1 Sediment Competence</b> (Worksheet 5-22)	Does not indicate excess competence	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed	$D_{100}$ of bed moved	Particles much larger than $D_{100}$ of bed moved	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>2 Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Does not indicate excess capacity	Slight excess energy: up to 10% increase above reference	Excess energy sufficient to increase load up to 50% of annual load	Excess energy transporting more than 50% of annual load	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>3 Degree of Channel Incision (BHR)</b> (Worksheet 5-12)	1.00 – 1.10	1.11 – 1.30	1.31 – 1.50	> 1.50	<b>2</b>
	1.00 (2)	(4)	(6)	(8)	
<b>4 Stream Succession States</b> (Worksheets 5-12 and 5-24)	Does not indicate incision or degradation	If BHR > 1.1 and stream type has W/d between 5–10	If BHR > 1.1 and stream type has W/d less than 5	(B→G), (C→G), (E→G), (D→G)	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>5 Confinement (MWR / MWR<sub>ref</sub>)</b> (Worksheet 5-14)	0.80 – 1.00	0.30 – 0.79	0.10 – 0.29	< 0.10	<b>1</b>
	1.16 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>9</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation</b> (use total points and check stability rating)	<i>Not Incised</i> 9 – 11 <input checked="" type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input type="checkbox"/>	<i>Degradation</i> > 27 <input type="checkbox"/>	

**Worksheet 5-28.** Channel enlargement.

Stream: <b>Trail Creek, E4 Good HWD Reach</b>		Stream Type: <b>E4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>X</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/23/2010</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1-4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	2
	at potential (2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	4
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	2
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	2
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>10</b>
<b>Category Point Range</b>					
<b>Channel Enlargement Prediction (use total points and check stability rating)</b>	<i>No Increase</i> 8 – 10 <input checked="" type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input type="checkbox"/>	<i>Extensive</i> > 24 <input type="checkbox"/>	

Worksheet 5-29. Overall sediment supply.

Stream: <b>Trail Creek, E4 Good HWD Reach</b>		Stream Type: <b>E4</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>X</b>		
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/23/2010</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1–5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	2	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	1	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	1	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	1	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	1	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>6</b>	
<b>Category Point Range</b>				
<b>Overall Sediment Supply Rating (use total points and check stability rating)</b>	<b>Low</b> 5 <input type="checkbox"/>	<b>Moderate</b> 6 – 10 <input checked="" type="checkbox"/>	<b>High</b> 11 – 15 <input type="checkbox"/>	<b>Very High</b> 16 – 20 <input type="checkbox"/>

Worksheet 5-32. Summary of stability condition categories.

Stream: <b>Trail Creek, E4 Good HWD Reach</b>		Date: <b>8/23/2010</b>		Location: <b>Pike National Forest, Colorado</b>		Stream Type: <b>E4</b>		Valley Type: <b>X</b>	
Observers: <b>K. Wright &amp; B. Kasun</b>		Bankfull Width (ft): <b>5.93</b>		Cross-Sectional Area (ft <sup>2</sup> ): <b>3.63</b>		Width of Flood-Prone Area (ft): <b>32.23</b>		Entrenchment Ratio: <b>5.44</b>	
Channel Dimension (Rifle XS 1+13)		Mean Bankfull Depth (ft): <b>0.61</b>		R <sub>d</sub> W <sub>bkf</sub> : <b>8.03</b>		MWR: <b>3.86</b>		Sinuosity: <b>1.46</b>	
Channel Pattern		L <sub>m</sub> W <sub>bkf</sub> : <b>4.3-8.26</b>		L <sub>m</sub> W <sub>bkf</sub> : <b>5.15-11.2</b>		R <sub>d</sub> W <sub>bkf</sub> : <b>7.5-1.75</b>		MWR: <b>2.75-5.33</b>	
River Profile & Bed Features		<input checked="" type="checkbox"/> Riffle/Pool <input type="checkbox"/> Step/Pool <input type="checkbox"/> Plane Bed <input type="checkbox"/> Convergence/Divergence <input type="checkbox"/> Dunes/Antidunes/Smooth Bed		Riffle		Pool		Slope	
		Depth Ratio (max to mean): <b>1.49</b>		Depth Ratio (max to mean): <b>1.8</b>		Pool Spacing: <b>2.4</b>		Valley: <b>0.0117</b>	
Level III Stream Stability Indices		Degree of Incision (Bank-Height Ratio): <b>1.0</b> Degree of Incision Stability Rating: <b>Stable</b>		Potential Composition/Density: <b>Same but w/o invasives</b> Meanander Patterns: <b>M3</b>		Modified Pfankuch Stability Rating (Numeric & Adjective Rating): <b>56 (Good)</b>		Remarks: Condition, Vigor & Usage of Existing Reach: <b>Exc. Veg but needs invasive weed control</b>	
Bank Erosion Summary		Reference W/d Ratio (W/d <sub>ref</sub> ): <b>9.72</b> Reference W/d Ratio (W/d <sub>ref</sub> ): <b>7.8</b>		Width/Depth Ratio State (W/d) / (W/d <sub>ref</sub> ): <b>1.25</b>		W/d Ratio State Stability Rating: <b>Mod. Unstable</b>		MWR / MWR <sub>ref</sub> Stability Rating: <b>1.2</b> MWR / MWR <sub>ref</sub> Stability Rating: <b>Unconfined</b>	
Sediment Capacity (POWERSED)		Annual Streambank Erosion Rate: <b>0.63</b> (tons/yr)		Curve Used: <b>Colorado</b>		Remarks: <b>Excellent Riparian Vegetation</b>			
Entrainment/Competence		Largest Particle from Bar Sample (mm): <b>23</b>		Existing Depth: <b>0.55</b>		Required Depth: <b>0.16</b>		Existing Slope: <b>0.008</b> Required Slope: <b>0.01</b>	
Successional Stage Shift		E → C → Gc → F → C → E		Existing Stream State (Type): <b>E</b>		Potential Stream State (Type): <b>E4</b>		Remarks/causes: <b>High Width/Depth Ratio</b>	
Lateral Stability		<input checked="" type="checkbox"/> Stable <input checked="" type="checkbox"/> Mod. Unstable <input type="checkbox"/> Unstable		<input type="checkbox"/> Insufficient Capacity <input type="checkbox"/> Excess Capacity		Remarks/causes: <b>Highly Unstable</b>			
Vertical Stability (Aggradation)		<input checked="" type="checkbox"/> No Deposition <input type="checkbox"/> Mod. Deposition <input type="checkbox"/> Ex. Deposition		<input type="checkbox"/> Aggradation		Remarks/causes:			
Vertical Stability (Degradation)		<input checked="" type="checkbox"/> Not Incised <input type="checkbox"/> Slightly Incised <input type="checkbox"/> Mod. Incised		<input type="checkbox"/> Degradation		Remarks/causes:			
Channel Enlargement		<input checked="" type="checkbox"/> No Increase <input type="checkbox"/> Slight Increase <input type="checkbox"/> Mod. Increase <input type="checkbox"/> Extensive		<input type="checkbox"/> Excessive		Remarks/causes:			
Sediment Supply (Channel Source)		<input type="checkbox"/> Low <input checked="" type="checkbox"/> Moderate <input type="checkbox"/> High <input type="checkbox"/> Very High		Remarks/causes: <b>Mod. b/c of High W/d, but has excellent vegetation &amp; trending toward low W/d E</b>					



# *Appendix C10*

**F4 Stream Type**

***Fair Stability Reach***



# Table of Contents

## *Appendix C10: F4 Fair Stability Reach*

<b>Reach Location &amp; Overview.....</b>	<b>C10-2</b>
<b>Survey Summary.....</b>	<b>C10-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C10-8</b>
<b><i>Velocity, Classification &amp; Morphological Relations.....</i></b>	<b>C10-8</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b><i>Stability Indices.....</i></b>	<b>C10-12</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b><i>BANCS Model – Streambank Erosion.....</i></b>	<b>C10-22</b>
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b><i>FLOWSED Model – Total Annual Sediment Yield.....</i></b>	<b>C10-25</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b><i>POWERSED Model– Sediment Transport Capacity to Assess Bed Stability.....</i></b>	<b>C12-27</b>
Worksheet 5-20a. Sediment transport prediction for the upstream condition.	
Worksheet 5-20b. Sediment transport prediction for the existing condition.	
<b><i>Sediment Competence/Entrainment.....</i></b>	<b>C10-29</b>
Worksheet 5-22. Sediment competence calculations.	
<b><i>Channel Stability Ratings.....</i></b>	<b>C10-30</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b><i>Summary.....</i></b>	<b>C10-36</b>
Worksheet 5-32. Summary of stability condition categories.	

## F4 Fair Reach Location & Overview

The F4 Fair representative reach is a recovering, perennial, entrenched stream located in the mainstem of West Monument Creek (**Figure C-1**). This reach is in a terraced alluvial Valley Type VIIIb, on a 4<sup>th</sup> order stream. The width/depth ratio of 14 is relatively low for an F4 stream type. The reach is near a road, which is influencing streambank erosion. The streamflow is seasonal by snowmelt and stormflow runoff. Flow is regulated by an upstream dam and will experience increased peak flows due to Waldo Canyon Fire.

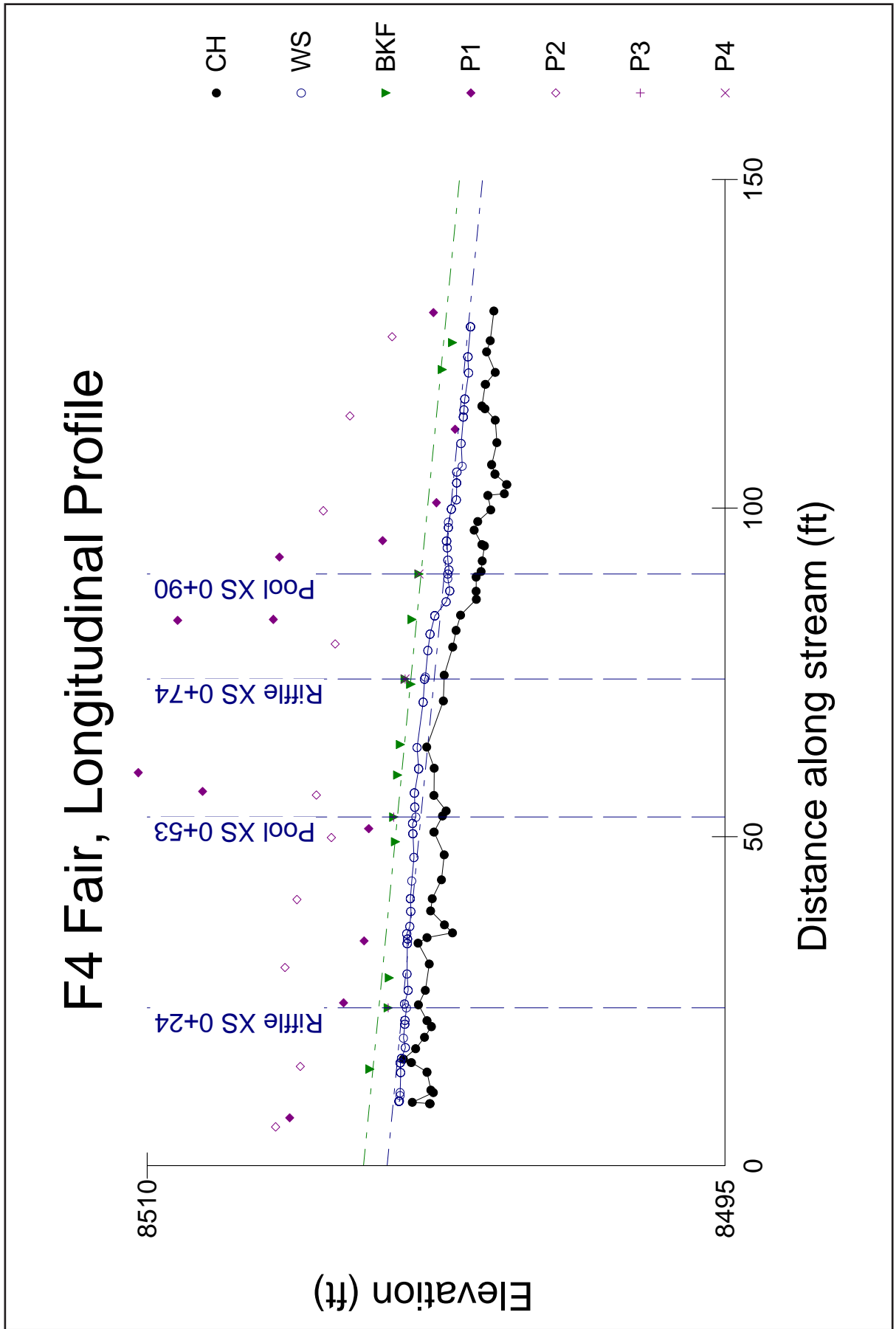
A POWERSED run was made to determine streambed stability, which predicted deposition. The channel has a predicted *Moderate Increase* in channel enlargement, and a *High* overall sediment supply. The reach has a unit erosion rate of 0.0589 tons/yr/ft.

The WRENSS model indicated that the water yield due to the fire increased from 2,460 acre-ft to 3,283.5 acre-ft, representing a total increase of 823.5 acre-ft per year. The corresponding bedload increased from 9.1 tons/year to 19.3 tons/yr, and suspended sediment increased from 39.9 tons/yr to 78.0 tons/yr, representing a total increase in sediment of 48.3 tons/yr. This sediment yield reflects increases due to the increased flows, even in a moderately unstable reach.

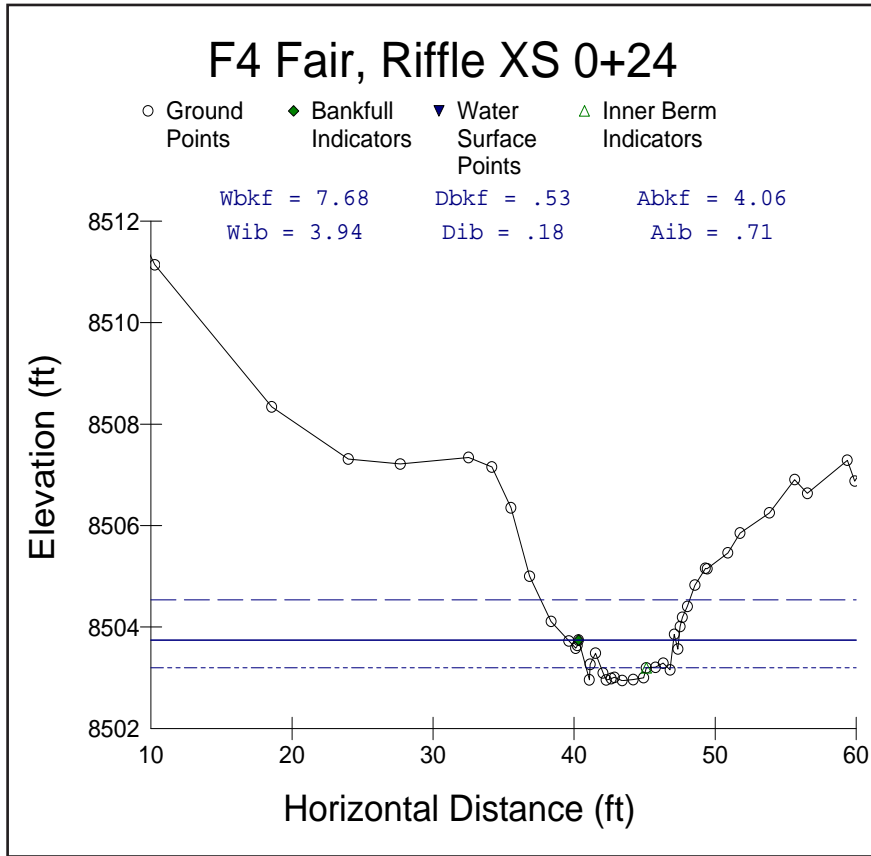
The photograph depicts the typical character of this representative F4 Fair stream type. The following graphs and summary worksheets provide the details of the morphology, hydraulics, streambank erosion rates, and stability conditions responsible for the overall “Fair” rating.



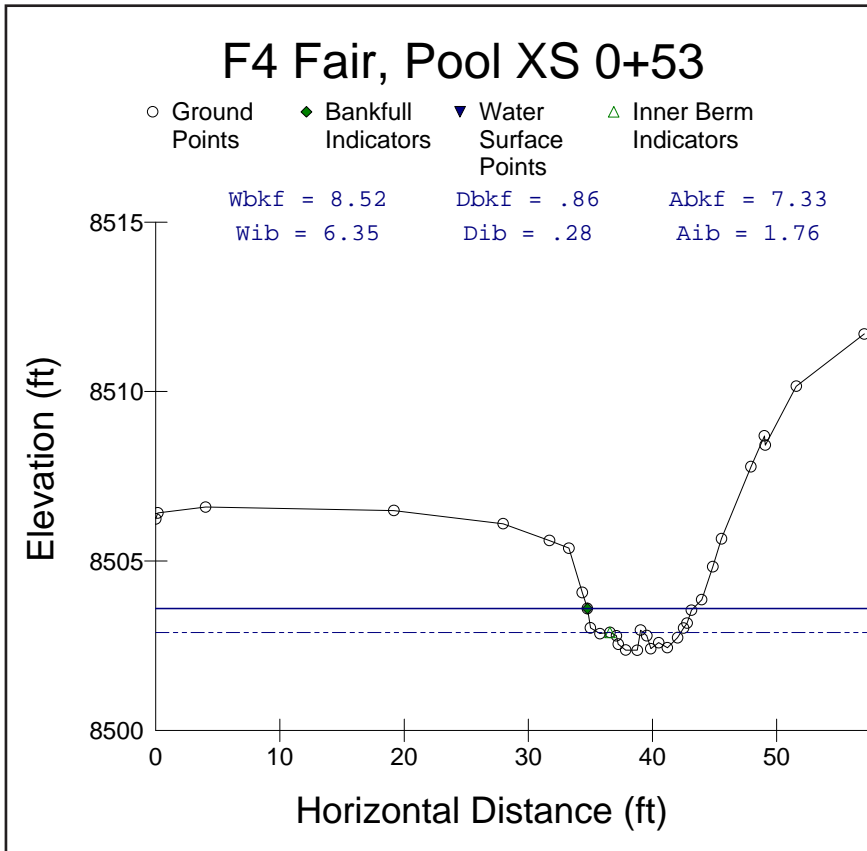
### Survey Summary



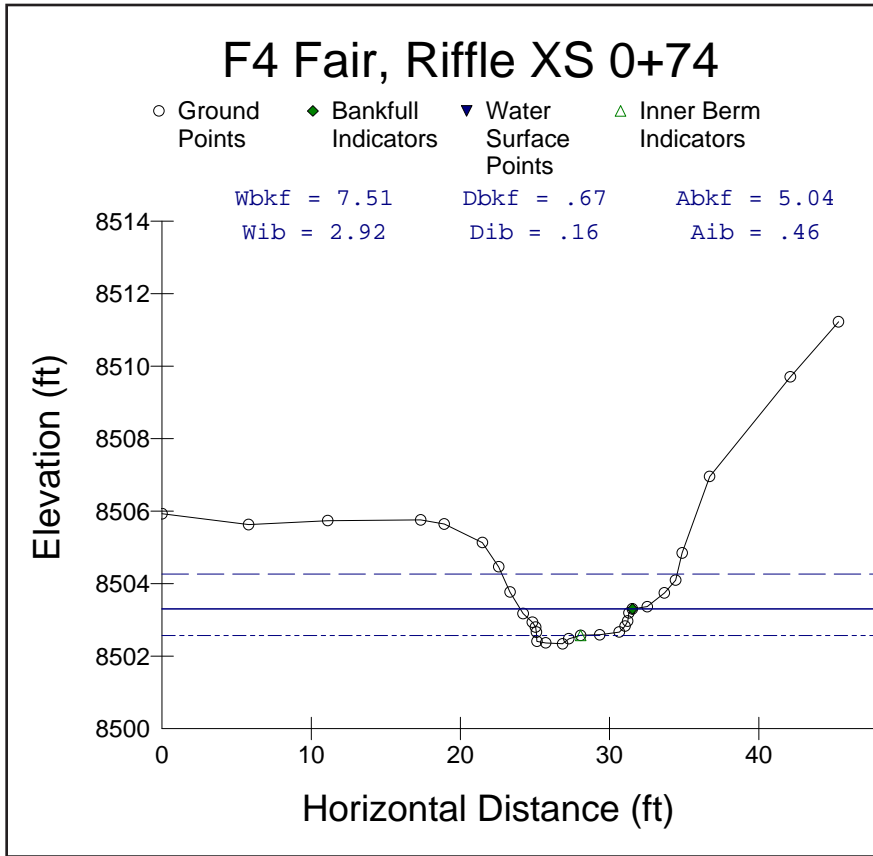
Longitudinal Profile (graph generated from RIVERMorph™)



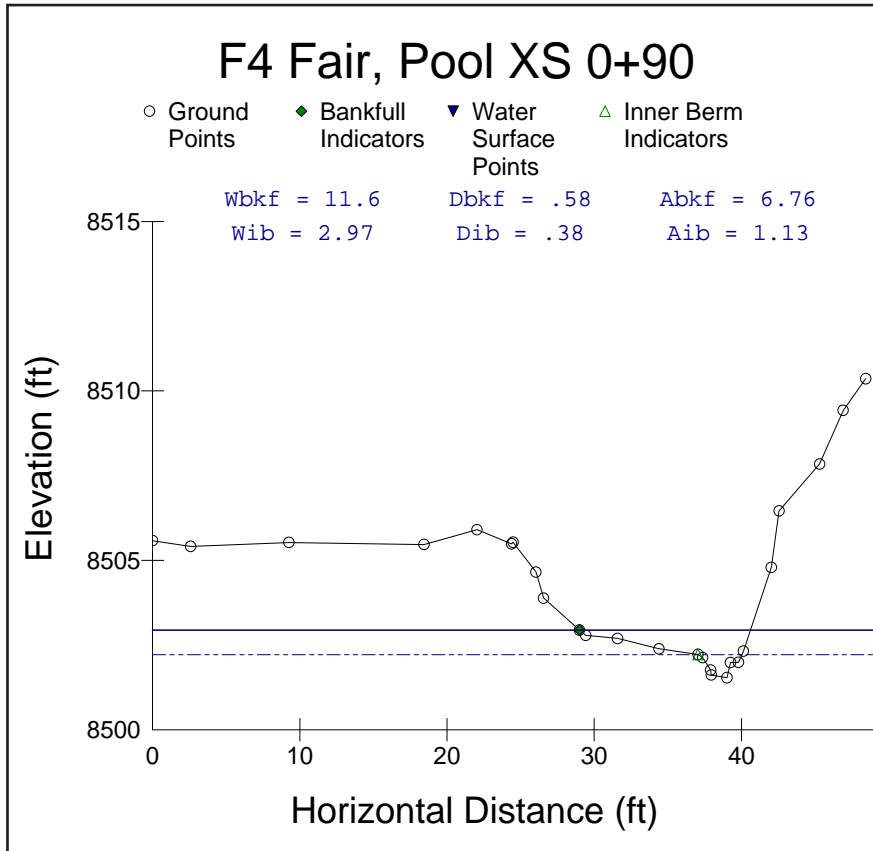
**Representative Cross-section 0+24** (graph generated from RIVERMorph™)



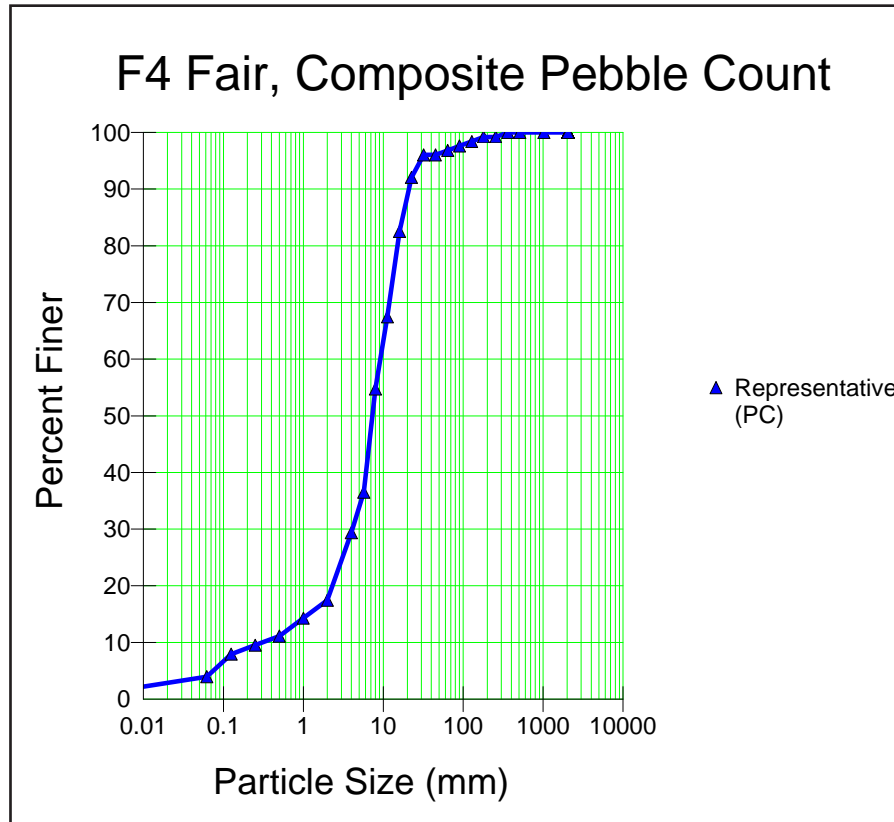
**Cross-section 0+53** (graph generated from RIVERMorph™)



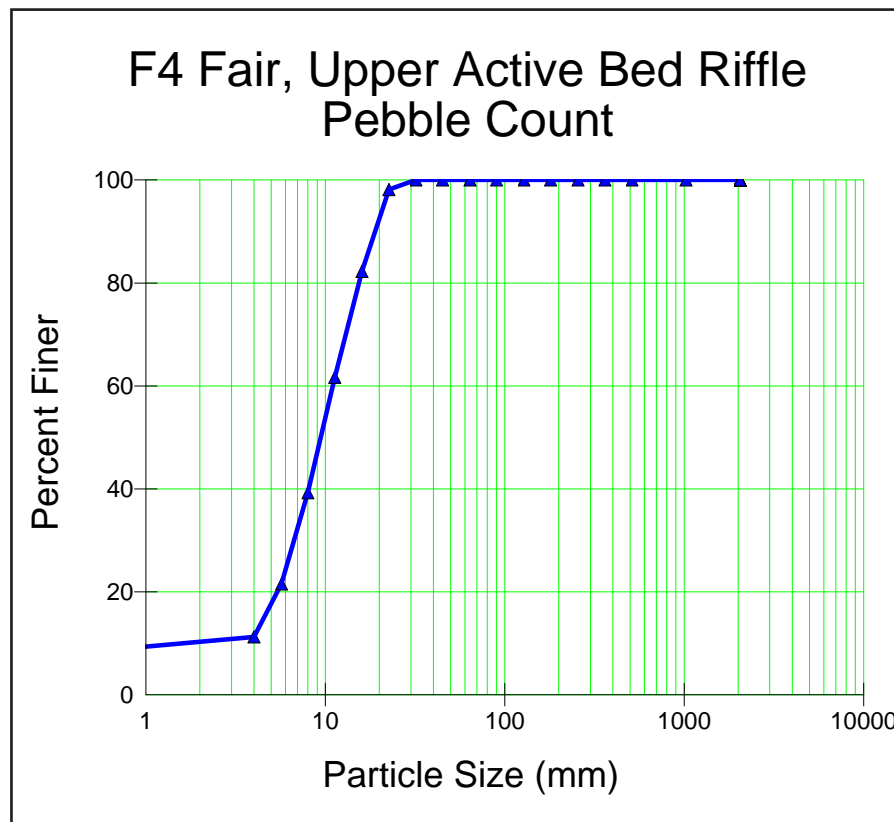
Cross-section 0+74 (graph generated from RIVERMorph™)



Cross-section 0+90 (graph generated from RIVERMorph™)

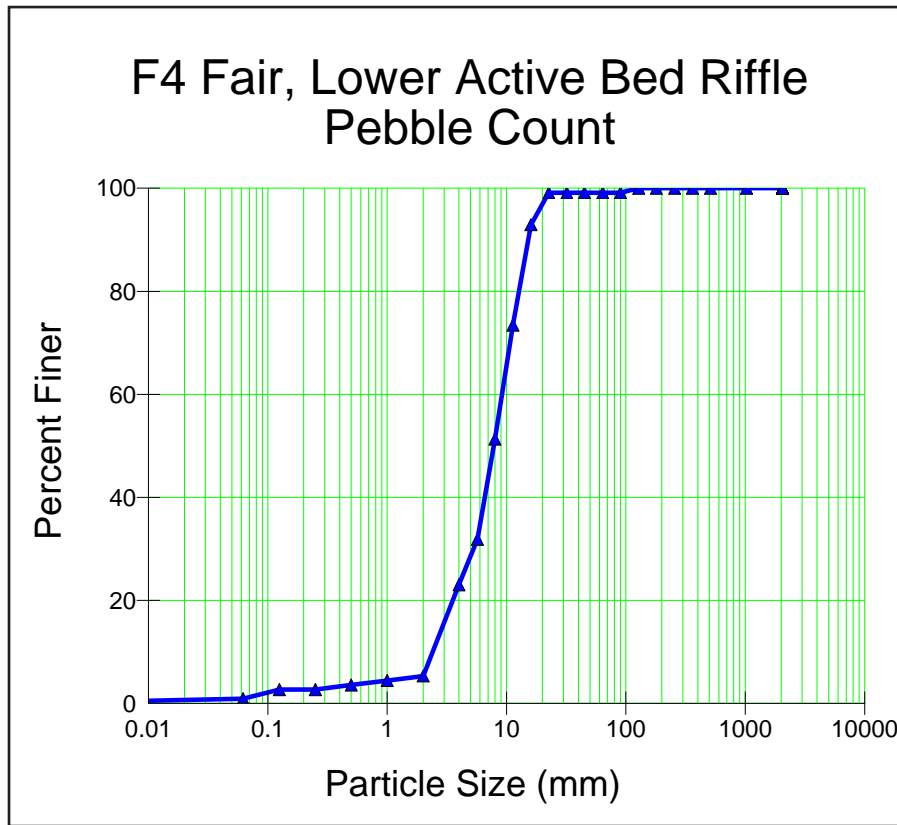


Composite Pebble Count (graph generated from RIVERMorph™)



Upper Active Bed Riffle Pebble Count (graph generated from RIVERMorph™)





Lower Active Bed Riffle Pebble Count (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates						
Stream:	West Monument F4 Fair			Location:	Pike National Forest, Colorado	
Date:	11/5/2012	Stream Type:	F4	Valley Type:	VIIIb	
Observers:	Rosgen et. al.			HUC:	__ __ __ __ __ __ __ __ __ __	
INPUT VARIABLES			OUTPUT VARIABLES			
Bankfull Riffle Cross-Sectional AREA	4.06	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.53	$d_{bkf}$ (ft)	
Bankfull Riffle WIDTH	7.7	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim (2 * d_{bkf}) + W_{bkf}$	8.74	$W_p$ (ft)	
$D_{84}$ at Riffle	13.9	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.05	$D_{84}$ (ft)	
Bankfull SLOPE	0.009	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	0.46	R (ft)	
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness $R(ft) / D_{84} (ft)$	10.22	$R / D_{84}$	
Drainage Area	10.88	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.365	$u^*$ (ft/sec)	
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE	
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$			2.97	ft / sec	12.06	cfs
2. Roughness Coefficient: a) Manning's n from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.037$			2.18	ft / sec	8.85	cfs
2. Roughness Coefficient: b) Manning's n from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.05$			1.62	ft / sec	6.58	cfs
2. Roughness Coefficient: c) Manning's n from Jarrett (USGS): $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for Stream Types A1, A2, A3, B1, B2, B3, C2 & E3 $n = 0.074$			1.09	ft / sec	4.43	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Darcy-Weisbach (Leopold, Wolman and Miller)			3.49	ft / sec	14.2	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)				ft / sec		cfs
4. Continuity Equations: a) Regional Curves $u = Q / A$ Return Period for Bankfull Discharge $Q =$ <input type="text"/> year				ft / sec		cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$				ft / sec		cfs
<b>Protrusion Height Options for the <math>D_{84}</math> Term in the Relative Roughness Relation (<math>R/D_{84}</math>) – Estimation Method 1</b>						
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.						
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.						
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.						
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.						

**Worksheet 5-3.** Level II stream classification.

Stream: <b>West Monument F4 Fair</b>	
Basin:	Drainage Area: <b>6963</b> acres <b>10.88</b> mi <sup>2</sup>
Location: <b>Pike National Forest, Colorado</b>	
Twp.&Rge:	Sec.&Qtr.:
Cross-Section Monuments (Lat./Long.): <b>XS 0+24</b>	Date: <b>11/05/2012</b>
Observers: <b>Rosgen et. al.</b>	Valley Type: <b>VIIIb</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>7.68</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A_{bkf} / W_{bkf}$ ).	<b>0.53</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>4.06</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>14.49</b>	ft/ft
<b>Maximum DEPTH (<math>d_{max}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>0.8</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>10.56</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>1.38</b>	ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the median or dominant diameter of channel materials, as sampled proportionately from the channel surface, between the bankfull stage and Thalweg elevations.	<b>7.4</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.0165</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope ( $S_{val} / S$ ).	<b>1.09</b>	

<b>Stream Type</b>	<b>F4</b>	<b>See Classification Key (Figure 2-14)</b>
--------------------	-----------	---

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>West Monument F4 Fair</b>		Location: <b>Pike National Forest, Colorado</b>							
Observers: <b>Rosgen et. al.</b>		Date: <b>11/05/12</b>		Valley Type: <b>VIIIb</b>		Stream Type: <b>F4</b>			
<b>River Reach Dimension Summary Data.....1</b>									
<b>Riffle Dimensions* ** * ** *</b>	<b>Riffle Dimensions* ** * ** *</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Width ( $W_{bkt}$ )	7.7	7.5	7.7	ft	Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	4.1	4.1	5.0
	Mean Riffle Depth ( $d_{bkt}$ )	0.53	0.53	0.67	ft	Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	12.9	11.2	14.5
	Maximum Riffle Depth ( $d_{max}$ )	0.88	0.80	0.96	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	1.660	1.509	1.811
	Width of Flood-Prone Area ( $W_{fpa}$ )	11.2	10.6	11.9	ft	Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )	1.5	1.4	1.6
	Riffle Inner Berm Width ( $W_{ib}$ )	3.4	2.9	3.9	ft	Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )	0.447	0.380	0.513
	Riffle Inner Berm Depth ( $d_{ib}$ )	0.17	0.16	0.18	ft	Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )	0.321	0.302	0.340
	Riffle Inner Berm Area ( $A_{ib}$ )	0.6	0.5	0.7	ft <sup>2</sup>	Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )	0.133	0.092	0.174
	Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )	20.2	18.5	21.9					
<b>Pool Dimensions* ** * ** *</b>	<b>Pool Dimensions* ** * ** *</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Pool Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Pool Width ( $W_{bkfp}$ )	10.1	8.5	11.6	ft	Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )	1.315	1.109	1.510
	Mean Pool Depth ( $d_{bkfp}$ )	0.72	0.58	0.86	ft	Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )	1.358	1.094	1.623
	Pool Cross-Sectional Area ( $A_{bkfp}$ )	7.1	6.8	7.3	ft	Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )	1.736	1.665	1.805
	Maximum Pool Depth ( $d_{maxp}$ )	1.32	1.23	1.40	ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	2.491	2.321	2.642
	Pool Inner Berm Width ( $W_{ibp}$ )	4.7	3.0	6.4	ft	Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )	0.461	0.294	0.629
	Pool Inner Berm Depth ( $d_{ibp}$ )	0.33	0.28	0.38	ft	Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )	0.458	0.389	0.528
	Pool Inner Berm Area ( $A_{ibp}$ )	1.5	1.1	1.8	ft <sup>2</sup>	Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )	0.206	0.160	0.250
	Point Bar Slope ( $S_{pb}$ )				ft/ft	Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )			
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Run Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Run Width ( $W_{bkfr}$ )				ft	Run Width to Riffle Width ( $W_{bkfr} / W_{bkt}$ )			
	Mean Run Depth ( $d_{bkfr}$ )				ft	Mean Run Depth to Mean Riffle Depth ( $d_{bkfr} / d_{bkt}$ )			
	Run Cross-Sectional Area ( $A_{bkfr}$ )				ft	Run Area to Riffle Area ( $A_{bkfr} / A_{bkt}$ )			
	Maximum Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )			
Run Width/Depth Ratio ( $W_{bkfr} / d_{bkfr}$ )				ft					
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Glide Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Glide Width ( $W_{bkfg}$ )				ft	Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )			
	Mean Glide Depth ( $d_{bkfg}$ )				ft	Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )			
	Glide Cross-Sectional Area ( $A_{bkfg}$ )				ft	Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )			
	Maximum Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )			
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )				ft/ft	Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )			
	Glide Inner Berm Width ( $W_{ibg}$ )				ft	Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )			
	Glide Inner Berm Depth ( $d_{ibg}$ )				ft	Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )			
Glide Inner Berm Area ( $A_{ibg}$ )				ft <sup>2</sup>	Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )				
<b>Step**</b>	<b>Step Dimensions**</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Step Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Step Width ( $W_{bkfs}$ )				ft	Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )			
	Mean Step Depth ( $d_{bkfs}$ )				ft	Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )			
	Step Cross-Sectional Area ( $A_{bkfs}$ )				ft	Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )			
	Maximum Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )									

**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>West Monument F4 Fair</b>		Location: <b>Pike National Forest, Colorado</b>						
Observers: <b>Rosgen et. al.</b>		Date: <b>11/5/2012</b>		Valley Type: <b>VIIIb</b>		Stream Type: <b>F4</b>		
<b>River Reach Summary Data.....2</b>								
<b>Hydraulics</b>	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )		<b>2.18</b>	ft/sec	Estimation Method		<b>Roughness Coefficient</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )		<b>8.85</b>	cfs	Drainage Area		<b>10.88</b> mi <sup>2</sup>	
<b>Channel Pattern</b>	<b>Geometry</b>			<b>Dimensionless Geometry Ratios</b>				
	Linear Wavelength ( $\lambda$ )	<b>53.1</b>	<b>50.9</b>	<b>55.2</b>	ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )	<b>6.91</b> <b>6.63</b> <b>7.19</b>	
	Stream Meander Length ( $L_m$ )	<b>60.5</b>	<b>56.0</b>	<b>65.0</b>	ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )	<b>7.88</b> <b>7.29</b> <b>8.46</b>	
	Radius of Curvature ( $R_c$ )	<b>12.3</b>	<b>8.8</b>	<b>25.0</b>	ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )	<b>1.60</b> <b>1.15</b> <b>3.26</b>	
	Belt Width ( $W_{bit}$ )	<b>26.4</b>			ft	Meander Width Ratio ( $W_{bit} / W_{bkt}$ )	<b>3.44</b>	
	Arc Length ( $L_a$ )	<b>12.8</b>	<b>6.2</b>	<b>15.0</b>	ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )	<b>1.67</b> <b>0.81</b> <b>1.95</b>	
	Riffle Length ( $L_r$ )	<b>3.4</b>	<b>0.8</b>	<b>6.5</b>	ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )	<b>0.45</b> <b>0.11</b> <b>0.85</b>	
	Individual Pool Length ( $L_p$ )	<b>8.8</b>	<b>4.3</b>	<b>20.2</b>	ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )	<b>1.15</b> <b>0.55</b> <b>2.63</b>	
Pool to Pool Spacing ( $P_s$ )	<b>18.6</b>	<b>9.3</b>	<b>47.1</b>	ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )	<b>2.42</b> <b>1.21</b> <b>6.13</b>		
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )		<b>0.0180</b>	ft/ft	Average Water Surface Slope (S)		<b>0.0165</b> ft/ft	
	Stream Length (SL)		<b>131.0</b>	ft	Valley Length (VL)		<b>120.6</b> ft	
	Sinuosity ( $S_{val} / S$ )				Sinuosity (SL / VL)		<b>1.09</b>	
	Low Bank Height (LBH)	start: <b>2.00</b> ft end: <b>3.00</b> ft	Max Bankfull Depth ( $d_{max}$ )		start: <b>0.90</b> ft end: <b>1.12</b> ft	Bank-Height Ratio (BHR) (LBH / $d_{max}$ )		start: <b>2.2</b> end: <b>2.7</b>
	<b>Facet Slopes</b>			<b>Dimensionless Facet Slope Ratios</b>				
	Riffle Slope ( $S_{rif}$ )	<b>0.0240</b>	<b>0.0120</b>	<b>0.0460</b>	ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.4545</b> <b>0.7273</b> <b>2.7879</b>	
	Run Slope ( $S_{run}$ )	<b>0.0910</b>	<b>0.0640</b>	<b>0.1380</b>	ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )	<b>5.515</b> <b>3.8788</b> <b>8.364</b>	
	Pool Slope ( $S_p$ )	<b>0.0040</b>	<b>0.0010</b>	<b>0.0060</b>	ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )	<b>0.2424</b> <b>0.0606</b> <b>0.3636</b>	
	Glide Slope ( $S_g$ )	<b>0.0120</b>	<b>0.0090</b>	<b>0.0190</b>	ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )	<b>0.7273</b> <b>0.5455</b> <b>1.1515</b>	
	Step Slope ( $S_s$ )				ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )		
	<b>Max Depths<sup>a</sup></b>			<b>Dimensionless Depth Ratios</b>				
	Max Riffle Depth ( $d_{max}$ )	<b>1.08</b>	<b>0.89</b>	<b>1.31</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>2.038</b> <b>1.679</b> <b>2.472</b>	
	Max Run Depth ( $d_{maxr}$ )	<b>1.10</b>	<b>0.67</b>	<b>1.49</b>	ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )	<b>2.075</b> <b>1.264</b> <b>2.811</b>	
Max Pool Depth ( $d_{maxp}$ )	<b>1.43</b>	<b>1.04</b>	<b>1.92</b>	ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	<b>2.698</b> <b>1.962</b> <b>3.623</b>		
Max Glide Depth ( $d_{maxg}$ )	<b>0.87</b>	<b>0.51</b>	<b>1.28</b>	ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )	<b>1.642</b> <b>0.962</b> <b>2.415</b>		
Max Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
<b>Channel Materials</b>	<b>Reach<sup>b</sup></b>		<b>Riffle<sup>c</sup></b>		<b>Bar</b>		<b>Protrusion Height<sup>d</sup></b>	
	% Silt/Clay	<b>3.97</b>	<b>0.00</b>		$D_{16}$	<b>1.54</b>	<b>4.79</b>	
	% Sand	<b>13.49</b>	<b>0.00</b>		$D_{35}$	<b>2.34</b>	<b>7.45</b>	
	% Gravel	<b>79.37</b>	<b>100.00</b>		$D_{50}$	<b>7.40</b>	<b>9.58</b>	
	% Cobble	<b>2.38</b>	<b>0.00</b>		$D_{84}$	<b>17.01</b>	<b>16.73</b>	
	% Boulder	<b>0.79</b>	<b>0.00</b>		$D_{95}$	<b>29.56</b>	<b>21.30</b>	
	% Bedrock	<b>0.00</b>	<b>0.00</b>		$D_{100}$	<b>361.99</b>	<b>32.00</b>	

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.

## Stability Indices


**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation					
Stream: <b>West Monument F4 Fair</b>			Location: <b>Pike National Forest, Colorado</b>		
Observers: <b>Rosgen et. al.</b>		Reference reach <input type="checkbox"/>	Disturbed (impacted reach) <input checked="" type="checkbox"/>	Date: <b>11/05/2012</b>	
Existing species composition: <b>Willow/Aspen dominated</b>			Potential species composition: <b>At potential</b>		
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition
<b>1. Overstory</b>	Canopy layer	<b>3%</b>	<b>10%</b>	Ponderosa	3%
				Blue Spruce	3%
				Aspen	94%
					0%
					0%
					0%
					100%
<b>2. Understory</b>	Shrub layer	<b>80%</b>	<b>80%</b>	Willows	90%
				Chokecherry	3%
				Rocky Mountain Maple	2%
				Rose	5%
					0%
					0%
					100%
<b>3. Ground level</b>	Herbaceous	<b>2%</b>	<b>2%</b>	Grass	70%
				Forbs	30%
					0%
					0%
					0%
	Leaf or needle litter	<b>5%</b>	<b>5%</b>	<b>Remarks:</b> Condition, vigor and/or usage of existing reach: <b>Bare ground under shaded canopy</b>	
	Bare ground	<b>3%</b>	<b>3%</b>		
					100%
*Based on crown closure. **Based on basal area to surface area.			<b>Column Total = 100%</b>		

Worksheet 5-7. Flow regime.

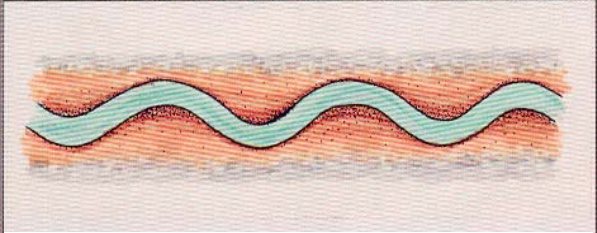

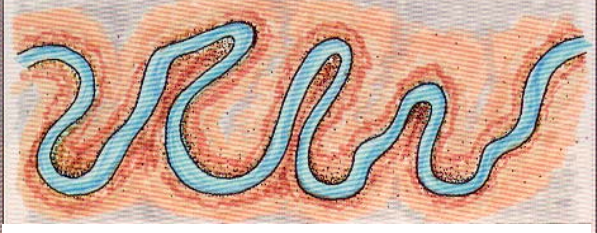
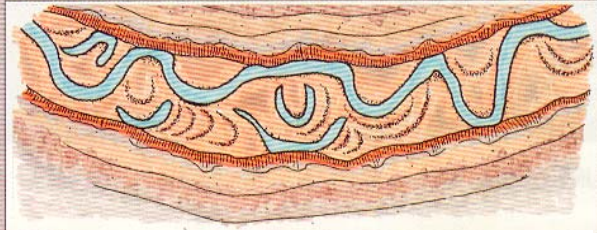

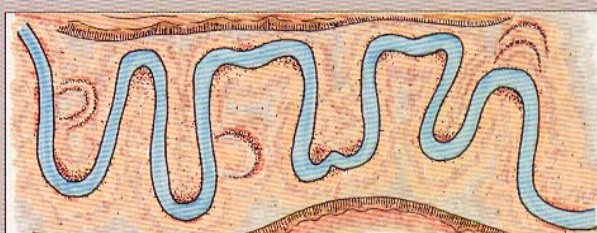
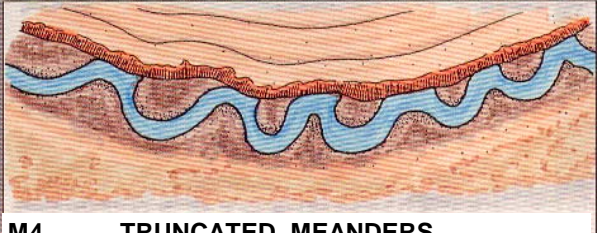
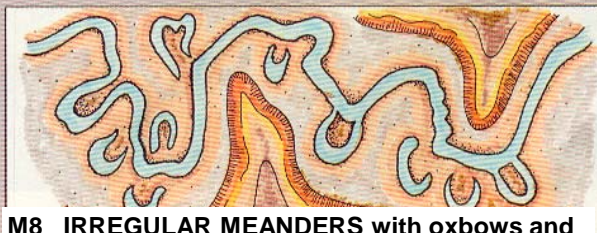
FLOW REGIME								
Stream: <b>West Monument F4 Fair</b>			Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>Rosgen et. al.</b>					Date: <b>11/5/2012</b>			
List ALL COMBINATIONS that APPLY.....☞			P1	P2	P7	P8		
General Category								
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation							
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
<b>P</b>	Perennial stream channels: Surface water persists yearlong.							
Specific Category								
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
<b>4</b>	Streamflow regulated by glacial melt.							
<b>5</b>	Ice flows/ice torrents from ice dam breaches.							
<b>6</b>	Alternating flow/backwater due to tidal influence.							
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.							
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
<b>9</b>	Rain-on-snow generated runoff.							

**Worksheet 5-8.** Stream order & stream size.

Stream Size and Order			
Stream:	West Monument F4 Fair		
Location:	Pike National Forest, Colorado		
Observers:	Rosgen et. al.		
Date:	11/5/2012		
Stream Size Category and Order 			<b>S-3(4)</b>
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0.305	<1	<input type="checkbox"/>
S-2	0.3 – 1.5	1 – 5	<input type="checkbox"/>
<b>S-3</b>	<b>1.5 – 4.6</b>	<b>5 – 15</b>	<input checked="" type="checkbox"/>
S-4	4.6 – 9	15 – 30	<input type="checkbox"/>
S-5	9 – 15	30 – 50	<input type="checkbox"/>
S-6	15 – 22.8	50 – 75	<input type="checkbox"/>
S-7	22.8 – 30.5	75 – 100	<input type="checkbox"/>
S-8	30.5 – 46	100 – 150	<input type="checkbox"/>
S-9	46 – 76	150 – 250	<input type="checkbox"/>
S-10	76 – 107	250 – 350	<input type="checkbox"/>
S-11	107 – 150	350 – 500	<input type="checkbox"/>
S-12	150 – 305	500 – 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
Stream Order			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			



Worksheet 5-9. Meander patterns.

Meander Patterns					
Stream: <b>West Monument F4 Fair</b>		Location: <b>Pike National Forest, CO</b>			
Observers: <b>Rosgen et. al.</b>		Date: <b>11/5/2012</b>			
List ALL CATEGORIES that APPLY	<b>M3</b>				
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>					
 <b>M1</b> <b>REGULAR MEANDERS</b>	 <b>M5</b> <b>UNCONFINED MEANDER SCROLLS</b>				
 <b>M2</b> <b>TORTUOUS MEANDERS</b>	 <b>M6</b> <b>CONFINED MEANDER SCROLLS</b>				
 <b>M3</b> <b>IRREGULAR MEANDERS</b>	 <b>M7</b> <b>DISTORTED MEANDER LOOPS</b>				
 <b>M4</b> <b>TRUNCATED MEANDERS</b>	 <b>M8</b> <b>IRREGULAR MEANDERS with oxbows and oxbow cutoffs</b>				

**Worksheet 5-10.** Depositional patterns.

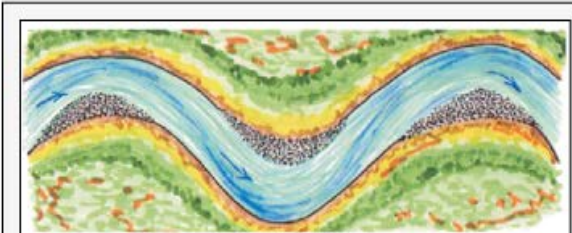
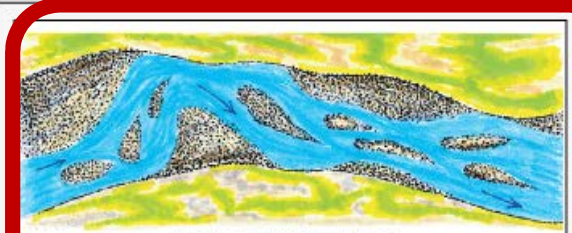

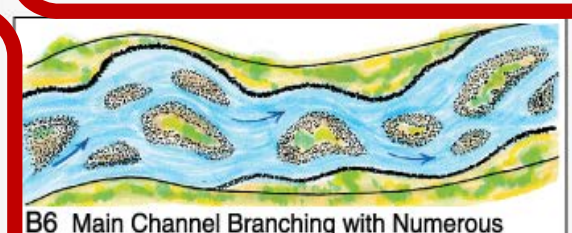

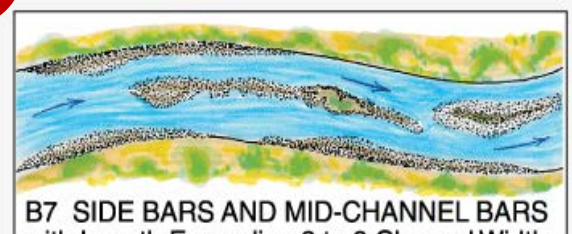
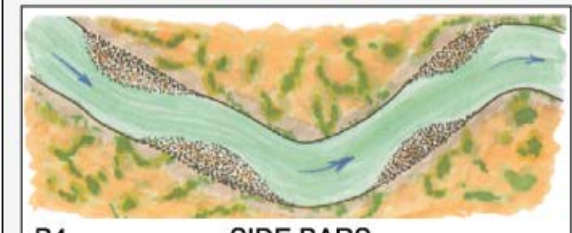
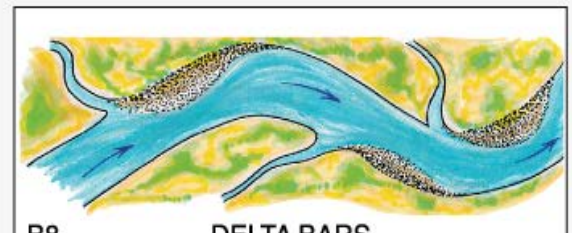
**Depositional Patterns**

Stream: **West Monument F4 Fair** Location: **Pike National Forest, Colorado**

Observers: **Rosgen et. al.** Date: **11/5/2012**

List ALL CATEGORIES that APPLY	<b>B2</b>	<b>B5</b>			
--------------------------------	-----------	-----------	--	--	--

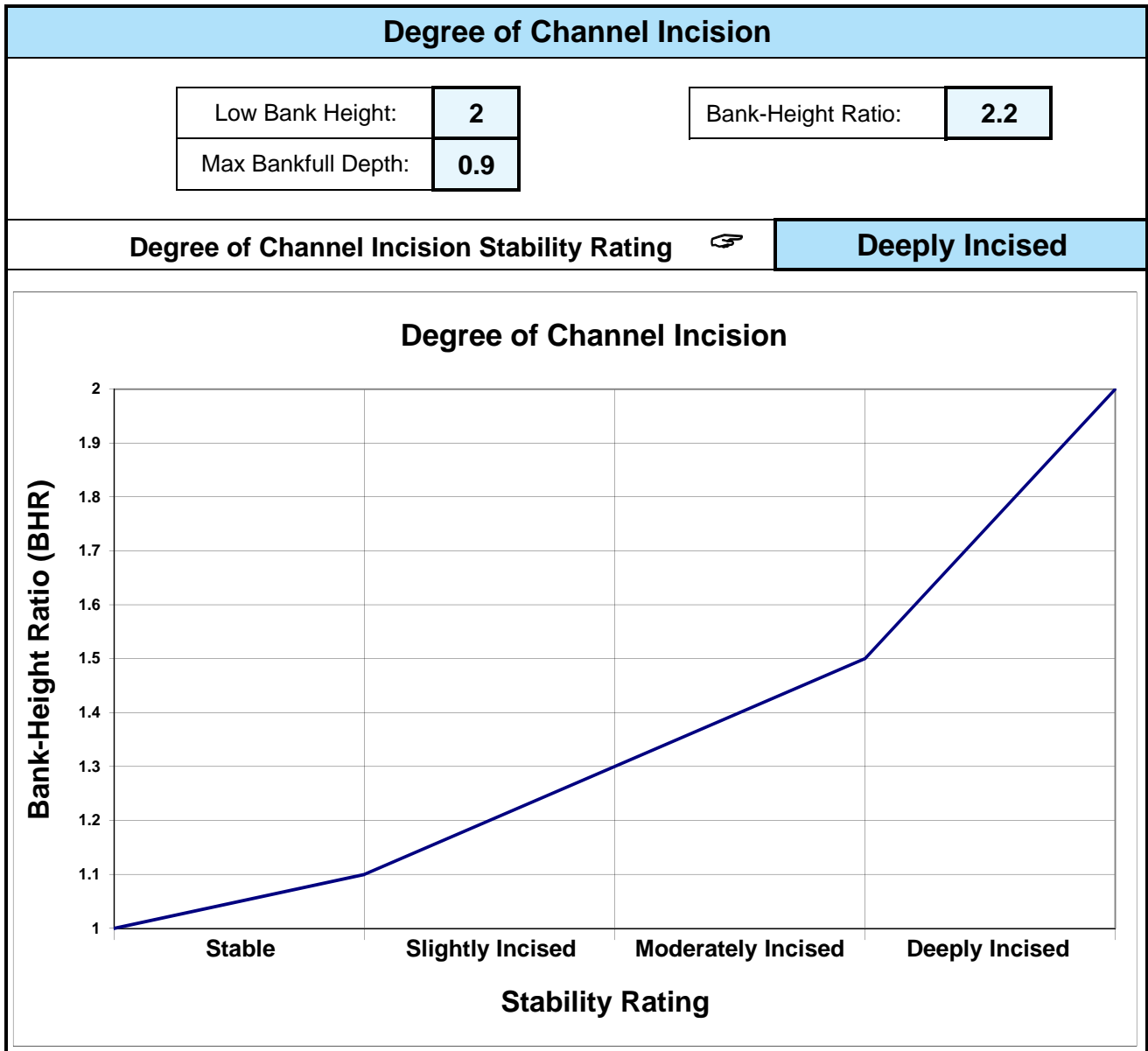
*Various Depositional Features modified from Galay et al. (1973)*

 <p><b>B1</b> POINT BARS</p>	 <p><b>B5</b> DIAGONAL BARS</p>
 <p><b>B2</b> POINT BARS with Few MID-CHANNEL BARS</p>	 <p><b>B6</b> Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</p>
 <p><b>B3</b> NUMEROUS MID-CHANNEL BARS</p>	 <p><b>B7</b> SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</p>
 <p><b>B4</b> SIDE BARS</p>	 <p><b>B8</b> DELTA BARS</p>

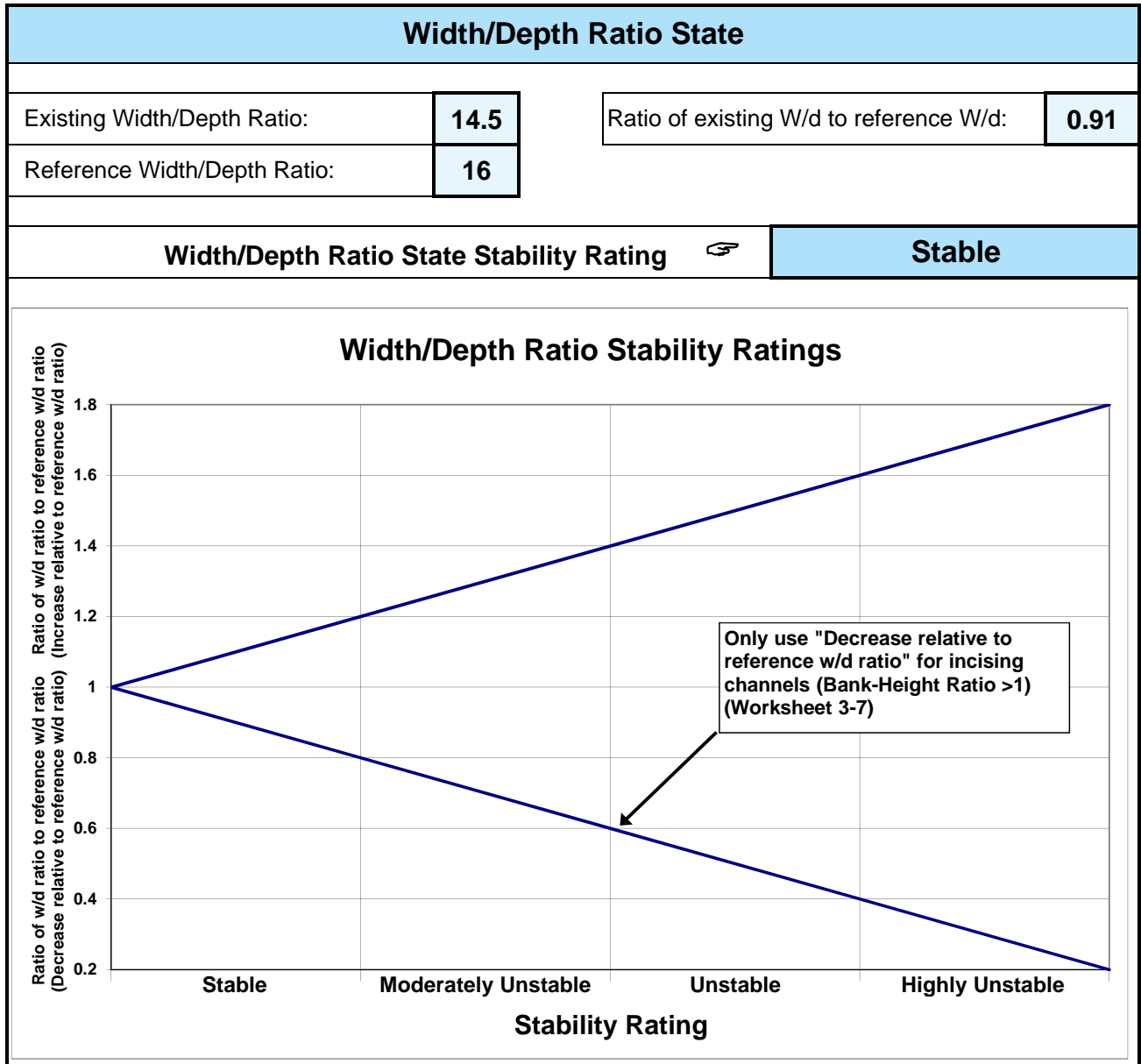
## Worksheet 5-11. Channel blockages.

Channel Blockages		
Stream: <b>West Monument F4 Fair</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>Rosgen et. al.</b>		Date: <b>11/5/2012</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input checked="" type="checkbox"/>
<b>D4</b> Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

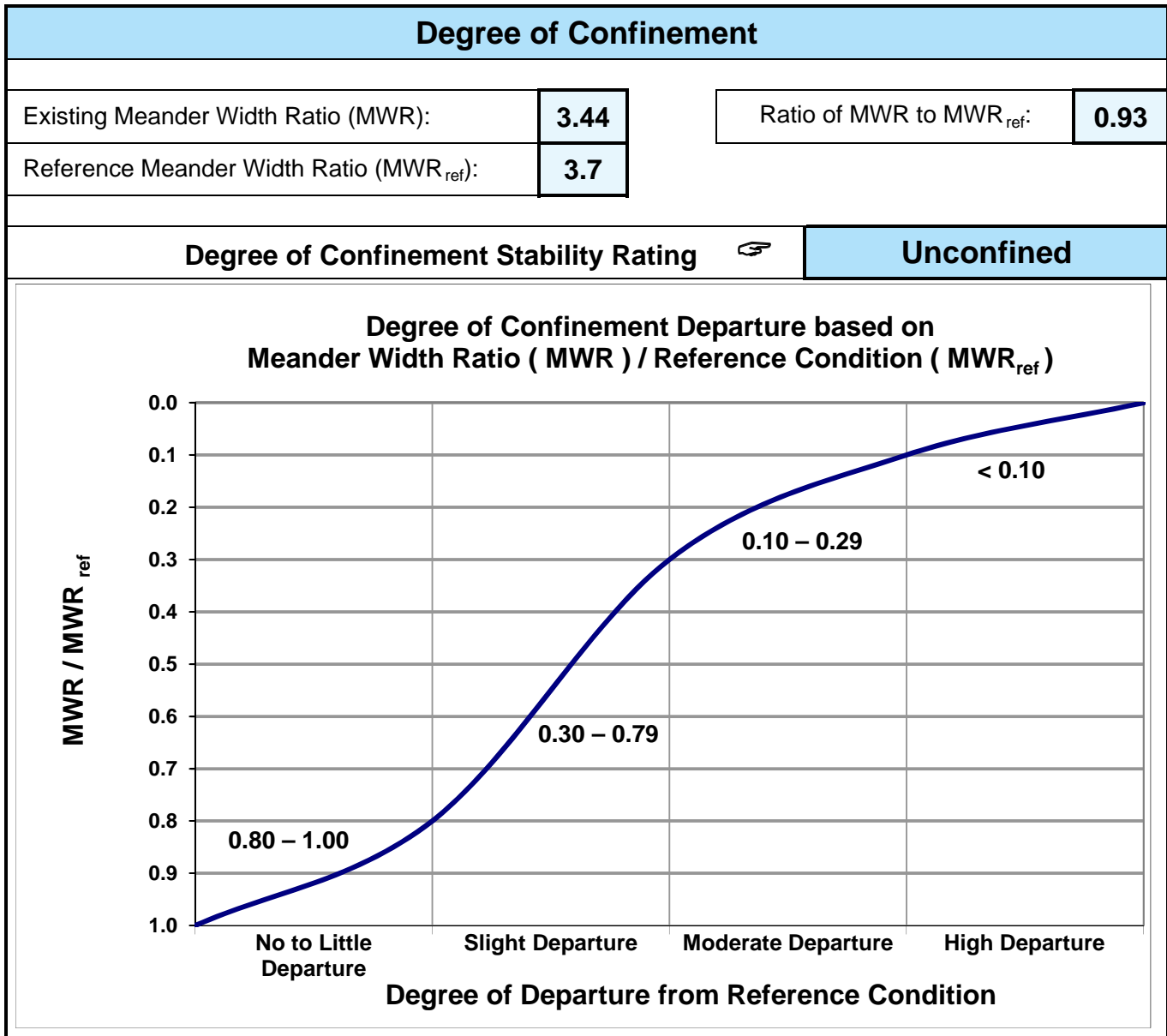
**Worksheet 5-12.** Degree of channel incision.



Worksheet 5-13. Width/depth ratio state.



**Worksheet 5-14.** Degree of channel confinement (lateral containment).



Worksheet 5-15. Pfankuch channel stability rating.

Stream: West Monument F4 Fair		Location: Pike National Forest, CO			Valley Type: VIIIb			Observers: Reosgen et al.			Date: 11/5/2012																																						
Loca-tion	Key Category	Excellent Description	Rating	Good Description	Rating	Fair Description	Rating	Poor Description	Rating																																								
Upper banks	1	Landform slope	2	Bank slope gradient <30%.	4	Bank slope gradient 40–60%.	5	Bank slope gradient > 60%.	8																																								
	2	Mass erosion	3	No evidence of past or future mass erosion.	7	Frequent or large, causing sediment nearly yearlong.	9	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.	12																																								
	3	Debris jam potential	2	Essentially absent from immediate channel area.	5	Moderate to heavy amounts, mostly larger sizes.	6	Moderate to heavy amounts, predominantly larger sizes.	8																																								
	4	Vegetative bank protection	3	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	5	70–90% density. Fewer species or less vigor suggest less dense or deep root mass.	9	<20% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.	12																																								
Lower banks	5	Channel capacity	1	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0–1.1.	2	Bankfull stage is contained within banks. Width/depth ratio departure from reference width/depth ratio = 1.0–1.2. Bank-Height Ratio (BHR) = 1.1–1.3.	3	Bankfull stage is not contained. Width/depth ratio departure from reference width/depth ratio = 1.2–1.4. Bank-Height Ratio (BHR) = 1.3.	4																																								
	6	Bank rock content	2	> 65% with large angular boulders. 12" + common.	4	40–65%. Mostly boulders and small cobbles 6–12".	6	20–40%. Most in the 3–6" diameter class.	8																																								
	7	Obstructions to flow	2	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition.	5	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	6	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	8																																								
	8	Cutting	5	Little or none. Infrequent raw banks <6".	9	Some, intermittently at outcurves and constrictions. Raw banks may be up to 12".	12	Significant. Cuts 12–24" high. Root mat overhangs and sloughing evident.	16																																								
	9	Deposition	4	Little or no enlargement of channel or point bars.	8	Some new bar increase, mostly from coarse gravel.	12	Moderate deposition of new gravel and coarse sand on old and some new bars.	16																																								
Bottom	10	Rock angularity	1	Sharp edges and corners. Plane surfaces rough.	2	Rounded corners and edges. Surfaces smooth and flat.	3	Corners and edges well rounded in 2 dimensions.	4																																								
	11	Brightness	1	Surfaces dull, dark or stained. Generally not bright.	2	Mostly dull, but may have <35% bright surfaces.	3	Mixture dull and bright, i.e., 35–65% mixture range.	4																																								
	12	Consolidation of particles	2	Assorted sizes tightly packed or overlapping.	4	Moderately packed with some overlapping.	6	Mostly loose assortment with no apparent overlap.	8																																								
	13	Bottom size distribution	4	No size change evident. Stable material 80–100%.	8	Distribution shift light. Stable material 50–80%.	12	Moderate change in sizes. Stable materials 20–50%.	16																																								
	14	Scouring and deposition	6	<5% of bottom affected by scour or deposition.	16	5–30% affected. Scour at constrictions and where grades steeper. Some deposition in pools.	20	30–50% affected. Deposits and scour at obstructions, constrictions and bends. Some filling of pools.	24																																								
	15	Aquatic vegetation	1	Abundant growth moss-like, dark green perennial. In swift water too.	2	Common. Algae forms in low velocity and pool areas. Moss here too.	3	Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick.	4																																								
			<b>Excellent total = 5</b>				<b>Good total = 48</b>				<b>Fair total = 20</b>				<b>Poor total = 24</b>																																		
<b>Stream type</b>	<b>A1</b>	<b>A2</b>	<b>A3</b>	<b>A4</b>	<b>A5</b>	<b>A6</b>	<b>B1</b>	<b>B2</b>	<b>B3</b>	<b>B4</b>	<b>B5</b>	<b>B6</b>	<b>C1</b>	<b>C2</b>	<b>C3</b>	<b>C4</b>	<b>C5</b>	<b>C6</b>	<b>D3</b>	<b>D4</b>	<b>D5</b>	<b>D6</b>	<b>Grand total = 97</b>																										
Good (Stable)	38-43	38-43	54-90	60-95	60-95	50-80	38-45	38-45	40-60	40-64	48-68	40-60	38-50	38-50	60-85	70-90	70-90	60-85	85-107	85-107	85-107	85-107	67-98																										
Fair (Mod. unstable)	44-47	44-47	91-129	96-132	96-142	81-110	46-58	46-58	61-78	65-84	69-88	61-78	51-61	51-61	86-105	91-110	91-110	86-105	108-132	108-132	108-132	108-132	99-125																										
Poor (Unstable)	48+	48+	130+	133+	143+	111+	59+	59+	79+	85+	89+	79+	62+	62+	106+	111+	111+	106+	133+	133+	133+	133+	126+																										
<b>Stream type</b>	<b>DA3</b>	<b>DA4</b>	<b>DA5</b>	<b>DA6</b>	<b>DA7</b>	<b>EA</b>	<b>E5</b>	<b>E6</b>	<b>F1</b>	<b>F2</b>	<b>F3</b>	<b>F4</b>	<b>F5</b>	<b>F6</b>	<b>G1</b>	<b>G2</b>	<b>G3</b>	<b>G4</b>	<b>G5</b>	<b>G6</b>																													
Good (Stable)	40-63	40-63	40-63	40-63	50-75	50-75	40-63	40-63	60-85	60-85	85-110	85-110	90-115	80-95	40-60	40-60	40-60	85-107	90-112	85-107																													
Fair (Mod. unstable)	64-86	64-86	64-86	64-86	76-96	76-96	64-86	64-86	86-105	86-105	111-125	111-125	116-130	96-110	61-78	61-78	108-120	108-120	113-125	108-120																													
Poor (Unstable)	87+	87+	87+	87+	87+	87+	87+	87+	106+	106+	126+	126+	131+	111+	79+	79+	121+	121+	126+	121+																													
																							<b>Modified channel stability rating =</b>	<b>Poor</b>																									

\*Rating is adjusted to potential stream type, not existing.

## BANCS Model – Streambank Erosion

**Worksheet 5-18.** Annual streambank erosion estimates.

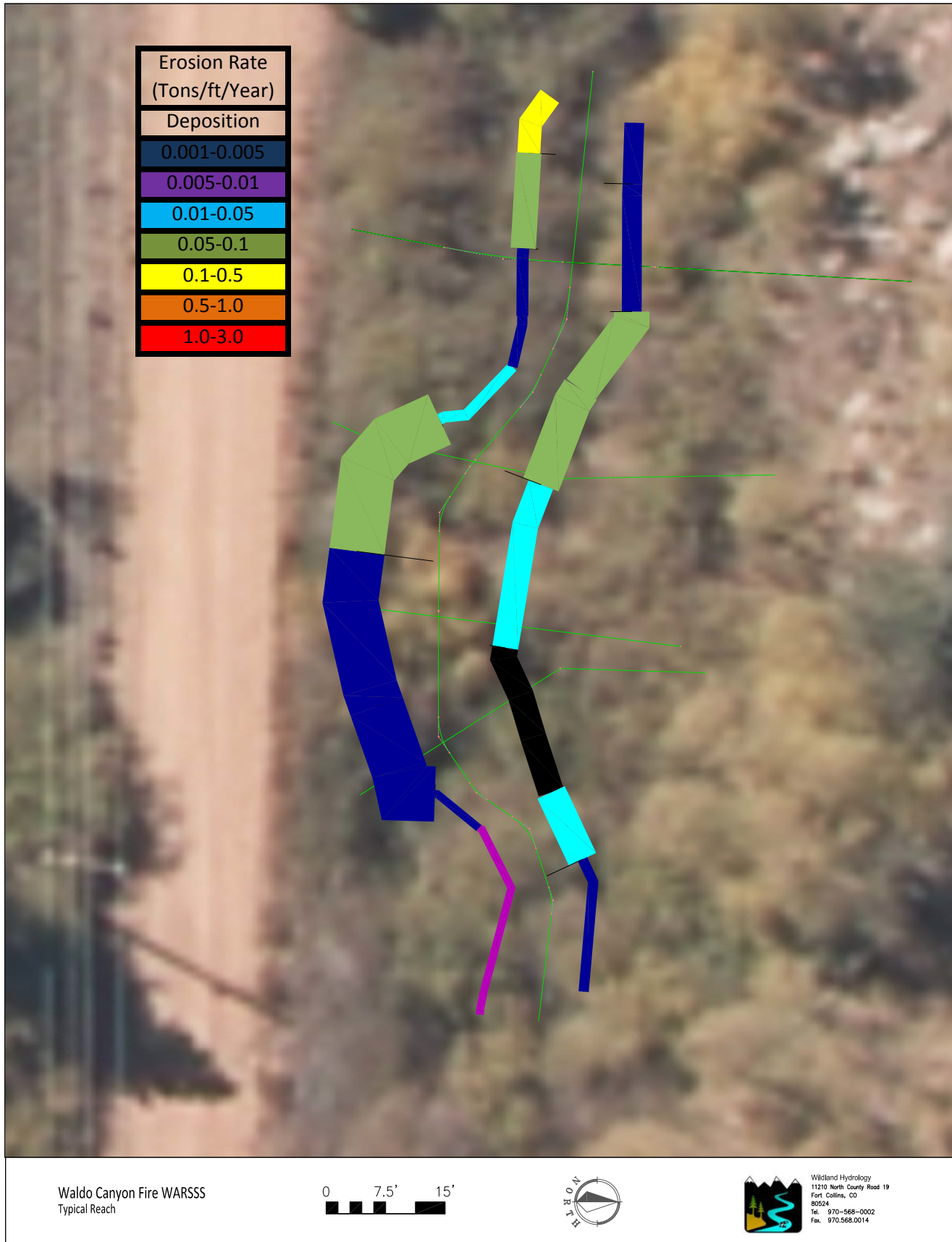
Stream: <b>West Monument F4 Fair</b>				Location:			
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>120</b>			Date: <b>11/5/2012</b>		
Observers: <b>Rosgen et. al.</b>		Valley Type: <b>VIIIb</b>		Stream Type: <b>F4</b>			
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 3-11) (adjective)	NBS rating (Worksheet 3-12) (adjective)	Bank erosion rate (Figure 3-9 or 3-10) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [[ $(4) \times (5) \times (6)$ ] (ft <sup>3</sup> /yr)	Erosion Rate (tons/yr/ft) {[( $7$ )/ $27$ ] $\times$ 1.3 / ( $5$ )}
1. LB 0+09 to 0+17	Very Low	Low	0.003	8.0	2.5	0.06	0.00036
2. LB 0+26 to 0+31	Moderate	High	0.420	5.0	4.5	9.45	0.09100
3. LB 0+00 to 0+09	Very Low	Very Low	0.0017	9.0	2.5	0.04	0.00020
4. LB 0+17 to 0+26	Moderate	Very Low	0.092	9.0	3.3	2.74	0.01460
5. LB 0+31 to 0+48	High	Moderate	0.380	17.0	4.8	31.01	0.08780
6. LB 0+48 to 0+71	Moderate	Low	0.153	23.0	3.3	11.61	0.02430
7. LB 0+97 to 1+09	Low	High	0.151	12.0	3.8	6.89	0.02760
8. LB 1+09 to 1+20	Low	Low	0.036	11.0	1.3	0.51	0.00220
9. RB 0+87 to 0+95	Very Low	Very Low	0.0017	8.0	1.0	0.01	0.00008
10. RB 0+80 to 0+87	High	Very High	0.810	7.0	4.0	22.68	0.15600
11. RB 0+60 to 0+80	Low	Moderate	0.073	20.0	1.0	1.45	0.00350
12. RB 0+46 to 0+60	Moderate	Moderate	0.282	14.0	7.0	27.64	0.09500
13. RB 0+38 to 0+46	Moderate	Low	0.153	8.0	1.4	1.71	0.01030
14. RB 0+29 to 0+38	Low	Moderate	0.073	9.0	1.3	0.85	0.00450
15. RB 0+17 to 0+29	Low	Low	0.036	12.0	1.5	0.64	0.00260
16. RB 0+05 to 0+17	Moderate	High	0.420	12.0	3.2	16.13	0.06470
17. RB 0+00 to 0+05	Very High	Very High	0.872	5.0	2.9	12.64	0.12180
18. RB 0+95 to 1+18	Low	Low	0.021	18.0	1.0	0.37	0.00100
19. RB 1+18 to 1+20	Moderate	Moderate	0.179	2.0	1.0	0.34	0.00820
20							
21							



**Worksheet 5-18, con't.** Annual streambank erosion estimates.

Stream: <b>West Monument F4 Fair</b>		Location:					
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>120</b>			Date: <b>11/5/2012</b>		
Observers: <b>Rosgen et. al.</b>		Valley Type: <b>VIIIb</b>			Stream Type: <b>F4</b>		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 3-11) (adjective)	NBS rating (Worksheet 3-12) (adjective)	Bank erosion rate (Figure 3-9 or 3-10) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [(4)×(5)×(6)] (ft <sup>3</sup> /yr)	Erosion Rate (tons/yr/ft) {[ (7)/27 ] × 1.3 / (5)}
22							
23							
24							
25							
26							
27							
28							
29							
30							
31							
32							
33							
34							
35							
36							
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					<b>Total Erosion (ft<sup>3</sup>/yr)</b>	<b>146.77</b>	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					<b>Total Erosion (yds<sup>3</sup>/yr)</b>	<b>5.44</b>	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					<b>Total Erosion (tons/yr)</b>	<b>7.07</b>	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					<b>Unit Erosion Rate (tons/yr/ft)</b>	<b>0.0589</b>	

### Streambank Erosion Map



## FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

From dimensioned flow-duration curve				From sediment rating curves				Calculate			Calculate sediment yield			
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Flow exceedence (%)	Daily mean discharge (cfs)	Mid-ordinate (%)	Time increment (percent)	Time increment (days)	Mid-ordinate streamflow (cfs)	Dimensionless streamflow	Dimensionless suspended sediment discharge (S/S <sub>sd</sub> )	Suspended sediment discharge (tons/day)	Dimensionless bedload discharge (b <sub>s</sub> /b <sub>skt</sub> )	Bedload (tons/day)	Time adjusted streamflow (cfs)	Suspended sediment [(5)×(9)] (tons)	Bedload sediment [(5)×(11)] (tons)	Suspended + bedload [(13)+(14)] (tons)
100.000	0.1													
90.000	0.2	95.00	10.00	36.50	0.1	0.02	0.1	0.0	0.0000	0.00	1.40	0.00	0.00	0.00
80.000	0.3	85.00	10.00	36.50	0.3	0.04	0.1	0.0	0.0000	0.00	2.80	0.00	0.00	0.00
70.000	0.4	75.00	10.00	36.50	0.3	0.05	0.1	0.0	0.0000	0.00	3.40	0.00	0.00	0.00
60.000	0.5	65.00	10.00	36.50	0.4	0.06	0.1	0.0	0.0000	0.00	4.20	0.00	0.00	0.00
50.000	0.6	55.00	10.00	36.50	0.5	0.08	0.1	0.0	0.0000	0.00	5.30	0.00	0.00	0.00
40.000	0.8	45.00	10.00	36.50	0.7	0.10	0.1	0.0	0.0000	0.00	7.00	0.00	0.00	0.00
30.000	1.1	35.00	10.00	36.50	1.0	0.14	0.1	0.0	0.0000	0.00	9.50	0.00	0.00	0.00
20.000	1.7	25.00	10.00	36.50	1.4	0.20	0.1	0.0	0.0001	0.00	13.90	0.00	0.00	0.00
10.000	3.1	15.00	10.00	36.50	2.4	0.34	0.1	0.0	0.0006	0.09	23.70	0.36	3.28	3.64
5.000	4.9	7.50	5.00	18.25	4.0	0.57	0.2	0.0	0.0021	0.26	19.80	0.36	4.75	5.11
4.000	5.5	4.50	1.00	3.65	5.2	0.74	0.3	0.1	0.0039	0.48	5.16	0.18	1.75	1.93
3.000	6.4	3.50	1.00	3.65	5.9	0.85	0.5	0.1	0.0053	0.65	5.92	0.29	2.37	2.66
2.000	7.6	2.50	1.00	3.65	7.0	1.00	0.6	0.1	0.0077	0.91	6.99	0.47	3.32	3.79
1.500	8.7	1.75	0.50	1.83	8.1	1.16	0.9	0.2	0.0107	1.30	4.07	0.38	2.37	2.75
1.000	10.6	1.25	0.50	1.83	9.7	1.38	1.3	0.4	0.0157	1.90	4.83	0.66	3.47	4.13
0.900	11.3	0.95	0.10	0.37	11.0	1.57	1.6	0.6	0.0194	2.51	1.09	0.20	0.92	1.12
0.800	11.9	0.85	0.10	0.37	11.6	1.66	1.6	0.7	0.0194	2.85	1.16	0.24	1.04	1.28
0.700	12.6	0.75	0.10	0.37	12.3	1.76	1.6	0.8	0.0194	3.20	1.23	0.29	1.17	1.46
0.600	13.4	0.65	0.10	0.37	13.0	1.86	1.6	1.0	0.0194	3.63	1.30	0.35	1.32	1.67
0.500	14.4	0.55	0.10	0.37	13.9	1.99	1.6	1.2	0.0194	4.19	1.39	0.44	1.53	1.97
0.250	16.6	0.38	0.25	0.91	15.5	2.21	1.6	1.8	0.0194	5.36	3.87	1.60	4.89	6.49
0.100	19.2	0.18	0.15	0.55	17.9	2.56	1.6	2.9	0.0194	7.39	2.69	1.56	4.05	5.61
0.050	20.6	0.08	0.05	0.18	19.9	2.84	1.6	4.1	0.0194	9.29	0.99	0.74	1.70	2.44
0.010	22.4	0.03	0.04	0.15	21.5	3.07	1.6	5.3	0.0194	10.97	0.86	0.77	1.60	2.37
0.005	22.4	0.01	0.01	0.02	22.4	3.20	1.6	6.1	0.0194	12.01	0.11	0.11	0.22	0.33
0.001	22.4	0.00	0.00	0.01	22.4	3.20	1.6	6.1	0.0194	12.01	0.09	0.09	0.18	0.27
<b>Annual totals:</b>											<b>9.1</b> (tons/yr)	<b>39.9</b> (tons/yr)	<b>49.0</b> (tons/yr)	

**Worksheet 19b.** Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

From dimensioned flow-duration curve				From sediment rating curves				Calculate		Calculate sediment yield				
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Flow exceedence (%)	Daily mean discharge (cfs)	Mid-ordinate (%)	Time increment (percent)	Time increment (days)	Mid-ordinate streamflow (cfs)	Dimensionless streamflow	Dimensionless suspended sediment discharge (S/S <sub>bed</sub> )	Suspended sediment discharge (tons/day)	Dimensionless bedload discharge (b <sub>y</sub> /b <sub>bed</sub> )	Bedload (tons/day)	Time adjusted streamflow (cfs)	Suspended sediment [(5)×(9)] (tons)	Bedload sediment [(5)×(11)] (tons)	Suspended + bedload [(13)+(14)] (tons)
						(Q/Q <sub>bed</sub> )								
100.000	0.1													
90.000	0.2	95.00	10.00	36.50	0.1	0.02	0.1	0.0	0.0000	0.00	1.40	0.00	0.00	0.00
80.000	0.3	85.00	10.00	36.50	0.3	0.04	0.1	0.0	0.0000	0.00	2.80	0.00	0.00	0.00
70.000	0.4	75.00	10.00	36.50	0.3	0.05	0.1	0.0	0.0000	0.00	3.40	0.00	0.00	0.00
60.000	0.5	65.00	10.00	36.50	0.4	0.06	0.1	0.0	0.0000	0.00	4.20	0.00	0.00	0.00
50.000	0.6	55.00	10.00	36.50	0.5	0.08	0.1	0.0	0.0000	0.00	5.30	0.00	0.00	0.00
40.000	0.8	45.00	10.00	36.50	0.7	0.10	0.1	0.0	0.0000	0.00	7.00	0.00	0.00	0.00
30.000	1.2	35.00	10.00	36.50	1.0	0.14	0.1	0.0	0.0000	0.00	10.00	0.00	0.00	0.00
20.000	2.5	25.00	10.00	36.50	1.8	0.26	0.1	0.0	0.0002	0.04	18.30	0.00	1.46	1.46
10.000	5.0	15.00	10.00	36.50	3.7	0.53	0.2	0.0	0.0018	0.22	37.30	0.73	8.03	8.76
5.000	7.5	7.50	5.00	18.25	6.2	0.89	0.5	0.1	0.0059	0.73	31.20	1.64	13.32	14.96
4.000	8.2	4.50	1.00	3.65	7.8	1.12	0.8	0.2	0.0098	1.17	7.81	0.66	4.27	4.93
3.000	9.3	3.50	1.00	3.65	8.7	1.25	1.0	0.3	0.0125	1.51	8.71	0.95	5.51	6.46
2.000	10.5	2.50	1.00	3.65	9.9	1.41	1.4	0.4	0.0165	1.99	9.87	1.42	7.26	8.68
1.500	11.7	1.75	0.50	1.83	11.1	1.58	1.6	0.6	0.0194	2.55	5.54	1.04	4.65	5.69
1.000	13.6	1.25	0.50	1.83	12.6	1.80	1.6	0.9	0.0194	3.41	6.30	1.59	6.22	7.81
0.900	14.2	0.95	0.10	0.37	13.9	1.99	1.6	1.2	0.0194	4.23	1.39	0.44	1.54	1.98
0.800	14.9	0.85	0.10	0.37	14.6	2.08	1.6	1.4	0.0194	4.67	1.46	0.52	1.70	2.22
0.700	15.5	0.75	0.10	0.37	15.2	2.18	1.6	1.6	0.0194	5.14	1.52	0.60	1.88	2.48
0.600	16.4	0.65	0.10	0.37	16.0	2.28	1.6	1.9	0.0194	5.70	1.60	0.70	2.08	2.78
0.500	17.3	0.55	0.10	0.37	16.8	2.41	1.6	2.3	0.0194	6.44	1.68	0.85	2.35	3.20
0.250	19.6	0.38	0.25	0.91	18.4	2.64	1.6	3.2	0.0194	7.86	4.61	2.87	7.17	10.04
0.100	22.2	0.18	0.15	0.55	20.9	2.99	1.6	4.8	0.0194	10.32	3.13	2.62	5.65	8.27
0.050	23.5	0.08	0.05	0.18	22.8	3.27	1.6	6.5	0.0194	12.57	1.14	1.18	2.29	3.47
0.010	25.3	0.03	0.04	0.15	24.4	3.49	1.6	8.1	0.0194	14.56	0.98	1.19	2.13	3.32
0.005	25.3	0.01	0.01	0.02	25.3	3.62	1.6	9.2	0.0194	15.77	0.13	0.17	0.29	0.46
0.001	25.3	0.00	0.00	0.01	25.3	3.62	1.6	9.2	0.0194	15.77	0.10	0.13	0.23	0.36
<b>Annual totals:</b>											<b>19.3</b>	<b>78.0</b>	<b>97.3</b>	

# POWERSED Model – Sediment Transport Capacity

**Worksheet 20a.** Sediment transport prediction representing the upstream supply up to bankfull for bedload and suspended sand sediment.

Flow-duration curve			Calculate				Hydraulic geometry				Measure		Calculate					
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	
Percentage of time	Daily mean discharge	Mid-ordinate stream-flow	Area	Width	Depth	Velocity	Slope	Shear stress	Stream power	Unit power	Time increment	Time increment	Daily mean bedload transport	Daily mean suspended sand transport	Time adjusted bedload transport	Time adjusted suspended sand transport	Time adjusted total transport	
(%)	(cfs)	(cfs)	(ft <sup>2</sup> )	(ft)	(ft)	(ft/s)	(ft/ft)	(lb/ft <sup>2</sup> )	(lb/s)	(lb/ft/s)	(%)	(days)	(tons/day)	(tons/day)	(tons)	(tons)	(tons)	
100.000	0.05									0.00					0.00	0.00	0.00	
90.000	0.23	0.14	0.23	3.31	0.07	0.49	0.0090	0.04	0.08	0.02	10.000	36.50	0.00	0.00	0.00	0.00	0.00	
80.000	0.32	0.28	0.38	3.95	0.10	0.64	0.0090	0.05	0.16	0.04	10.000	36.50	0.00	0.00	0.00	0.00	0.00	
70.000	0.37	0.34	0.45	4.22	0.11	0.71	0.0090	0.06	0.19	0.05	10.000	36.50	0.00	0.00	0.00	0.00	0.00	
60.000	0.46	0.42	0.53	4.47	0.12	0.78	0.0090	0.07	0.24	0.05	10.000	36.50	0.00	0.00	0.00	0.00	0.00	
50.000	0.60	0.53	0.61	4.57	0.13	0.83	0.0090	0.07	0.30	0.07	10.000	36.50	0.00	0.00	0.00	0.00	0.00	
40.000	0.79	0.70	0.73	4.72	0.15	0.91	0.0090	0.09	0.39	0.08	10.000	36.50	0.00	0.00	0.00	0.00	0.00	
30.000	1.11	0.95	0.90	4.95	0.18	1.03	0.0090	0.10	0.53	0.11	10.000	36.50	0.00	0.00	0.00	0.00	0.00	
20.000	1.67	1.39	1.16	5.22	0.22	1.17	0.0090	0.12	0.78	0.15	10.000	36.50	0.00	0.00	0.00	0.00	0.00	
10.000	3.06	2.37	1.66	5.65	0.29	1.41	0.0090	0.16	1.33	0.24	10.000	36.50	0.09	0.01	3.00	0.00	4.00	
5.000	4.86	3.96	2.33	6.03	0.39	1.69	0.0090	0.21	2.22	0.37	5.000	18.25	0.26	0.02	5.00	0.00	5.00	
4.000	5.46	5.16	2.78	6.20	0.45	1.85	0.0090	0.24	2.90	0.47	1.000	3.65	0.48	0.05	2.00	0.00	2.00	
3.000	6.39	5.92	3.04	6.32	0.48	1.94	0.0090	0.26	3.32	0.53	1.000	3.65	0.65	0.08	2.00	0.00	3.00	
2.000	7.59	6.99	3.41	6.52	0.52	2.05	0.0090	0.28	3.93	0.60	1.000	3.65	0.91	0.13	3.00	0.00	4.00	
1.500	8.70	8.14	3.83	6.92	0.55	2.12	0.0090	0.30	4.57	0.66	0.500	1.83	1.25	0.19	2.00	0.00	3.00	
1.000	10.60	9.65																
0.900	11.30	10.95																
0.800	11.94	11.62																
0.700	12.59	12.27																
0.600	13.42	13.00																
0.500	14.35	13.88																
0.250	16.62	15.48																
0.100	19.21	17.91																
0.050	20.55	19.88																
0.010	22.36	21.45																
0.005	22.36	22.36																
0.001	22.36	22.36																
Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr):														17.9	2.1	19.7		

**Worksheet 20b.** Sediment transport prediction for the existing condition reach compared to the upstream sediment supply to assess bed stability.

Flow-duration curve			Calculate				Hydraulic geometry				Measure		Calculate							
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)			
Percentage of time	Daily mean discharge	Mid-ordinate stream-flow	Area	Width	Depth	Velocity	Slope	Shear stress	Stream power	Unit power	Time increment	Time increment	Daily mean bedload transport	Daily mean suspended sand transport	Time adjusted bedload transport	Time adjusted suspended sand transport	Time adjusted total transport			
(%)	(cfs)	(cfs)	(ft <sup>2</sup> )	(ft)	(ft)	(ft/s)	(ft/ft)	(lb/ft <sup>2</sup> )	(lb/s)	(lb/ft/s)	(%)	(days)	(tons/day)	(tons/day)	(tons)	(tons)	(tons)			
100.000	0.05								0.00						0.00	0.00	0.00			
90.000	0.23	0.14	0.21	2.95	0.07	0.63	0.0090	0.04	0.08	0.03	10.000	36.50	0.00	0.00	0.00	0.00	0.00			
80.000	0.32	0.28	0.32	3.08	0.10	0.77	0.0090	0.05	0.16	0.05	10.000	36.50	0.00	0.00	0.00	0.00	0.00			
70.000	0.37	0.34	0.37	3.13	0.12	0.83	0.0090	0.06	0.19	0.06	10.000	36.50	0.00	0.00	0.00	0.00	0.00			
60.000	0.46	0.42	0.43	3.21	0.13	0.91	0.0090	0.07	0.24	0.07	10.000	36.50	0.00	0.00	0.00	0.00	0.00			
50.000	0.60	0.53	0.52	3.31	0.16	1.03	0.0090	0.08	0.30	0.09	10.000	36.50	0.00	0.00	0.00	0.00	0.00			
40.000	0.79	0.70	0.65	3.83	0.17	1.06	0.0090	0.09	0.39	0.10	10.000	36.50	0.00	0.00	0.00	0.00	0.00			
30.000	1.11	0.95	0.84	4.60	0.18	1.12	0.0090	0.09	0.53	0.12	10.000	36.50	0.00	0.00	0.00	0.00	0.00			
20.000	1.67	1.39	1.10	5.19	0.21	1.23	0.0090	0.11	0.78	0.15	10.000	36.50	0.00	0.00	0.00	0.00	0.00			
10.000	3.06	2.37	1.61	5.87	0.27	1.46	0.0090	0.13	1.33	0.23	10.000	36.50	0.09	0.01	3.00	0.00	4.00			
5.000	4.86	3.96	2.27	6.29	0.36	1.73	0.0090	0.17	2.22	0.35	5.000	18.25	0.22	0.02	4.00	0.00	4.00			
4.000	5.46	5.16	2.71	6.47	0.42	1.91	0.0090	0.20	2.90	0.45	1.000	3.65	0.43	0.05	2.00	0.00	2.00			
3.000	6.39	5.92	2.99	6.71	0.45	1.97	0.0090	0.21	3.32	0.49	1.000	3.65	0.52	0.06	2.00	0.00	2.00			
2.000	7.59	6.99	3.38	7.05	0.48	2.07	0.0090	0.23	3.93	0.56	1.000	3.65	0.78	0.11	3.00	0.00	3.00			
1.500	8.70	8.14	3.80	7.44	0.51	2.14	0.0090	0.24	4.57	0.61	0.500	1.83	0.95	0.16	2.00	0.00	2.00			
1.000	10.60	9.65																		
0.900	11.30	10.95																		
0.800	11.94	11.62																		
0.700	12.59	12.27																		
0.600	13.42	13.00																		
0.500	14.35	13.88																		
0.250	16.62	15.48																		
0.100	19.21	17.91																		
0.050	20.55	19.88																		
0.010	22.36	21.45																		
0.005	22.36	22.36																		
0.001	22.36	22.36																		
Notes:																				
															Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr):			15.4	1.9	17.2
															Upstream total annual sediment comparative reach (tons/yr) (WS 5-20a):			17.8	2.0	19.8
															Difference in sediment transport capacity (tons/yr) (+ or -):			-2.4	-0.1	-2.6
															Stability evaluation: Aggradation, Degradation or Stable:			Aggradation		

## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>West Monument F4 Fair</b>		Stream Type: <b>F4</b>	
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIIb</b>	
Observers: <b>Rosgen et. al.</b>		Date: <b>11/05/2012</b>	
<b>Enter Required Information for Existing Condition</b>			
9.6	$D_{50}$	Riffle bed material $D_{50}$ (mm)	
0.0	$D_{50}^{\wedge}$	Bar sample $D_{50}$ (mm)	
0.197	$D_{max}$	Largest particle from <b>Bed Material</b> (ft)	60 (mm) 304.8 mm/ft
0.01650	$S$	Existing bankfull water surface slope (ft/ft)	
0.53	$d$	Existing bankfull mean depth (ft)	
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment	
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>			
0.00	$D_{50}/D_{50}^{\wedge}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 ( D_{50}/D_{50}^{\wedge} )^{-0.872}$
6.26	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 ( D_{max}/D_{50} )^{-0.887}$
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED: <b>2</b>
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>			
N/A	$d$	Required bankfull mean depth (ft)	$d = \frac{\tau^* (\gamma_s - 1) D_{max}}{S}$ (use $D_{max}$ in ft)
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>			
N/A	$S$	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^* (\gamma_s - 1) D_{max}}{d}$ (use $D_{max}$ in ft)
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading			
<b>Sediment Competence Using Dimensional Shear Stress</b>			
0.294	Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d ) $\gamma = 62.4$ , $d =$ existing depth, $S =$ existing slope		
Shields 21.8	CO 61.84	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ (Figure 5-49)	
Shields 0.779	CO 0.283	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) (Figure 5-49)	
Shields 1.40	CO 0.51	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm) $\tau =$ predicted shear stress, $\gamma = 62.4$ , $S =$ existing slope	$d = \frac{\tau}{\gamma S}$
Shields 0.0235	CO 0.0085	Predicted slope required to initiate movement of measured $D_{max}$ (mm) $\tau =$ predicted shear stress, $\gamma = 62.4$ , $d =$ existing depth	$S = \frac{\tau}{\gamma d}$
Check: <input checked="" type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading			

## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>West Monument F4 Fair</b>	Stream Type: <b>F4</b>
Location: <b>Pike National Forest, CO</b>	Valley Type: <b>VIIIb</b>
Observers: <b>Rosgen et. al.</b>	Date: <b>11/05/2012</b>
Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)	Stability Rating (Check Appropriate Rating)
Stream Type at potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	<input checked="" type="checkbox"/> Stable
(E→C), (C→High W/d C)	<input type="checkbox"/> Moderately Unstable
(G→F), (F→D), (C→F)	<input checked="" type="checkbox"/> Unstable
(C→D), (B→G), (D→G), (C→G), (E→G)	<input type="checkbox"/> Highly Unstable



Worksheet 5-25. Lateral stability.

Stream: <b>West Monument F4 Fair</b>		Stream Type: <b>F4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIIb</b>			
Observers: <b>Rosgen et. al.</b>		Date: <b>11/05/2012</b>			
Lateral stability criteria (choose one stability category for each criterion 1–5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	4
	(2)	(4)	(6)	(8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	4
	(1)	(2)	(3)	(4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		1
	(1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	6
	(2)	(4)	(6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	1
	(1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>14</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input type="checkbox"/>	<i>Unstable</i> 13 – 21 <input checked="" type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	

**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>West Monument F4 Fair</b>		Stream Type: <b>F4 Fair</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIIb</b>			
Observers: <b>Rosgen et. al.</b>		Date: <b>11/05/2012</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
1 <b>Sediment competence</b> (Worksheet 5-22)	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope-slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	2
	(2)	(4)	(6)	(8)	
2 <b>Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	2
	(2)	(4)	(6)	(7)	
3 <b>W/d Ratio State</b> (Worksheet 5-13)	1.0 – 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	4
	(2)	(4)	(6)	(8)	
4 <b>Stream Succession States</b> (Worksheet 5-24)	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	6
	(2)	(4)	(6)	(8)	
5 <b>Depositional Patterns</b> (Worksheet 5-10)	B1	B2, B4	B3, B5	B6, B7, B8	NA
	(1)	(2)	(3)	(4)	
6 <b>Debris / Blockages</b> (Worksheet 5-11)	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	1
	(1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>15</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
<b>Vertical Stability for Excess Deposition / Aggradation (use total points and check stability rating)</b>	<i>No Deposition</i> 10 – 14 <input type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input checked="" type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input type="checkbox"/>	<i>Aggradation</i> > 30 <input type="checkbox"/>	

Worksheet 5-27. Vertical stability – degradation.

Stream: <b>West Monument F4 Fair</b>		Stream Type: <b>F4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIIb</b>			
Observers: <b>Rosgen et. al.</b>		Date: <b>11/05/2012</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>1 Sediment Competence (Worksheet 5-22)</b>	Does not indicate excess competence <b>(2)</b>	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed <b>(4)</b>	$D_{100}$ of bed moved <b>(6)</b>	Particles much larger than $D_{100}$ of bed moved <b>(8)</b>	<b>2</b>
<b>2 Sediment Capacity (POWERSED) (Worksheet 5-20)</b>	Does not indicate excess capacity <b>(2)</b>	Slight excess energy: up to 10% increase above reference <b>(4)</b>	Excess energy sufficient to increase load up to 50% of annual load <b>(6)</b>	Excess energy transporting more than 50% of annual load <b>(8)</b>	<b>2</b>
<b>3 Degree of Channel Incision (BHR) (Worksheet 5-12)</b>	1.00 – 1.10 <b>(2)</b>	1.11 – 1.30 <b>(4)</b>	1.31 – 1.50 <b>(6)</b>	$> 1.50$ <b>(8)</b>	<b>8</b>
<b>4 Stream Succession States (Worksheets 5-12 and 5-24)</b>	Does not indicate incision or degradation <b>(2)</b>	If BHR $> 1.1$ and stream type has W/d between 5–10 <b>(4)</b>	If BHR $> 1.1$ and stream type has W/d less than 5 <b>(6)</b>	(B→G), (C→G), (E→G), (D→G) <b>(8)</b>	<b>2</b>
<b>5 Confinement (MWR / MWR<sub>ref</sub>) (Worksheet 5-14)</b>	0.80 – 1.00 <b>(1)</b>	0.30 – 0.79 <b>(2)</b>	0.10 – 0.29 <b>(3)</b>	$< 0.10$ <b>(4)</b>	<b>1</b>
<b>Total Points</b>					<b>15</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation (use total points and check stability rating)</b>	<i>Not Incised</i> 9 – 11 <input type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input checked="" type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input type="checkbox"/>	<i>Degradation</i> $> 27$ <input type="checkbox"/>	

**Worksheet 5-28.** Channel enlargement.

Stream: <b>Mest Monument F4 Fair</b>		Stream Type: <b>F4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIIb</b>			
Observers: <b>Rosgen et. al.</b>		Date: <b>11/05/2012</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1-4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	6
	(2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	4
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	4
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	4
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>18</b>
<b>Category Point Range</b>					
<b>Channel Enlargement Prediction (use total points and check stability rating)</b>	<i>No Increase</i> 8 – 10 <input type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input checked="" type="checkbox"/>	<i>Extensive</i> > 24 <input type="checkbox"/>	

Worksheet 5-29. Overall sediment supply.

Stream: <b>West Monument F4 Fair</b>		Stream Type: <b>F4</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIIb</b>		
Observers: <b>Rosgen et. al.</b>		Date: <b>11/05/2012</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1–5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	2	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	2	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	2	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	2	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	4	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>12</b>	
<b>Category Point Range</b>				
Overall Sediment Supply Rating (use total points and check stability rating)	<b>Low</b> 5 <input type="checkbox"/>	<b>Moderate</b> 6 – 10 <input type="checkbox"/>	<b>High</b> 11 – 15 <input checked="" type="checkbox"/>	<b>Very High</b> 16 – 20 <input type="checkbox"/>

Worksheet 5-32. Summary of stability condition categories.

Stream: <b>West Monument F4 Fair</b>		Location: <b>Pike National Forest, Colorado</b>	
Observers: <b>Rosgen et. al.</b>		Date: <b>11/5/2012</b>	Stream Type: <b>F4</b> Valley Type: <b>VIIIb</b>
<b>Channel Dimension</b>	Mean Bankfull Depth (ft): <b>0.53</b>	Bankfull Width (ft): <b>7.68</b>	Cross-Sectional Area (ft <sup>2</sup> ): <b>4.06</b> Width of Flood-Prone Area (ft): <b>14.49</b> Entrenchment Ratio: <b>1.38</b>
<b>Channel Pattern</b>	Mean: $\lambda/W_{bkt}$ : <b>6.91</b> Range: $\lambda/W_{bkt}$ : <b>6.63-7.19</b>	$L_m/W_{bkt}$ : <b>7.88</b> $R_c/W_{bkt}$ : <b>7.29-8.46</b>	$R_c/W_{bkt}$ : <b>1.6</b> MWR: <b>3.44</b> Sinuosity: <b>1.09</b>
<b>River Profile &amp; Bed Features</b>	Check: <input checked="" type="checkbox"/> Riffle/Pool <input type="checkbox"/> Step/Pool <input type="checkbox"/> Plane Bed <input type="checkbox"/> Convergence/Divergence <input type="checkbox"/> Dunes/Antidunes/Smooth Bed	Riffle Pool	Pool-to-Pool Ratio
	Max Bankfull Depth (ft): <b>0.8</b>	Depth Ratio (max to mean): <b>1.51</b>	Valley: <b>0.018</b> Water Surface: <b>0.0165</b>
<b>Level III Stream Stability Indices</b>	Riparian Vegetation: <b>Willow/Aspen Dominated</b>	Potential Composition/Density: <b>At Potential</b>	Remarks: Condition, Vigor & Usage of Existing Reach:
	Flow Regime: <b>P1, P2, P7, P8 &amp; Order: S-3(4)</b>	Meander Patterns: <b>M3</b>	Depositional Patterns: <b>B2, B5</b> Debris/Channel Blockages: <b>D3</b>
	Degree of Incision (Bank-Height Ratio): <b>2.2</b>	Degree of Incision Stability Rating: <b>Deeply Incised</b>	Modified Pfankuch Stability Rating: <b>97 (Poor)</b>
	Width/depth Ratio (W/d): <b>14.49</b>	Reference W/d Ratio (W/d <sub>ref</sub> ): <b>16</b>	W/d Ratio State Stability Rating: <b>Stable</b>
Meander Width Ratio (MWR): <b>3.44</b>	Reference MWR <sub>ref</sub> : <b>3.7</b>	MWR / MWR <sub>ref</sub> Stability Rating: <b>Stable</b>	
<b>Bank Erosion Summary</b>	Length of Reach Studied (ft): <b>120</b>	Annual Streambank Erosion Rate: <b>7.06</b> (tons/yr) <b>0.0588</b> (tons/yr/ft)	Curve Used: <b>Colorado</b> Remarks: <b>Used Yellowstone curve for very low BEHI</b>
<b>Sediment Capacity (POWERSED)</b>	<input checked="" type="checkbox"/> Sufficient Capacity <input type="checkbox"/> Insufficient Capacity <input type="checkbox"/> Excess Capacity	Remarks:	
<b>Entrainment/Competence</b>	Largest Particle from Bar Sample (mm): <b>60</b>	$\tau =$ <b>0.283</b> $\tau^* =$ <b>N/A</b>	Existing Depth: <b>0.53</b> Required Depth: <b>0.51</b> Existing Slope: <b>0.017</b> Required Slope: <b>0.01</b>
<b>Successional Stage Shift</b>	<b>Bc</b> → <b>G</b> → <b>F</b> → <b>Bc</b> → <b>Bc</b> → <b>F4</b>	Existing Stream State (Type): <b>F4</b>	Potential Stream State (Type): <b>B4c</b>
<b>Lateral Stability</b>	<input type="checkbox"/> Stable <input type="checkbox"/> Mod. Unstable <input checked="" type="checkbox"/> Unstable	Remarks/causes: <b>Moderately high banks</b>	
<b>Vertical Stability (Aggradation)</b>	<input type="checkbox"/> No Deposition <input checked="" type="checkbox"/> Mod. Deposition <input type="checkbox"/> Ex. Deposition	Remarks/causes: <b>Aggradation</b>	
<b>Vertical Stability (Degradation)</b>	<input type="checkbox"/> Not Incised <input checked="" type="checkbox"/> Slightly Incised <input type="checkbox"/> Mod. Incised	Remarks/causes: <b>Degradation</b>	
<b>Channel Enlargement</b>	<input type="checkbox"/> No Increase <input checked="" type="checkbox"/> Slight Increase <input type="checkbox"/> Mod. Increase <input type="checkbox"/> Extensive	Remarks/causes: <b>One large raw bank</b>	
<b>Sediment Supply (Channel Source)</b>	<input type="checkbox"/> Low <input type="checkbox"/> Moderate <input checked="" type="checkbox"/> High <input type="checkbox"/> Very High	Remarks/causes: <b>Contribution from near by road.</b>	

# *Appendix C11*

## **F4b Stream Type** *Fair-Poor Stability Reach*





# Table of Contents

## Appendix C11: F4b Fair-Poor Reach

<b>Reach Location &amp; Overview.....</b>	<b>C11-2</b>
<b>Survey Summary.....</b>	<b>C11-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C11-8</b>
<b>Velocity, Classification &amp; Morphological Relations.....</b>	<b>C11-8</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b>Stability Indices.....</b>	<b>C11-12</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b>BANCS Model – Streambank Erosion.....</b>	<b>C11-22</b>
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b>FLOWSED Model – Total Annual Sediment Yield.....</b>	<b>C11-24</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b>POWERSED Model– Sediment Transport Capacity to Assess Bed Stability.....</b>	<b>C11-26</b>
Worksheet 5-20a. Sediment transport prediction for the upstream condition.	
Worksheet 5-20b. Sediment transport prediction for the existing condition.	
<b>Sediment Competence/Entrainment.....</b>	<b>C11-28</b>
Worksheet 5-22. Sediment competence calculations.	
<b>Channel Stability Ratings.....</b>	<b>C11-29</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b>Summary.....</b>	<b>C11-35</b>
Worksheet 5-32. Summary of stability condition categories.	

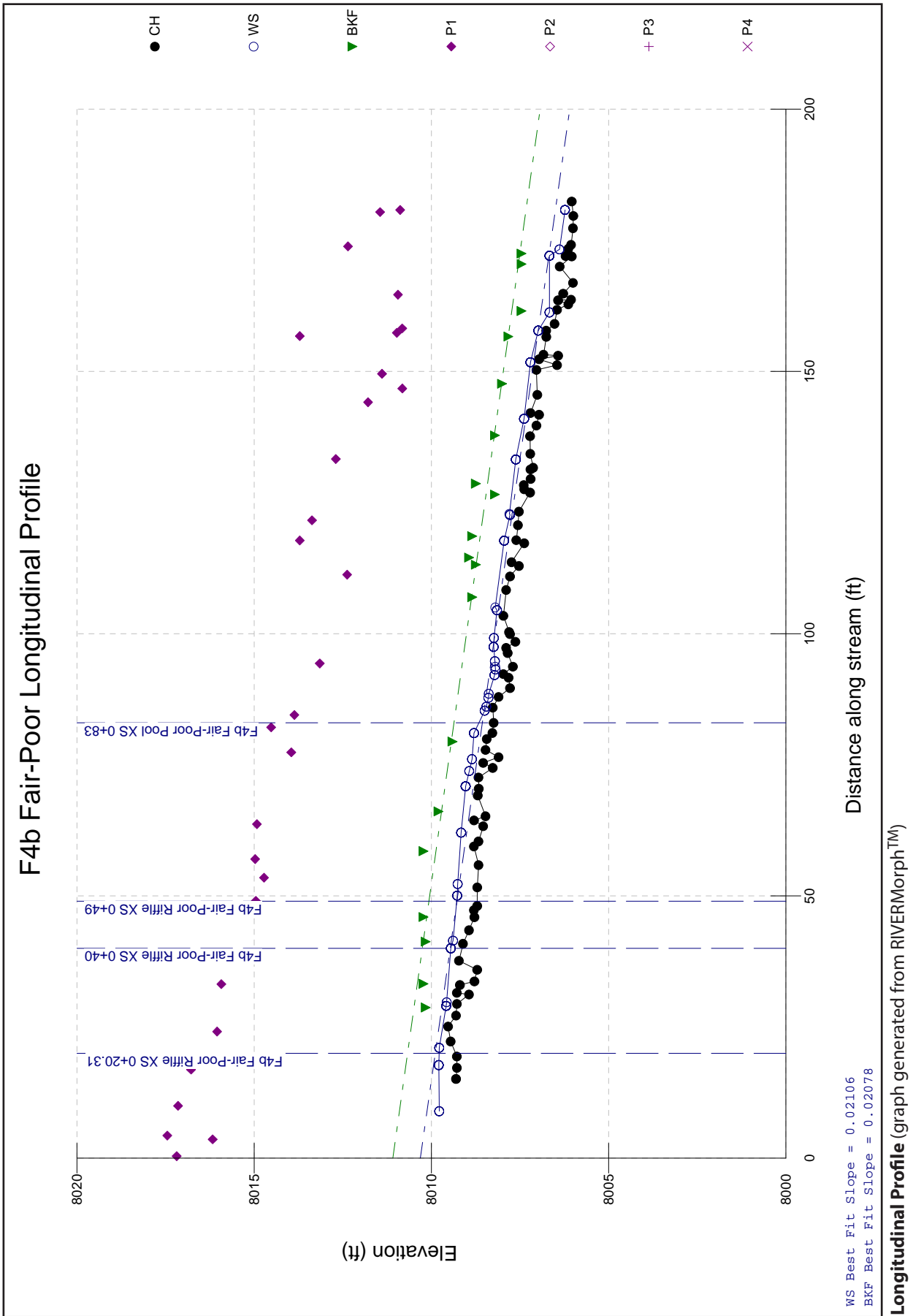
## F4b Fair-Poor Reach Location & Overview

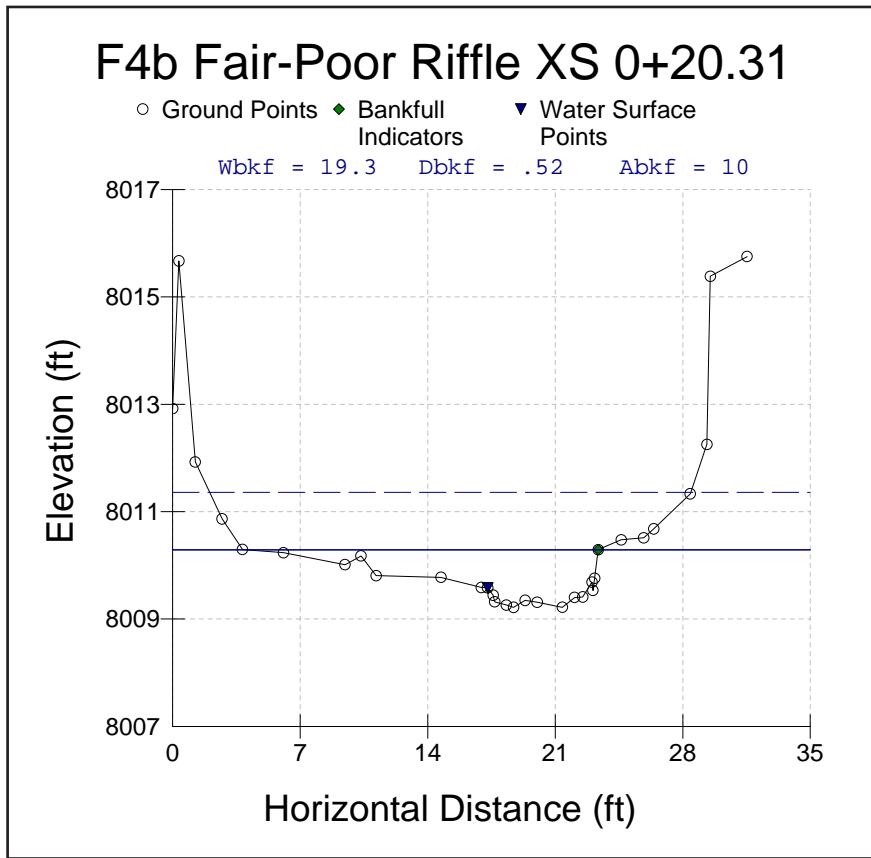
The F4b Fair-Poor representative reach is a 4<sup>th</sup> order, perennial, relatively steep gradient, entrenched stream located in lower Trail Creek (see location map **Figure C-2**). The photograph depicts an entrenched channel with evident bank erosion, yet colonization of riparian vegetation indicating a potential shift from an F4b to B4 stream type. The stream is apparently trying to recover from past flood and high sediment supply impacts. The width/depth ratio of 38 is still very high and will continue to promote excess deposition in this gulch-fill, alluvial Valley Type VIIIa. The stream is still enlarging due to the high peak flows following the fire. The potential stable stream type in this valley type is a B4; thus a POWERSED run was made to determine streambed stability, which indicated approximately 78 *tons/yr* of deposition. The streambank erosion rate of 0.024 *tons/yr/ft* is an order of magnitude larger than the B4 reference rate of 0.0048 *tons/yr/ft*. The sediment supply rating is *High*, typical of an F4 stream type, due to the high banks on both sides and the sediment deposition in the bed. The “Fair-Poor” rating indicates a higher potential accelerated increase in flow-related sediment compared to the same-sized, B4 reference stream type. The WRENSS model indicated that the water yield due to the fire increased from 3,213 *acre-ft* to 5,052 *acre-ft*, representing an increase of 1,839 *acre-ft*. The FLOWSED model indicated that bedload increased from 40 *tons/yr* to 257 *tons/yr* and suspended sediment increased from 63 *tons/yr* to 549 *tons/yr*, representing a total increase in sediment of 702 *tons/yr*. This increase is the result of increased sediment supply due to the unstable banks and high width/depth ratio that encourages increased sediment deposition in the streambed.

The following graphs and summary worksheets provide the detail of the morphology, hydraulics, streambank erosion rates, and stability conditions responsible for the overall “Fair-Poor” rating.

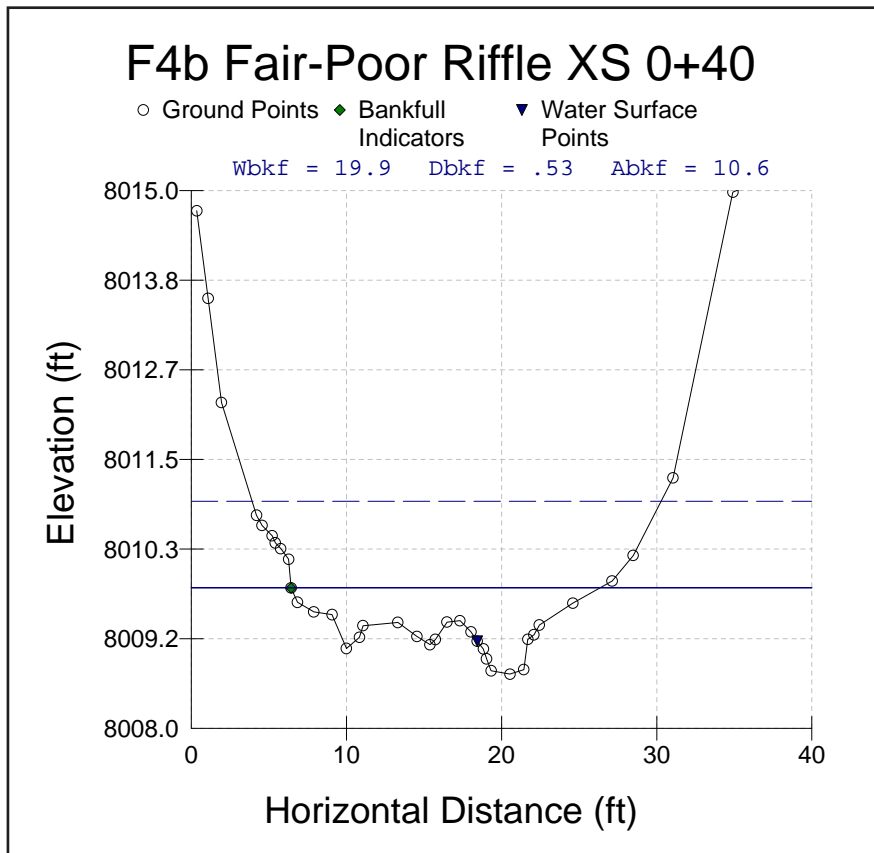


# Survey Summary

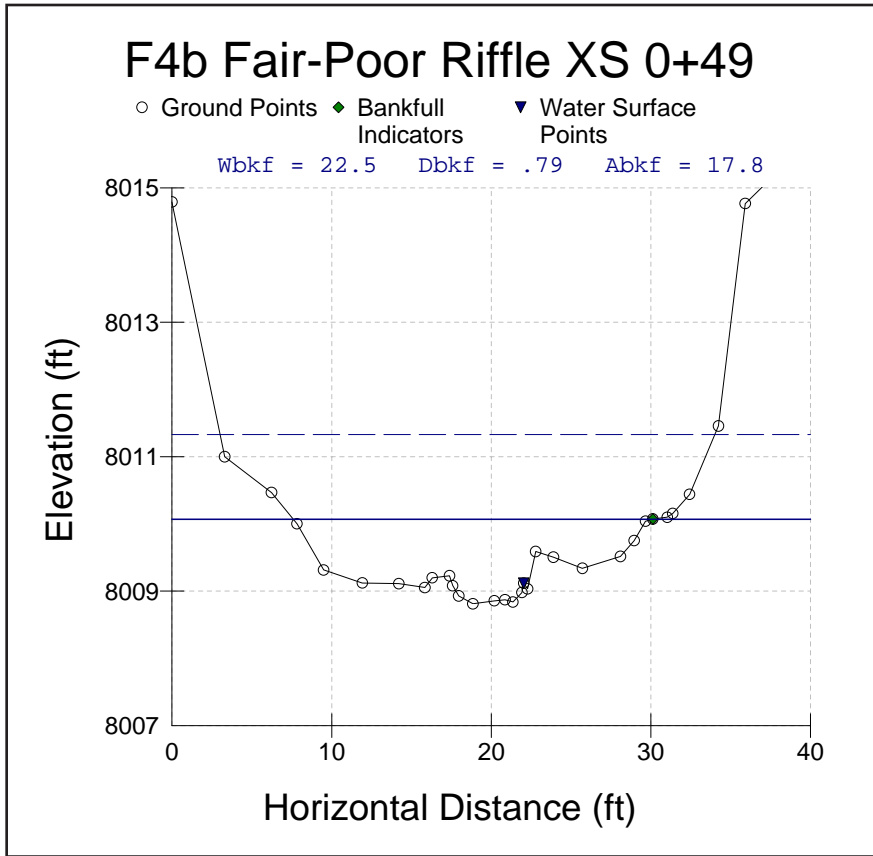




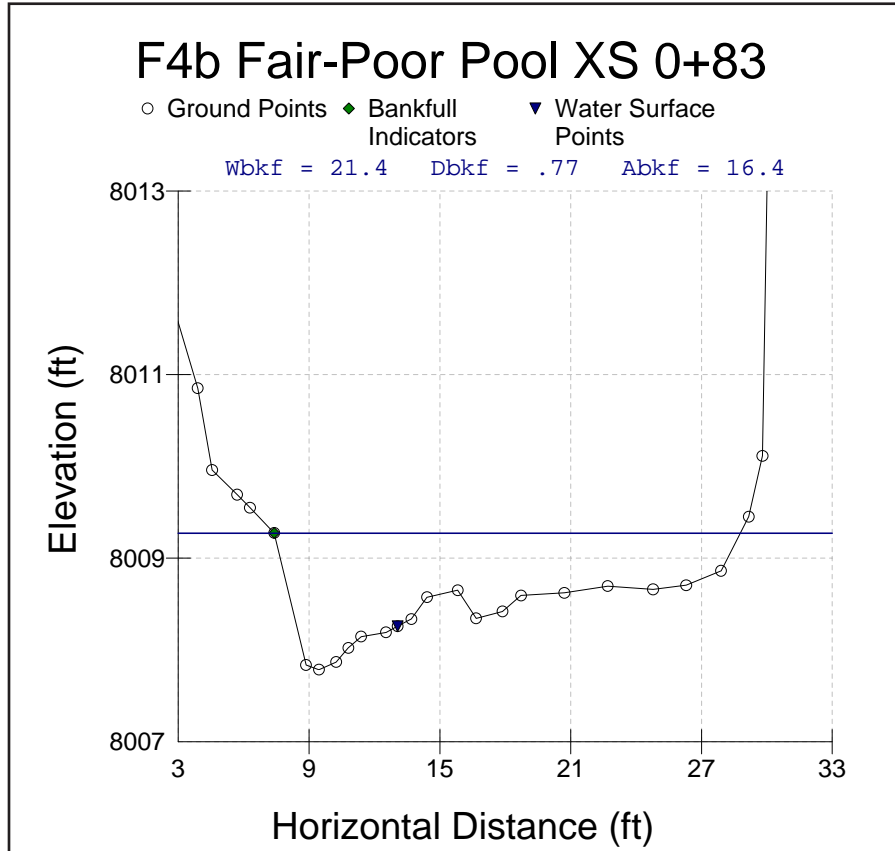
Riffle Cross-section 0+20.31 (graph generated from RIVERMorph™)



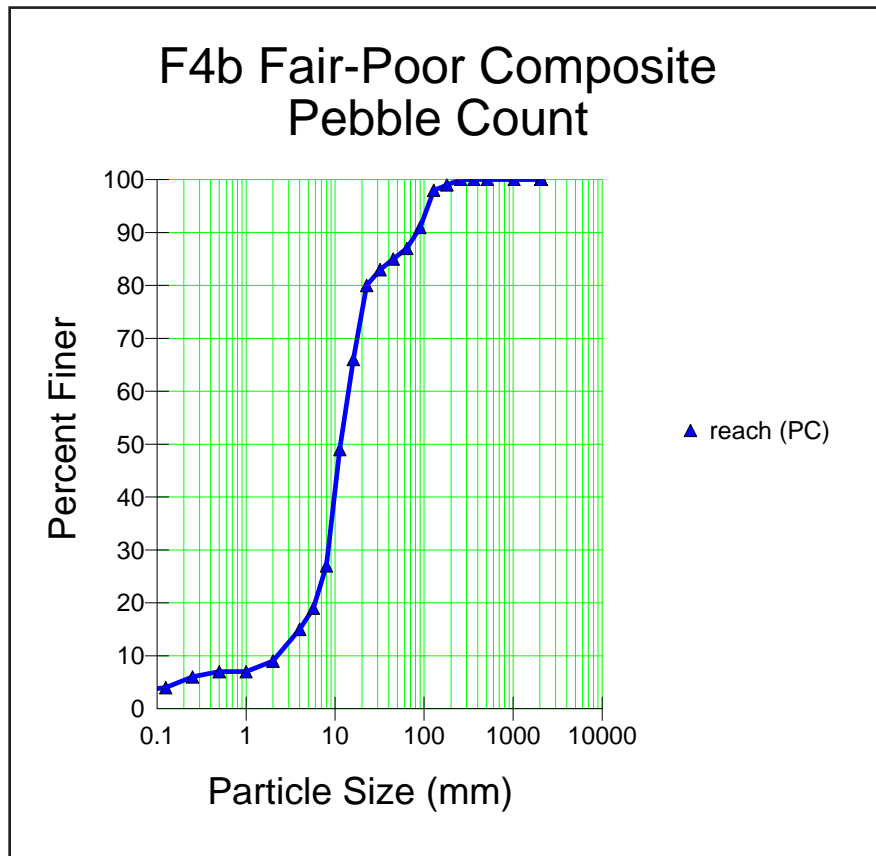
Representative Riffle Cross-section 0+40 (graph generated from RIVERMorph™)



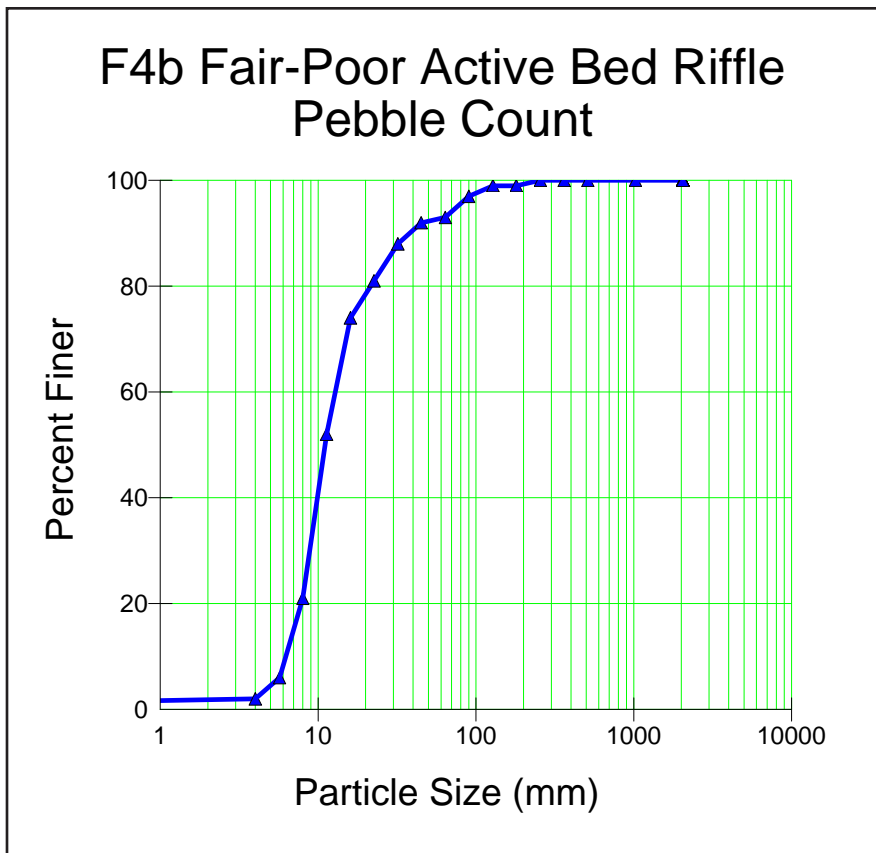
Riffle Cross-section 0+49 (graph generated from RIVERMorph™)



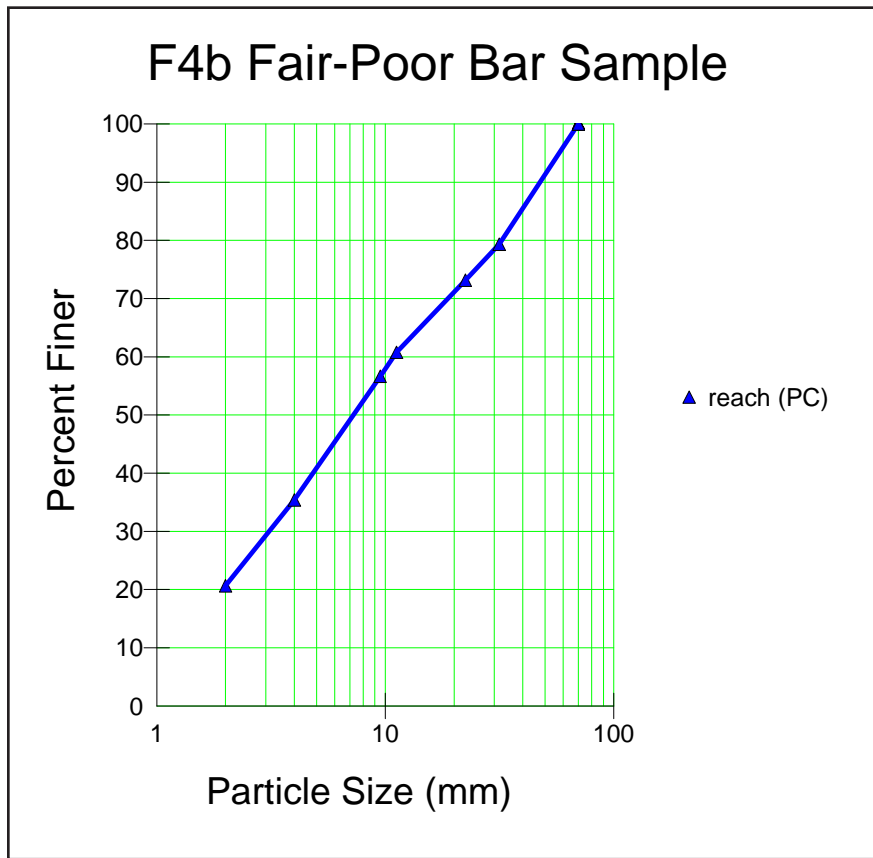
Pool Cross-Section 0+83 (graph generated from RIVERMorph™)



Composite Pebble Count (graph generated from RIVERMorph™)



Active Bed Riffle Pebble Count (graph generated from RIVERMorph™)



**Bar Sample** (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates						
Stream:	Trail Creek, F4b Fair-Poor Reach			Location:	Riffle XS 0+40, Pike N.F., Colorado	
Date:	8/26/2010	Stream Type:	F4b	Valley Type:	VIII	
Observers:	K. Wright, L. Chavez et al.			HUC:	___ - ___ - ___ - ___ - ___ - ___ - ___ - ___ - ___ - ___	
INPUT VARIABLES			OUTPUT VARIABLES			
Bankfull Riffle Cross-Sectional AREA	10.6	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.53	$d_{bkf}$ (ft)	
Bankfull Riffle WIDTH	19.9	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim (2 * d_{bkf}) + W_{bkf}$	20.59	$W_p$ (ft)	
$D_{84}$ at Riffle	26.6	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.09	$D_{84}$ (ft)	
Bankfull SLOPE	0.021	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	0.51	R (ft)	
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness $R(ft) / D_{84}(ft)$	5.89	$R / D_{84}$	
Drainage Area	10.7	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.590	$u^*$ (ft/sec)	
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE	
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$			4.24	ft / sec	44.97 cfs	
2. Roughness Coefficient: a) Manning's n from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.038$			3.65	ft / sec	38.69 cfs	
2. Roughness Coefficient: b) Manning's n from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.05$			2.77	ft / sec	29.40 cfs	
2. Roughness Coefficient: c) Manning's n from Jarrett (USGS): $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ <small>Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for Stream Types A1, A2, A3, B1, B2, B3, C2 &amp; E3</small> $n = 0.100$			1.39	ft / sec	14.71 cfs	
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)				ft / sec	cfs	
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)				ft / sec	cfs	
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q =$ <input type="text"/> year $u = Q / A$				ft / sec	cfs	
4. Continuity Equations: b) USGS Gage Data $u = Q / A$				ft / sec	cfs	
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation ( $R/D_{84}$ ) – Estimation Method 1						
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.						
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.						
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.						
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.						



**Worksheet 5-3.** Level II stream classification.

Stream: <b>Trail Creek, F4b Fair-Poor Reach</b>	
Basin:	Drainage Area: acres <b>10.7</b> mi <sup>2</sup>
Location: <b>Pike National Forest, Colorado</b>	
Twp.&Rge:	Sec.&Qtr.:
Cross-Section Monuments (Lat./Long.): <b>Riffle XS 0+40</b> Date: <b>8/26/10</b>	
Observers: <b>K. Wright, L. Chavez, D. Butler &amp; D. Bohon</b> Valley Type: <b>VIII</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>19.9</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A_{bkf} / W_{bkf}$ ).	<b>0.53</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>10.6</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>37.6</b>	ft/ft
<b>Maximum DEPTH (<math>d_{max}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>1.13</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>26.36</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>1.32</b>	ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the median or dominant diameter of channel materials, as sampled proportionately from the channel surface, between the bankfull stage and Thalweg elevations.	<b>12</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.021</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope ( $S_{val} / S$ ).	<b>1.03</b>	

<div style="border: 1px solid black; padding: 5px; display: inline-block;">Stream Type</div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: #e0f0ff;"><b>F4b</b></div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;">See Classification Key (Figure 2-14)</div>
--	--	---

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, F4b Fair-Poor Reach</b>		Location: <b>Pike National Forest, Colorado</b>							
Observers: <b>K. Wright, L. Chavez et al.</b>		Date: <b>8/26/2010</b>		Valley Type: <b>VIII</b>		Stream Type: <b>F4b</b>			
<b>River Reach Dimension Summary Data.....1</b>									
<b>Riffle Dimensions* ** * ** *</b>	<b>Riffle Dimensions* ** * ** *</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	
	Riffle Width ( $W_{bkt}$ )	<b>20.4</b>	<b>19.3</b>	<b>22.0</b>	ft	Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	<b>12.6</b>	<b>10.0</b>	<b>17.2</b>
	Mean Riffle Depth ( $d_{bkt}$ )	<b>0.61</b>	<b>0.52</b>	<b>0.78</b>	ft	Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	<b>34.3</b>	<b>28.2</b>	<b>37.1</b>
	Maximum Riffle Depth ( $d_{max}$ )	<b>1.35</b>	<b>1.26</b>	<b>1.50</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>2.213</b>	<b>2.066</b>	<b>2.459</b>
	Width of Flood-Prone Area ( $W_{fpa}$ )	<b>27.9</b>	<b>26.4</b>	<b>31.0</b>	ft	Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )	<b>1.3</b>	<b>1.3</b>	<b>1.4</b>
	Riffle Inner Berm Width ( $W_{ib}$ )	<b>7.9</b>			ft	Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )	<b>0.386</b>		
	Riffle Inner Berm Depth ( $d_{ib}$ )	<b>0.31</b>			ft	Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )	<b>0.508</b>		
	Riffle Inner Berm Area ( $A_{ib}$ )	<b>2.5</b>			ft <sup>2</sup>	Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )	<b>0.195</b>		
	Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )	<b>25.4</b>							
<b>Pool Dimensions* ** * ** *</b>	<b>Pool Dimensions* ** * ** *</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Pool Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	
	Pool Width ( $W_{bkfp}$ )	<b>21.4</b>			ft	Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )	<b>1.048</b>		
	Mean Pool Depth ( $d_{bkfp}$ )	<b>0.77</b>			ft	Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )	<b>1.262</b>		
	Pool Cross-Sectional Area ( $A_{bkfp}$ )	<b>16.4</b>			ft	Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )	<b>1.304</b>		
	Maximum Pool Depth ( $d_{maxp}$ )	<b>1.49</b>			ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	<b>2.443</b>		
	Pool Inner Berm Width ( $W_{ibp}$ )	<b>13.0</b>			ft	Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )	<b>0.608</b>		
	Pool Inner Berm Depth ( $d_{ibp}$ )	<b>0.30</b>			ft	Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )	<b>0.390</b>		
	Pool Inner Berm Area ( $A_{ibp}$ )	<b>4.0</b>			ft <sup>2</sup>	Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )	<b>0.240</b>		
	Point Bar Slope ( $S_{pb}$ )	<b>0.370</b>			ft/ft	Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )	<b>43.3</b>		
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Run Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	
	Run Width ( $W_{bkfr}$ )				ft	Run Width to Riffle Width ( $W_{bkfr} / W_{bkt}$ )			
	Mean Run Depth ( $d_{bkfr}$ )				ft	Mean Run Depth to Mean Riffle Depth ( $d_{bkfr} / d_{bkt}$ )			
	Run Cross-Sectional Area ( $A_{bkfr}$ )				ft	Run Area to Riffle Area ( $A_{bkfr} / A_{bkt}$ )			
	Maximum Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )			
Run Width/Depth Ratio ( $W_{bkfr} / d_{bkfr}$ )				ft					
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Glide Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	
	Glide Width ( $W_{bkfg}$ )				ft	Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )			
	Mean Glide Depth ( $d_{bkfg}$ )				ft	Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )			
	Glide Cross-Sectional Area ( $A_{bkfg}$ )				ft	Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )			
	Maximum Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )			
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )				ft/ft	Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )			
	Glide Inner Berm Width ( $W_{ibg}$ )				ft	Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )			
	Glide Inner Berm Depth ( $d_{ibg}$ )				ft	Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )			
Glide Inner Berm Area ( $A_{ibg}$ )				ft <sup>2</sup>	Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )				
<b>Step**</b>	<b>Step Dimensions**</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Step Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	
	Step Width ( $W_{bkfs}$ )				ft	Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )			
	Mean Step Depth ( $d_{bkfs}$ )				ft	Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )			
	Step Cross-Sectional Area ( $A_{bkfs}$ )				ft	Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )			
	Maximum Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )									

**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, F4b Fair-Poor Reach</b>	Location: <b>Pike National Forest, Colorado</b>
Observers: <b>K. Wright, L. Chavez et al.</b>	Date: <b>8/26/2010</b> Valley Type: <b>VIII</b> Stream Type: <b>F4b</b>

<b>Hydraulics</b>	<b>River Reach Summary Data.....2</b>				
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )	<b>2.77</b>	ft/sec	Estimation Method	<b>"n" by Stream Type</b>
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )	<b>29.4</b>	cfs	Drainage Area	<b>10.3</b> mi <sup>2</sup>

	Geometry			Dimensionless Geometry Ratios					
	Mean	Min	Max	Mean	Min	Max			
<b>Channel Pattern</b>	Linear Wavelength ( $\lambda$ )			ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )				
	Stream Meander Length ( $L_m$ )			ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )				
	Radius of Curvature ( $R_c$ )			ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )				
	Belt Width ( $W_{bit}$ )	<b>24.0</b>		ft	Meander Width Ratio ( $W_{bit} / W_{bkt}$ )	<b>1.18</b>			
	Arc Length ( $L_a$ )			ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )				
	Riffle Length ( $L_r$ )	<b>1.7</b>	<b>0.1</b>	<b>5.5</b>	ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )	<b>0.08</b>	<b>0.004</b>	<b>0.27</b>
	Individual Pool Length ( $L_p$ )	<b>2.1</b>	<b>0.7</b>	<b>4.3</b>	ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )	<b>0.10</b>	<b>0.03</b>	<b>0.21</b>
	Pool to Pool Spacing ( $P_s$ )	<b>3.9</b>	<b>0.4</b>	<b>11.9</b>	ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )	<b>0.19</b>	<b>0.02</b>	<b>0.58</b>

<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )	<b>0.0215</b>	ft/ft	Average Water Surface Slope (S)	<b>0.021</b>	ft/ft	Sinuosity ( $S_{val} / S$ )	<b>1.03</b>	
	Stream Length (SL)	<b>202.0</b>	ft	Valley Length (VL)	<b>197.0</b>	ft	Sinuosity (SL / VL)	<b>1.03</b>	
	Low Bank Height (LBH)	start: <b>1.45</b> ft end: <b>2.25</b> ft		Max Bankfull Depth ( $d_{max}$ )	start: <b>1.36</b> ft end: <b>1.20</b> ft		Bank-Height Ratio (BHR) (LBH / $d_{max}$ )	start: <b>1.1</b> end: <b>1.9</b>	
	<b>Facet Slopes</b>			<b>Dimensionless Facet Slope Ratios</b>					
	Riffle Slope ( $S_{rif}$ )	<b>0.0310</b>	<b>0.0040</b>	<b>0.0700</b>	ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.4762</b>	<b>0.1905</b>	<b>3.3333</b>
	Run Slope ( $S_{run}$ )	<b>0.0600</b>	<b>0.0190</b>	<b>0.2280</b>	ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )	<b>2.8571</b>	<b>0.9048</b>	<b>10.857</b>
	Pool Slope ( $S_p$ )	<b>0.0210</b>	<b>0.0000</b>	<b>0.0560</b>	ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )	<b>1.0000</b>	<b>0.0001</b>	<b>2.6667</b>
	Glide Slope ( $S_g$ )	<b>0.0250</b>	<b>0.0060</b>	<b>0.0730</b>	ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )	<b>1.1905</b>	<b>0.2857</b>	<b>3.4762</b>
	Step Slope ( $S_s$ )				ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )			
	<b>Max Depths<sup>a</sup></b>			<b>Dimensionless Depth Ratios</b>					
	Max Riffle Depth ( $d_{max}$ )	<b>1.35</b>	<b>1.26</b>	<b>1.50</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>2.213</b>	<b>2.066</b>	<b>2.459</b>
	Max Run Depth ( $d_{maxr}$ )	<b>1.22</b>	<b>1.00</b>	<b>1.41</b>	ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )	<b>2.000</b>	<b>1.639</b>	<b>2.311</b>
	Max Pool Depth ( $d_{maxp}$ )	<b>1.40</b>	<b>1.12</b>	<b>1.65</b>	ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	<b>2.295</b>	<b>1.836</b>	<b>2.705</b>
	Max Glide Depth ( $d_{maxg}$ )	<b>1.07</b>	<b>0.89</b>	<b>1.35</b>	ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )	<b>1.754</b>	<b>1.459</b>	<b>2.213</b>
	Max Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			

	Reach <sup>b</sup>			Riffle <sup>c</sup>			Bar			Protrusion Height <sup>d</sup>		
<b>Channel Materials</b>	% Silt/Clay	<b>0</b>	<b>0</b>	<b>0</b>	$D_{16}$	<b>4.4</b>	<b>7.2</b>	<b>0.0</b>				mm
	% Sand	<b>9</b>	<b>0</b>	<b>21</b>	$D_{35}$	<b>9.2</b>	<b>9.5</b>	<b>4.0</b>				mm
	% Gravel	<b>78</b>	<b>93</b>	<b>7</b>	$D_{50}$	<b>11.6</b>	<b>11.1</b>	<b>7.8</b>				mm
	% Cobble	<b>13</b>	<b>7</b>	<b>2</b>	$D_{84}$	<b>38.5</b>	<b>26.6</b>	<b>40.2</b>				mm
	% Boulder				$D_{95}$	<b>111.7</b>	<b>77.0</b>	<b>60.7</b>				mm
	% Bedrock				$D_{100}$	<b>256.0</b>	<b>256.0</b>	<b>70.0</b>				mm

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.  
<sup>b</sup> Composite sample of riffles and pools within the designated reach. <sup>c</sup> Active bed of a riffle. <sup>d</sup> Height of roughness feature above bed.

## Stability Indices


**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation									
Stream: <b>Trail Creek, F4b Fair-Poor Reach</b>		Location: <b>Pike National Forest, Colorado</b>							
Observers: <b>K. Wright, L. Chavez, D. Butler &amp; D. Bohon</b>		Reference reach <input type="checkbox"/>	Disturbed (impacted reach) <input checked="" type="checkbox"/>	Date: <b>8/26/2010</b>					
Existing species composition: <b>Willow, Aspen, Grass/Forb</b>		Potential species composition: <b>Mature Willow, Aspen, Grass/Forb</b>							
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition				
<b>1. Overstory</b>	Canopy layer	15%	5%	Aspen	9%				
				Salix Spp.	90%				
				Water birch	1%				
				100%					
<b>2. Understory</b>	Shrub layer		49%	Willow	100%				
				100%					
				<b>3. Ground level</b>	Herbaceous		40%	Grass (Poa, Agrostis, wheat forbs-Veronica, yarrow, Epilobium)	60%
								Weeds (thistle, smartweed)	36%
<b>3. Ground level</b>	Leaf or needle litter		3%	Remarks: Condition, vigor and/or usage of existing reach:					
				<b>3. Ground level</b>	Bare ground		3%	100%	
								100%	
*Based on crown closure. **Based on basal area to surface area.			<b>Column total = 100%</b>						

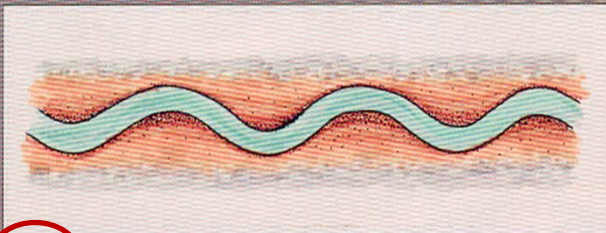



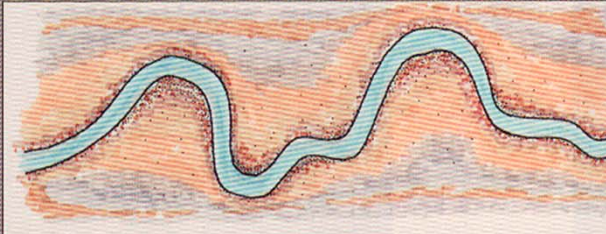
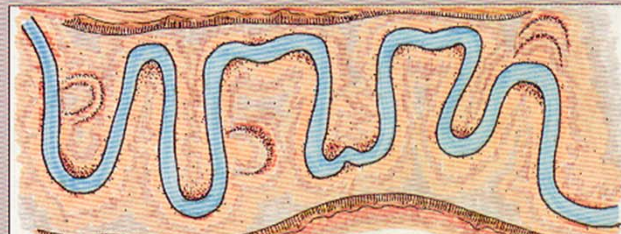
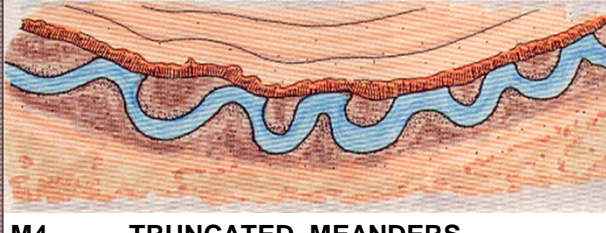
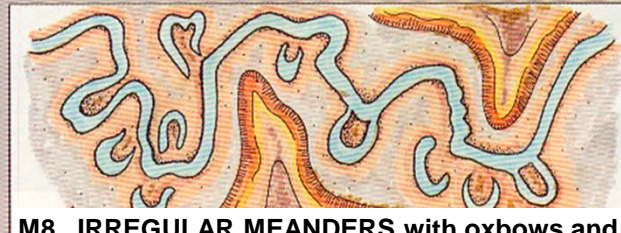
**Worksheet 5-7.** Flow regime.

FLOW REGIME								
Stream: <b>Trail Creek, F4b Fair-Poor</b>			Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>K. Wright, L. Chavez, D. Butler &amp; D. Bohon</b>						Date: <b>8/26/2010</b>		
List ALL COMBINATIONS that APPLY.....☞			P1	P2	P8			
General Category								
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation							
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
<b>P</b>	Perennial stream channels: Surface water persists yearlong.							
Specific Category								
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
<b>4</b>	Streamflow regulated by glacial melt.							
<b>5</b>	Ice flows/ice torrents from ice dam breaches.							
<b>6</b>	Alternating flow/backwater due to tidal influence.							
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.							
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
<b>9</b>	Rain-on-snow generated runoff.							

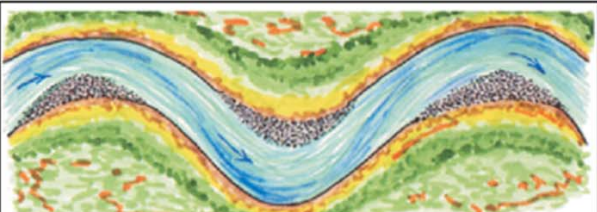
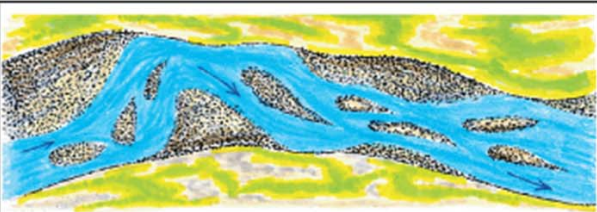

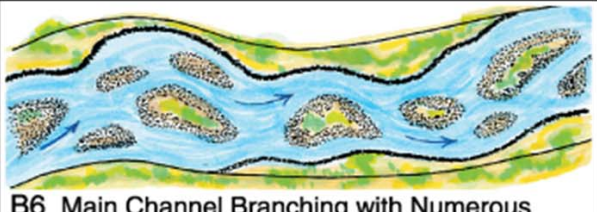




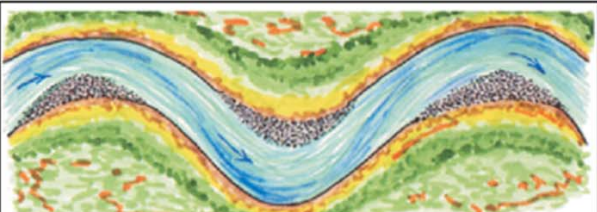
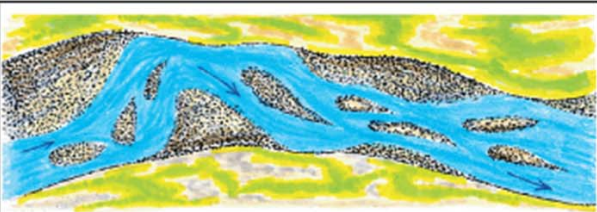

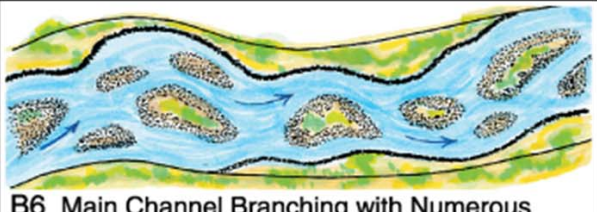




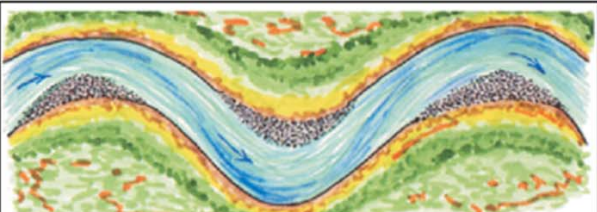
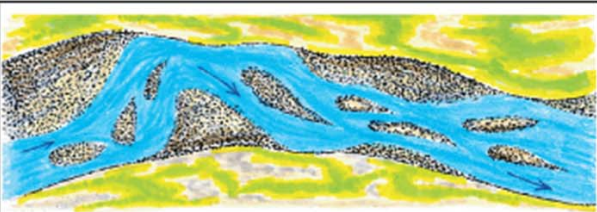

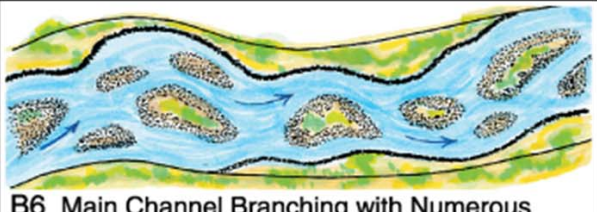




**Worksheet 5-8.** Stream order & stream size.

<b>Stream Size and Order</b>			
Stream:	<b>Trail Creek, F4b Fair-Poor Reach</b>		
Location:	<b>Pike National Forest, Colorado</b>		
Observers:	<b>K. Wright, L. Chavez <i>et al.</i></b>		
Date:	<b>8/26/2010</b>		
<b>Stream Size Category and Order</b> 			<b>S-4(4)</b>
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0.305	<1	<input type="checkbox"/>
S-2	0.3 – 1.5	1 – 5	<input type="checkbox"/>
S-3	1.5 – 4.6	5 – 15	<input type="checkbox"/>
<b>S-4</b>	<b>4.6 – 9</b>	<b>15 – 30</b>	<input checked="" type="checkbox"/>
S-5	9 – 15	30 – 50	<input type="checkbox"/>
S-6	15 – 22.8	50 – 75	<input type="checkbox"/>
S-7	22.8 – 30.5	75 – 100	<input type="checkbox"/>
S-8	30.5 – 46	100 – 150	<input type="checkbox"/>
S-9	46 – 76	150 – 250	<input type="checkbox"/>
S-10	76 – 107	250 – 350	<input type="checkbox"/>
S-11	107 – 150	350 – 500	<input type="checkbox"/>
S-12	150 – 305	500 – 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
<b>Stream Order</b>			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			

Worksheet 5-9. Meander patterns.

<b>Meander Patterns</b>					
Stream: <b>Trail Creek, F4b Fair-Poor Reach</b>			Location: <b>Pike National Forest, CO</b>		
Observers: <b>K. Wright, L. Chavez et al.</b>			Date: <b>8/26/2010</b>		
List ALL CATEGORIES that APPLY		<b>M1</b>			
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>					
					
<b>M1</b> <b>REGULAR MEANDERS</b>	<b>M5</b> <b>UNCONFINED MEANDER SCROLLS</b>				
					
<b>M2</b> <b>TORTUOUS MEANDERS</b>	<b>M6</b> <b>CONFINED MEANDER SCROLLS</b>				
					
<b>M3</b> <b>IRREGULAR MEANDERS</b>	<b>M7</b> <b>DISTORTED MEANDER LOOPS</b>				
					
<b>M4</b> <b>TRUNCATED MEANDERS</b>	<b>M8</b> <b>IRREGULAR MEANDERS with oxbows and</b>				

**Worksheet 5-10.** Depositional patterns.

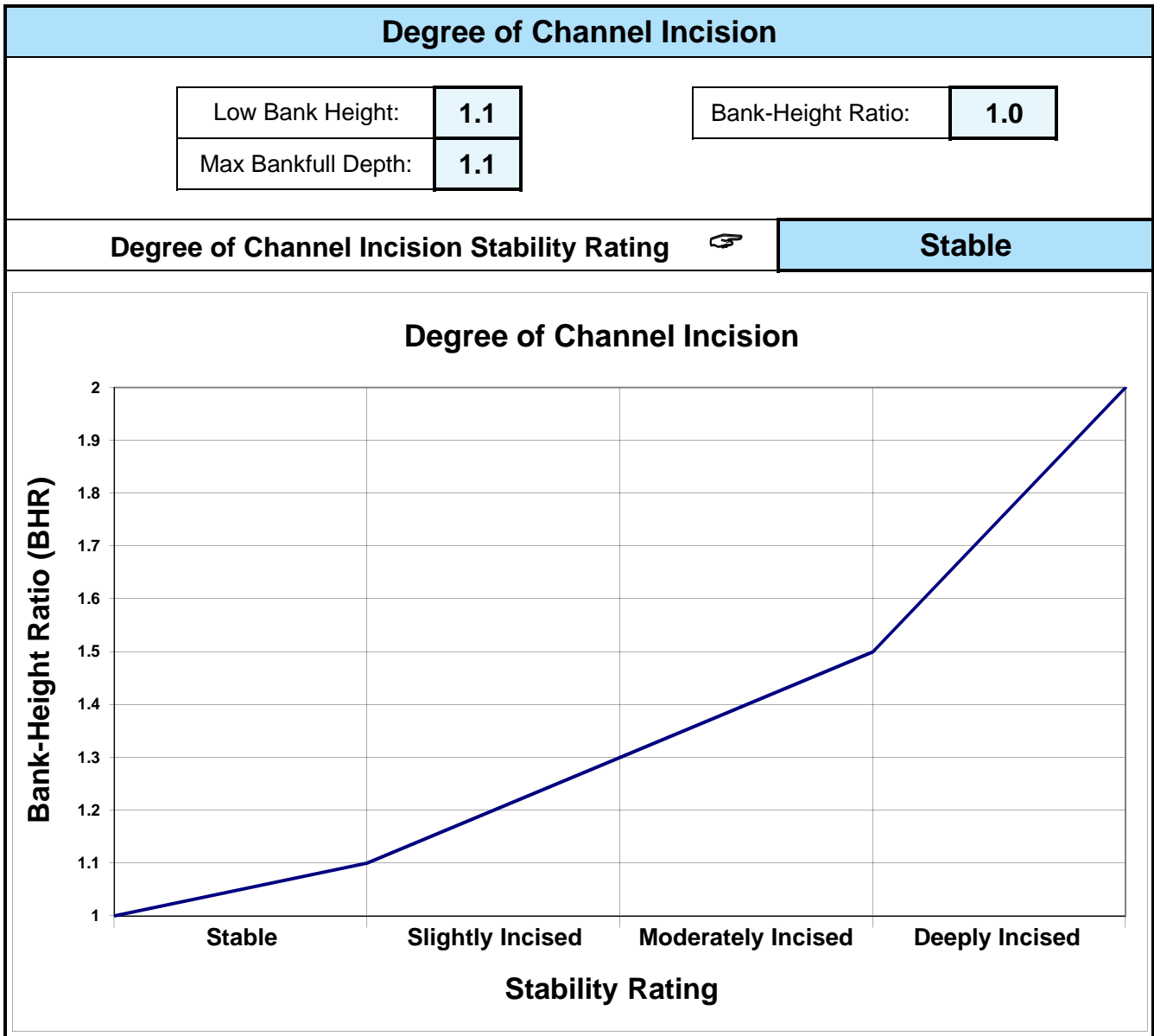
<b>Depositional Patterns</b>													
Stream: <b>Trail Creek, F4b Fair-Poor Reach</b>			Location: <b>Pike National Forest, Colorado</b>										
Observers: <b>K. Wright, L. Chavez et al.</b>			Date: <b>8/26/2010</b>										
List ALL CATEGORIES that APPLY	<b>B3</b>	<b>B4</b>											
<i>Various Depositional Features modified from Galay et al. (1973)</i>													
<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 50%; padding: 5px; vertical-align: top;">  <p><b>B1</b> POINT BARS</p> </td> <td style="width: 50%; padding: 5px; vertical-align: top;">  <p><b>B5</b> DIAGONAL BARS</p> </td> </tr> <tr> <td style="padding: 5px; vertical-align: top;">  <p><b>B2</b> POINT BARS with Few MID-CHANNEL BARS</p> </td> <td style="padding: 5px; vertical-align: top;">  <p><b>B6</b> Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</p> </td> </tr> <tr> <td style="padding: 5px; vertical-align: top;">  <p><b>B3</b> NUMEROUS MID-CHANNEL BARS</p> </td> <td style="padding: 5px; vertical-align: top;">  <p><b>B7</b> SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</p> </td> </tr> <tr> <td style="padding: 5px; vertical-align: top;">  <p><b>B4</b> SIDE BARS</p> </td> <td style="padding: 5px; vertical-align: top;">  <p><b>B8</b> DELTA BARS</p> </td> </tr> </table>						 <p><b>B1</b> POINT BARS</p>	 <p><b>B5</b> DIAGONAL BARS</p>	 <p><b>B2</b> POINT BARS with Few MID-CHANNEL BARS</p>	 <p><b>B6</b> Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</p>	 <p><b>B3</b> NUMEROUS MID-CHANNEL BARS</p>	 <p><b>B7</b> SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</p>	 <p><b>B4</b> SIDE BARS</p>	 <p><b>B8</b> DELTA BARS</p>
 <p><b>B1</b> POINT BARS</p>	 <p><b>B5</b> DIAGONAL BARS</p>												
 <p><b>B2</b> POINT BARS with Few MID-CHANNEL BARS</p>	 <p><b>B6</b> Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</p>												
 <p><b>B3</b> NUMEROUS MID-CHANNEL BARS</p>	 <p><b>B7</b> SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</p>												
 <p><b>B4</b> SIDE BARS</p>	 <p><b>B8</b> DELTA BARS</p>												



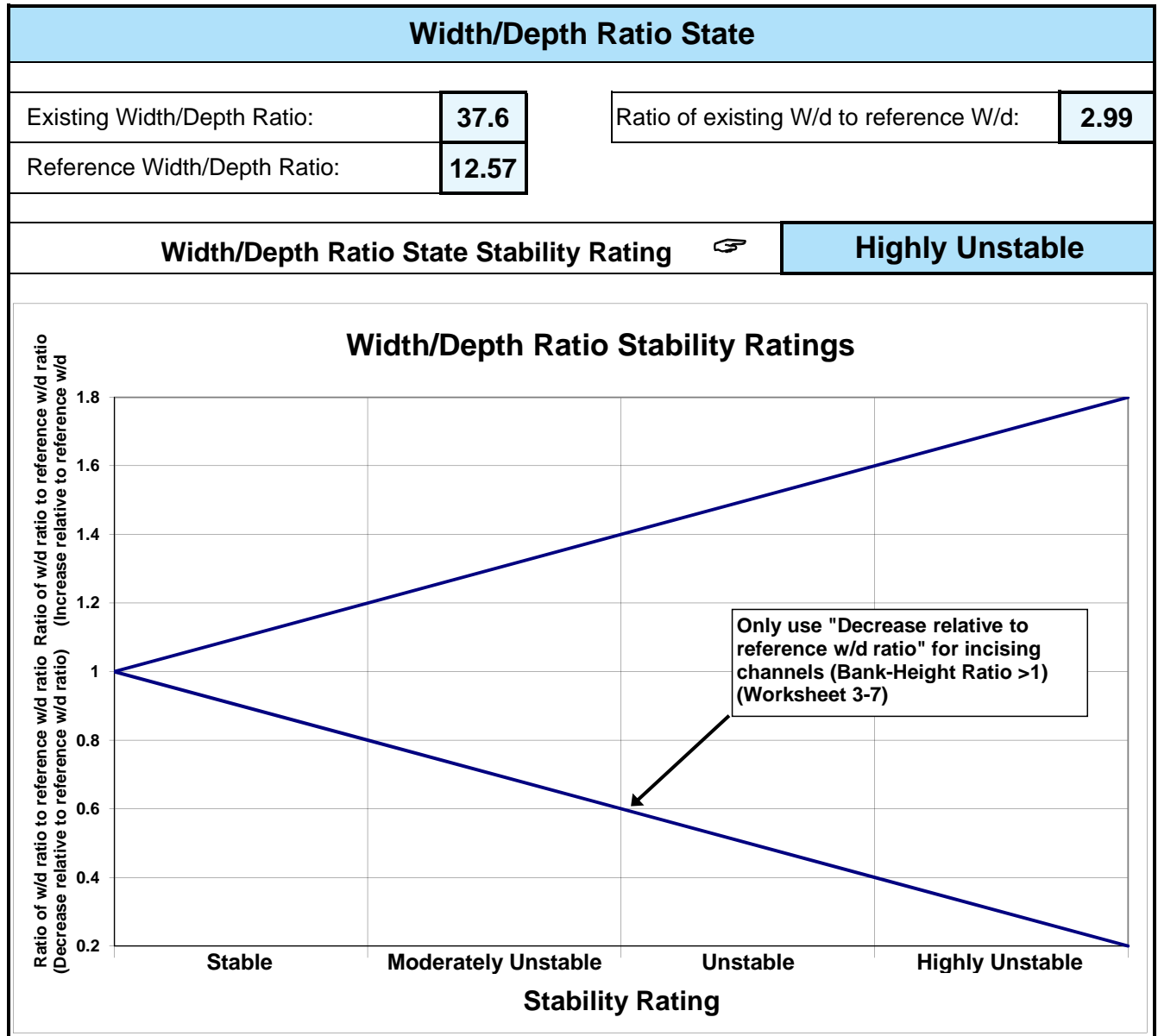
## Worksheet 5-11. Channel blockages.

Channel Blockages		
Stream: <b>Trail Creek, F4b Fair-Poor Reach</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>K. Wright, L. Chavez <i>et al.</i></b>		Date: <b>8/26/2010</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input checked="" type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input type="checkbox"/>
<b>D4</b> Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

**Worksheet 5-12.** Degree of channel incision.



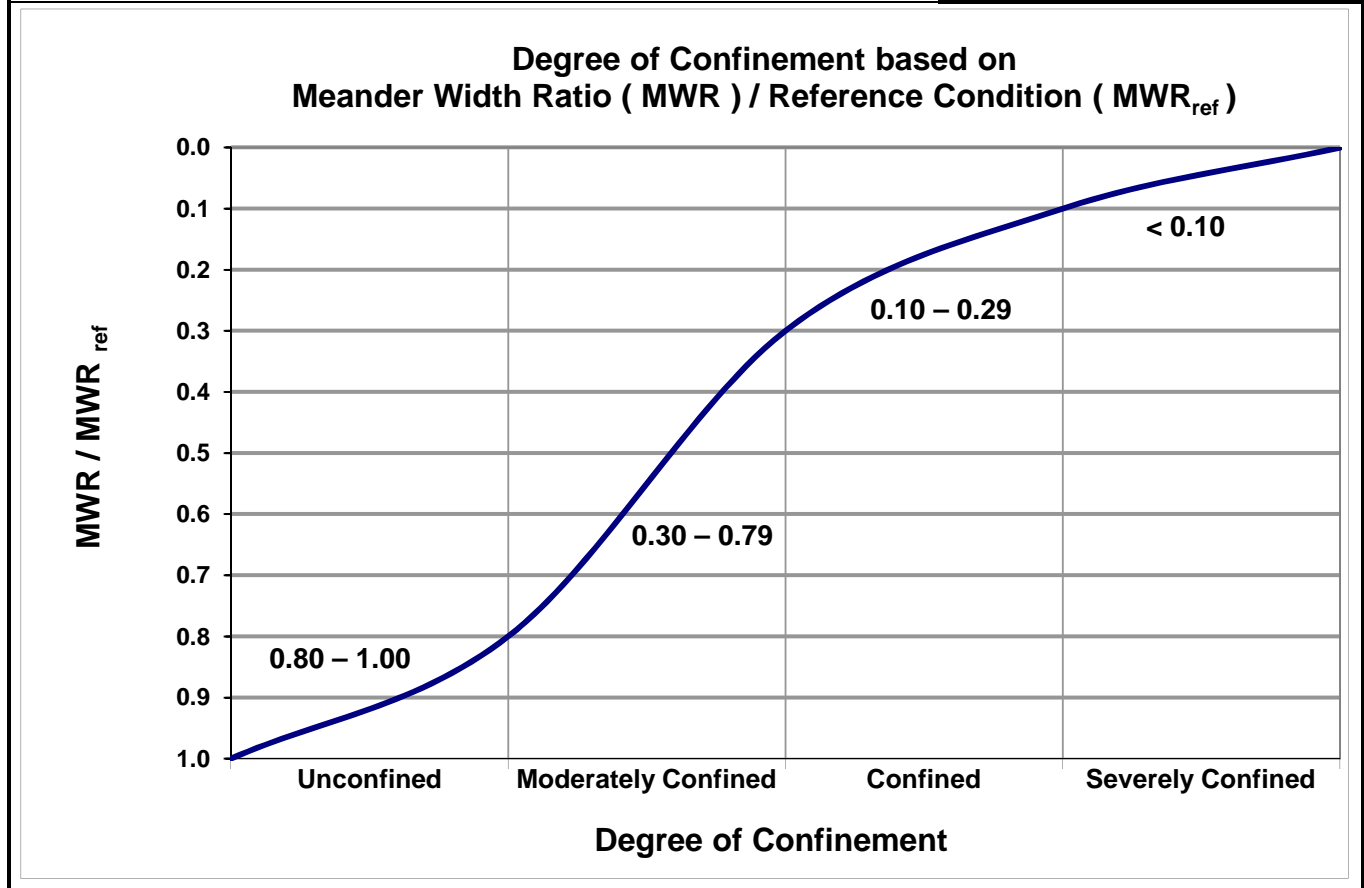
**Worksheet 5-13.** Width/depth ratio state.



**Worksheet 5-14.** Degree of channel confinement (lateral containment).

Degree of Confinement			
Existing Meander Width Ratio (MWR):	<b>1.18</b>	Ratio of MWR to $MWR_{ref}$ :	<b>0.44</b>
Reference Meander Width Ratio ( $MWR_{ref}$ ):	<b>2.7</b>		

<b>Degree of Confinement Stability Rating</b>	<b>Mod. Confined</b>
---	----------------------



**Worksheet 5-15. Pfrankuch channel stability rating.**

Stream: Trail Creek, F4b Fair-Poor Reach		Location: Pike National Forest, CO		Valley Type: VIII		Observers: K. Wright, L. Chavez et al.		Date: 8/26/2010																	
Local- tion	Key Category	Excellent Description	Rating	Good Description	Rating	Fair Description	Rating	Poor Description	Rating																
Upper banks	1	Landform slope	2	Bank slope gradient <30%.	4	Bank slope gradient 40-60%.	6	Bank slope gradient > 60%.	8																
	2	Mass erosion	3	No evidence of past or future mass erosion.	6	Frequent or large, causing sediment nearly yearlong.	8	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.	12																
	3	Debris jam potential	2	Essentially absent from immediate channel area.	4	Moderate to heavy amounts, mostly larger sizes.	6	Moderate to heavy amounts, predominantly larger sizes.	8																
	4	Vegetative bank protection	3	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	7	50-70% density. Lower vigor and fewer species from a shallow, discontinuous root mass.	9	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.	12																
Lower banks	5	Channel capacity	1	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0.	2	Bankfull stage is not contained. Width/depth ratio departure from reference width/depth ratio = 1.2-1.4. Bank-Height Ratio (BHR) = 1.1-1.3.	3	Bankfull stage is not contained. over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.	4																
	6	Bank rock content	2	> 65% with large angular boulders. 12"+ common.	4	20-40%. Mostly boulders and small cobbles 6-12".	6	<20% rock fragments of gravel sizes, 1-3" or less.	8																
	7	Obstructions to flow	2	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	4	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	6	Frequent obstructions and deflectors cause bank erosion yearlong. Sediment traps full, channel migration occurring.	8																
	8	Cutting	4	Little or none. Infrequent raw banks <6".	6	Significant. Cuts 12-24" high. Root mat overhangs and sloughing evident.	9	Almost continuous cuts, some over 24" high. Failure of overhangs frequent.	16																
Bottom	9	Deposition	4	Little or no enlargement of channel or point bars.	8	Moderate deposition of new gravel and coarse sand on old and some new bars.	12	Extensive deposit of predominantly fine particles. Accelerated bar development.	16																
	10	Rock angularity	1	Sharp edges and corners. Plane surfaces rough.	2	Rounded corners and edges. Surfaces smooth and flat.	3	Well rounded in all dimensions, surfaces smooth.	4																
	11	Brightness	1	Surfaces dull, dark or stained. Generally not bright.	2	Mostly dull, but may have <35% bright surfaces.	3	Predominantly bright, > 65%, exposed or scoured surfaces.	4																
	12	Consolidation of particles	2	Assorted sizes tightly packed or overlapping.	4	Moderately packed with some overlapping.	6	No packing evident. Loose assortment, easily moved.	8																
	13	Bottom size distribution	4	No size change evident. Stable material 80-100%.	8	Distribution shift light. Stable material 50-80%.	14	Marked distribution change. Stable materials 0-20%.	16																
	14	Scouring and deposition	6	<5% of bottom affected by scour or deposition.	12	5-30% affected. Scour at constrictions and where grades steepen. Some deposition in pools.	18	More than 50% of the bottom in a state of flux or change nearly yearlong.	24																
	15	Aquatic vegetation	1	Abundant growth moss-like, dark green perennial. In swift water too.	2	Common. Algae forms in low velocity and pool areas. Moss here too.	3	Perennial types scarce or absent. Yellow-green, short-term bloom may be present.	4																
		<b>Excellent total = 4</b>		<b>Good total = 19</b>		<b>Fair total = 56</b>		<b>Poor total = 24</b>																	
<b>Stream type</b>	<b>A1</b>	<b>A2</b>	<b>A3</b>	<b>A4</b>	<b>A5</b>	<b>A6</b>	<b>B1</b>	<b>B2</b>	<b>B3</b>	<b>B4</b>	<b>B5</b>	<b>B6</b>	<b>C1</b>	<b>C2</b>	<b>C3</b>	<b>C4</b>	<b>C5</b>	<b>C6</b>	<b>D3</b>	<b>D4</b>	<b>D5</b>	<b>D6</b>	<b>Grand total = 103</b>		
Good (Stable)	38-43	38-43	54-90	60-95	60-95	50-80	38-45	38-45	40-60	48-68	40-60	38-50	38-50	38-50	60-85	70-90	60-85	60-85	85-107	85-107	85-107	85-107	85-107	67-98	
Fair (Mod. unstable)	44-47	44-47	91-129	96-132	96-142	81-110	46-58	46-58	61-78	69-88	61-78	51-61	51-61	51-61	86-105	91-110	86-105	86-105	108-132	108-132	108-132	108-132	108-132	99-125	
Poor (Unstable)	48+	48+	130+	133+	143+	111+	59+	59+	79+	85+	79+	62+	62+	62+	106+	111+	106+	106+	133+	133+	133+	133+	133+	126+	
<b>Stream type</b>	<b>DA3</b>	<b>DA4</b>	<b>DA5</b>	<b>DA6</b>	<b>E3</b>	<b>E4</b>	<b>E5</b>	<b>E6</b>	<b>F1</b>	<b>F2</b>	<b>F3</b>	<b>F4</b>	<b>F5</b>	<b>F6</b>	<b>G1</b>	<b>G2</b>	<b>G3</b>	<b>G4</b>	<b>G5</b>	<b>G6</b>				<b>*Potential stream type = B4</b>	
Good (Stable)	40-63	40-63	40-63	40-63	50-75	50-75	50-75	40-63	60-85	85-110	85-110	90-115	90-115	80-95	40-60	40-60	85-107	85-107	90-112	90-112	85-107				<b>Modified channel stability rating = B4</b>
Fair (Mod. unstable)	64-86	64-86	64-86	64-86	76-96	76-96	76-96	64-86	86-105	86-105	111-125	111-125	116-130	96-110	61-78	61-78	108-120	108-120	113-125	113-125	108-120				<b>Grand total = 103</b>
Poor (Unstable)	87+	87+	87+	87+	97+	97+	97+	87+	106+	106+	126+	126+	131+	111+	79+	79+	121+	121+	126+	126+	126+				<b>Existing stream type = F4</b>

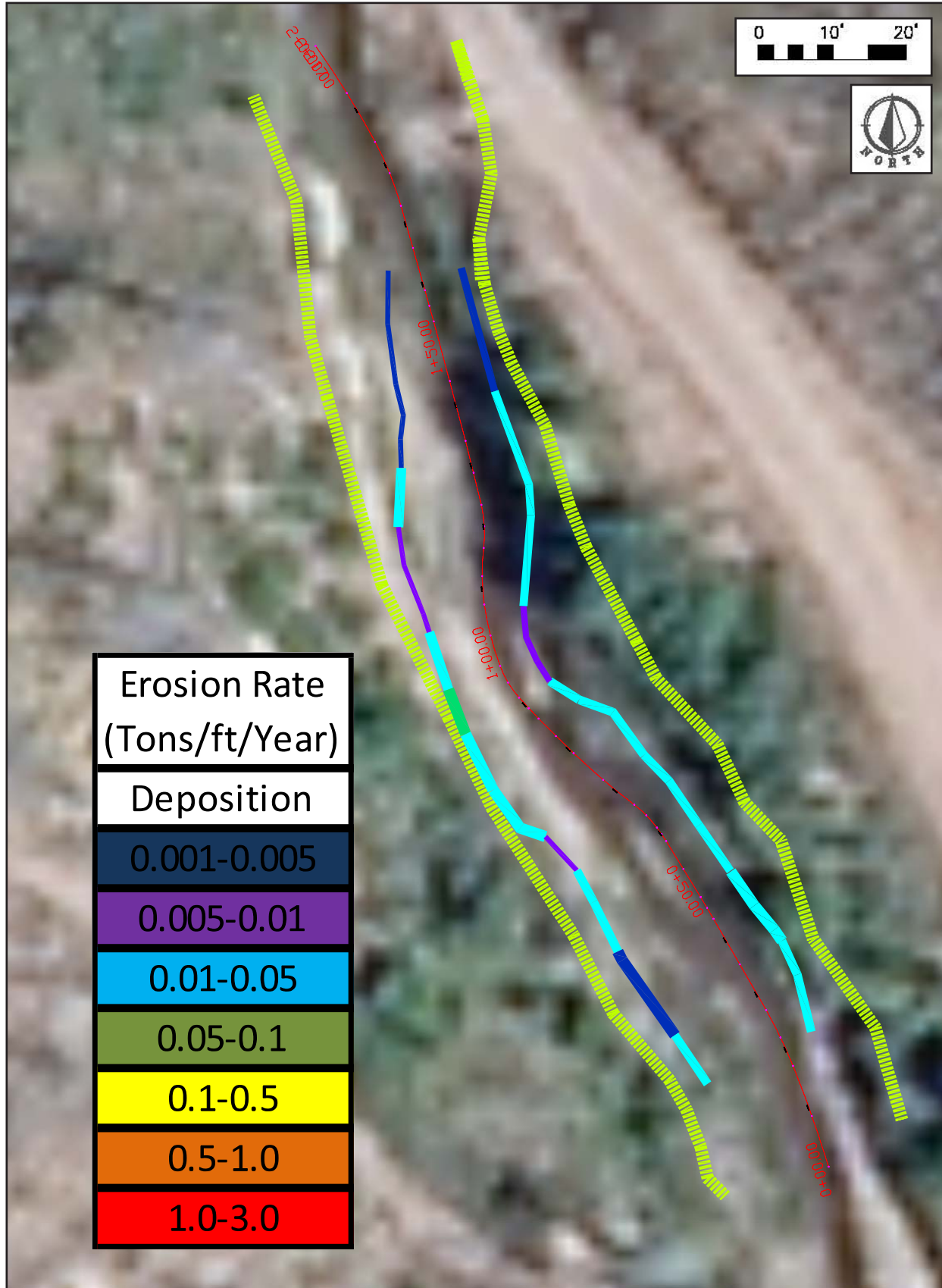
\*Rating is adjusted to potential stream type, not existing.

## BANCS Model – Streambank Erosion

**Worksheet 5-18.** Annual streambank erosion estimates.

Stream: <b>Trail Creek, F4b Fair-Poor Reach</b>				Location: <b>Pike National Forest, Colorado</b>			
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>221</b>		Date: <b>8/26/2010</b>			
Observers: <b>K. Wright, L. Chavez et al.</b>		Valley Type: <b>VIII</b>		Stream Type: <b>F4b</b>			
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 5-16) (adjective)	NBS rating (Worksheet 5-17) (adjective)	Bank erosion rate (Figure 5-34 or 5- 35) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [[4]x(5)x(6)] (ft <sup>3</sup> /yr)	Erosion Rate (tons/yr/ft) {[(7)/27] × 1.3 / (5)}
1. 1-13 RB	Moderate	Moderate	0.25348	13.0	1.4	4.48	0.01660
2. 85-100 LB	Very High	Moderate	0.37957	15.0	1.8	10.25	0.03290
3. 172-182 RB	Moderate	Low	0.15287	10.0	4.5	6.88	0.03312
4. 1-10 LB	Moderate	Low	0.15287	10.0	1.4	2.08	0.01001
5. 13-29 RB	Moderate	Low	0.15287	16.0	1.8	4.28	0.01288
6. 10-35 LB	Low	Moderate	0.07435	25.0	1.4	2.53	0.00487
7. 35-48 LB	Low	Low	0.03566	13.0	1.4	0.63	0.00233
8. 29-62 RB	Moderate	Moderate	0.25348	33.0	1.4	11.38	0.01660
9. 48-85 LB	Moderate	Moderate	0.25348	37.0	0.8	7.50	0.00976
10. 62-86 RB	Low	High	0.15505	24.0	1.0	3.72	0.00747
11. 86-101 RB	Moderate	High	0.42031	15.0	1.0	6.30	0.02024
12. 100-114 LB	High	Moderate	0.37957	15.0	1.8	10.25	0.03290
13. 101-137 RB	Low	Low	0.03566	36.0	0.8	1.03	0.00137
14. 114-121 LB	High	Very High	0.87205	7.0	1.8	10.99	0.07558
15. 121-134 LB	Very High	High	0.57533	13.0	1.6	11.97	0.04432
16. 137-172 RB	Low	Moderate	0.07435	35.0	1.3	3.38	0.00465
17. 134-154 LB	Moderate	Low	0.15287	20.0	0.8	2.45	0.00589
18. 154-172 LB	Moderate	Moderate	0.25348	18.0	1.6	7.30	0.01953
19. 172-215 LB	Low	Low	0.03566	43.0	0.8	1.23	0.00137
20. 182-221 RB	Low	Low	0.03566	39.0	1.2	1.67	0.00206
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					Total Erosion (ft <sup>3</sup> /yr)	<b>110.29</b>	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					Total Erosion (yds <sup>3</sup> /yr)	<b>4.08</b>	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					Total Erosion (tons/yr)	<b>5.31</b>	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					Total Erosion (tons/yr/ft)	<b>0.0240</b>	

Streambank Erosion Map



## FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Equation Type		Equation Source				Equation				Bankfull Discharge (cfs)		Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)	
1. Bedload Sediment		"Good/Fair" Pagosa				$y = -0.0113 + 1.0139x^{2.1929}$				29.4		0.0163		22.55	
2. Suspended Sediment		"Good/Fair" Pagosa				$y = 0.0636 + 0.9326x^{2.4085}$									
From Dimensional Flow-Duration Curve															
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	Calculate		Calculate Sediment Yield		
Percentage of Time	Daily Mean Discharge (cfs)	Mid-Ordinate (%)	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimension-less Streamflow	Dimension-less Suspended Sediment Discharge	Suspended Sediment Discharge (tons/day)	Dimension-less Bedload Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow [(5)×(6)]	Suspended Sediment [(5)×(9)]	Bedload Sediment [(5)×(11)]	Suspended Sediment + Bedload Sediment [(13)+(14)]	
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>med</sub> )	(S/S <sub>med</sub> )	(tons/day)	(b <sub>y</sub> /b <sub>med</sub> )	(tons/day)	(cfs)	(tons)	(tons)	(tons)	(tons)
0%	74.8														
0.10%	64.2	0.05%	0.09%	0.34	69.5	2.363	7.461	31.56	6.670	10.33	23.8	10.83	3.55	14.38	
0.25%	55.5	0.08%	0.15%	0.55	59.9	2.036	5.232	19.07	4.809	7.45	32.8	10.44	4.08	14.52	
0.50%	48.0	0.13%	0.25%	0.91	51.8	1.761	3.706	11.68	3.494	5.41	47.2	10.66	4.94	15.60	
0.75%	41.0	0.13%	0.25%	0.91	44.5	1.513	2.592	7.02	2.502	3.88	40.6	6.41	3.54	9.94	
1%	35.4	0.13%	0.25%	0.91	38.2	1.300	1.817	4.23	1.790	2.77	34.9	3.86	2.53	6.39	
1.5%	30.4	0.25%	0.50%	1.83	32.9	1.120	1.289	2.59	1.289	2.00	60.1	4.72	3.64	8.36	
2%	25.4	0.25%	0.50%	1.83	27.9	0.949	0.886	1.50	0.893	1.38	50.9	2.75	2.52	5.27	
3%	21.4	0.50%	1.00%	3.65	23.4	0.795	0.600	0.85	0.602	0.93	85.3	3.12	3.40	6.52	
4%	18.3	0.50%	1.00%	3.65	19.8	0.674	0.424	0.51	0.415	0.64	72.3	1.87	2.35	4.22	
5%	16.3	0.50%	1.00%	3.65	17.3	0.587	0.322	0.34	0.304	0.47	63.0	1.24	1.72	2.95	
10%	10.2	2.50%	5.00%	18.25	13.2	0.450	0.200	0.16	0.165	0.26	241.5	2.94	4.66	7.60	
20%	5.6	5.00%	10.00%	36.50	7.9	0.269	0.103	0.05	0.045	0.07	288.1	1.81	2.57	4.37	
30%	3.7	5.00%	10.00%	36.50	4.6	0.158	0.075	0.02	0.006	0.01	169.5	0.77	0.36	1.13	
40%	2.6	5.00%	10.00%	36.50	3.2	0.108	0.068	0.01	0.000	0.00	115.8	0.48	0.00	0.48	
50%	2.0	5.00%	10.00%	36.50	2.3	0.079	0.066	0.01	0.000	0.00	84.7	0.34	0.00	0.34	
60%	1.5	5.00%	10.00%	36.50	1.8	0.061	0.065	0.01	0.000	0.00	65.0	0.26	0.00	0.26	
70%	1.2	5.00%	10.00%	36.50	1.4	0.047	0.064	0.01	0.000	0.00	50.8	0.20	0.00	0.20	
80%	1.1	5.00%	10.00%	36.50	1.2	0.039	0.064	0.00	0.000	0.00	42.4	0.17	0.00	0.17	
90%	0.8	5.00%	10.00%	36.50	0.9	0.032	0.064	0.00	0.000	0.00	33.9	0.13	0.00	0.13	
100%	0.2	5.00%	10.00%	36.50	0.5	0.016	0.064	0.00	0.000	0.00	16.9	0.07	0.00	0.07	
<b>Annual Totals:</b>										1,619.7	63.0	39.9	102.9		
										(cfs)	(tons/yr)	(tons/yr)	(tons/yr)	(tons/yr)	
										3,212.7					
										(acre-ft)					



**Worksheet 19b.** Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Equation Type		Equation Source				Equation		Bankfull Discharge (cfs)			Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)				
		"Good/Fair" Pagosa				$y = -0.0113 + 1.0139x^{2.1929}$		29.4			0.0310		44.00				
		"Good/Fair" Pagosa				$y = 0.06336 + 0.9326x^{2.4085}$											
		From Dimensional Flow-Duration Curve						From Sediment Rating Curves						Calculate		Calculate Sediment Yield	
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)			
Percentage of Time	Daily Mean Discharge	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Sediment Discharge	Suspended Sediment Discharge	Dimensionless Bedload Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow	Suspended Sediment	Bedload Sediment	Suspended Sediment + Bedload Sediment			
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>bed</sub> )	(S/S <sub>bed</sub> )	(tons/day)	(b <sub>p</sub> /b <sub>bed</sub> )	(tons/day)	(cfs)	(tons)	(tons)	[(13)×(14)]			
0%	97.4																
0.10%	86.8	0.05%	0.09%	0.34	92.1	3.132	14.647	160.23	12.384	36.58	31.6	54.97	12.55	67.52			
0.25%	78.2	0.08%	0.15%	0.55	82.5	2.805	11.247	110.19	9.723	28.71	45.2	60.33	15.72	76.05			
0.50%	70.6	0.13%	0.25%	0.91	74.4	2.530	8.784	77.61	7.750	22.89	67.9	70.82	20.89	91.71			
0.75%	63.6	0.13%	0.25%	0.91	67.1	2.282	6.867	54.74	6.180	18.25	61.2	49.95	16.66	66.60			
1%	58.1	0.13%	0.25%	0.91	60.8	2.069	5.436	39.28	4.982	14.71	55.5	35.84	13.43	49.27			
1.5%	52.7	0.25%	0.50%	1.83	55.4	1.884	4.351	28.63	4.055	11.97	101.1	52.24	21.85	74.10			
2%	47.4	0.25%	0.50%	1.83	50.0	1.702	3.420	20.33	3.243	9.58	91.3	37.10	17.48	54.58			
3%	43.3	0.50%	1.00%	3.65	45.3	1.542	2.712	14.61	2.611	7.71	165.5	53.33	28.15	81.48			
4%	38.5	0.50%	1.00%	3.65	40.9	1.391	2.128	10.34	2.079	6.14	149.3	37.74	22.41	60.15			
5%	34.0	0.50%	1.00%	3.65	36.2	1.232	1.606	6.91	1.592	4.70	132.2	25.23	17.16	42.39			
10%	21.2	2.50%	5.00%	18.25	27.6	0.939	0.865	2.84	0.872	2.58	503.8	51.78	47.00	98.78			
20%	7.5	5.00%	10.00%	36.50	14.3	0.488	0.229	0.39	0.199	0.59	523.6	14.26	21.44	35.70			
30%	3.8	5.00%	10.00%	36.50	5.7	0.193	0.081	0.05	0.016	0.05	206.8	2.00	1.74	3.73			
40%	2.6	5.00%	10.00%	36.50	3.2	0.110	0.068	0.03	0.000	0.00	118.2	0.96	0.00	0.96			
50%	2.0	5.00%	10.00%	36.50	2.3	0.079	0.066	0.02	0.000	0.00	84.7	0.66	0.00	0.66			
60%	1.5	5.00%	10.00%	36.50	1.8	0.061	0.065	0.01	0.000	0.00	65.0	0.50	0.00	0.50			
70%	1.2	5.00%	10.00%	36.50	1.4	0.047	0.064	0.01	0.000	0.00	50.8	0.39	0.00	0.39			
80%	1.1	5.00%	10.00%	36.50	1.2	0.039	0.064	0.01	0.000	0.00	42.4	0.32	0.00	0.32			
90%	0.8	5.00%	10.00%	36.50	0.9	0.032	0.064	0.01	0.000	0.00	33.9	0.26	0.00	0.26			
100%	0.2	5.00%	10.00%	36.50	0.5	0.016	0.064	0.00	0.000	0.00	16.9	0.13	0.00	0.13			
<b>Annual Totals:</b>											2,547.0 (cfs)		548.8 (tons/yr)		805.3 (tons/yr)		
											5,051.9 (acre-ft)						

# POWERSED Model – Sediment Transport Capacity

**Worksheet 20a.** Sediment transport prediction representing the upstream supply up to bankfull for bedload and suspended sand sediment.

Stream: Trail Creek, Upstream Existing Sediment Supply		Location: Pike National Forest, Colorado (Used GOOD-FAIR Curves)		Date: 08/14/10													
Observers: S=0.21, Q=29.4, 23.4, Bed.=0682, S.Sand=22		Stream Type: F4b		Gage Station #: Used Post-Fire Dimensionless F-D C.													
Valley Type: VIII		Stream Type: F4b		Gage Station #: Used Post-Fire Dimensionless F-D C.													
Calculate			Measure														
Flow-duration curve			Hydraulic geometry														
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
Percentage of time	Daily mean discharge	Mid-ordinate stream-flow	Area	Width	Depth	Velocity	Slope	Shear stress	Stream power	Unit power	Time increment	Time increment	Daily mean bedload transport	Daily mean suspended sand transport	Time adjusted bedload transport	Time adjusted suspended sand transport	Time adjusted total transport
(%)	(cfs)	(cfs)	(ft <sup>2</sup> )	(ft)	(ft)	(ft/s)	(ft/ft)	(lb/ft <sup>2</sup> )	(lb/s)	(lb/ftvs)	(%)	(days)	(tons/day)	(tons/day)	(tons)	(tons)	(tons)
100.00%	0.15										0%				0.00	0.00	0.00
90.00%	0.77	0.46	0.64	5.68	0.11	0.67	0.0210	0.15	0.60	0.11	10%	36.50	0.00	0.00	0.00	0.00	0.00
80.00%	1.08	0.93	1.03	6.44	0.16	0.86	0.0210	0.21	1.22	0.19	10%	36.50	0.00	0.00	0.00	0.00	0.00
70.00%	1.24	1.16	1.20	6.68	0.18	0.93	0.0210	0.23	1.52	0.23	10%	36.50	0.00	0.00	0.00	0.00	0.00
60.00%	1.55	1.40	1.37	6.92	0.20	1.01	0.0210	0.26	1.83	0.26	10%	36.50	0.00	0.01	0.00	0.00	0.36
50.00%	2.01	1.78	1.60	7.17	0.22	1.09	0.0210	0.29	2.33	0.32	10%	36.50	0.00	0.01	0.00	0.00	0.36
40.00%	2.63	2.32	1.91	7.48	0.26	1.19	0.0210	0.33	3.04	0.41	10%	36.50	0.00	0.01	0.00	0.00	0.36
30.00%	3.84	3.24	2.39	7.88	0.30	1.34	0.0210	0.39	4.25	0.54	10%	36.50	0.00	0.01	0.00	0.00	0.36
20.00%	7.49	5.67	3.47	8.55	0.41	1.62	0.0210	0.52	7.43	0.87	10%	36.50	0.04	0.03	1.46	1.09	2.55
10.00%	21.20	14.35	6.52	10.06	0.65	2.20	0.0210	0.83	18.80	1.87	10%	36.50	0.60	0.20	21.90	7.30	29.20
5.00%	34.01	27.61	13.39	22.98	0.58	2.06	0.0210	0.75	36.18	1.57	5%	18.25	2.64	1.46	48.18	26.64	74.82
4.00%	38.45	36.23															
3.00%	43.33	40.89															
2.00%	47.35	45.34															
1.50%	52.70	50.03															
1.00%	58.05	55.38															
0.75%	63.58	60.82															
0.50%	70.59	67.09															
0.25%	78.14	74.37															
0.10%	86.77	82.46															
0.0060%	97.36	92.07															
Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr):														71.5	36.5	108.0	

**Worksheet 20b.** Sediment transport prediction for the existing condition reach compared to the upstream sediment supply to assess bed stability.

Stream: Trail Creek, F4b Fair Riffle XS 0+40		Location: Pike National Forest, Colorado (Used GOOD-FAIR Curves)		Gage Station #: Used Post-Fire Dimensionless F-D C.		Date: 08/14/10											
Observers: S=021, Q=29.4, 23.4, Bed=-0682, S.Sand=22		Stream Type: F4b		Valley Type: VIII		Gage Station #: Used Post-Fire Dimensionless F-D C.											
Flow-duration curve		Calculate				Calculate											
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
Percentage of time	Daily mean discharge	Mid-ordinate stream-flow	Area	Width	Depth	Velocity	Slope	Shear stress	Stream power	Unit power	Time increment	Time increment	Daily mean bedload transport	Daily mean suspended sand transport	Time adjusted bedload transport	Time adjusted suspended sand transport	Time adjusted total transport
(%)	(cfs)	(cfs)	(ft <sup>2</sup> )	(ft)	(ft)	(ft/s)	(ft/ft)	(lb/ft <sup>2</sup> )	(lb/s)	(lb/ft/s)	(%)	(days)	(tons/day)	(tons/day)	(tons)	(tons)	(tons)
100.00%	0.15										0%				0.00	0.00	0.00
90.00%	0.77	0.46	0.38	2.47	0.15	1.19	0.0210	0.19	0.60	0.24	10%	36.50	0.00	0.00	0.00	0.00	0.00
80.00%	1.08	0.93	0.60	2.67	0.22	1.52	0.0210	0.28	1.22	0.46	10%	36.50	0.00	0.00	0.00	0.00	0.00
70.00%	1.24	1.16	0.72	2.96	0.24	1.60	0.0210	0.30	1.52	0.51	10%	36.50	0.00	0.00	0.00	0.00	0.00
60.00%	1.55	1.40	0.86	3.46	0.25	1.62	0.0210	0.30	1.83	0.53	10%	36.50	0.00	0.01	0.00	0.36	0.36
50.00%	2.01	1.78	1.11	4.56	0.24	1.61	0.0210	0.30	2.33	0.51	10%	36.50	0.00	0.01	0.00	0.36	0.36
40.00%	2.63	2.32	1.49	6.46	0.23	1.56	0.0210	0.28	3.04	0.47	10%	36.50	0.00	0.01	0.00	0.36	0.36
30.00%	3.84	3.24	1.96	7.77	0.25	1.64	0.0210	0.31	4.25	0.55	10%	36.50	0.00	0.01	0.00	0.36	0.36
20.00%	7.49	5.67	3.42	13.80	0.25	1.65	0.0210	0.31	7.43	0.54	10%	36.50	0.00	0.02	0.00	0.73	0.73
10.00%	21.20	14.35	6.53	17.38	0.38	2.19	0.0210	0.48	18.80	1.08	10%	36.50	0.17	0.10	6.21	3.65	9.86
5.00%	34.01	27.61	10.17	19.69	0.52	2.71	0.0210	0.65	36.18	1.84	5%	18.25	0.60	0.38	10.95	6.94	17.89
4.00%	38.45	36.23															
3.00%	43.33	40.89															
2.00%	47.35	45.34															
1.50%	52.70	50.03															
1.00%	58.05	55.38															
0.75%	63.58	60.82															
0.50%	70.59	67.09															
0.25%	78.14	74.37															
0.10%	86.77	82.46															
0.0060%	97.36	92.07															

Notes:		Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr):		17.2	12.8	29.9
		Upstream total annual sediment supply (tons/yr) (Worksheet 5-20a):		71.5	36.5	108.0
		Difference in sediment transport capacity (tons/yr) (+ or -):		-54.3	-23.7	-78.1
		Stability evaluation: Aggradation, Degradation or Stable:		Aggradation, > 72% Reduction in Transport		

## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>Trail Creek, F4b Fair-Poor Reach</b>		Stream Type: <b>F4b</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>K. Wright, L. Chavez, D. Butler &amp; D. Bohon</b>		Date: <b>8/26/2010</b>			
<b>Enter Required Information for Existing Condition</b>					
11.1	$D_{50}$	Riffle bed material $D_{50}$ (mm)			
7.8	$\hat{D}_{50}$	Bar sample $D_{50}$ (mm)			
0.23	$D_{max}$	Largest particle from bar sample (ft)	70	(mm)	304.8 mm/ft
0.021	S	Existing bankfull water surface slope (ft/ft)			
0.53	d	Existing bankfull mean depth (ft)			
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment			
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>					
1.43	$D_{50}/\hat{D}_{50}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 ( D_{50}/\hat{D}_{50} )^{-0.872}$		
6.31	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 ( D_{max}/D_{50} )^{-0.887}$		
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED:		
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	d	Required bankfull mean depth (ft)	$d = \frac{\tau^* (\gamma_s - 1) D_{max}}{S}$ (use $D_{max}$ in ft)		
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	S	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^* (\gamma_s - 1) D_{max}}{d}$ (use $D_{max}$ in ft)		
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					
<b>Sediment Competence Using Dimensional Shear Stress</b>					
0.695		Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d ) $\gamma = 62.4$ , d = existing depth, S = existing slope			
Shields 50	CO 120	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ (Figure 5-49)			
Shields 1.0	CO 0.35	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) (Figure 5-49)			
Shields 0.76	CO 0.27	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm)		$d = \frac{\tau}{\gamma S}$	
Shields 0.0302	CO 0.0106	Predicted slope required to initiate movement of measured $D_{max}$ (mm)		$S = \frac{\tau}{\gamma d}$	
Check: <input checked="" type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					

## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>Trail Creek, F4b Fair-Poor</b>	Stream Type: <b>F4b</b>
Location: <b>Pike National Forest, CO</b>	Valley Type: <b>VIII</b>
Observers: <b>K. Wright, L. Chavez et al.</b>	Date: <b>8/26/2010</b>
<b>Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)</b>	<b>Stability Rating (Check Appropriate Rating)</b>
Stream Type at potential, (C→E), <b>(F<sub>b</sub>→B)</b> , (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	<input checked="" type="checkbox"/> Stable
(E→C), (C→High W/d C)	<input type="checkbox"/> Moderately Unstable
(G→F), (F→D), (C→F),	<input type="checkbox"/> Unstable
(C→D), (B→G), (D→G), (C→G), (E→G)	<input type="checkbox"/> Highly Unstable

**Worksheet 5-25.** Lateral stability.

Stream: <b>Trail Creek, F4b Fair-Poor Reach</b>		Stream Type: <b>F4b</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>K. Wright, L. Chavez, D. Butler &amp; D. Bohon</b>		Date: <b>8/26/2010</b>			
Lateral stability criteria (choose one stability category for each criterion 1-5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	8
	(2)	(4)	(6)	3.0 (8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	3
	(1)	(2)	B3, B4 (3)	(4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		1
	M1 (1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	4
	(2)	M/L, MM (4)	(6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	2
	(1)	0.44 (2)	(3)	(4)	
<b>Total Points</b>					<b>18</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input type="checkbox"/>	<i>Unstable</i> 13 – 21 <input checked="" type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	

**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>Trail Creek, F4b Fair-Poor Reach</b>		Stream Type: <b>F4b</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>K. Wright, L. Chavez, D. Butler &amp; D. Bohon</b>		Date: <b>8/26/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
1 <b>Sediment competence</b> (Worksheet 3-22)	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope-slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	2
	(2)	(4)	(6)	(8)	
2 <b>Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	8
	(2)	(4)	(6)	(8)	
3 <b>W/d Ratio State</b> (Worksheet 5-13)	1.0 – 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	8
	(2)	(4)	(6)	3.0 (8)	
4 <b>Stream Succession States</b> (Worksheet 5-24)	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	2
	Fb to B (2)	(4)	(6)	(8)	
5 <b>Depositional Patterns</b> (Worksheet 5-10)	B1	B2, B4	B3, B5	B6, B7, B8	3
	(1)	(2)	B3, B4 (3)	(4)	
6 <b>Debris / Blockages</b> (Worksheet 5-11)	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	1
	D1 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>24</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
<b>Vertical Stability for Excess Deposition / Aggradation</b> (use total points and check stability rating)	<i>No Deposition</i> 10 – 14 <input type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input checked="" type="checkbox"/>	<i>Aggradation</i> > 30 <input type="checkbox"/>	

**Worksheet 5-27.** Vertical stability – degradation.

Stream: <b>Trail Creek, F4b Fair-Poor Reach</b>		Stream Type: <b>F4b</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>K. Wright, L. Chavez, D. Butler &amp; D. Bohon</b>		Date: <b>8/26/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>1 Sediment Competence</b> (Worksheet 5-22)	Does not indicate excess competence  <b>(2)</b>	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed  <b>(4)</b>	$D_{100}$ of bed moved  <b>(6)</b>	Particles much larger than $D_{100}$ of bed moved  <b>(8)</b>	<b>2</b>
<b>2 Sediment Capacity</b> (POWERSED) (Worksheet 5-20)	Does not indicate excess capacity  <b>(2)</b>	Slight excess energy: up to 10% increase above reference  <b>(4)</b>	Excess energy sufficient to increase load up to 50% of annual load  <b>(6)</b>	Excess energy transporting more than 50% of annual load  <b>(8)</b>	<b>2</b>
<b>3 Degree of Channel Incision (BHR)</b> (Worksheet 5-12)	1.00 – 1.10  <b>(2)</b>	1.11 – 1.30  <b>(4)</b>	1.31 – 1.50  <b>(6)</b>	> 1.50  <b>(8)</b>	<b>2</b>
<b>4 Stream Succession States</b> (Worksheets 5-12 and 5-24)	Does not indicate incision or degradation  <b>(2)</b>	If BHR > 1.1 and stream type has W/d between 5–10  <b>(4)</b>	If BHR > 1.1 and stream type has W/d less than 5  <b>(6)</b>	(B→G), (C→G), (E→G), (D→G)  <b>(8)</b>	<b>2</b>
<b>5 Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.80 – 1.00  <b>(1)</b>	0.30 – 0.79  <b>0.44 (2)</b>	0.10 – 0.29  <b>(3)</b>	< 0.10  <b>(4)</b>	<b>2</b>
<b>Total Points</b>					<b>10</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation</b> (use total points and check stability rating)	<b>Not Incised</b> 9 – 11 <input checked="" type="checkbox"/>	<b>Slightly Incised</b> 12 – 18 <input type="checkbox"/>	<b>Moderately Incised</b> 19 – 27 <input type="checkbox"/>	<b>Degradation</b> > 27 <input type="checkbox"/>	



Worksheet 5-28. Channel enlargement.

Stream: <b>Trail Creek, F4b Fair-Poor Reach</b>		Stream Type: <b>F4b</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>K. Wright, L. Chavez, D. Butler &amp; D. Bohon</b>		Date: <b>8/26/2010</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1-4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	2
	<b>Fb to B</b> (2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	6
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	6
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	2
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>16</b>
<b>Category Point Range</b>					
<b>Channel Enlargement Prediction (use total points and check stability rating)</b>	<i>No Increase</i> 8 – 10 <input type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input checked="" type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input type="checkbox"/>	<i>Extensive</i> > 24 <input type="checkbox"/>	

**Worksheet 5-29.** Overall sediment supply.

Stream: <b>Trail Creek, F4b Fair-Poor Reach</b>		Stream Type: <b>F4b</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>		
Observers: <b>K. Wright, L. Chavez, D. Butler &amp; D. Bohon</b>		Date: <b>8/26/2010</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1-5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	3	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	3	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	1	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	2	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	4	
	<i>Fair: Mod. Unstable</i>	2		
		3		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>13</b>	
<b>Category Point Range</b>				
Overall Sediment Supply Rating (use total points and check stability rating)	<i>Low</i> 5 <input type="checkbox"/>	<i>Moderate</i> 6 – 10 <input type="checkbox"/>	<i>High</i> 11 – 15 <input checked="" type="checkbox"/>	<i>Very High</i> 16 – 20 <input type="checkbox"/>

Worksheet 5-32. Summary of stability condition categories.

Stream: <b>Trail Creek, F4b Fair-Poor Reach</b>		Location: <b>Pike National Forest, Colorado</b>	
Observers: <b>Wright, Chavez, Butler, Bohon</b>		Stream Type: <b>F4b</b> Valley Type: <b>VIII</b>	
Date: <b>8/26/2010</b>		Width of Flood-Prone Area (ft): <b>26.336</b> Entrenchment Ratio: <b>1.32</b>	
Channel Dimension (Rifle XS 0+40)		Cross-Sectional Area (ft <sup>2</sup> ): <b>10.6</b>	
Mean Bankfull Depth (ft): <b>0.53</b>		R <sub>d</sub> W <sub>bkt</sub> : <b>N/A</b> MWR: <b>1.18</b> Sinuosity: <b>1.03</b>	
Channel Pattern		L <sub>m</sub> /W <sub>bkt</sub> : <b>N/A</b>	
River Profile & Bed Features		<input checked="" type="checkbox"/> Riffle/Pool <input type="checkbox"/> Step/Pool <input type="checkbox"/> Plane Bed <input type="checkbox"/> Convergence/Divergence <input type="checkbox"/> Dunes/Antidunes/Smooth Bed <input type="checkbox"/> Max Bankfull Depth (ft): <b>1.35</b> <input type="checkbox"/> Riffle <input type="checkbox"/> Pool <input type="checkbox"/> Depth Ratio (max to mean): <b>2.21</b> <input type="checkbox"/> Riffle <input type="checkbox"/> Pool <input type="checkbox"/> Pool Spacing: <b>2.3</b> <input type="checkbox"/> Valley: <b>0.0215</b> <input type="checkbox"/> Slope <input type="checkbox"/> Water Surface: <b>0.021</b>	
Level III Stream Stability Indices		Riparian Vegetation: <b>Willow, Aspen, Grass, Forb</b> <input type="checkbox"/> Current Composition/Density: <b>Same but mature species</b> <input type="checkbox"/> Potential Composition/Density: Flow Regime: <b>P1, P2, P8 &amp; Order: S-4(4)</b> <input type="checkbox"/> Meaner Patterns: <b>M1</b> <input type="checkbox"/> Depositional Patterns: <b>B3, B4</b> <input type="checkbox"/> Debris/Channel Blockages: <b>D1</b> Degree of Incision (Bank-Height Ratio): <b>1.0</b> <input type="checkbox"/> Degree of Incision Stability Rating: <b>Stable</b> <input type="checkbox"/> Modified Pfankuch Stability Rating (Numeric & Adjective Rating): <b>103 (Fair-Poor)</b>	
Bank Erosion Summary		Width/depth Ratio (W/d): <b>37.6</b> <input type="checkbox"/> Reference W/d Ratio (W/d <sub>ref</sub> ): <b>12.6</b> <input type="checkbox"/> Width/Depth Ratio State (W/d) / (W/d <sub>ref</sub> ): <b>2.99</b> <input type="checkbox"/> W/d Ratio State Stability Rating: <b>Highly Unstable</b> Meander Width Ratio (MWR): <b>1.18</b> <input type="checkbox"/> Reference MWR <sub>ref</sub> : <b>2.7</b> <input type="checkbox"/> Degree of confinement (MWR / MWR <sub>ref</sub> ): <b>0.44</b> <input type="checkbox"/> MWR / MWR <sub>ref</sub> Stability Rating: <b>Moderately Confined</b> Length of Reach Studied (ft): <b>221</b> <input type="checkbox"/> Annual Streambank Erosion Rate: <b>5.31</b> (tons/yr) <input type="checkbox"/> Curve Used: <b>Colorado</b> <input type="checkbox"/> Remarks:	
Sediment Capacity (POWERSED)		<input type="checkbox"/> Sufficient Capacity <input checked="" type="checkbox"/> Insufficient Capacity <input type="checkbox"/> Excess Capacity <input type="checkbox"/> Excess Capacity Remarks: <b>&gt; 70% Reduction in Transport Capacity</b>	
Entrainment/Competence		Largest Particle from Bar Sample (mm): <b>70</b> <input type="checkbox"/> τ = <b>0.695</b> <input type="checkbox"/> τ* = <b>N/A</b> <input type="checkbox"/> Existing Depth: <b>0.53</b> <input type="checkbox"/> Required Depth: <b>0.27</b> <input type="checkbox"/> Existing Slope: <b>0.021</b> <input type="checkbox"/> Required Slope: <b>0.03</b>	
Successional Stage Shift		B → G → <b>Fb</b> → B → → <input type="checkbox"/> Existing Stream State (Type): <b>F4b</b> <input type="checkbox"/> Potential Stream State (Type): <b>B4</b>	
Lateral Stability		<input type="checkbox"/> Stable <input type="checkbox"/> Mod. Unstable <input checked="" type="checkbox"/> Unstable <input type="checkbox"/> Highly Unstable <input type="checkbox"/> Remarks/causes:	
Vertical Stability (Aggradation)		<input type="checkbox"/> No Deposition <input type="checkbox"/> Mod. Deposition <input checked="" type="checkbox"/> Ex. Deposition <input type="checkbox"/> Aggradation <input type="checkbox"/> Remarks/causes:	
Vertical Stability (Degradation)		<input checked="" type="checkbox"/> Not Incised <input type="checkbox"/> Slightly Incised <input type="checkbox"/> Mod. Incised <input type="checkbox"/> Degradation <input type="checkbox"/> Remarks/causes:	
Channel Enlargement		<input type="checkbox"/> No Increase <input checked="" type="checkbox"/> Slight Increase <input type="checkbox"/> Mod. Increase <input type="checkbox"/> Extensive <input type="checkbox"/> Remarks/causes: <b>Trending toward B</b>	
Sediment Supply (Channel Source)		<input type="checkbox"/> Low <input type="checkbox"/> Moderate <input checked="" type="checkbox"/> High <input type="checkbox"/> Very High <input type="checkbox"/> Remarks/causes: <b>Banks sloughed in and vegetated, trending toward B stream type</b>	



## *Appendix C12*

# **F4b Stream Type** *Poor Stability Reach*



# Table of Contents

## *Appendix C12: F4b Poor Stability Reach*

<b>Reach Location &amp; Overview.....</b>	<b>C12-2</b>
<b>Survey Summary.....</b>	<b>C12-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C12-8</b>
<b><i>Velocity, Classification &amp; Morphological Relations.....</i></b>	<b>C12-8</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b><i>Stability Indices.....</i></b>	<b>C12-12</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b><i>BANCS Model – Streambank Erosion.....</i></b>	<b>C12-22</b>
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b><i>FLOWSED Model – Total Annual Sediment Yield.....</i></b>	<b>C12-25</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b><i>POWERSED Model– Sediment Transport Capacity to Assess Bed Stability.....</i></b>	<b>C12-27</b>
Worksheet 5-20a. Sediment transport prediction for the upstream condition.	
Worksheet 5-20b. Sediment transport prediction for the existing condition.	
<b><i>Sediment Competence/Entrainment.....</i></b>	<b>C12-29</b>
Worksheet 5-22. Sediment competence calculations.	
<b><i>Channel Stability Ratings.....</i></b>	<b>C12-30</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b><i>Summary.....</i></b>	<b>C12-36</b>
Worksheet 5-32. Summary of stability condition categories.	

## F4b Poor Reach Location & Overview

This F4b Poor reach is a 3<sup>rd</sup> order, perennial, relatively steep gradient, entrenched stream located in Northfield Gulch (**Figure C-1**). The width/depth ratio of 22 is high and will continue to promote high streambank erosion in this gulch-fill, alluvial Valley Type VIIIa. The stream is continuing to enlarge due to high peak flows following the fire. The potential stable channel in this valley type is a B4 stream type.

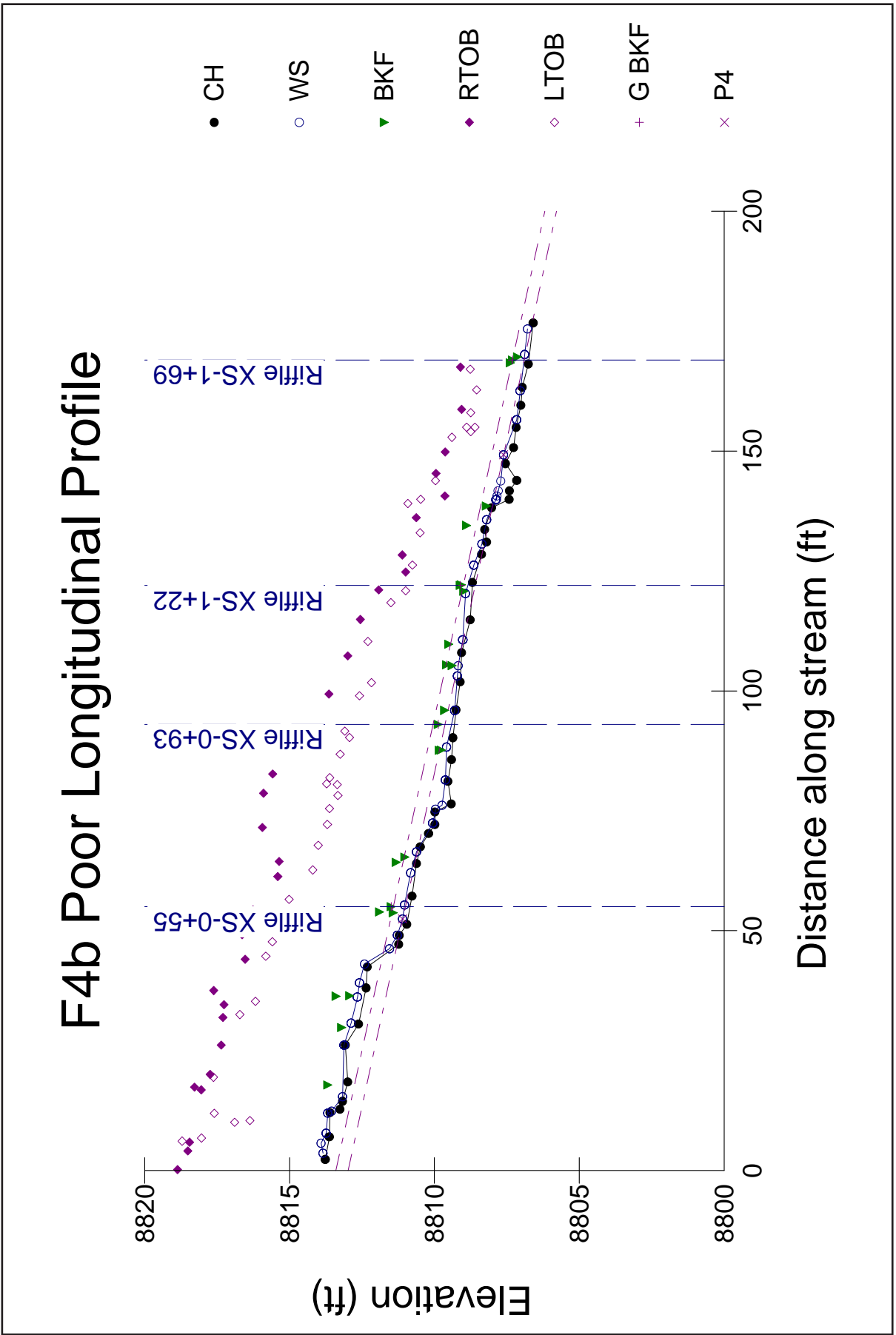
A POWERSED run was made to determine streambed stability, which predicted deposition. The stability rating is “Poor” due to a Pfankuch stability rating of 143 (“Poor”) and a high streambank erosion rate of *0.27 tons/yr/ft*. The sediment supply rating is *High*, typical of an F4b stream type, due to the high banks on both sides and deposition in the bed. The “Poor” stability rating indicates a higher potential of accelerated increases in flow-related sediment compared to the same-sized B4 reference stream type. The WRENSS model indicated that the water yield due to the fire increased from *119.1 acre-ft* to *159.6 acre-ft*, representing a total increase of *40.5 acre-ft pre year*. The corresponding bedload increased from *0.1 tons/year* to *68.9 tons/yr*, and suspended sediment increase from *14.6 tons/yr* to *1151.5 tons/yr*, representing a total increase in sediment of *1,205.7 tons/yr*. This sediment yield increase is extremely high for a stream with a bankfull discharge of 2.31 cfs.

The photograph depicts the typical character of this representative F4b Poor stream type. The following graphs and summary worksheets provide the detail of the morphology, hydraulics, streambank erosion rates, and stability conditions responsible for the overall “Poor” rating.

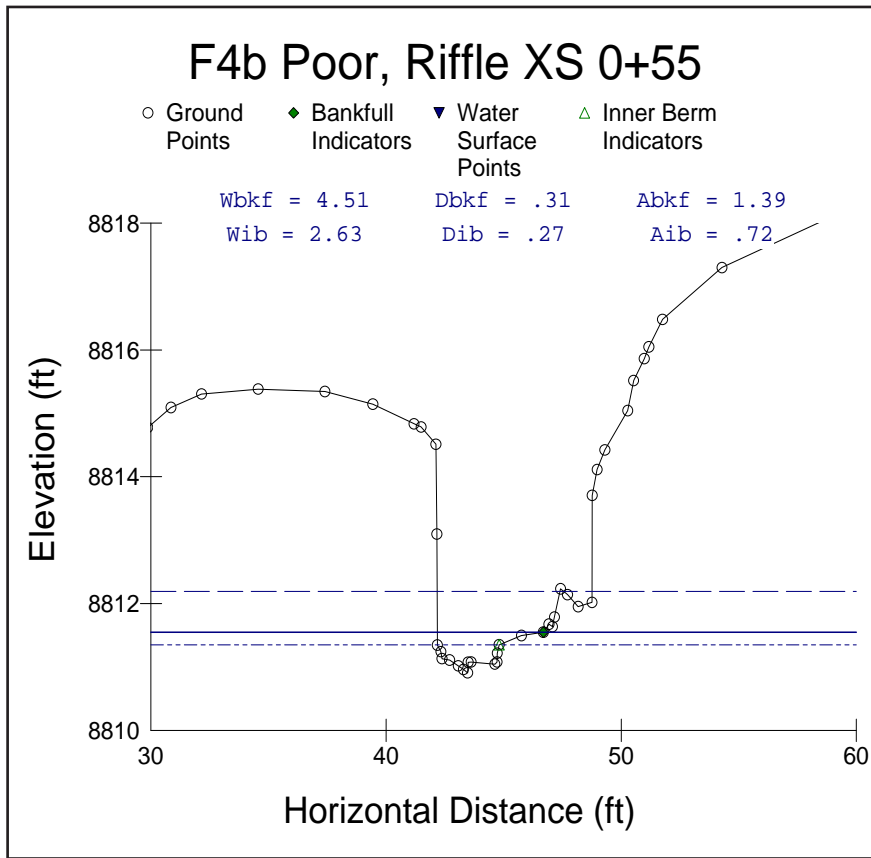




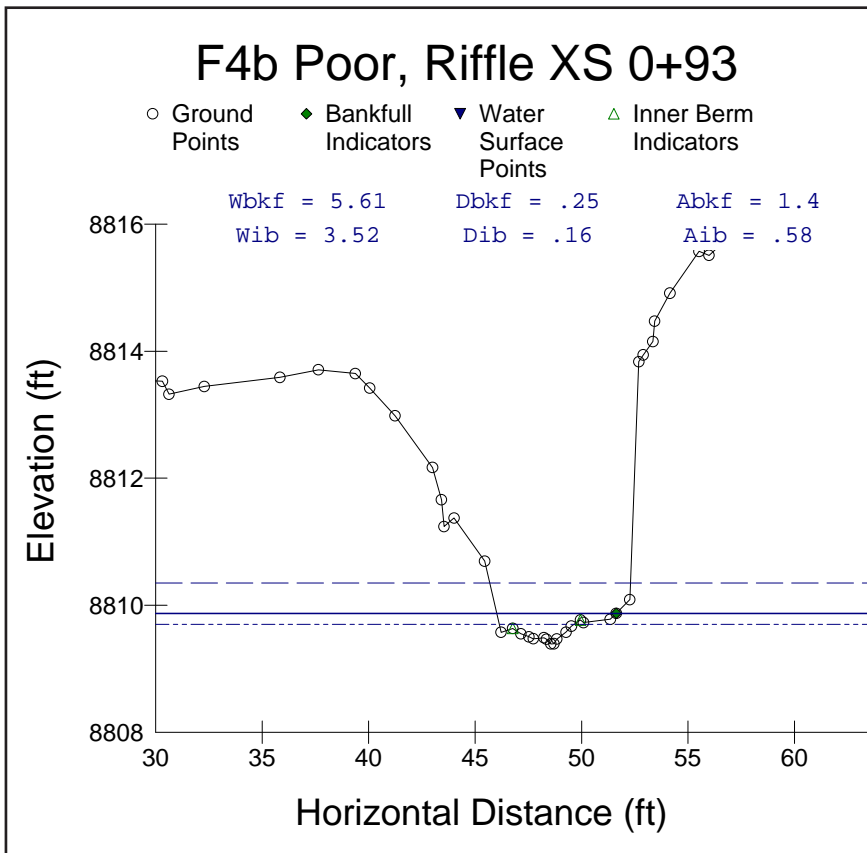
# Survey Summary



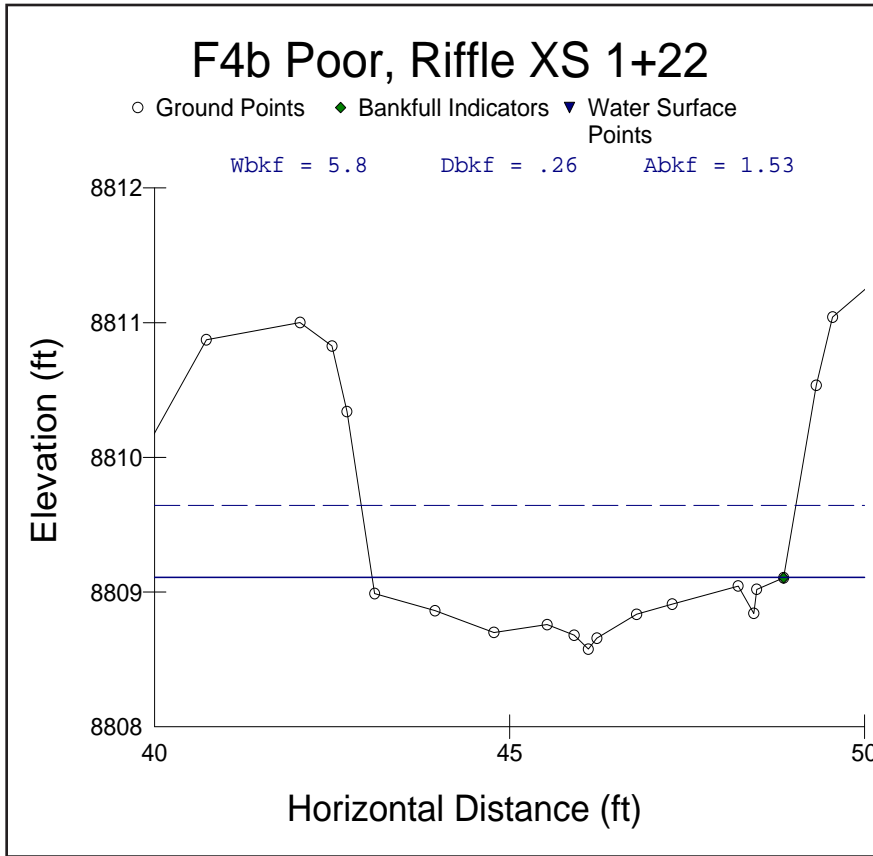
Longitudinal Profile (graph generated from RIVERMorph™)



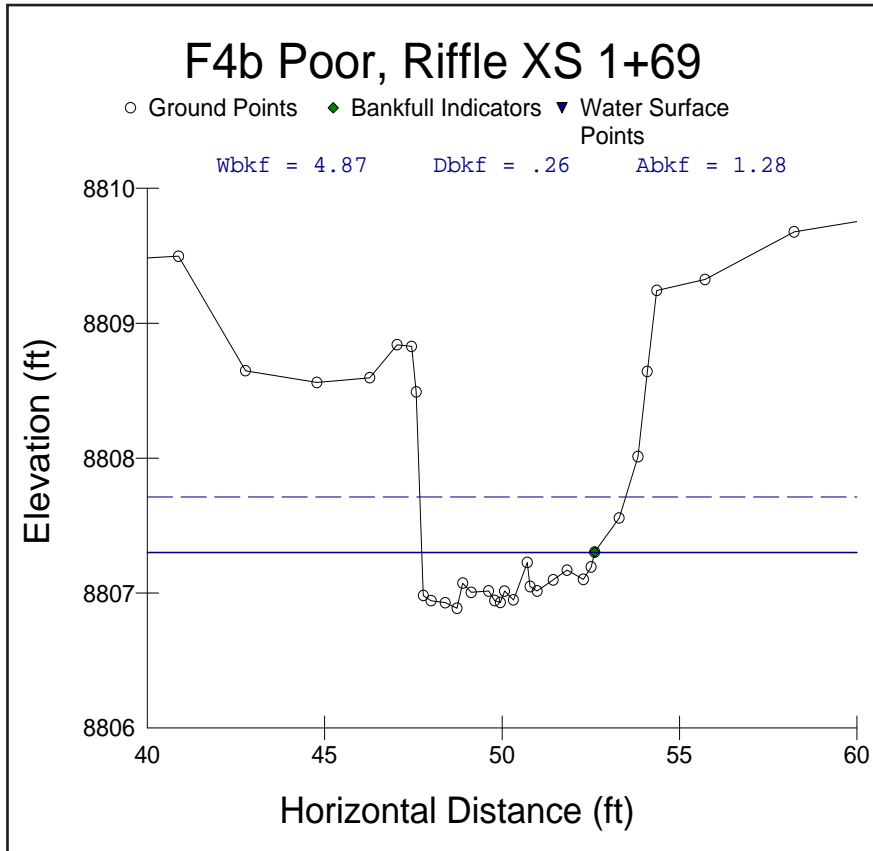
Cross-section 0+55 (graph generated from RIVERMorph™)



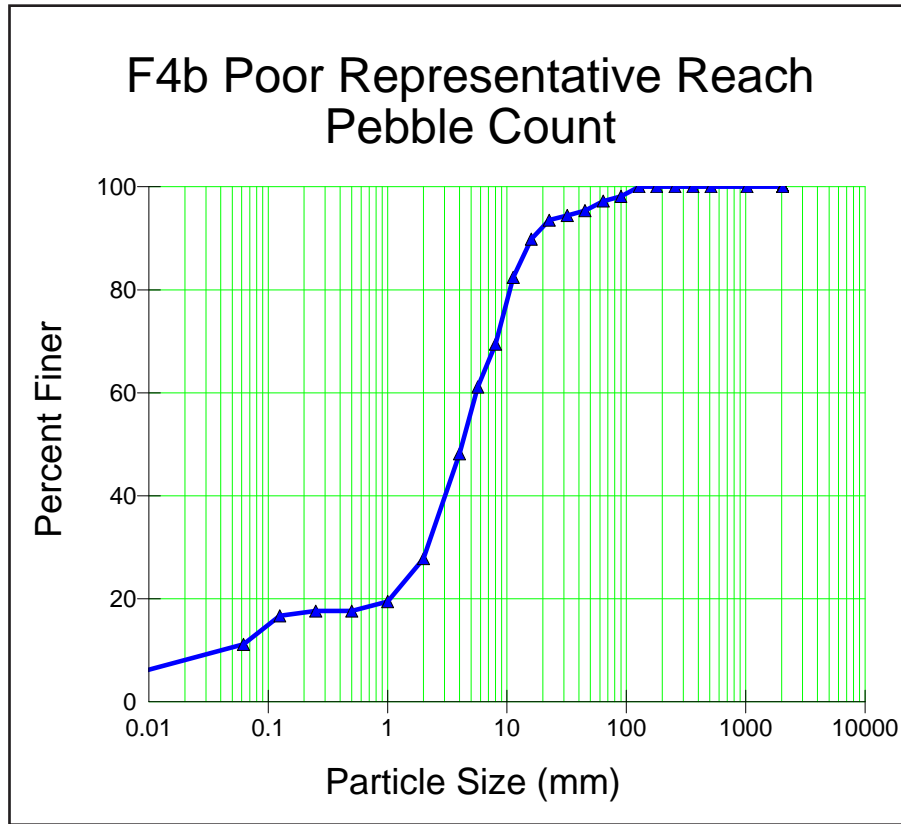
Cross-section 0+93 (graph generated from RIVERMorph™)



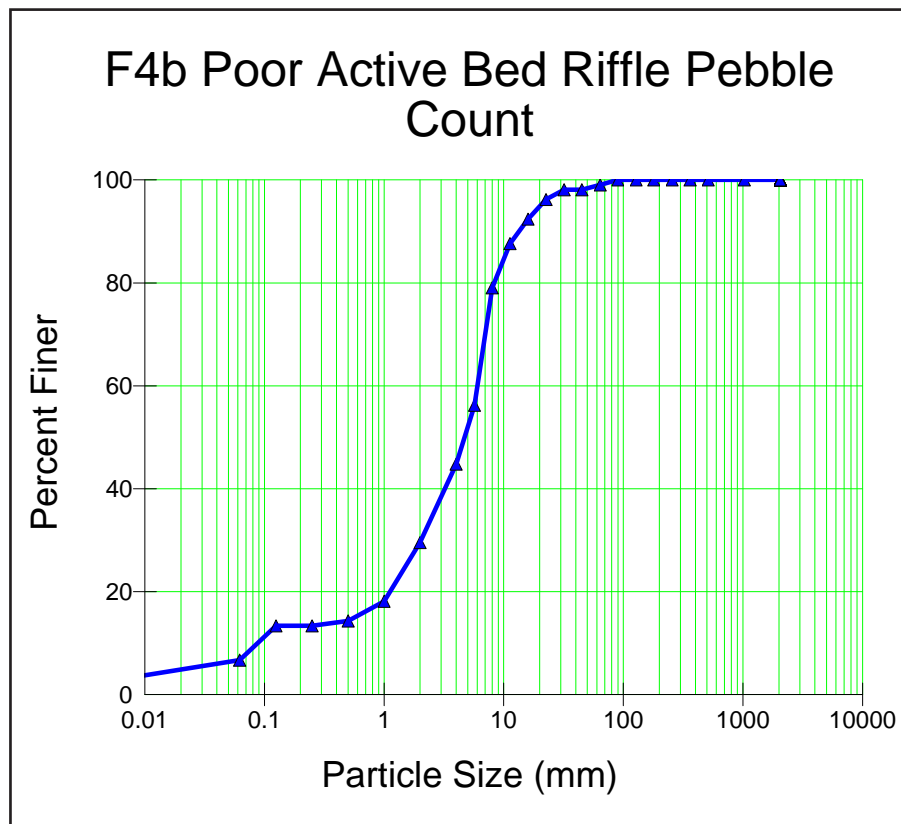
**Representative Cross-section 1+22** (graph generated from RIVERMorph™)



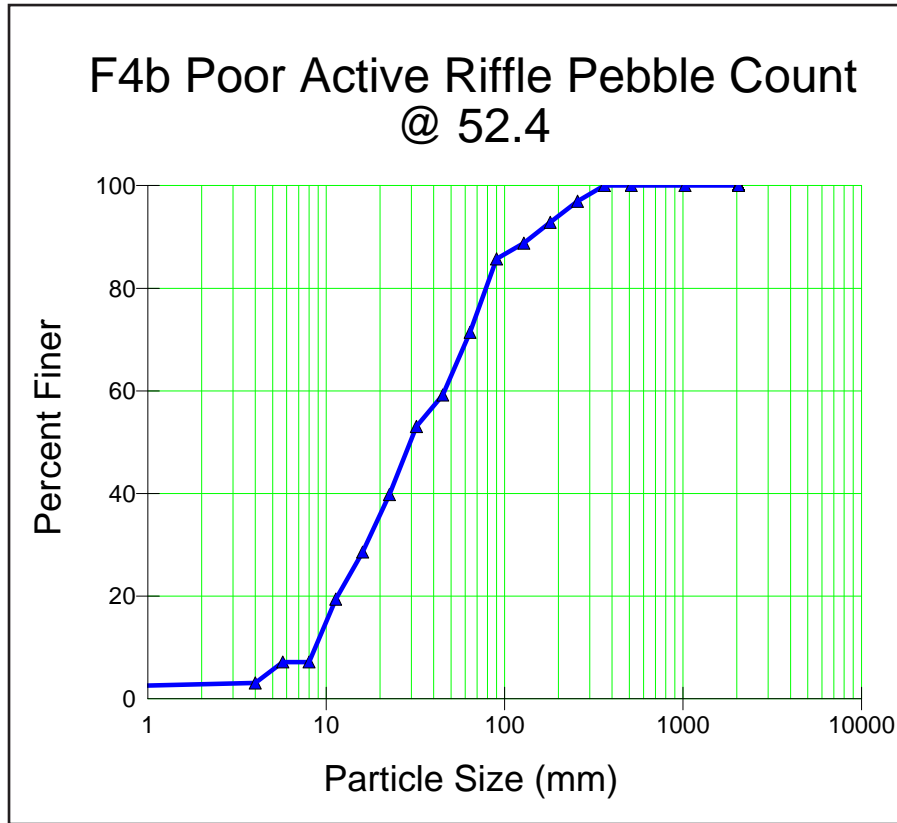
**Cross-section 1+69** (graph generated from RIVERMorph™)



Composite Pebble Count (graph generated from RIVERMorph™)



Upper Active Bed Riffle Pebble Count (graph generated from RIVERMorph™)



Active Bed Riffle Pebble Count at 52.4 (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates					
Stream:	Northfield Gulch			Location:	F4b Poor XS @ 1+22
Date:	11/2/2012	Stream Type:	F4b	Valley Type:	VIIa
Observers:	Rosgen, et. al.			HUC:	__ __ __ __ __ __ __ __ __ __
INPUT VARIABLES			OUTPUT VARIABLES		
Bankfull Riffle Cross-Sectional AREA	1.53	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.26	$d_{bkf}$ (ft)
Bankfull Riffle WIDTH	5.8	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim (2 * d_{bkf}) + W_{bkf}$	6.25	$W_p$ (ft)
$D_{84}$ at Riffle	9.9	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.03	$D_{84}$ (ft)
Bankfull SLOPE	0.04	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	0.24	R (ft)
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness $R(ft) / D_{84} (ft)$	7.53	$R / D_{84}$
Drainage Area	0.31	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.520	$u^*$ (ft/sec)
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$			4.09	ft / sec	6.26 cfs
2. Roughness Coefficient: a) Manning's n from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.057$			1.91	ft / sec	2.92 cfs
2. Roughness Coefficient: b) Manning's n from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.057$			1.91	ft / sec	2.92 cfs
2. Roughness Coefficient: c) Manning's n from Jarrett (USGS): $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for Stream Types A1, A2, A3, B1, B2, B3, C2 & E3 $n = 0.137$			0.80	ft / sec	1.22 cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Darcy-Weisbach (Leopold, Wolman and Miller)			4.34	ft / sec	6.6 cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)				ft / sec	cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q =$ <input type="text"/> year $u = Q / A$				ft / sec	cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$				ft / sec	cfs
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation ( $R/D_{84}$ ) – Estimation Method 1					
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.					
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.					
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.					
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.					

**Worksheet 5-3.** Level II stream classification.

Stream: <b>NorthfieldGulch, Reach - F4b Poor</b>	
Basin:	Drainage Area: <b>201</b> acres <b>0.31</b> mi <sup>2</sup>
Location: <b>Pike National Forest, Colorado</b>	
Twp.&Rge:	Sec.&Qtr.:
Cross-Section Monuments (Lat./Long.): <b>XS 1+22</b> Date: <b>11/2/2012</b>	
Observers: <b>Rosgen, et. al.</b>	Valley Type: <b>VIIa</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>5.8</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A_{bkf} / W_{bkf}$ ).	<b>0.26</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>1.53</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>22.31</b>	ft/ft
<b>Maximum DEPTH (<math>d_{max}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>0.53</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>6.12</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>1.06</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the median or dominant diameter of channel materials, as sampled proportionately from the channel surface, between the bankfull stage and Thalweg elevations.	<b>4.22</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.036</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope ( $S_{val} / S$ ).	<b>1.05</b>	

<b>Stream Type</b>	<b>F4b</b>	<b>See Classification Key (Figure 2-14)</b>
--------------------	------------	---

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Northfield Gulch F4b Pool</b>				Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>Rosgen et. al.</b>		Date: <b>11/2/12</b>		Valley Type: <b>VIIIA</b>		Stream Type: <b>F4b</b>			
<b>River Reach Dimension Summary Data.....1</b>									
<b>Riffle Dimensions* ** ***</b>	<b>Riffle Dimensions* ** ***</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Width ( $W_{bkt}$ )	5.2	4.5	5.8	ft	Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	1.4	1.3	1.5
	Mean Riffle Depth ( $d_{bkt}$ )	0.27	0.25	0.31	ft	Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	19.5	14.6	22.4
	Maximum Riffle Depth ( $d_{max}$ )	0.52	0.41	0.64	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	1.900	1.577	2.065
	Width of Flood-Prone Area ( $W_{fpa}$ )	6.2	5.8	6.6	ft	Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )	1.2	1.1	1.4
	Riffle Inner Berm Width ( $W_{ib}$ )	3.9	2.6	5.1	ft	Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )	0.743	0.583	0.903
	Riffle Inner Berm Depth ( $d_{ib}$ )	0.22	0.17	0.27	ft	Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )	0.781	0.681	0.883
	Riffle Inner Berm Area ( $A_{ib}$ )	0.8	0.7	0.9	ft <sup>2</sup>	Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )	0.566	0.516	0.615
	Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )	19.7	9.6	29.8					
<b>Pool Dimensions* ** ***</b>	<b>Pool Dimensions* ** ***</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Pool Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Pool Width ( $W_{bkfp}$ )				ft	Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )			
	Mean Pool Depth ( $d_{bkfp}$ )				ft	Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )			
	Pool Cross-Sectional Area ( $A_{bkfp}$ )				ft	Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )			
	Maximum Pool Depth ( $d_{maxp}$ )				ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )			
	Pool Inner Berm Width ( $W_{ibp}$ )				ft	Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )			
	Pool Inner Berm Depth ( $d_{ibp}$ )				ft	Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )			
	Pool Inner Berm Area ( $A_{ibp}$ )				ft <sup>2</sup>	Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )			
	Point Bar Slope ( $S_{pb}$ )				ft/ft	Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )			
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Run Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Run Width ( $W_{bkfr}$ )				ft	Run Width to Riffle Width ( $W_{bkfr} / W_{bkt}$ )			
	Mean Run Depth ( $d_{bkfr}$ )				ft	Mean Run Depth to Mean Riffle Depth ( $d_{bkfr} / d_{bkt}$ )			
	Run Cross-Sectional Area ( $A_{bkfr}$ )				ft	Run Area to Riffle Area ( $A_{bkfr} / A_{bkt}$ )			
	Maximum Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )			
	Run Width/Depth Ratio ( $W_{bkfr} / d_{bkfr}$ )				ft				
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Glide Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Glide Width ( $W_{bkfg}$ )				ft	Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )			
	Mean Glide Depth ( $d_{bkfg}$ )				ft	Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )			
	Glide Cross-Sectional Area ( $A_{bkfg}$ )				ft	Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )			
	Maximum Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )			
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )				ft/ft	Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )			
	Glide Inner Berm Width ( $W_{ibg}$ )				ft	Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )			
	Glide Inner Berm Depth ( $d_{ibg}$ )				ft	Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )			
Glide Inner Berm Area ( $A_{ibg}$ )				ft <sup>2</sup>	Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )				
<b>Step**</b>	<b>Step Dimensions**</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Step Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Step Width ( $W_{bkfs}$ )				ft	Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )			
	Mean Step Depth ( $d_{bkfs}$ )				ft	Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )			
	Step Cross-Sectional Area ( $A_{bkfs}$ )				ft	Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )			
	Maximum Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
	Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )								



**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Northfield Gulch F4b Poor</b>		Location: <b>Pike National Forest, Colorado</b>																						
Observers: <b>Rosgen et. al.</b>		Date: <b>11/2/2012</b>		Valley Type: <b>VIIa</b>		Stream Type: <b>F4b</b>																		
<b>Hydraulics</b>	<b>River Reach Summary Data.....2</b>																							
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $U_{bkt}$ )		<b>1.91</b> ft/sec		Estimation Method		<b>Friction Factor</b>																	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )		<b>2.92</b> cfs		Drainage Area		<b>0.30</b> mi <sup>2</sup>																	
<b>Channel Pattern</b>	<b>Geometry</b>			<b>Mean</b>			<b>Min</b>			<b>Max</b>			<b>Dimensionless Geometry Ratios</b>			<b>Mean</b>			<b>Min</b>			<b>Max</b>		
	Linear Wavelength ( $\lambda$ )			<b>63.0</b>									Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )			<b>12.12</b>								
	Stream Meander Length ( $L_m$ )			<b>68.0</b>									Stream Meander Length Ratio ( $L_m / W_{bkt}$ )			<b>13.08</b>								
	Radius of Curvature ( $R_c$ )			<b>34.5</b>			<b>32.0</b>			<b>37.0</b>			Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )			<b>6.63</b>			<b>6.15</b>			<b>7.12</b>		
	Belt Width ( $W_{bit}$ )			<b>25.0</b>									Meander Width Ratio ( $W_{bit} / W_{bkt}$ )			<b>10.45</b>			<b>5.94</b>			<b>18.51</b>		
	Arc Length ( $L_a$ )			<b>33.0</b>			<b>33.0</b>			<b>33.0</b>			Arc Length to Riffle Width ( $L_a / W_{bkt}$ )			<b>6.35</b>			<b>6.35</b>			<b>6.35</b>		
	Riffle Length ( $L_r$ )			<b>20.4</b>			<b>17.8</b>			<b>24.4</b>			Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )			<b>3.92</b>			<b>3.42</b>			<b>4.69</b>		
	Individual Pool Length ( $L_p$ )			<b>6.2</b>			<b>5.0</b>			<b>7.4</b>			Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )			<b>1.19</b>			<b>0.96</b>			<b>1.43</b>		
Pool to Pool Spacing ( $P_s$ )			<b>66.1</b>			<b>66.1</b>			<b>66.1</b>			Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )			<b>12.71</b>			<b>12.71</b>			<b>12.71</b>			
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )		<b>0.0378</b>		ft/ft		Average Water Surface Slope (S)		<b>0.0360</b>		ft/ft		Sinuosity ( $S_{val} / S$ )		<b>1.05</b>									
	Stream Length (SL)		<b>167.0</b>		ft		Valley Length (VL)		<b>159.0</b>		ft		Sinuosity (SL / VL)		<b>1.05</b>									
	Low Bank Height (LBH)		start: <b>4.37</b> ft		end: <b>2.09</b> ft		Max Bankfull Depth ( $d_{max}$ )		start: <b>0.50</b> ft		end: <b>0.43</b> ft		Bank-Height Ratio (BHR) (LBH / $d_{max}$ )		start: <b>8.7</b>		end: <b>4.8</b>							
	<b>Facet Slopes</b>			<b>Mean</b>			<b>Min</b>			<b>Max</b>			<b>Dimensionless Facet Slope Ratios</b>			<b>Mean</b>			<b>Min</b>			<b>Max</b>		
	Riffle Slope ( $S_{rif}$ )			<b>0.540</b>			<b>0.490</b>			<b>0.570</b>			Riffle Slope to Average Water Surface Slope ( $S_{rif} / S$ )			<b>15.000</b>			<b>13.611</b>			<b>15.833</b>		
	Run Slope ( $S_{run}$ )			<b>0.820</b>			<b>0.680</b>			<b>0.960</b>			Run Slope to Average Water Surface Slope ( $S_{run} / S$ )			<b>22.778</b>			<b>18.889</b>			<b>26.667</b>		
	Pool Slope ( $S_p$ )			<b>1.120</b>			<b>1.010</b>			<b>1.220</b>			Pool Slope to Average Water Surface Slope ( $S_p / S$ )			<b>31.111</b>			<b>28.056</b>			<b>33.889</b>		
	Glide Slope ( $S_g$ )			<b>0.780</b>			<b>0.550</b>			<b>0.960</b>			Glide Slope to Average Water Surface Slope ( $S_g / S$ )			<b>21.667</b>			<b>15.278</b>			<b>26.667</b>		
	Step Slope ( $S_s$ )												Step Slope to Average Water Surface Slope ( $S_s / S$ )											
	<b>Max Depths<sup>a</sup></b>			<b>Mean</b>			<b>Min</b>			<b>Max</b>			<b>Dimensionless Depth Ratios</b>			<b>Mean</b>			<b>Min</b>			<b>Max</b>		
	Max Riffle Depth ( $d_{max}$ )			<b>0.54</b>			<b>0.49</b>			<b>0.57</b>			Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )			<b>2.000</b>			<b>1.815</b>			<b>2.111</b>		
	Max Run Depth ( $d_{maxr}$ )			<b>0.82</b>			<b>0.68</b>			<b>0.96</b>			Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )			<b>3.037</b>			<b>2.519</b>			<b>3.556</b>		
	Max Pool Depth ( $d_{maxp}$ )			<b>1.12</b>			<b>1.01</b>			<b>1.22</b>			Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )			<b>4.148</b>			<b>3.741</b>			<b>4.519</b>		
	Max Glide Depth ( $d_{maxg}$ )			<b>0.87</b>			<b>0.55</b>			<b>0.96</b>			Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )			<b>3.222</b>			<b>2.037</b>			<b>3.556</b>		
	Max Step Depth ( $d_{maxs}$ )												Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )											
<b>Channel Materials</b>			<b>Reach<sup>b</sup></b>		<b>Riffle<sup>c</sup></b>		<b>Bar</b>		<b>Reach<sup>b</sup></b>		<b>Riffle<sup>c</sup></b>		<b>Bar</b>		<b>Protrusion Height<sup>d</sup></b>									
	% Silt/Clay		<b>11.11</b>		<b>6.67</b>				$D_{16}$		<b>0.12</b>		<b>0.72</b>				<b>10.39</b> mm							
	% Sand		<b>16.67</b>		<b>22.85</b>				$D_{35}$		<b>2.71</b>		<b>2.72</b>				<b>19.78</b> mm							
	% Gravel		<b>69.44</b>		<b>69.53</b>				$D_{50}$		<b>4.24</b>		<b>4.78</b>				<b>29.83</b> mm							
	% Cobble		<b>2.78</b>		<b>0.95</b>				$D_{84}$		<b>12.31</b>		<b>9.91</b>				<b>86.89</b> mm							
	% Boulder		<b>0.00</b>		<b>0.00</b>				$D_{95}$		<b>39.83</b>		<b>20.54</b>				<b>219.86</b> mm							
	% Bedrock		<b>0.00</b>		<b>0.00</b>				$D_{100}$		<b>128.00</b>		<b>90.00</b>				<b>362.00</b> mm							

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.

## Stability Indices

**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation					
Stream: <b>Northfield Gulch, F4b Poor</b>			Location: <b>Pike National Forest, Colorado</b>		
Observers: <b>Rosgen et. al.</b>		Reference reach <input type="checkbox"/>	Disturbed (impacted reach) <input checked="" type="checkbox"/>	Date: <b>11/2/2012</b>	
Existing species composition: <b>Burnt trees &amp; young aspen</b>			Potential species composition: <b>Aspen, Doug-fir, Ponderosa pine, Spruce</b>		
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition
<b>1. Overstory</b>	Canopy layer	5%	25%	<b>Aspen</b>	2%
				<b>Douglass-Fir</b>	5%
				<b>Ponderoso Pine</b>	3%
					0%
					0%
					10%
<b>2. Understory</b>	Shrub layer	5%	5%	<b>Willow</b>	40%
				<b>Aspen</b>	60%
					0%
					0%
					0%
					100%
<b>3. Ground level</b>	Herbaceous	40%	40%	<b>Grass</b>	80%
				<b>Forbs</b>	20%
					0%
					0%
					0%
					100%
	Leaf or needle litter	5%	25%	<b>Remarks:</b> Condition, vigor and/or usage of existing reach: <b>Burnt tress dominate landscape, few young aspen repopulating.</b>	
	Bare ground				
			<b>Column total = 100%</b>		


\*Based on crown closure.

\*\*Based on basal area to surface area.

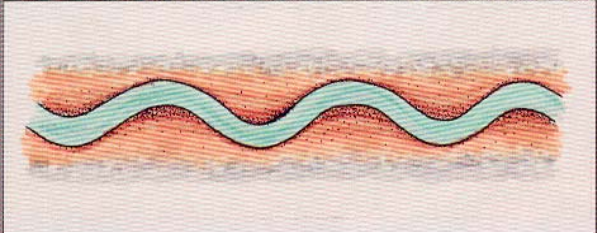

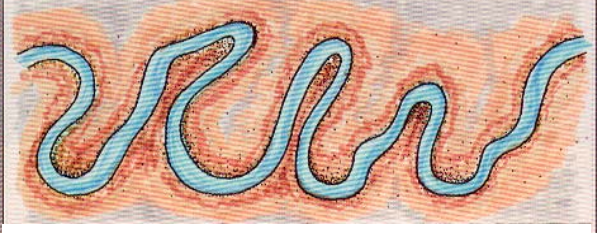
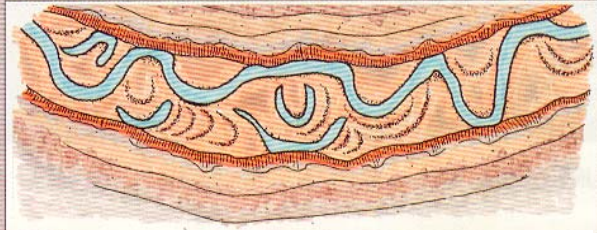
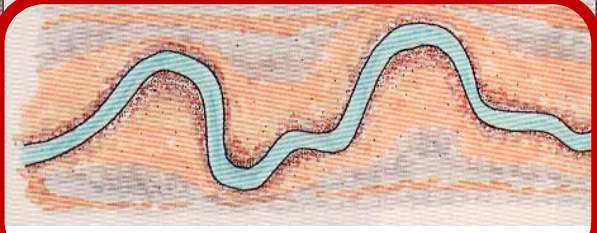
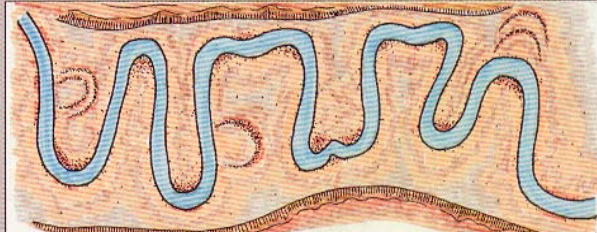
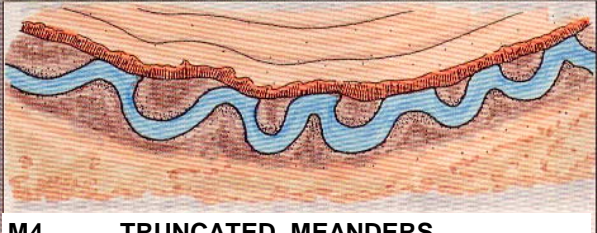
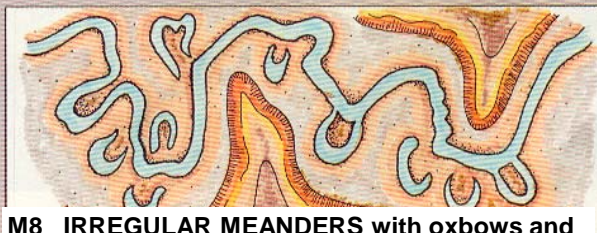
Worksheet 5-7. Flow regime.

<b>FLOW REGIME</b>								
Stream: <b>Northfield Gulch F4b Poor</b>			Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>Rosgen et. al.</b>			Date: <b>11/2/2012</b>					
<b>List ALL COMBINATIONS that APPLY.....</b>	<b>P1</b>	<b>P2</b>	<b>P8</b>					
<b>General Category</b>								
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation							
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
<b>P</b>	Perennial stream channels: Surface water persists yearlong.							
<b>Specific Category</b>								
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
<b>4</b>	Streamflow regulated by glacial melt.							
<b>5</b>	Ice flows/ice torrents from ice dam breaches.							
<b>6</b>	Alternating flow/backwater due to tidal influence.							
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.							
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
<b>9</b>	Rain-on-snow generated runoff.							

**Worksheet 5-8.** Stream order & stream size.

Stream Size and Order			
Stream:	Northfield Gulch F4b Poor		
Location:	Pike National Forest, Colorado		
Observers:	Rosgen et. al.		
Date:	11/2/2012		
Stream Size Category and Order 			<b>S-3(3)</b>
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0.305	<1	<input type="checkbox"/>
S-2	0.3 – 1.5	1 – 5	<input type="checkbox"/>
<b>S-3</b>	<b>1.5 – 4.6</b>	<b>5 – 15</b>	<input checked="" type="checkbox"/>
S-4	4.6 – 9	15 – 30	<input type="checkbox"/>
S-5	9 – 15	30 – 50	<input type="checkbox"/>
S-6	15 – 22.8	50 – 75	<input type="checkbox"/>
S-7	22.8 – 30.5	75 – 100	<input type="checkbox"/>
S-8	30.5 – 46	100 – 150	<input type="checkbox"/>
S-9	46 – 76	150 – 250	<input type="checkbox"/>
S-10	76 – 107	250 – 350	<input type="checkbox"/>
S-11	107 – 150	350 – 500	<input type="checkbox"/>
S-12	150 – 305	500 – 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
Stream Order			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			

Worksheet 5-9. Meander patterns.

Meander Patterns					
Stream: <b>Northfield Gulch F4b Poor</b>		Location: <b>Pike National Forest, CO</b>			
Observers: <b>Rosgen et. al.</b>		Date: <b>11/2/2012</b>			
List ALL CATEGORIES that APPLY	<b>M3</b>				
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>					
 <b>M1 REGULAR MEANDERS</b>	 <b>M5 UNCONFINED MEANDER SCROLLS</b>				
 <b>M2 TORTUOUS MEANDERS</b>	 <b>M6 CONFINED MEANDER SCROLLS</b>				
 <b>M3 IRREGULAR MEANDERS</b>	 <b>M7 DISTORTED MEANDER LOOPS</b>				
 <b>M4 TRUNCATED MEANDERS</b>	 <b>M8 IRREGULAR MEANDERS with oxbows and oxbow cutoffs</b>				

**Worksheet 5-10.** Depositional patterns.

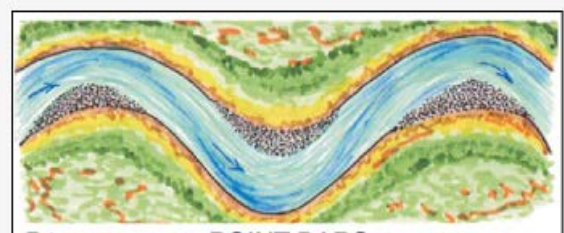
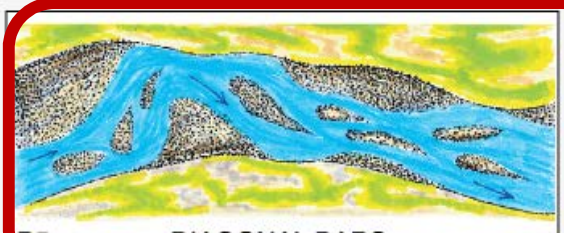
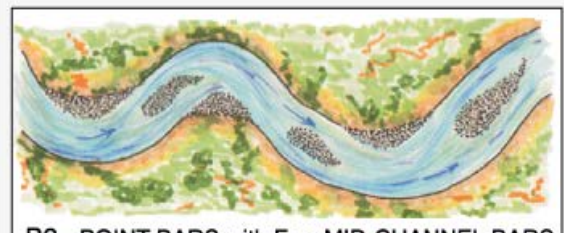

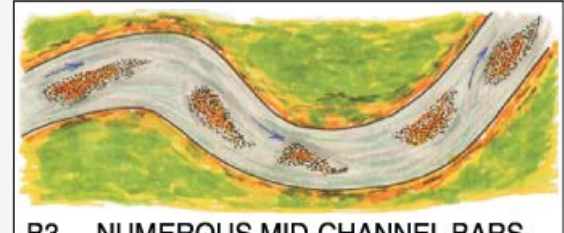


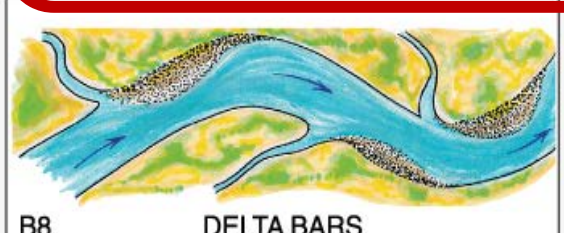
**Depositional Patterns**

Stream: **Northfield Gulch F4b Poor** Location: **Pike National Forest, Colorado**

Observers: **Rosgen et. al.** Date: **11/2/2012**

List ALL CATEGORIES that APPLY	<b>B5</b>	<b>B6</b>	<b>B7</b>		
--------------------------------	-----------	-----------	-----------	--	--

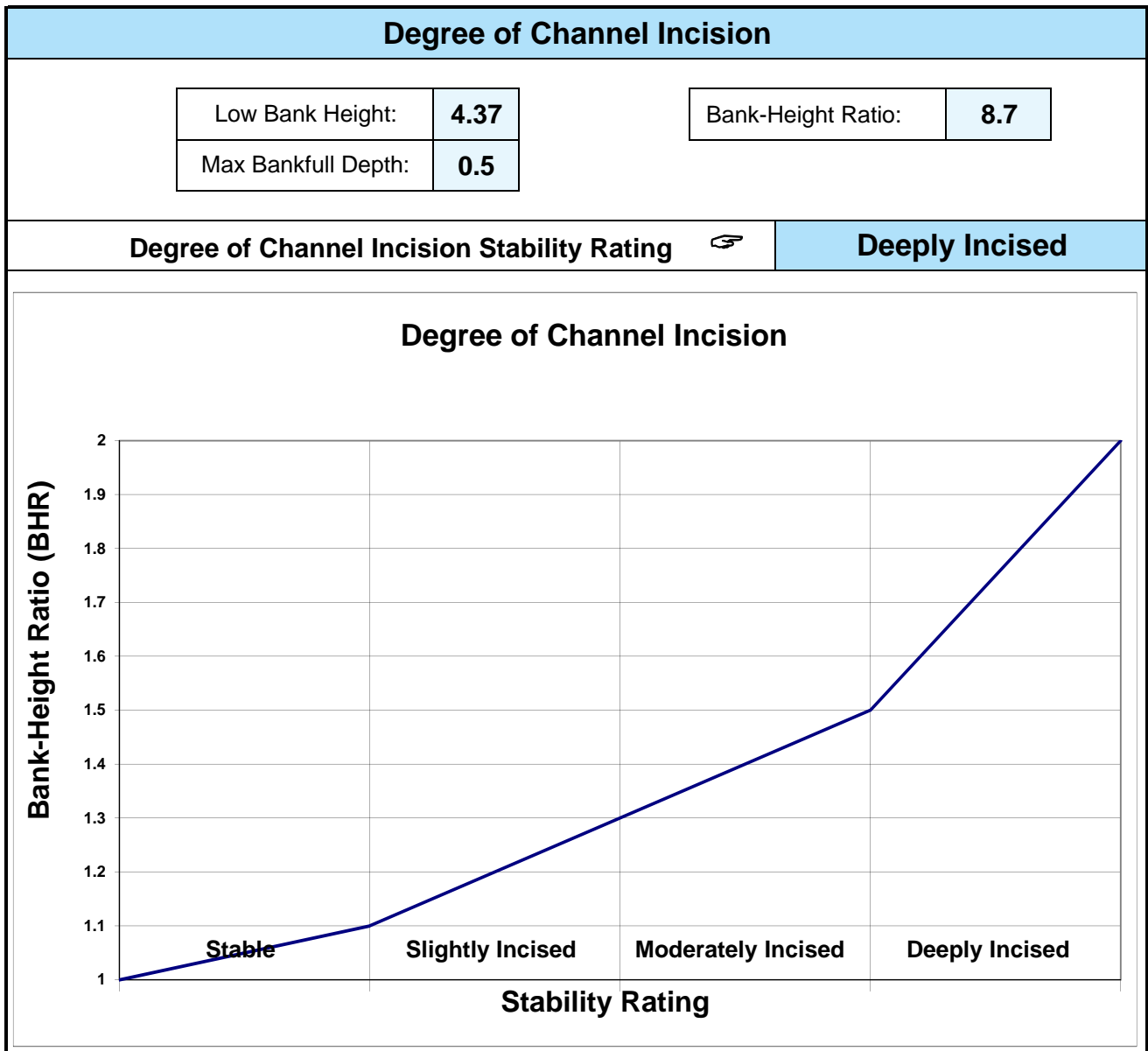
*Various Depositional Features modified from Galay et al. (1973)*

 <p><b>B1</b> POINT BARS</p>	 <p><b>B5</b> DIAGONAL BARS</p>
 <p><b>B2</b> POINT BARS with Few MID-CHANNEL BARS</p>	 <p><b>B6</b> Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</p>
 <p><b>B3</b> NUMEROUS MID-CHANNEL BARS</p>	 <p><b>B7</b> SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</p>
 <p><b>B4</b> SIDE BARS</p>	 <p><b>B8</b> DELTA BARS</p>

## Worksheet 5-11. Channel blockages.

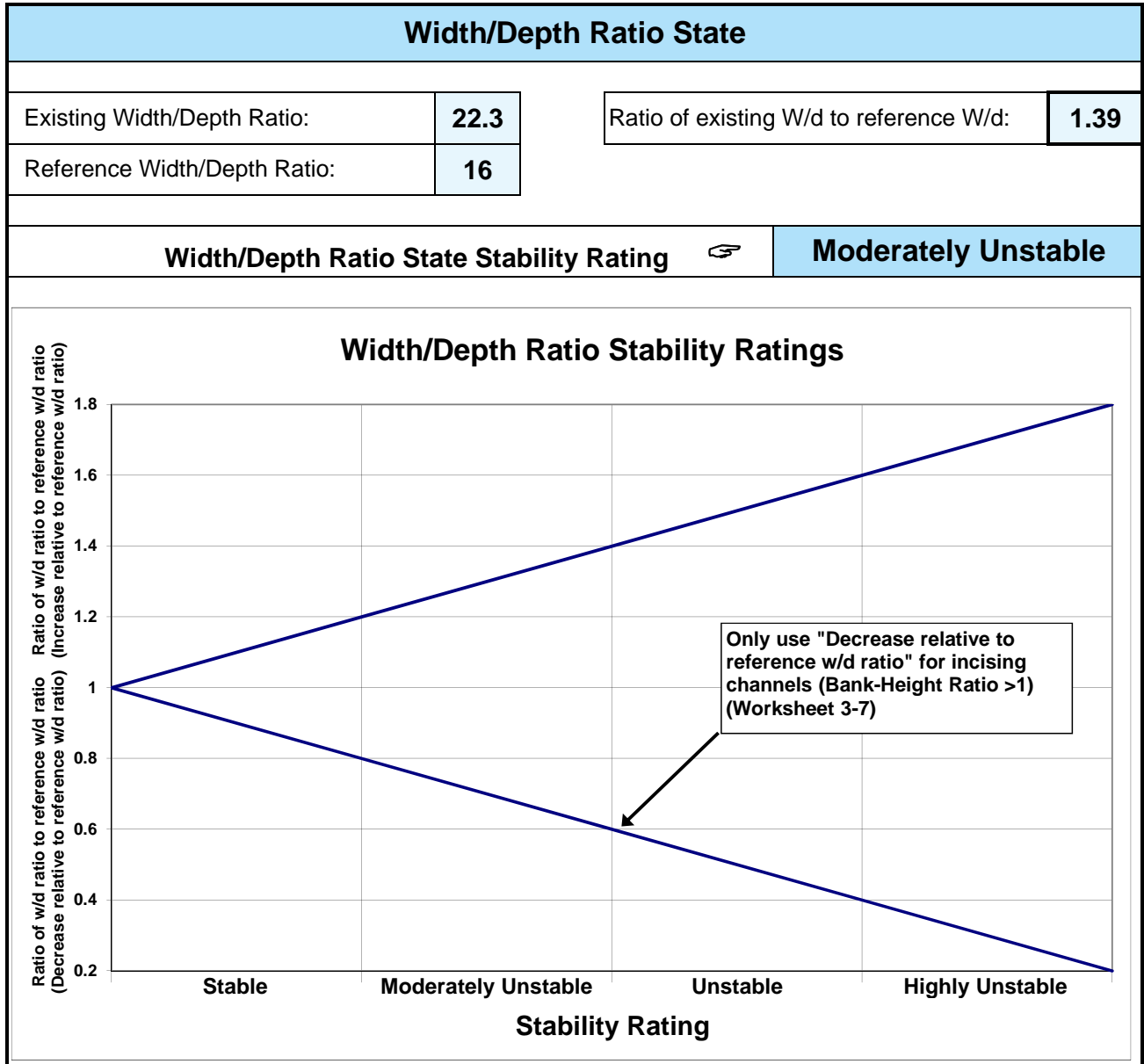
Channel Blockages		
Stream: <b>Northfield Gulch F4b Poor</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>Rosgen et. al.</b>		Date: <b>11/2/2012</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
D1 None	Minor amounts of small, floatable material.	<input type="checkbox"/>
D2 Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input checked="" type="checkbox"/>
D3 Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input type="checkbox"/>
D4 Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
D5 Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
D6 Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
D7 Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
D8 Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
D9 Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
D10 Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

**Worksheet 5-12.** Degree of channel incision.

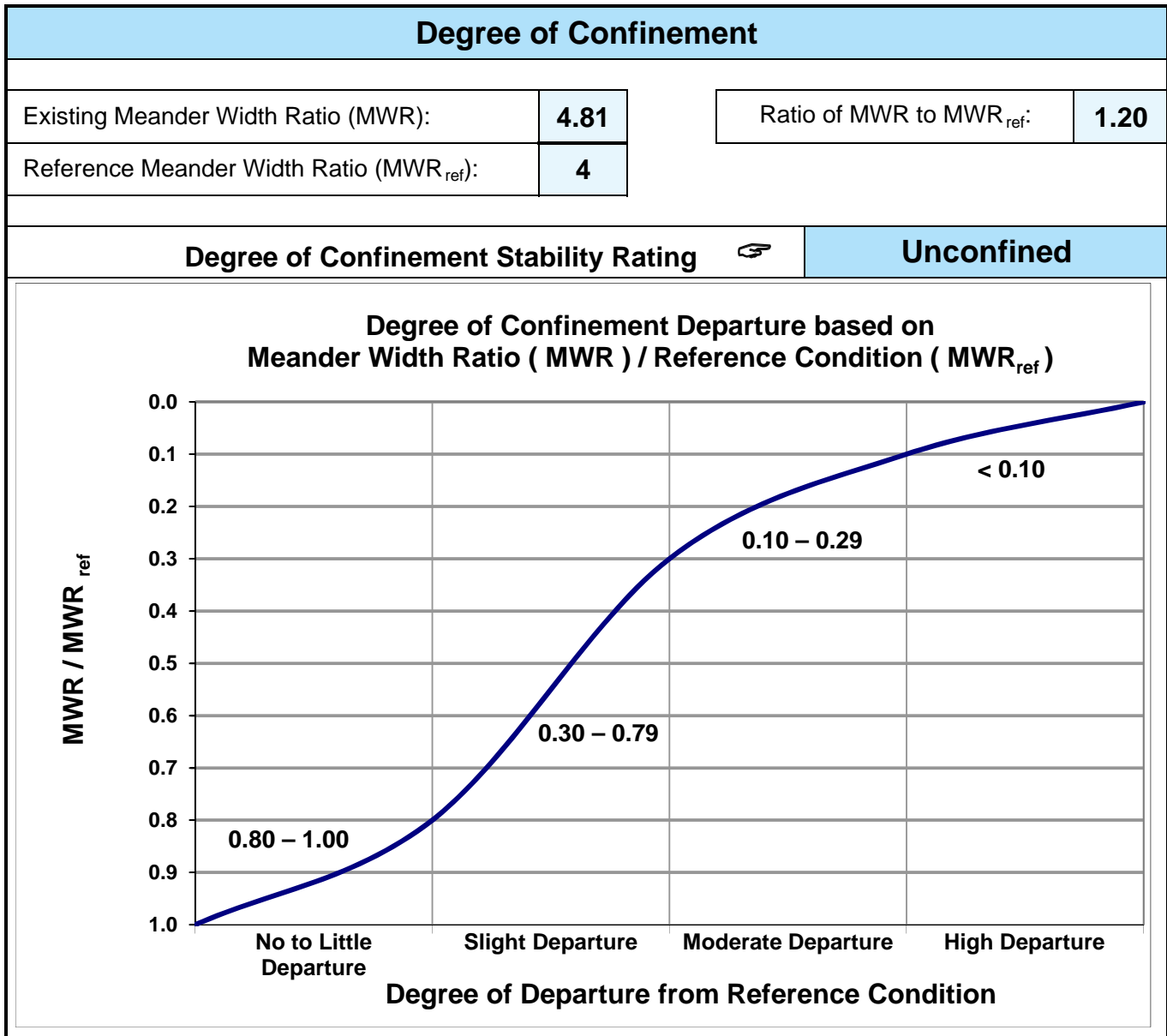




Worksheet 5-13. Width/depth ratio state.



**Worksheet 5-14.** Degree of channel confinement (lateral containment).



**Worksheet 5-15. Pfankuch channel stability rating.**

Stream: Northfield Gulch F4b Poor		Location: Pike National Forest, CO		Valley Type: Villa		Observers: Rosgen et al.		Date: 11/2/2012	
Loca-tion	Key	Category	Excellent	Good	Fair	Rating	Description	Rating	Description
			Description	Description	Description				
Upper banks	1	Landform slope	Bank slope gradient <30%.	Bank slope gradient 30–40%.	Bank slope gradient 40–60%.	4	Bank slope gradient > 60%.	6	Bank slope gradient > 60%.
	2	Mass erosion	No evidence of past or future mass erosion.	Infrequent. Mostly healed over. Low future potential.	Frequent or large, causing sediment nearly yearlong.	3	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.	9	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.
	3	Debris jam potential	Essentially absent from immediate channel area.	Present, but mostly small twigs and limbs.	Moderate to heavy amounts, mostly larger sizes.	2	Moderate to heavy amounts, mostly larger sizes.	5	Moderate to heavy amounts, predominantly larger sizes.
	4	Vegetative bank protection	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	70–90% density. Fewer species or less vigor suggest less dense or deep root mass.	50–70% density. Lower vigor and fewer species from a shallow, discontinuous root mass.	3	50–70% density. Lower vigor and fewer species from a shallow, discontinuous root mass.	9	>50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.
Lower banks	5	Channel capacity	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0–1.1.	Bankfull stage is contained within banks. Width/depth ratio departure from reference width/depth ratio = 1.0–1.2. Bank-Height Ratio (BHR) = 1.1–1.3.	Bankfull stage is not contained. Width/depth ratio departure from reference width/depth ratio = 1.2–1.4. Bank-Height Ratio (BHR) > 1.3.	1	Bankfull stage is not contained. Width/depth ratio departure from reference width/depth ratio = 1.2–1.4. Bank-Height Ratio (BHR) > 1.3.	2	Bankfull stage is not contained; over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.
	6	Bank rock content	> 65% with large angular boulders. 12"+ common.	40–65%. Mostly boulders and small cobbles 6–12".	20–40%. Most in the 3–6" diameter class.	2	40–65%. Mostly boulders and small cobbles 6–12".	4	<20% rock fragments of gravel sizes, 1–3" or less.
	7	Obstructions to flow	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	2	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	4	Frequent obstructions and deflectors cause bank erosion yearlong. Sediment traps full, channel migration occurring.
	8	Cutting	Little or none. Infrequent raw banks <6".	Some, intermittently at outcrops and constrictions. Raw banks may be up to 12".	Significant. Cuts 12–24" high. Root mat overhangs and sloughing evident.	4	Some, intermittently at outcrops and constrictions. Raw banks may be up to 12".	9	Almost continuous cuts, some over 24" high. Failure of overhangs frequent.
Bottom	9	Deposition	Little or no enlargement of channel or point bars.	Some new bar increase, mostly from coarse gravel.	Moderate deposition of new gravel and coarse sand on old and some new bars.	4	Little or no enlargement of channel or point bars.	8	Extensive deposit of predominantly fine particles. Accelerated bar development.
	10	Rock angularity	Sharp edges and corners. Plane surfaces rough.	Rounded corners and edges. Surfaces smooth and flat.	Comers and edges well rounded in 2 dimensions.	1	Sharp edges and corners. Plane surfaces rough.	2	Well rounded in all dimensions, surfaces smooth.
	11	Brightness	Surfaces dull, dark or stained. Generally not bright.	Mostly dull, but may have <35% bright surfaces.	Mixture dull and bright, i.e., 35–65% mixture range.	1	Surfaces dull, dark or stained. Generally not bright.	2	Predominantly bright, > 65%, exposed or scoured surfaces.
	12	Consolidation of particles	Assorted sizes tightly packed or overlapping.	Moderately packed with some overlapping.	Mostly loose assortment with no apparent overlap.	2	Assorted sizes tightly packed or overlapping.	4	No packing evident. Loose assortment, easily moved.
Stream type	13	Bottom size distribution	No size change evident. Stable material 80–100%.	Distribution shift light. Stable material 50–80%.	Moderate change in sizes. Stable materials 20–50%.	4	No size change evident. Stable material 80–100%.	8	Marked distribution change. Stable materials 0–20%.
	14	Scouring and deposition	<5% of bottom affected by scour or deposition.	5–30% affected. Scour at constrictions and where grades steeper. Some deposition in pools.	30–50% affected. Deposits and scour at obstructions, constrictions and bends. Some filling of pools.	4	<5% of bottom affected by scour or deposition.	12	More than 50% of the bottom in a state of flux or change nearly yearlong.
	15	Aquatic vegetation	Abundant growth moss-like, dark green perennial. In swift water too.	Common. Algae forms in low velocity and pool areas. Moss here too.	Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick.	1	Abundant growth moss-like, dark green perennial. In swift water too.	2	Perennial types scarce or absent. Yellow-green, short-term bloom may be present.
				<b>Excellent total = 0</b>	<b>Good total = 0</b>	<b>Fair total = 13</b>		<b>Poor total = 130</b>	
		<b>Grand total = 143</b>		<b>Existing stream type = F4b</b>		<b>*Potential stream type = B4</b>		<b>Modified channel stability rating = Poor</b>	

\*Rating is adjusted to potential stream type, not existing.

## BANCS Model – Streambank Erosion

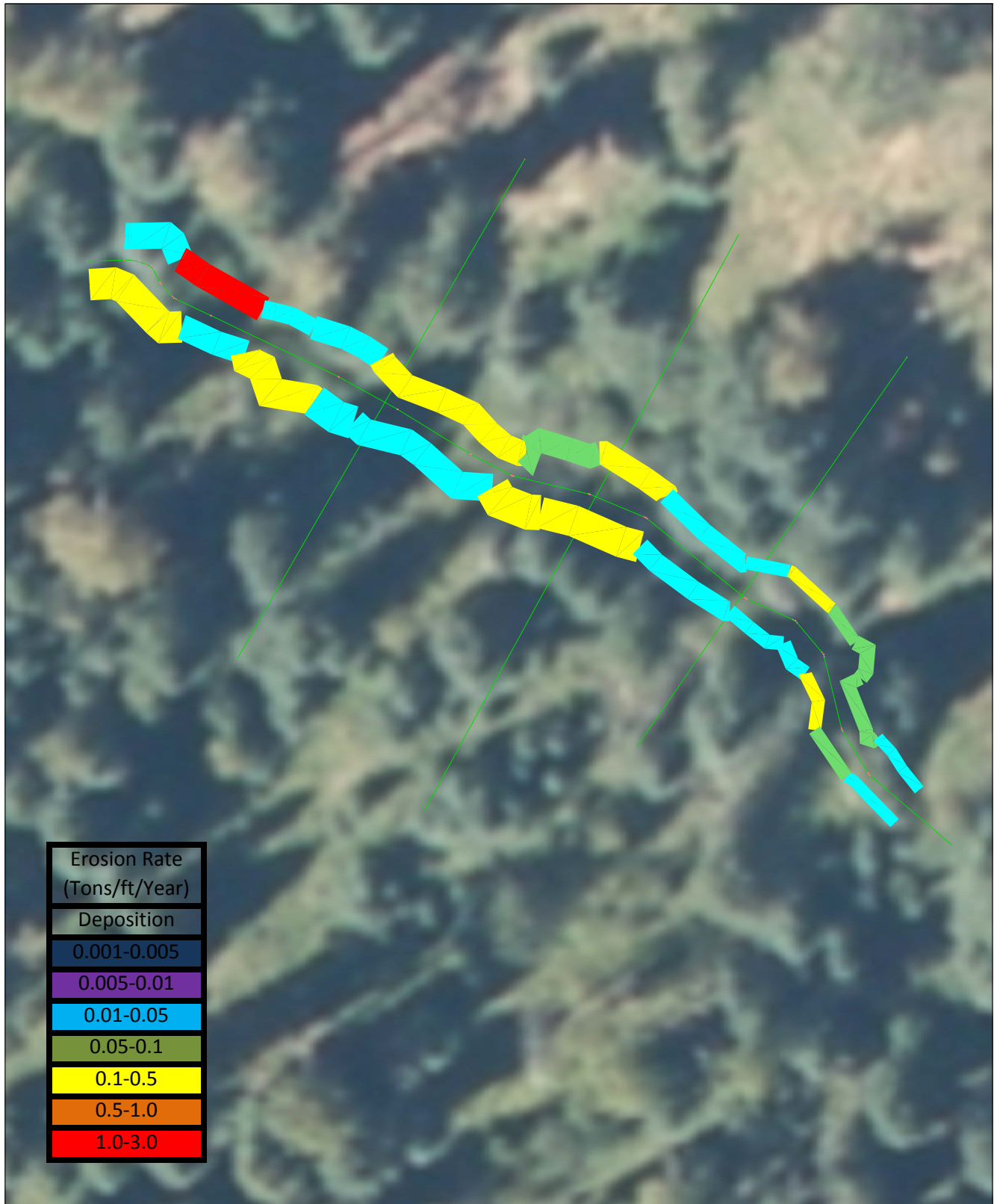
**Worksheet 5-18.** Annual streambank erosion estimates.

Stream: <b>Northfield Gulch Fb4 Poor</b>				Location: <b>Fb4 Poor</b>			
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>167</b>			Date: <b>11/2/2012</b>		
Observers: <b>Rosgen et. al.</b>		Valley Type: <b>Villa</b>		Stream Type: <b>F4b</b>			
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 3-11) (adjective)	NBS rating (Worksheet 3-12) (adjective)	Bank erosion rate (Figure 3-9 or 3-10) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [[ $(4) \times (5) \times (6)$ ] (ft <sup>3</sup> /yr)	Erosion Rate (tons/yr/ft) [[ $(7)/27$ ] × 1.3 / (5)]
1. L0 -12	Extreme	Very Low	0.165	12.0	4.3	8.51	0.03420
2. L12-28	Extreme	Very High	7.027	16.0	4.2	472.21	1.42100
3. L28-36	Extreme	Very Low	0.165	8.0	2.9	3.83	0.02300
4. L36-49	High	Very Low	0.165	13.0	3.9	8.36	0.03100
5. L49-75	Very High	High	0.664	26.0	4.2	72.52	0.13430
6. L78-88	Very High	Low	0.250	10.0	3.8	9.50	0.04570
7. L88-100	Very High	Low	0.529	12.0	3.8	24.12	0.09680
8. L100-116	Very High	Very Low	0.190	16.0	3.0	9.12	0.02744
9. L116-123	Very High	Very Low	0.165	7.0	2.1	2.42	0.01670
10. L123-131	Very High	Very High	2.066	8.0	2.0	32.40	0.19500
11. L131-135	High	Low	0.529	4.0	2.0	4.15	0.05000
12. L135-141	High	Low	0.529	6.0	2.5	7.94	0.06370
13. L141-152	High	Low	0.529	9.0	2.2	10.47	0.05600
14. L152-167	Moderate	Low	0.168	15.0	1.8	4.54	0.01460
15. R0-17	Very High	Very High	0.832	17.0	5.1	72.17	0.20440
16. R17-28	Very High	Very Low	0.190	11.0	4.0	8.36	0.03659
17. R28-42	High	High	0.664	14.0	4.9	45.56	0.15670
18. R42-49	High	Very Low	0.160	7.0	5.4	6.03	0.04150
19. R49-75	Moderate	Very Low	0.090	26.0	4.5	10.53	0.01950
20. R75-83	Very High	Moderate	0.380	8.0	5.7	17.33	0.10430
21. R83-100	Very High	Low	0.529	17.0	5.1	45.86	0.13000

**Worksheet 5-18, con't.** Annual streambank erosion estimates.

Stream: <b>Northfield Gulch Fb4 Poor</b>		Location: <b>Fb4 Poor</b>					
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>167</b>				Date: <b>11/2/2012</b>	
Observers: <b>Rosgen et. al.</b>		Valley Type: <b>VIIa</b>			Stream Type: <b>F4b</b>		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 3-11) (adjective)	NBS rating (Worksheet 3-12) (adjective)	Bank erosion rate (Figure 3-9 or 3-10) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [(4)×(5)×(6)] (ft <sup>3</sup> /yr)	Erosion Rate (tons/yr/ft) {[(7)/27] × 1.3 / (5)}
22 R100-119	Extreme	Very Low	0.200	19.0	3.3	12.54	0.03178
23 R119-124	Very High	Very Low	0.368	5.0	2.3	4.23	0.04070
24 R124-137	Low	Moderate	0.100	13.0	2.5	3.19	0.01180
25 R137-145	Very High	Very High	1.573	8.0	2.1	26.43	0.15910
26 R145-154	Very High	Low	0.529	9.0	2.1	10.00	0.05350
27 R154-167	Moderate	Low	0.168	13.0	1.9	4.04	0.01500
28							
29							
30							
31							
32							
33							
34							
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					Total Erosion (ft <sup>3</sup> /yr)	<b>936.36</b>	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					Total Erosion (yds <sup>3</sup> /yr)	<b>34.68</b>	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					Total Erosion (tons/yr)	<b>45.08</b>	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					Unit Erosion Rate (tons/yr/ft)	<b>0.2700</b>	

### Streambank Erosion Map



Erosion Rate (Tons/ft/Year)
Deposition
0.001-0.005
0.005-0.01
0.01-0.05
0.05-0.1
0.1-0.5
0.5-1.0
1.0-3.0

Waldo Canyon Fire WARSSS  
Typical Reach



Wildland Hydrology  
11210 North County Road 19  
Fort Collins, CO  
80524  
Tel. 970-568-0002  
Fax. 970.568.0014

# FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

(1)	From dimensioned flow-duration curve					From sediment rating curves					Calculate			Calculate sediment yield		
	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)		
Flow exceedence (%)	Daily mean discharge (cfs)	Mid-ordinate (%)	Time increment (percent)	Time increment (days)	Mid-ordinate streamflow (cfs)	Dimensionless streamflow	Dimensionless suspended sediment discharge ( $S/S_{bed}$ )	Suspended sediment discharge (tons/day)	Dimensionless bedload discharge ( $b/b_{bed}$ )	Bedload (tons/day)	Time adjusted streamflow (cfs)	Suspended sediment [(5)x(9)] (tons)	Bedload [(5)x(11)] (tons)	Suspended + bedload [(13)+(14)] (tons)		
100.000	0.0															
90.000	0.1	95.00	10.00	36.50	0.1	0.02	5.9	0.0	0.0253	0.00	0.50	0.00	0.00	0.00		
80.000	0.1	85.00	10.00	36.50	0.1	0.04	5.9	0.0	0.0253	0.00	1.00	0.00	0.00	0.00		
70.000	0.1	75.00	10.00	36.50	0.1	0.05	5.9	0.0	0.0253	0.00	1.10	0.00	0.00	0.00		
60.000	0.2	65.00	10.00	36.50	0.1	0.06	5.9	0.0	0.0253	0.00	1.40	0.00	0.00	0.00		
50.000	0.2	55.00	10.00	36.50	0.2	0.07	5.9	0.0	0.0253	0.00	1.70	0.00	0.00	0.00		
40.000	0.3	45.00	10.00	36.50	0.2	0.10	5.9	0.0	0.0253	0.00	2.30	0.00	0.00	0.00		
30.000	0.4	35.00	10.00	36.50	0.3	0.14	5.9	0.0	0.0259	0.00	3.20	0.00	0.00	0.00		
20.000	0.6	25.00	10.00	36.50	0.5	0.20	6.0	0.0	0.0288	0.00	4.60	0.00	0.00	0.00		
10.000	1.0	15.00	10.00	36.50	0.8	0.34	6.4	0.0	0.0394	0.04	7.80	0.00	1.46	1.46		
5.000	1.6	7.50	5.00	18.25	1.3	0.57	9.0	0.0	0.0754	0.09	6.55	0.00	1.64	1.64		
4.000	1.8	4.50	1.00	3.65	1.7	0.74	13.8	0.0	0.1196	0.17	1.71	0.00	0.62	0.62		
3.000	2.1	3.50	1.00	3.65	2.0	0.85	19.0	0.0	0.1565	0.22	1.96	0.00	0.80	0.80		
2.000	2.5	2.50	1.00	3.65	2.3	1.00	29.5	0.0	0.2189	0.35	2.31	0.00	1.28	1.28		
1.500	2.9	1.75	0.50	1.83	2.7	1.16	47.2	0.0	0.3042	0.48	1.34	0.00	0.88	0.88		
1.000	3.5	1.25	0.50	1.83	3.2	1.38	82.3	0.0	0.4434	0.69	1.59	0.02	1.26	1.28		
0.900	3.7	0.95	0.10	0.37	3.6	1.57	113.4	0.0	0.5477	0.91	0.36	0.00	0.33	0.33		
0.800	4.0	0.85	0.10	0.37	3.8	1.66	113.4	0.0	0.5477	1.04	0.38	0.00	0.38	0.38		
0.700	4.2	0.75	0.10	0.37	4.1	1.75	113.4	0.0	0.5477	1.17	0.41	0.00	0.43	0.43		
0.600	4.4	0.65	0.10	0.37	4.3	1.86	113.4	0.0	0.5477	1.30	0.43	0.01	0.47	0.48		
0.500	4.7	0.55	0.10	0.37	4.6	1.99	113.4	0.0	0.5477	1.51	0.46	0.01	0.55	0.56		
0.250	5.5	0.38	0.25	0.91	5.1	2.22	113.4	0.0	0.5477	1.94	1.28	0.03	1.77	1.80		
0.100	6.4	0.18	0.15	0.55	5.9	2.56	113.4	0.0	0.5477	2.64	0.89	0.02	1.45	1.47		
0.050	6.8	0.08	0.05	0.18	6.6	2.84	113.4	0.1	0.5477	3.33	0.33	0.01	0.61	0.62		
0.010	7.4	0.03	0.04	0.15	7.1	3.07	113.4	0.1	0.5477	3.93	0.28	0.01	0.57	0.58		
0.005	7.4	0.01	0.01	0.02	7.4	3.20	113.4	0.1	0.5477	4.32	0.04	0.00	0.08	0.08		
0.001	7.4	0.00	0.00	0.01	7.4	3.20	113.4	0.1	0.5477	4.32	0.03	0.00	0.06	0.06		
Annual totals:											0.1 (tons/yr)	14.6 (tons/yr)	14.7 (tons/yr)			

**Worksheet 19b.** Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

From dimensioned flow-duration curve				From sediment rating curves				Calculate		Calculate sediment yield				
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Flow exceedence (%)	Daily mean discharge (cfs)	Mid-ordinate (%)	Time increment (percent)	Time increment (days)	Mid-ordinate streamflow (cfs)	Dimensionless streamflow	Dimensionless suspended sediment discharge ( $S/S_{bed}$ )	Suspended sediment discharge (tons/day)	Dimensionless bedload discharge	Bedload (tons/day)	Time adjusted streamflow (cfs)	Suspended sediment [(5)×(9)] (tons)	Bedload sediment [(5)×(11)] (tons)	Suspended + bedload [(13)+(14)] (tons)
			(%)	(days)		( $Q/Q_{bed}$ )			( $b_y/b_{bed}$ )					
100.000	0.0													
90.000	0.1	95.00	10.00	36.50	0.0	0.02	5.9	0.0	0.0253	1.04	0.40	0.00	37.96	37.96
80.000	0.1	85.00	10.00	36.50	0.1	0.04	5.9	0.0	0.0253	1.04	1.00	0.00	37.96	37.96
70.000	0.1	75.00	10.00	36.50	0.1	0.05	5.9	0.0	0.0253	1.04	1.10	0.00	37.96	37.96
60.000	0.2	65.00	10.00	36.50	0.1	0.06	5.9	0.0	0.0253	1.04	1.40	0.00	37.96	37.96
50.000	0.2	55.00	10.00	36.50	0.2	0.07	5.9	0.0	0.0253	1.04	1.70	0.00	37.96	37.96
40.000	0.3	45.00	10.00	36.50	0.2	0.10	5.9	0.0	0.0253	1.08	2.30	0.00	39.42	39.42
30.000	0.4	35.00	10.00	36.50	0.3	0.14	6.0	0.0	0.0261	1.12	3.30	0.36	40.88	41.24
20.000	0.8	25.00	10.00	36.50	0.6	0.26	6.1	0.0	0.0324	1.38	6.10	0.36	50.37	50.73
10.000	1.7	15.00	10.00	36.50	1.2	0.54	8.5	0.0	0.0689	2.94	12.40	1.09	107.31	108.40
5.000	2.5	7.50	5.00	18.25	2.1	0.90	22.0	0.1	0.1760	7.56	10.40	2.19	137.97	140.16
4.000	2.7	4.50	1.00	3.65	2.6	1.12	41.7	0.3	0.2798	12.05	2.59	1.06	43.98	45.04
3.000	3.1	3.50	1.00	3.65	2.9	1.25	59.3	0.5	0.3558	15.34	2.89	1.68	55.99	57.67
2.000	3.5	2.50	1.00	3.65	3.3	1.42	89.9	0.8	0.4693	20.22	3.27	2.88	73.80	76.68
1.500	3.9	1.75	0.50	1.83	3.7	1.59	113.4	1.3	0.5477	26.31	1.83	2.41	48.02	50.43
1.000	4.5	1.25	0.50	1.83	4.2	1.81	113.4	2.4	0.5477	35.47	2.09	4.34	64.73	69.07
0.900	4.7	0.95	0.10	0.37	4.6	2.00	113.4	3.7	0.5477	44.45	0.46	1.36	16.22	17.58
0.800	4.9	0.85	0.10	0.37	4.8	2.09	113.4	4.6	0.5477	49.55	0.48	1.68	18.09	19.77
0.700	5.2	0.75	0.10	0.37	5.0	2.18	113.4	5.6	0.5477	54.73	0.50	2.05	19.98	22.03
0.600	5.4	0.65	0.10	0.37	5.3	2.29	113.4	7.0	0.5477	61.30	0.53	2.56	22.37	24.93
0.500	5.7	0.55	0.10	0.37	5.6	2.42	113.4	9.0	0.5477	69.42	0.56	3.27	25.34	28.61
0.250	6.5	0.38	0.25	0.91	6.1	2.65	113.4	13.7	0.5477	85.88	1.53	12.46	78.37	90.83
0.100	7.3	0.18	0.15	0.55	6.9	2.99	113.4	24.2	0.5477	114.74	1.04	13.23	62.82	76.05
0.050	7.8	0.08	0.05	0.18	7.6	3.27	113.4	36.7	0.5477	141.83	0.38	6.70	25.88	32.58
0.010	8.4	0.03	0.04	0.15	8.1	3.50	113.4	50.0	0.5477	165.93	0.32	7.30	24.23	31.53
0.005	8.4	0.01	0.01	0.02	8.4	3.63	113.4	59.2	0.5477	180.88	0.04	1.08	3.30	4.38
0.001	8.4	0.00	0.00	0.01	8.4	3.63	113.4	59.2	0.5477	180.88	0.03	0.86	2.64	3.50
Annual totals:											68.9 (tons/yr)	1151.5 (tons/yr)	1220.4 (tons/yr)	



# POWERSED Model – Sediment Transport Capacity

**Worksheet 20a.** Sediment transport prediction representing the upstream supply up to bankfull for bedload and suspended sand sediment.

Flow-duration curve			Calculate				Hydraulic geometry				Measure		Calculate					
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	
Percentage of time	Daily mean discharge	Mid-ordinate stream-flow	Area	Width	Depth	Velocity	Slope	Shear stress	Stream power	Unit power	Time increment	Time increment	Daily mean bedload transport	Daily mean suspended sand transport	Time adjusted bedload transport [(13)×(14)]	Time adjusted suspended sand transport [(13)×(15)]	Time adjusted total transport [(16)+(17)]	
(%)	(cfs)	(cfs)	(ft <sup>2</sup> )	(ft)	(ft)	(ft/s)	(ft/ft)	(lb/ft <sup>2</sup> )	(lb/s)	(lb/ft/s)	(%)	(days)	(tons/day)	(tons/day)	(tons)	(tons)	(tons)	
100.000	0.01									0.00					0.00	0.00	0.00	
90.000	0.08	0.04	0.09	1.92	0.05	0.63	0.0360	0.10	0.09	0.05	10.000	36.50	0.00	0.00	0.00	0.00	0.00	
80.000	0.11	0.10	0.13	2.02	0.06	0.72	0.0360	0.14	0.22	0.11	10.000	36.50	1.04	0.00	38.00	0.00	38.00	
70.000	0.12	0.11	0.14	2.03	0.07	0.73	0.0360	0.15	0.25	0.12	10.000	36.50	1.04	0.00	38.00	0.00	38.00	
60.000	0.15	0.14	0.16	2.08	0.08	0.78	0.0360	0.17	0.31	0.15	10.000	36.50	1.04	0.00	38.00	0.00	38.00	
50.000	0.20	0.17	0.18	2.13	0.08	0.82	0.0360	0.19	0.38	0.18	10.000	36.50	1.04	0.00	38.00	0.00	38.00	
40.000	0.26	0.23	0.22	2.23	0.10	0.90	0.0360	0.22	0.52	0.23	10.000	36.50	1.08	0.00	39.00	0.00	39.00	
30.000	0.40	0.33	0.29	2.39	0.12	1.05	0.0360	0.27	0.74	0.31	10.000	36.50	1.12	0.01	41.00	0.00	41.00	
20.000	0.82	0.61	0.45	2.67	0.17	1.31	0.0360	0.37	1.37	0.51	10.000	36.50	1.38	0.01	50.00	0.00	51.00	
10.000	1.67	1.24	0.73	3.02	0.24	1.66	0.0360	0.52	2.79	0.92	10.000	36.50	2.94	0.03	107.00	1.00	108.00	
5.000	2.48	2.08	1.07	3.48	0.31	1.94	0.0360	0.66	4.67	1.34	5.000	18.25	7.56	0.12	138.00	2.00	140.00	
4.000	2.71	2.59	1.27	3.86	0.33	2.04	0.0360	0.70	5.82	1.51	1.000	3.65	11.97	0.19	44.00	1.00	44.00	
3.000	3.07	2.89																
2.000	3.48	3.27																
1.500	3.87	3.67																
1.000	4.49	4.18																
0.900	4.72	4.61																
0.800	4.94	4.83																
0.700	5.15	5.04																
0.600	5.43	5.29																
0.500	5.73	5.58																
0.250	6.48	6.11																
0.100	7.34	6.91																
0.050	7.78	7.56																
0.010	8.38	8.08																
0.005	8.38	8.38																
0.001	8.38	8.38																
														Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr):		571.7	4.8	576.3

**Worksheet 20b.** Sediment transport prediction for the existing condition reach compared to the upstream sediment supply to assess bed stability.

(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)		
Percentage of time	Daily mean discharge (cfs)	Mid-ordinate stream-flow (cfs)	Area (ft <sup>2</sup> )	Width (ft)	Depth (ft)	Velocity (ft/s)	Slope (ft/ft)	Shear stress (lb/ft <sup>2</sup> )	Stream power (lb/s)	Unit power (lb/ft/s)	Time increment (%)	Time increment (days)	Daily mean bedload transport (tons/day)	Daily mean suspended sand transport (tons/day)	Time adjusted bedload transport [(13)x(14)] (tons)	Time adjusted suspended sand transport [(13)x(15)] (tons)	Time adjusted total transport [(16)+(17)] (tons)		
100.000	0.01								0.00						0.00	0.00	0.00		
90.000	0.08	0.04	0.06	1.40	0.04	0.59	0.0360	0.09	0.09	0.06	10.000	36.50	1.04	0.00	38.00	0.00	38.00		
80.000	0.11	0.10	0.11	1.71	0.06	0.73	0.0360	0.14	0.22	0.13	10.000	36.50	1.04	0.00	38.00	0.00	38.00		
70.000	0.12	0.11	0.11	1.76	0.06	0.75	0.0360	0.14	0.25	0.14	10.000	36.50	1.04	0.00	38.00	0.00	38.00		
60.000	0.15	0.14	0.14	1.92	0.07	0.82	0.0360	0.16	0.31	0.16	10.000	36.50	1.04	0.00	38.00	0.00	38.00		
50.000	0.20	0.17	0.16	2.07	0.08	0.89	0.0360	0.17	0.38	0.18	10.000	36.50	1.04	0.00	38.00	0.00	38.00		
40.000	0.26	0.23	0.21	2.38	0.09	1.03	0.0360	0.19	0.52	0.22	10.000	36.50	1.08	0.00	39.00	0.00	39.00		
30.000	0.40	0.33	0.27	2.63	0.10	1.15	0.0360	0.22	0.74	0.28	10.000	36.50	1.12	0.01	41.00	0.00	41.00		
20.000	0.82	0.61	0.42	3.10	0.14	1.36	0.0360	0.29	1.37	0.44	10.000	36.50	1.30	0.01	47.00	0.00	48.00		
10.000	1.67	1.24	0.76	4.39	0.17	1.61	0.0360	0.37	2.79	0.64	10.000	36.50	1.86	0.02	68.00	1.00	69.00		
5.000	2.48	2.08	1.12	5.41	0.21	1.82	0.0360	0.45	4.67	0.86	5.000	18.25	2.72	0.04	50.00	1.00	50.00		
4.000	2.71	2.59	1.28	5.53	0.23	1.97	0.0360	0.50	5.82	1.05	1.000	3.65	4.36	0.09	16.00	0.00	16.00		
3.000	3.07	2.89	1.38	5.59	0.25	2.05	0.0360	0.53	6.49	1.16	1.000	3.65	5.57	0.13	20.00	0.00	21.00		
2.000	3.48	3.27																	
1.500	3.87	3.67																	
1.000	4.49	4.18																	
0.900	4.72	4.61																	
0.800	4.94	4.83																	
0.700	5.15	5.04																	
0.600	5.43	5.29																	
0.500	5.73	5.58																	
0.250	6.48	6.11																	
0.100	7.34	6.91																	
0.050	7.78	7.56																	
0.010	8.38	8.08																	
0.005	8.38	8.38																	
0.001	8.38	8.38																	
Notes:																			
															Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr):		471.5	3.0	474.4
															Upstream total annual sediment comparative reach (tons/yr) (WS 5-20a):		571.5	4.7	576.2
															Difference in sediment transport capacity (tons/yr) (+ or -):		-100.0	-1.7	-101.8
Stability evaluation: Aggradation, Degradation or Stable:																			
<b>Aggradation</b>																			

## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>Northfield Gulch F4b Poor</b>		Stream Type: <b>F4b</b>	
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>Villa</b>	
Observers: <b>Rosgen et. al.</b>		Date: <b>11/2/2012</b>	
<b>Enter Required Information for Existing Condition</b>			
4.8	$D_{50}$	Riffle bed material $D_{50}$ (mm)	
0.0	$\hat{D}_{50}$	Bar sample $D_{50}$ (mm)	
0.410	$D_{max}$	Largest particle from <b>Bed Material</b> (ft)	125 (mm) 304.8 mm/ft
0.03500	$S$	Existing bankfull water surface slope (ft/ft)	
0.26	$d$	Existing bankfull mean depth (ft)	
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment	
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>			
N/A	$D_{50}/\hat{D}_{50}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 (D_{50}/\hat{D}_{50})^{-0.872}$
N/A	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 (D_{max}/D_{50})^{-0.887}$
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED: <b>2</b>
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>			
N/A	$d$	Required bankfull mean depth (ft)	$d = \frac{\tau^* (\gamma_s - 1) D_{max}}{S}$ (use $D_{max}$ in ft)
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>			
N/A	$S$	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^* (\gamma_s - 1) D_{max}}{d}$ (use $D_{max}$ in ft)
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading			
<b>Sediment Competence Using Dimensional Shear Stress</b>			
0.568	Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d) $\gamma = 62.4$ , $d =$ existing depth, $S =$ existing slope		
Shields 43.23	CO 100.3	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ (Figure 5-49)	
Shields 1.573	CO 0.766	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) (Figure 5-49)	
Shields 0.72	CO 0.35	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm) $\tau =$ predicted shear stress, $\gamma = 62.4$ , $S =$ existing slope	$d = \frac{\tau}{\gamma S}$
Shields 0.0970	CO 0.0472	Predicted slope required to initiate movement of measured $D_{max}$ (mm) $\tau =$ predicted shear stress, $\gamma = 62.4$ , $d =$ existing depth	$S = \frac{\tau}{\gamma d}$
Check: <input type="checkbox"/> Stable <input checked="" type="checkbox"/> Aggrading <input type="checkbox"/> Degrading			

## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>Northfield Gulch F4b Poor</b>	Stream Type: <b>F4b</b>
Location: <b>Pike National Forest, CO</b>	Valley Type: <b>VIIa</b>
Observers: <b>Rosgen et. al.</b>	Date: <b>11/2/2012</b>
Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)	Stability Rating (Check Appropriate Rating)
Stream Type at potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	<input type="checkbox"/> Stable
(E→C), (C→High W/d C)	<input type="checkbox"/> Moderately Unstable
(G→F), (F→D), (C→F)	<input checked="" type="checkbox"/> Unstable
(C→D), (B→G), (D→G), (C→G), (E→G)	<input type="checkbox"/> Highly Unstable

Worksheet 5-25. Lateral stability.

Stream: <b>Northfield Gulch F4b Poor</b>		Stream Type: <b>F4b</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIIa</b>			
Observers: <b>Rosgen et. al.</b>		Date: <b>11/2/2012</b>			
Lateral stability criteria (choose one stability category for each criterion 1–5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	6
	(2)	(4)	(6)	(8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	4
	(1)	(2)	(3)	(4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		1
	(1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	8
	(2)	(4)	(6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	1
	(1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>20</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input type="checkbox"/>	<i>Unstable</i> 13 – 21 <input checked="" type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	

**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>Northfield Gulch F4b Poor</b>		Stream Type: <b>F4b</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIa</b>			
Observers: <b>Rosgen et. al.</b>		Date: <b>11/2/2012</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
1 <b>Sediment competence (Worksheet 5-22)</b>	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope—slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	4
	(2)	(4)	(6)	(8)	
2 <b>Sediment Capacity (POWERSED) (Worksheet 5-20)</b>	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	8
	(2)	(4)	(6)	(8)	
3 <b>W/d Ratio State (Worksheet 5-13)</b>	1.0 – 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	6
	(2)	(4)	(6)	(8)	
4 <b>Stream Succession States (Worksheet 5-24)</b>	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	6
	(2)	(4)	(6)	(8)	
5 <b>Depositional Patterns (Worksheet 5-10)</b>	B1	B2, B4	B3, B5	B6, B7, B8	1
	(1)	(2)	(3)	(4)	
6 <b>Debris / Blockages (Worksheet 5-11)</b>	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	1
	(1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>26</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
Vertical Stability for Excess Deposition / Aggradation (use total points and check stability rating)	<i>No Deposition</i> 10 – 14 <input type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input checked="" type="checkbox"/>	<i>Aggradation</i> > 30 <input type="checkbox"/>	

Worksheet 5-27. Vertical stability – degradation.

Stream: <b>Northfield Gulch F4b Poor</b>		Stream Type: <b>F4b</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIa</b>			
Observers: <b>Rosgen et. al.</b>		Date: <b>11/2/2012</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>1 Sediment Competence (Worksheet 5-22)</b>	Does not indicate excess competence <b>(2)</b>	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed <b>(4)</b>	$D_{100}$ of bed moved <b>(6)</b>	Particles much larger than $D_{100}$ of bed moved <b>(8)</b>	<b>2</b>
<b>2 Sediment Capacity (POWERSED) (Worksheet 5-20)</b>	Does not indicate excess capacity <b>(2)</b>	Slight excess energy: up to 10% increase above reference <b>(4)</b>	Excess energy sufficient to increase load up to 50% of annual load <b>(6)</b>	Excess energy transporting more than 50% of annual load <b>(8)</b>	<b>2</b>
<b>3 Degree of Channel Incision (BHR) (Worksheet 5-12)</b>	1.00 – 1.10 <b>(2)</b>	1.11 – 1.30 <b>(4)</b>	1.31 – 1.50 <b>(6)</b>	> 1.50 <b>(8)</b>	<b>8</b>
<b>4 Stream Succession States (Worksheets 5-12 and 5-24)</b>	Does not indicate incision or degradation <b>(2)</b>	If BHR > 1.1 and stream type has W/d between 5–10 <b>(4)</b>	If BHR > 1.1 and stream type has W/d less than 5 <b>(6)</b>	(B→G), (C→G), (E→G), (D→G) <b>(8)</b>	<b>2</b>
<b>5 Confinement (MWR / MWR<sub>ref</sub>) (Worksheet 5-14)</b>	0.80 – 1.00 <b>(1)</b>	0.30 – 0.79 <b>(2)</b>	0.10 – 0.29 <b>(3)</b>	< 0.10 <b>(4)</b>	<b>1</b>
<b>Total Points</b>					<b>15</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation (use total points and check stability rating)</b>	<i>Not Incised</i> 9 – 11 <input type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input checked="" type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input type="checkbox"/>	<i>Degradation</i> > 27 <input type="checkbox"/>	

**Worksheet 5-28.** Channel enlargement.

Stream: <b>Northfield Gulch F4b Poor</b>		Stream Type: <b>F4b</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIa</b>			
Observers: <b>Rosgen et. al.</b>		Date: <b>11/2/2012</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1-4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	6
	(2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	6
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	6
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	4
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>22</b>
<b>Category Point Range</b>					
<b>Channel Enlargement Prediction (use total points and check stability rating)</b>	<i>No Increase</i> 8 – 10 <input type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input checked="" type="checkbox"/>	<i>Extensive</i> > 24 <input type="checkbox"/>	



Worksheet 5-29. Overall sediment supply.

Stream: <b>Northfield Gulch F4b Poor</b>		Stream Type: <b>F4b</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIa</b>		
Observers: <b>Rosgen et. al.</b>		Date: <b>11/2/2012</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1–5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	3	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	3	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	2	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	3	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	4	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>15</b>	
<b>Category Point Range</b>				
Overall Sediment Supply Rating (use total points and check stability rating)	<i>Low</i> 5 <input type="checkbox"/>	<i>Moderate</i> 6 – 10 <input type="checkbox"/>	<i>High</i> 11 – 15 <input checked="" type="checkbox"/>	<i>Very High</i> 16 – 20 <input type="checkbox"/>

Worksheet 5-32. Summary of stability condition categories.

Stream: <b>Northfield Gulch F4b Poor</b>		Location: <b>Pike National Forest, Colorado</b>	
Observers: <b>Rosgen et. al.</b>		Valley Type: <b>VIIa</b>	
Date: <b>11/2/2012</b>		Stream Type: <b>F4b</b>	
Channel Dimension	Mean Bankfull Depth (ft): <b>0.26</b>	Bankfull Width (ft): <b>5.8</b>	Cross-Sectional Area (ft <sup>2</sup> ): <b>1.53</b>
	Width of Flood-Prone Area (ft): <b>22.31</b>	Entrenchment Ratio: <b>1.06</b>	
Channel Pattern	Mean: $L_m/W_{bkt}$ : <b>10.86</b>	$R_d/W_{bkt}$ : <b>11.72</b>	MWR: <b>4.31</b>
	Range: $L_m/W_{bkt}$ : <b>0.00 - 0.00</b>	$R_d/W_{bkt}$ : <b>0.00 - 0.00</b>	Sinuosity: <b>1.05</b>
River Profile & Bed Features	Check: <input type="checkbox"/> Riffle/Pool <input type="checkbox"/> Step/Pool <input checked="" type="checkbox"/> Plane Bed <input type="checkbox"/> Convergence/Divergence <input type="checkbox"/> Dunes/Antidunes/Smooth Bed	Riffle Pool	Pool-to-Pool Ratio
	Max Bankfull Depth (ft): <b>0.53</b>	Depth Ratio (max to mean): <b>2.04</b>	Valley: <b>0.0378</b>
Level III Stream Stability Indices	Riparian Vegetation: <b>&lt; 5% Annual Grass/Forb</b>	Potential Composition/Density: <b>Willow/Alder/Grass/Aspen</b>	Remarks: Condition, Vigor & Usage of Existing Reach: <b>Burnt, 5% Ponderosa Pine Aerial</b>
	Flow Regime: <b>P1, P2, P8 &amp; Order: S-3(3)</b>	Meander Patterns: <b>M3</b>	Debris/Channel Blockages: <b>B5, B6, B7 D2</b>
Bank Erosion Summary	Degree of Incision (Bank-Height Ratio): <b>8.7</b>	Degree of Incision Stability Rating: <b>Deeply Incised</b>	Modified Pfankuch Stability Rating: <b>143 (Poor)</b>
	Width/depth Ratio (W/d): <b>52</b>	Reference W/d Ratio (W/d <sub>ref</sub> ): <b>12.6</b>	W/d Ratio State Stability Rating: <b>Highly Unstable</b>
Sediment Capacity (POWERSED)	Meander Width Ratio (MWR): <b>4.81</b>	Reference MWR <sub>ref</sub> : <b>4</b>	MWR / MWR <sub>ref</sub> Stability Rating: <b>Unstable</b>
	Length of Reach Studied (ft): <b>167</b>	Annual Streambank Erosion Rate: <b>43.13</b> (tons/yr)	Curve Used: <b>Colorado</b>
Entrainment/Competence	<input type="checkbox"/> Sufficient Capacity <input type="checkbox"/> Insufficient Capacity <input checked="" type="checkbox"/> Excess Capacity	Remarks: <b>Used Yellowstone curve for very low BEHI</b>	
	Largest Particle from Bar Sample (mm): <b>125</b>	$\tau =$ <b>0.528</b>	$\tau^* =$ <b>N/A</b>
Successional Stage Shift	$\tau =$ <b>G</b> → <b>Fb</b> → <b>B</b> → <b>A</b>	Existing Depth: <b>0.19</b>	Required Depth: <b>0.07</b>
	<b>B</b> → <b>G</b> → <b>Fb</b> → <b>B</b> → <b>A</b>	Existing Stream State (Type): <b>F4b</b>	Potential Stream State (Type): <b>B4</b>
Lateral Stability	<input type="checkbox"/> Stable <input type="checkbox"/> Mod. Unstable <input checked="" type="checkbox"/> Unstable <input type="checkbox"/> Highly Unstable	Remarks/causes: <b>Fire and Flood effects</b>	
	<input type="checkbox"/> No Deposition <input type="checkbox"/> Mod. Deposition <input checked="" type="checkbox"/> Ex. Deposition <input type="checkbox"/> Aggradation	Remarks/causes: <b>Fire and Flood effects</b>	
Vertical Stability (Aggradation)	<input type="checkbox"/> Not Incised <input checked="" type="checkbox"/> Slightly Incised <input type="checkbox"/> Mod. Incised <input type="checkbox"/> Degradation	Remarks/causes: <b>Fire and Flood effects</b>	
	<input type="checkbox"/> No Increase <input type="checkbox"/> Slight Increase <input checked="" type="checkbox"/> Mod. Increase <input type="checkbox"/> Extensive	Remarks/causes: <b>Fire and Flood effects</b>	
Channel Enlargement	<input type="checkbox"/> Low <input type="checkbox"/> Moderate <input checked="" type="checkbox"/> High <input type="checkbox"/> Very High	Remarks/causes: <b>Fire and Flood effects</b>	
	<input type="checkbox"/> Sediment Supply (Channel Source)	Remarks/causes: <b>Been in flood after fire.</b>	

## *Appendix C13*

# **F4b Stream Type**

## *Poor Stability Mainstem*

### *Reach*



# Table of Contents

## *Appendix C13: F4b Poor Mainstem Reach*

<b>Reach Location &amp; Overview.....</b>	<b>C13-2</b>
<b>Survey Summary.....</b>	<b>C13-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C13-10</b>
<b><i>Velocity, Classification &amp; Morphological Relations.....</i></b>	<b>C13-10</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b><i>Stability Indices.....</i></b>	<b>C13-14</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b><i>BANCS Model – Streambank Erosion.....</i></b>	<b>C13-24</b>
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b><i>FLOWSED Model – Total Annual Sediment Yield.....</i></b>	<b>C13-26</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b><i>POWERSED Model– Sediment Transport Capacity to Assess Bed Stability.....</i></b>	<b>C13-28</b>
Worksheet 5-20a. Sediment transport prediction for the upstream condition.	
Worksheet 5-20b. Sediment transport prediction for the existing condition.	
<b><i>Sediment Competence/Entrainment.....</i></b>	<b>C13-30</b>
Worksheet 5-22. Sediment competence calculations.	
<b><i>Channel Stability Ratings.....</i></b>	<b>C13-31</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b><i>Summary.....</i></b>	<b>C13-37</b>
Worksheet 5-32. Summary of stability condition categories.	

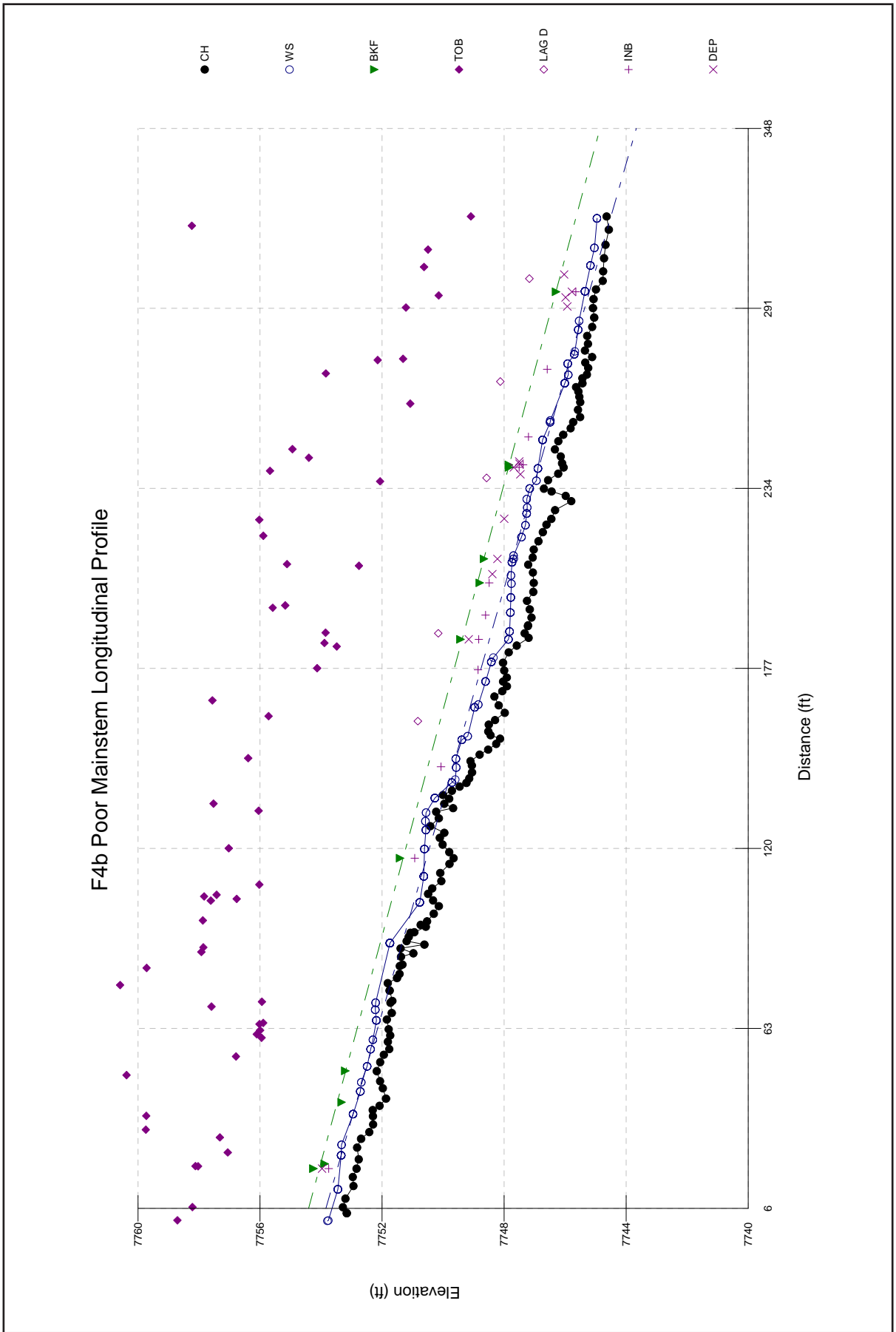
## F4b Poor Mainstem Reach Location & Overview

The F4b Poor Mainstem representative reach is a 3<sup>rd</sup> order, perennial, relatively steep gradient, entrenched stream located in the Trail Creek Mainstem (see location map **Figure C-2**). The width/depth ratio of 32 is very high and will continue to promote excess deposition and high bank erosion in this gulch-fill, alluvial Valley Type VIIIa. The stream is still enlarging due to the high peak flows following the fire. The potential stable stream type in this valley type is a B4; thus a POWERSED run was made to determine streambed stability, which indicated approximately 1,077 tons/yr of deposition. The stability rating is “Poor” due to a Pfankuch stability rating of “Poor” and the extremely high streambank erosion rate of 0.472 tons/yr/ft. This rate is two and a half orders of magnitude larger than the B4 reference rate of 0.0048 tons/yr/ft. The sediment supply rating is *High*, typical of an F4 stream type, due to the high banks on both sides and the sediment deposition in the bed. The “Poor” stability rating indicates a higher potential accelerated increase in flow-related sediment compared to the same-sized B4 reference stream type. The WRENSS model indicated that the water yield increased from 3,917 acre-ft to 6,376 acre-ft, representing a total increase of 2,458 acre-ft. The corresponding bedload increased from 43 tons/yr to 5,471 tons/yr and suspended sediment increased from 99 tons/yr to 9,354 tons/yr, representing a total increase in sediment of 14,683 tons/yr. This increase is the result of the increased sediment supply due to the unstable banks and high width/depth ratio that encourages increased sediment deposition in the streambed. This increased sediment loading is equivalent to 1,130 ten-yard, end dump truck loads per year. For a stark comparison, the reference condition total sediment increase, for the same bankfull discharge and relatively similar streamflow, is only 557 tons/yr.

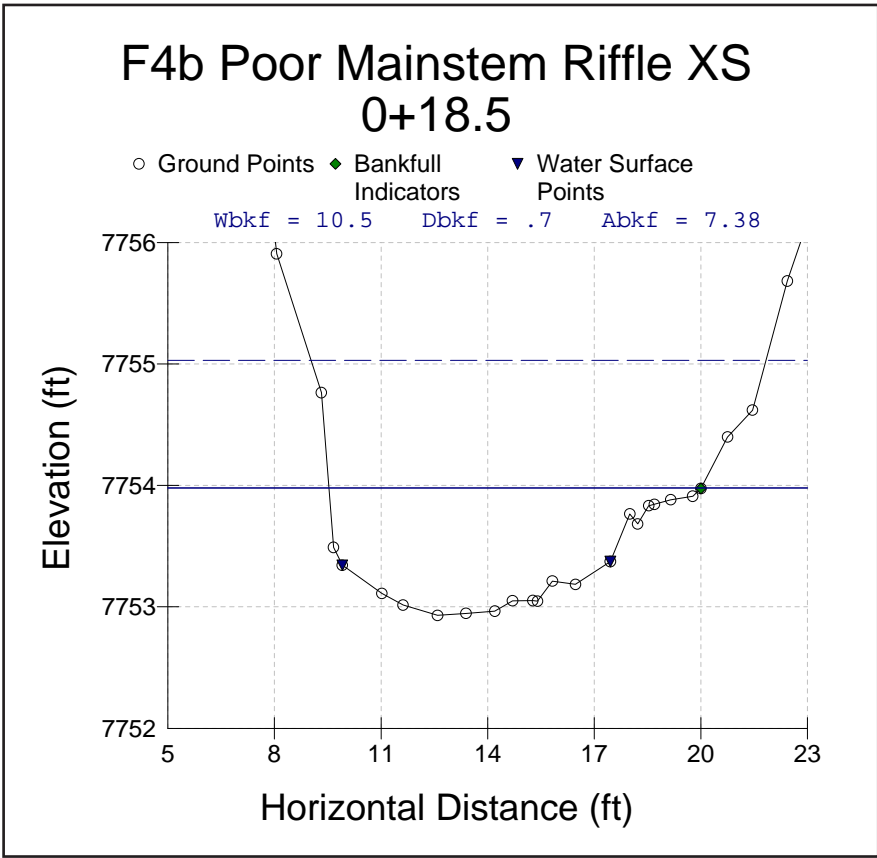
The photograph depicts the typical character of this representative F4b Poor stream type. The following graphs and summary worksheets provide the detail of the morphology, hydraulics, streambank erosion rates, and stability conditions responsible for the overall “Poor” rating.



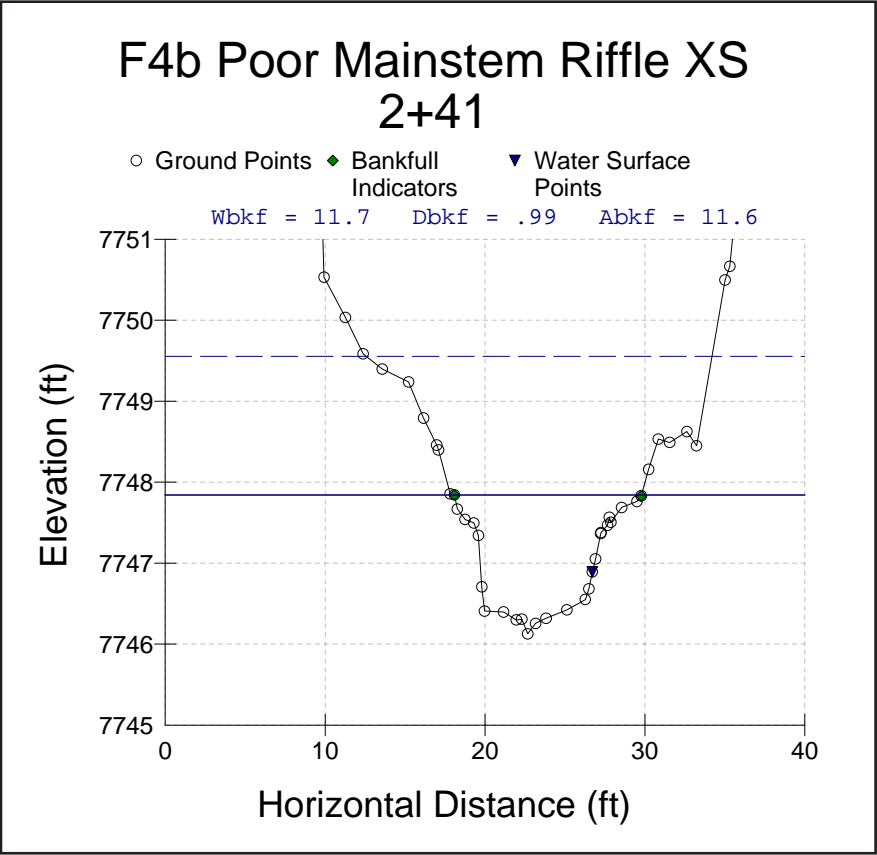
# Survey Summary



Longitudinal Profile (graph generated from RIVERMorph™)

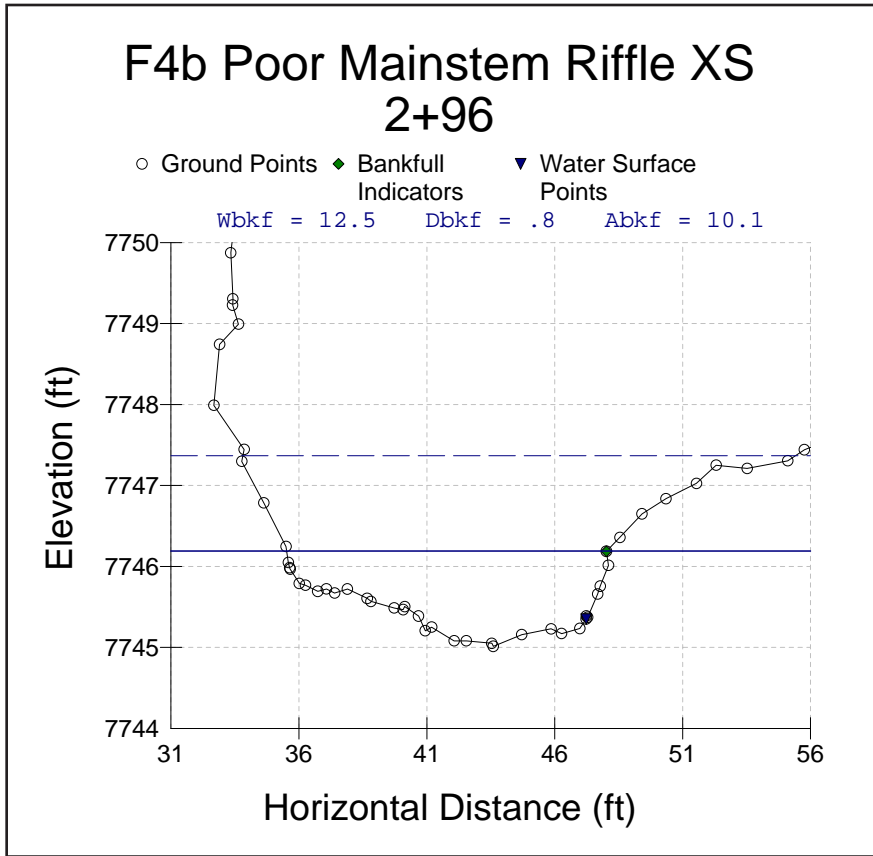


Riffle Cross-section 0+18.5 (graph generated from RIVERMorph™)

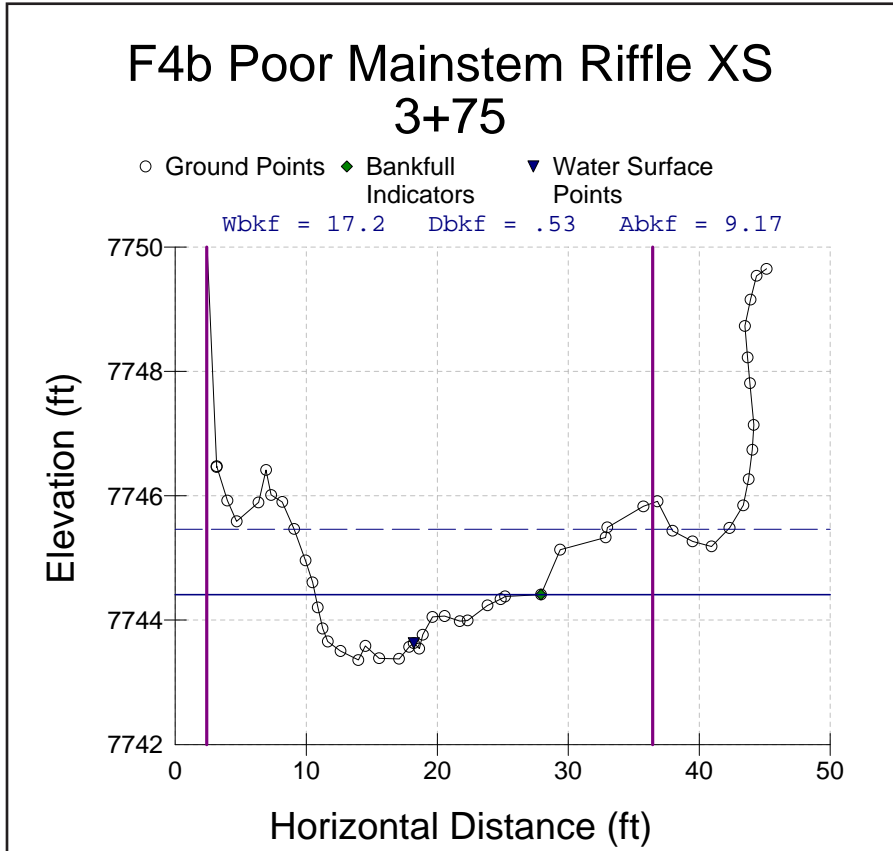


Riffle Cross-section 2+41 (graph generated from RIVERMorph™)

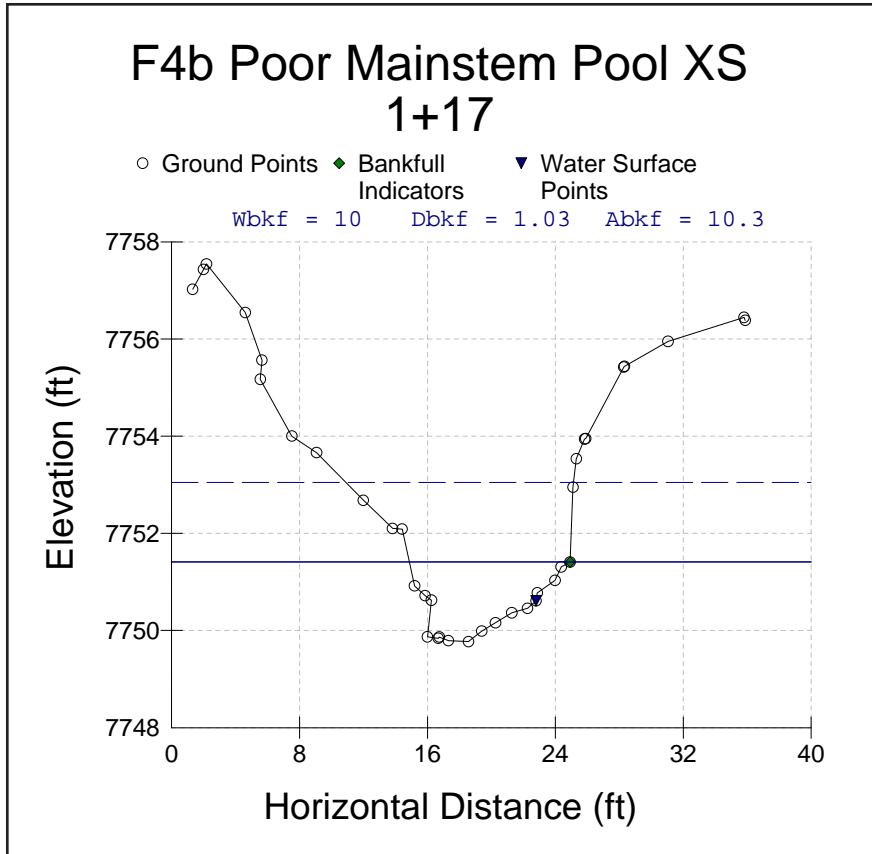




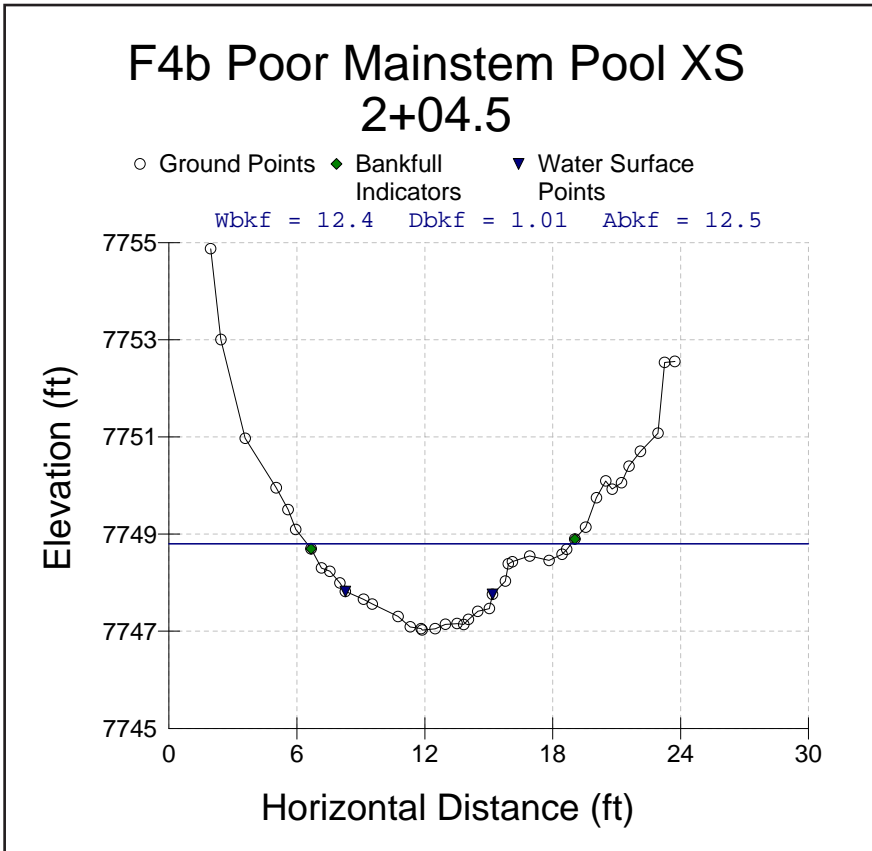
Riffle Cross-section 2+96 (graph generated from RIVERMorph™)



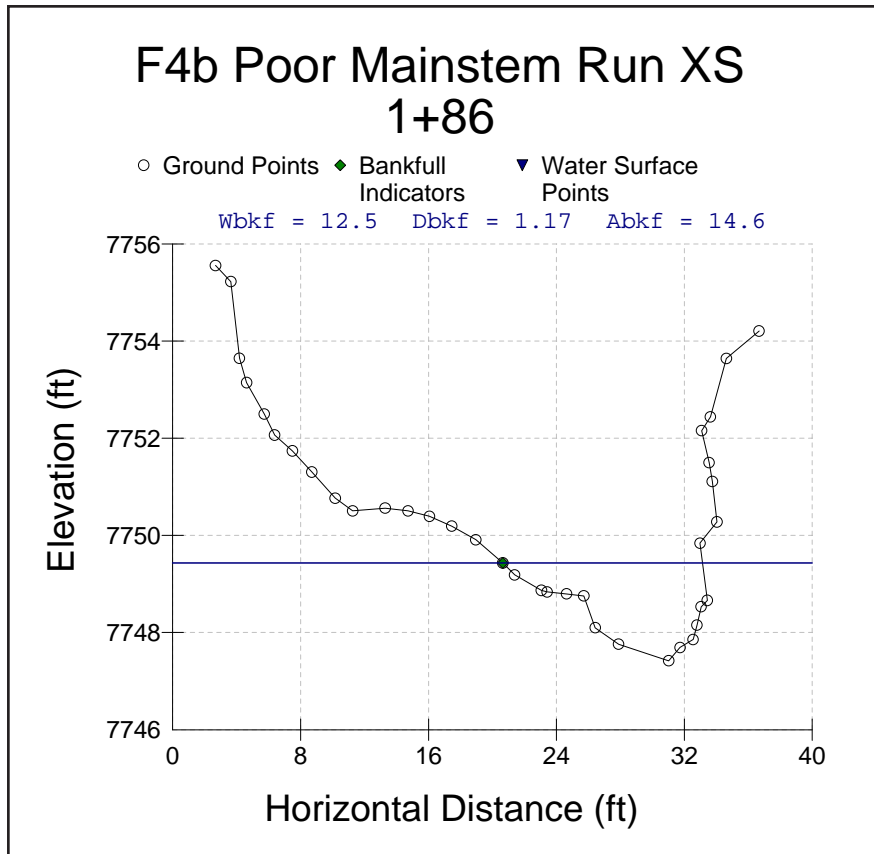
Representative Cross-Section 3+75 (graph generated from RIVERMorph™)



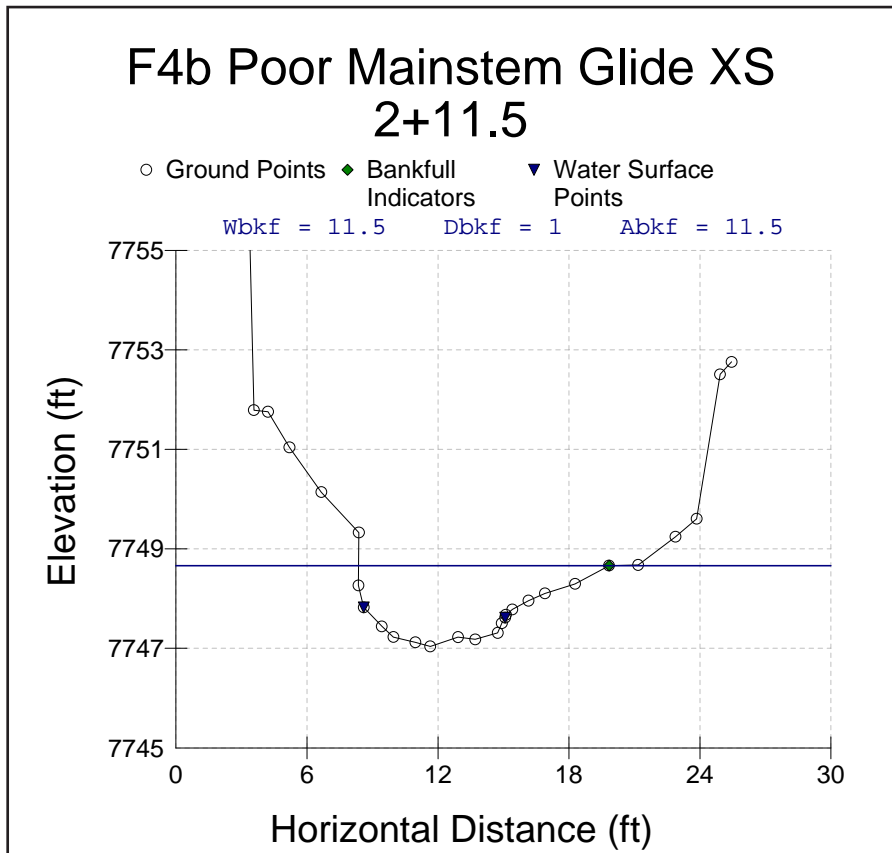
Pool Cross-section 1+17 (graph generated from RIVERMorph™)



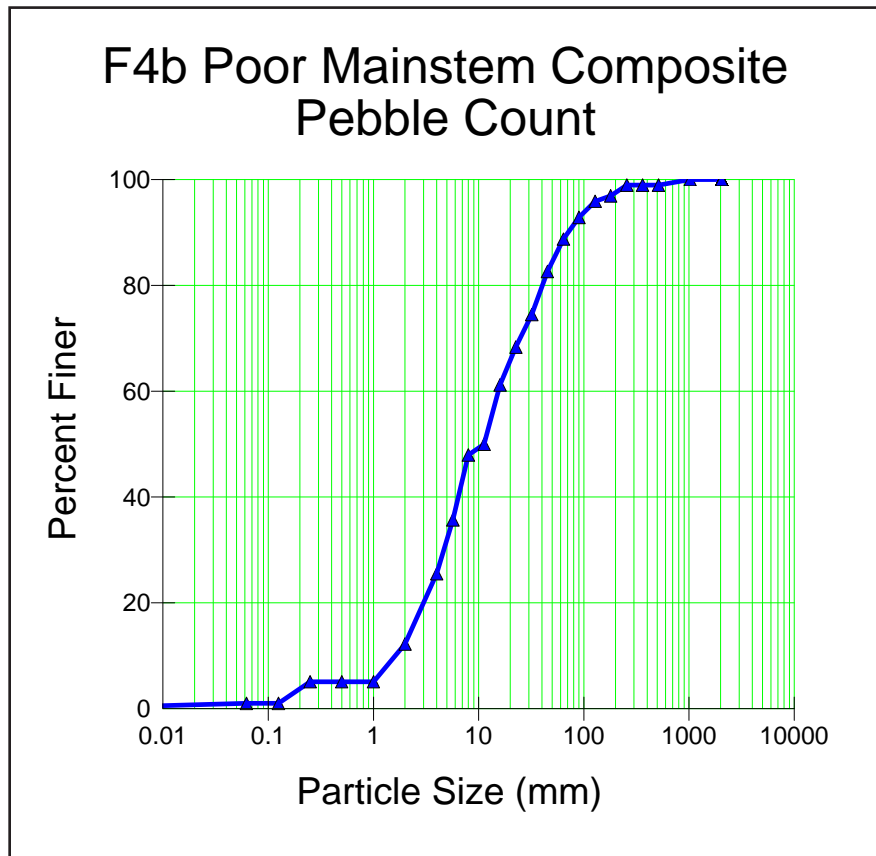
Pool Cross-section 2+04.5 (graph generated from RIVERMorph™)



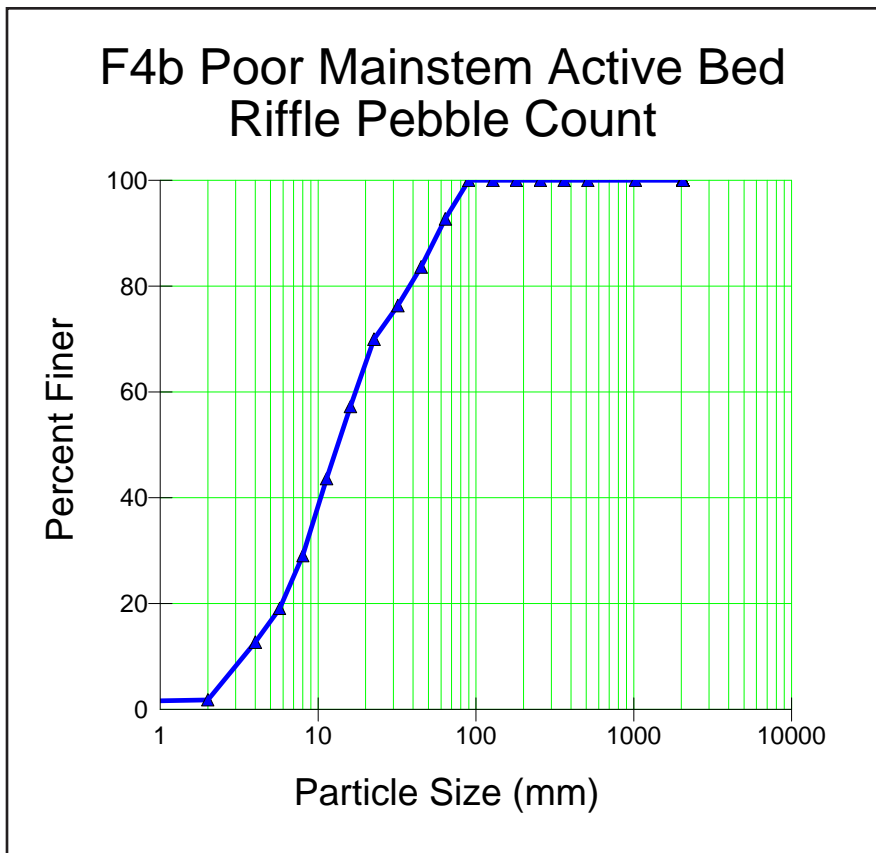
Run Cross-section 1+86 (graph generated from RIVERMorph™)



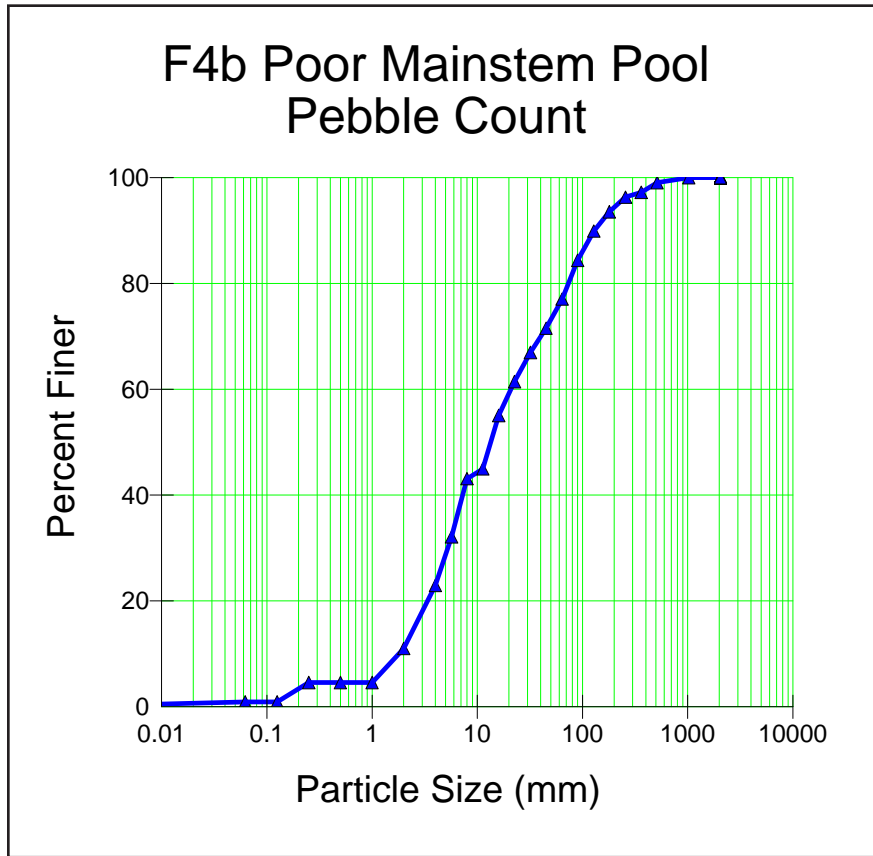
Glide Cross-Section 2+11.5 (graph generated from RIVERMorph™)



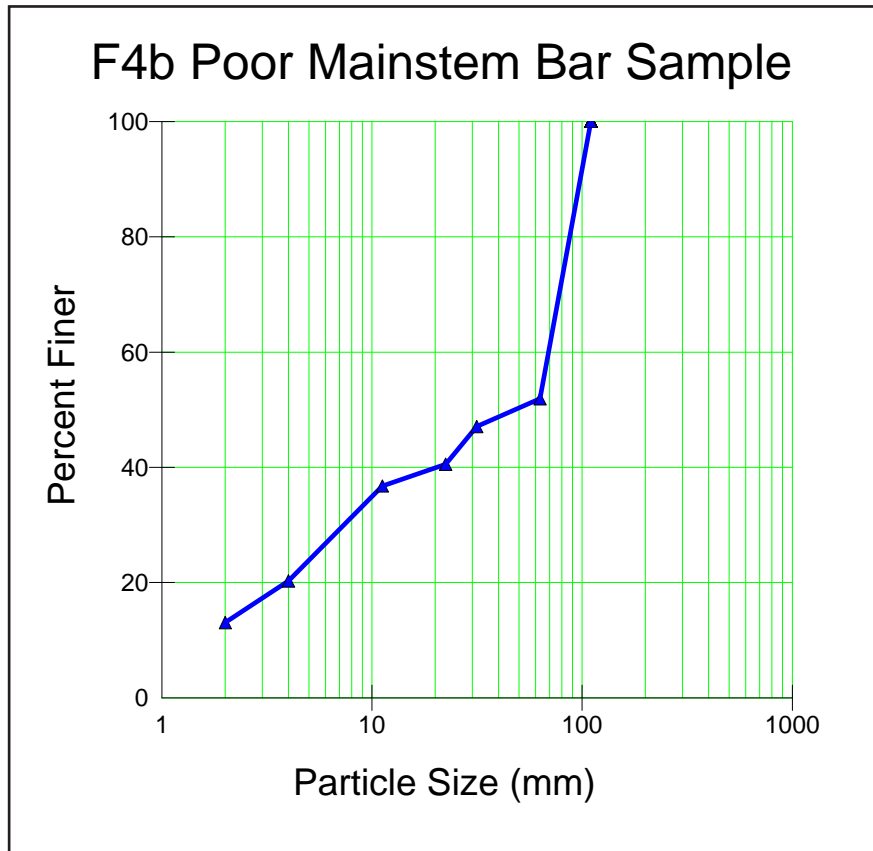
Composite Pebble Count (graph generated from RIVERMorph™)



Active Bed Riffle Pebble Count (graph generated from RIVERMorph™)



**Pool Pebble Count** (graph generated from RIVERMorph™)



**Bar Sample** (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

**Worksheet 5-2.** Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates							
Stream:	Trail Creek, F4b Poor Mainstem			Location:	XS Riffle 3+75, Pike N.F., CO		
Date:	8/12/2010	Stream Type:	F4b	Valley Type:	VIII		
Observers:	Rosgen <i>et al.</i>			HUC:	_ _ _ _ _		
INPUT VARIABLES				OUTPUT VARIABLES			
Bankfull Riffle Cross-Sectional AREA	9.17	$A_{bkf}$ (ft <sup>2</sup> )		Bankfull Riffle Mean DEPTH	0.53	$d_{bkf}$ (ft)	
Bankfull Riffle WIDTH	17.2	$W_{bkf}$ (ft)		Wetted PERIMETER $\sim (2 * d_{bkf}) + W_{bkf}$	18.22	$W_p$ (ft)	
$D_{84}$ at Riffle	45.8	Dia. (mm)		$D_{84}$ (mm) / 304.8	0.15	$D_{84}$ (ft)	
Bankfull SLOPE	0.028	$S_{bkf}$ (ft / ft)		Hydraulic RADIUS $A_{bkf} / W_p$	0.50	R (ft)	
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )		Relative Roughness $R(ft) / D_{84}(ft)$	3.35	$R / D_{84}$	
Drainage Area	14.3	DA (mi <sup>2</sup> )		Shear Velocity $u^* = (gRS)^{1/2}$	0.674	$u^*$ (ft/sec)	
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE	
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$				3.91	ft / sec	35.85	cfs
2. Roughness Coefficient: a) Manning's <i>n</i> from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.05$				3.16	ft / sec	28.93	cfs
2. Roughness Coefficient: b) Manning's <i>n</i> from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.057$				2.77	ft / sec	25.38	cfs
2. Roughness Coefficient: c) Manning's <i>n</i> from Jarrett (USGS): $n = 0.39 * S^{0.38} * R^{-0.16}$ <small>Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for Stream Types A1, A2, A3, B1, B2, B3, C2 &amp; E3</small> $n = 0.112$				1.41	ft / sec	12.93	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)					ft / sec		cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)					ft / sec		cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q =$ <input type="text"/> year $u = Q / A$					ft / sec		cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation ( $R/D_{84}$ ) – Estimation Method 1							
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.							
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.							
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.							
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.							

Worksheet 5-3. Level II stream classification.

Stream: <b>Trail Creek, F4b Poor Mainstem Reach</b>	
Basin:	Drainage Area: acres <b>14.3</b> mi <sup>2</sup>
Location: <b>Pike National Forest, Colorado</b>	
Twp.&Rge:	Sec.&Qtr.:
Cross-Section Monuments (Lat./Long.): <b>Riffle XS 3+75</b> Date: <b>8/13/10</b>	
Observers: <b>Rosgen et al.</b> Valley Type: <b>VIII</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>17.15</b> ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A_{bkf} / W_{bkf}$ ).	<b>0.53</b> ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>9.17</b> ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>32.4</b> ft/ft
<b>Maximum DEPTH (<math>d_{max}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>1.05</b> ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>24.04</b> ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>1.40</b> ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the median or dominant diameter of channel materials, as sampled proportionately from the channel surface, between the bankfull stage and Thalweg elevations.	<b>30</b> mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.028</b> ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope ( $S_{val} / S$ ).	<b>1.25</b>

<b>Stream Type</b>	<b>F4b</b>	<b>See Classification Key (Figure 2-14)</b>
--------------------	------------	---

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, F4b Poor Mainstem Reach</b>		Location: <b>Pike National Forest, Colorado</b>						
Observers: <b>Rosgen et al.</b>		Date: <b>8/12/2010</b>		Valley Type: <b>VIII</b>		Stream Type: <b>F4b</b>		
<b>River Reach Dimension Summary Data.....1</b>								
<b>Riffle Dimensions*, **, ***</b>	<b>Riffle Dimensions* ***, ***</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Width ( $W_{bkt}$ )	13.0	10.5	17.2	ft Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	9.54	7.38	11.56
	Mean Riffle Depth ( $d_{bkt}$ )	0.76	0.53	0.99	ft Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	18.69	11.82	32.36
	Maximum Riffle Depth ( $d_{max}$ )	1.25	1.05	1.71	ft Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	1.67	1.48	1.98
	Width of Flood-Prone Area ( $W_{fpa}$ )	17.9	12.8	24.0	ft Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )	1.38	1.22	1.54
	Riffle Inner Berm Width ( $W_{ib}$ )	5.7	5.4	6.0	ft Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )	0.44	0.42	0.46
	Riffle Inner Berm Depth ( $d_{ib}$ )	0.12	0.09	0.17	ft Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )	0.16	0.12	0.23
	Riffle Inner Berm Area ( $A_{ib}$ )	0.7	0.5	1.0	ft <sup>2</sup> Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )	0.08	0.06	0.11
	Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )	47.5	45.0	50.0				
<b>Pool Dimensions*, **, ***</b>	<b>Pool Dimensions* ***, ***</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Pool Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Pool Width ( $W_{bkfp}$ )	11.2	10.1	12.4	ft Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )	0.866	0.776	0.955
	Mean Pool Depth ( $d_{bkfp}$ )	1.02	1.01	1.03	ft Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )	1.351	1.338	1.364
	Pool Cross-Sectional Area ( $A_{bkfp}$ )	11.4	10.3	12.5	ft Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )	1.198	1.084	1.312
	Maximum Pool Depth ( $d_{maxp}$ )	1.71	1.64	1.77	ft Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	2.265	2.172	2.344
	Pool Inner Berm Width ( $W_{ibp}$ )	4.8	3.4	6.1	ft Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )	0.428	0.303	0.544
	Pool Inner Berm Depth ( $d_{ibp}$ )	0.31	0.18	0.44	ft Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )	0.304	0.176	0.431
	Pool Inner Berm Area ( $A_{ibp}$ )	1.6	0.6	2.7	ft <sup>2</sup> Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )	0.143	0.052	0.234
	Point Bar Slope ( $S_{pb}$ )	0.220	0.190	0.240	ft/ft Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )	15.5	11.0	19.7
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Run Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Run Width ( $W_{bkfr}$ )	12.5			ft Run Width to Riffle Width ( $W_{bkfr} / W_{bkt}$ )	0.963		
	Mean Run Depth ( $d_{bkfr}$ )	1.17			ft Mean Run Depth to Mean Riffle Depth ( $d_{bkfr} / d_{bkt}$ )	1.550		
	Run Cross-Sectional Area ( $A_{bkfr}$ )	14.6			ft Run Area to Riffle Area ( $A_{bkfr} / A_{bkt}$ )	1.532		
	Maximum Run Depth ( $d_{maxr}$ )	2.01			ft Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )	2.662		
	Run Width/Depth Ratio ( $W_{bkfr} / d_{bkfr}$ )	10.7			ft			
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Glide Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Glide Width ( $W_{bkfg}$ )	11.5			ft Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )	0.884		
	Mean Glide Depth ( $d_{bkfg}$ )	1.00			ft Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )	1.325		
	Glide Cross-Sectional Area ( $A_{bkfg}$ )	11.5			ft Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )	1.206		
	Maximum Glide Depth ( $d_{maxg}$ )	1.62			ft Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )	2.146		
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )	11.5			ft/ft Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )			
	Glide Inner Berm Width ( $W_{ibg}$ )				ft Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )			
	Glide Inner Berm Depth ( $d_{ibg}$ )				ft Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )			
Glide Inner Berm Area ( $A_{ibg}$ )				ft <sup>2</sup> Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )				
<b>Step**</b>	<b>Step Dimensions**</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Step Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Step Width ( $W_{bkfs}$ )				ft Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )			
	Mean Step Depth ( $d_{bkfs}$ )				ft Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )			
	Step Cross-Sectional Area ( $A_{bkfs}$ )				ft Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )			
	Maximum Step Depth ( $d_{maxs}$ )				ft Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )								



**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, F4b Poor Mainstem Reach</b>		Location: <b>Pike National Forest, Colorado</b>								
Observers: <b>Rosgen et al.</b>		Date: <b>8/12/2010</b>	Valley Type: <b>VIII</b>							
		Stream Type: <b>F4b</b>								
<b>River Reach Summary Data.....2</b>										
<b>Hydraulics</b>	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )	<b>3.91</b>	ft/sec	Estimation Method	<b><math>u/u^*</math></b>					
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )	<b>35.85</b>	cfs	Drainage Area	<b>14.3</b> mi <sup>2</sup>					
<b>Channel Pattern</b>	<b>Geometry</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Dimensionless Geometry Ratios</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		
	Linear Wavelength ( $\lambda$ )	<b>119.8</b>	<b>93.0</b>	<b>143.2</b>	ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )	<b>9.90</b>	<b>7.69</b>	<b>11.83</b>	
	Stream Meander Length ( $L_m$ )	<b>129.93</b>	<b>95.70</b>	<b>155.20</b>	ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )	<b>10.74</b>	<b>7.91</b>	<b>12.83</b>	
	Radius of Curvature ( $R_c$ )	<b>35.6</b>	<b>28.8</b>	<b>45.0</b>	ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )	<b>2.75</b>	<b>2.22</b>	<b>3.47</b>	
	Belt Width ( $W_{bit}$ )	<b>25.8</b>	<b>15.1</b>	<b>36.6</b>	ft	Meander Width Ratio ( $W_{bit} / W_{bkt}$ )	<b>1.99</b>	<b>1.17</b>	<b>2.82</b>	
	Arc Length ( $L_a$ )	<b>48.4</b>	<b>34.5</b>	<b>70.5</b>	ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )	<b>3.74</b>	<b>2.66</b>	<b>5.44</b>	
	Riffle Length ( $L_r$ )	<b>7.5</b>	<b>1.7</b>	<b>31.1</b>	ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )	<b>0.58</b>	<b>0.13</b>	<b>2.40</b>	
	Individual Pool Length ( $L_p$ )	<b>9.9</b>	<b>3.6</b>	<b>31.1</b>	ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )	<b>0.77</b>	<b>0.28</b>	<b>2.40</b>	
Pool to Pool Spacing ( $P_s$ )	<b>18.3</b>	<b>2.9</b>	<b>67.4</b>	ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )	<b>1.41</b>	<b>0.22</b>	<b>5.20</b>		
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )	<b>0.0350</b>	ft/ft	Average Water Surface Slope ( $S$ )	<b>0.028</b>	ft/ft	Sinuosity ( $S_{val} / S$ )	<b>1.25</b>		
	Stream Length (SL)	<b>320.1</b>	ft	Valley Length (VL)	<b>256.1</b>	ft	Sinuosity (SL / VL)	<b>1.25</b>		
	Low Bank Height (LBH)	start: <b>4.10</b> ft end: <b>1.40</b> ft		Max Bankfull Depth ( $d_{max}$ )	start: <b>1.47</b> ft end: <b>1.47</b> ft		Bank-Height Ratio (BHR) (LBH / $d_{max}$ )	start: <b>2.8</b> end: <b>1.0</b>		
	<b>Facet Slopes</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Dimensionless Facet Slope Ratios</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		
	Riffle Slope ( $S_{rif}$ )	<b>0.0420</b>	<b>0.0060</b>	<b>0.0990</b>	ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.5000</b>	<b>0.2143</b>	<b>3.5357</b>	
	Run Slope ( $S_{run}$ )	<b>0.0510</b>	<b>0.0030</b>	<b>0.1540</b>	ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )	<b>1.8214</b>	<b>0.1071</b>	<b>5.5000</b>	
	Pool Slope ( $S_p$ )	<b>0.0190</b>	<b>0.0000</b>	<b>0.0460</b>	ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )	<b>0.6786</b>	<b>0.0000</b>	<b>1.6429</b>	
	Glide Slope ( $S_g$ )	<b>0.0100</b>	<b>0.0040</b>	<b>0.0170</b>	ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )	<b>0.3571</b>	<b>0.1429</b>	<b>0.6071</b>	
	Step Slope ( $S_s$ )				ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )				
	<b>Max Depths<sup>a</sup></b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Dimensionless Depth Ratios</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		
	Max Riffle Depth ( $d_{max}$ )	<b>1.49</b>	<b>1.29</b>	<b>1.71</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>1.974</b>	<b>1.709</b>	<b>2.265</b>	
	Max Run Depth ( $d_{maxr}$ )	<b>2.01</b>			ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )	<b>2.662</b>			
	Max Pool Depth ( $d_{maxp}$ )	<b>1.71</b>			ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	<b>2.265</b>			
	Max Glide Depth ( $d_{maxg}$ )	<b>1.62</b>			ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )	<b>2.146</b>			
Max Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )					
<b>Channel Materials</b>		<b>Reach<sup>b</sup></b>	<b>Riffle<sup>c</sup></b>	<b>Bar</b>		<b>Reach<sup>b</sup></b>	<b>Riffle<sup>c</sup></b>	<b>Bar</b>	<b>Protrusion Height<sup>d</sup></b>	
	% Silt/Clay	<b>1</b>	<b>0</b>	<b>0</b>		$D_{16}$	<b>2.57</b>	<b>4.87</b>	<b>2.82</b>	mm
	% Sand	<b>11</b>	<b>2</b>	<b>13</b>		$D_{35}$	<b>5.58</b>	<b>9.34</b>	<b>8.91</b>	mm
	% Gravel	<b>77</b>	<b>91</b>	<b>40</b>		$D_{50}$	<b>11.30</b>	<b>13.49</b>	<b>50.63</b>	mm
	% Cobble	<b>10</b>	<b>7</b>	<b>47</b>		$D_{84}$	<b>49.18</b>	<b>45.75</b>	<b>94.37</b>	mm
	% Boulder	<b>1</b>	<b>0</b>	<b>0</b>		$D_{95}$	<b>116.58</b>	<b>72.12</b>	<b>105.12</b>	mm
	% Bedrock					$D_{100}$	<b>1023.95</b>	<b>90.00</b>	<b>110.00</b>	mm

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.  
<sup>b</sup> Composite sample of riffles and pools within the designated reach.      <sup>c</sup> Active bed of a riffle.      <sup>d</sup> Height of roughness feature above bed.

## Stability Indices


**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation					
Stream: <b>Trail Creek, F4b Poor Mainstem</b>		Location: <b>Pike National Forest, Colorado</b>			
Observers: <b>Rosgen et al.</b>		Reference reach <input type="checkbox"/>	Disturbed (impacted reach) <input checked="" type="checkbox"/>	Date: <b>8/13/2010</b>	
Existing species composition: <b>Alder, Willow, Grass/Forb, Aspen</b>		Potential species composition: <b>Spruce, Willow, Alder, Carex/Juncus</b>			
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition
<b>1. Overstory</b>	Canopy layer	<b>&lt;10%</b>	<b>&lt;5%</b>	<b>Alder</b>	<b>27%</b>
					100%
	<b>2. Understory</b>	Shrub layer	<b>30%</b>	<b>Willow</b>	<b>30%</b>
				<b>Alder</b>	<b>5%</b>
				100%	
<b>3. Ground level</b>	Herbaceous	<b>40%</b>	<b>Forbs</b>	<b>25%</b>	
			<b>Perennial Grasses</b>	<b>55%</b>	
			<b>Toadflax</b>	<b>10%</b>	
			<b>Thistle</b>	<b>5%</b>	
			<b>Mullen</b>	<b>2%</b>	
	<b>Hairgrass</b>	<b>2%</b>			
Leaf or needle litter			<b>Remarks:</b> Condition, vigor and/or usage of existing reach: <b>Active bank erosion precludes active colonization of willows; invasive species are colonizing disturbed sites</b>		
Bare ground					
					100%
*Based on crown closure. **Based on basal area to surface area.			<b>Column total = 100%</b>		

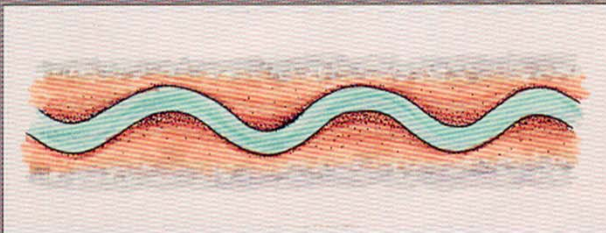



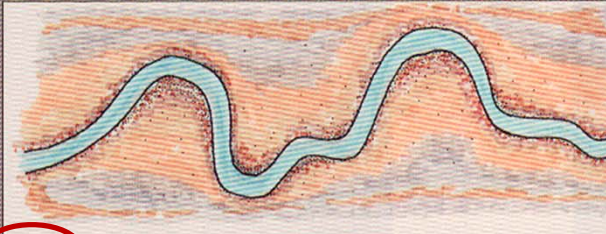
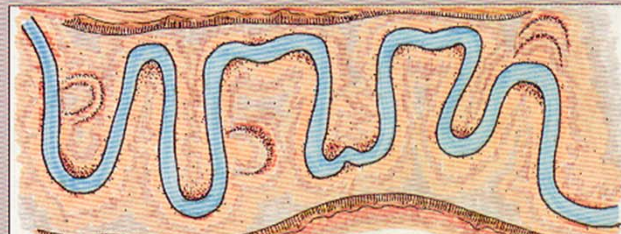
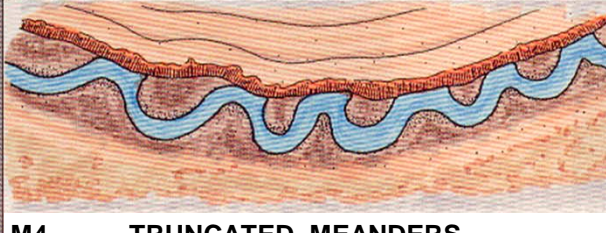
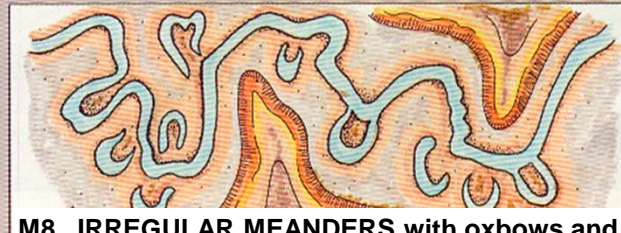
Worksheet 5-7. Flow regime.

FLOW REGIME								
Stream: <b>Trail Creek, F4b Poor Mainstem</b>			Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>Rosgen et al.</b>						Date: <b>8/13/2010</b>		
List ALL COMBINATIONS that APPLY.....☞			P1	P2	P8			
General Category								
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation							
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
<b>P</b>	Perennial stream channels: Surface water persists yearlong.							
Specific Category								
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
<b>4</b>	Streamflow regulated by glacial melt.							
<b>5</b>	Ice flows/ice torrents from ice dam breaches.							
<b>6</b>	Alternating flow/backwater due to tidal influence.							
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.							
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
<b>9</b>	Rain-on-snow generated runoff.							

**Worksheet 5-8.** Stream order & stream size.

Stream Size and Order			
Stream:		Trail Creek, F4b Poor Mainstem Reach	
Location:		Pike National Forest, Colorado	
Observers:		Rosgen <i>et al.</i>	
Date:		8/13/2010	
Stream Size Category and Order 			S-4(3)
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0.305	<1	<input type="checkbox"/>
S-2	0.3 – 1.5	1 – 5	<input type="checkbox"/>
S-3	<del>1.5 – 4.6</del>	<del>5 – 15</del>	<input type="checkbox"/>
<b>S-4</b>	<b>4.6 – 9</b>	<b>15 – 30</b>	<input checked="" type="checkbox"/>
S-5	9 – 15	30 – 50	<input type="checkbox"/>
S-6	15 – 22.8	50 – 75	<input type="checkbox"/>
S-7	22.8 – 30.5	75 – 100	<input type="checkbox"/>
S-8	30.5 – 46	100 – 150	<input type="checkbox"/>
S-9	46 – 76	150 – 250	<input type="checkbox"/>
S-10	76 – 107	250 – 350	<input type="checkbox"/>
S-11	107 – 150	350 – 500	<input type="checkbox"/>
S-12	150 – 305	500 – 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
Stream Order			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			

Worksheet 5-9. Meander patterns.

<b>Meander Patterns</b>				
Stream:	Trail Creek, F4b Poor Mainstem Reach	Location:	Pike National Forest, CO	
Observers:	Rosgen <i>et al.</i>	Date:	8/13/2010	
List ALL CATEGORIES that APPLY	<b>M3</b>			
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>				
	<b>M1</b> <b>REGULAR MEANDERS</b>			
	<b>M2</b> <b>TORTUOUS MEANDERS</b>			
	<b>M3</b> <b>IRREGULAR MEANDERS</b>			
	<b>M4</b> <b>TRUNCATED MEANDERS</b>			

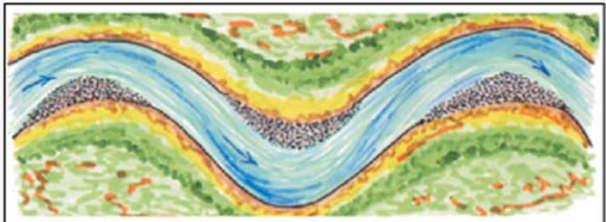
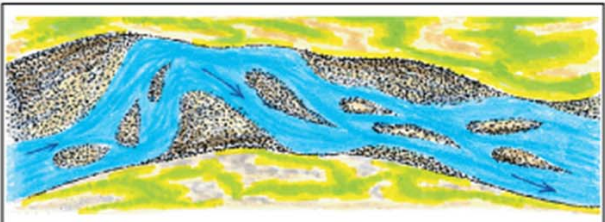

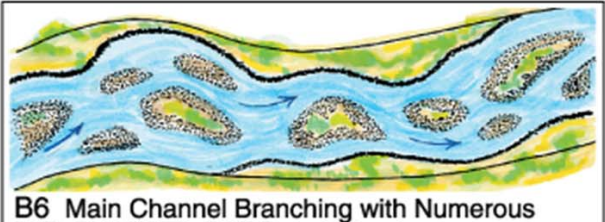
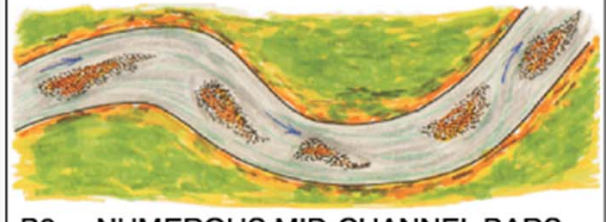
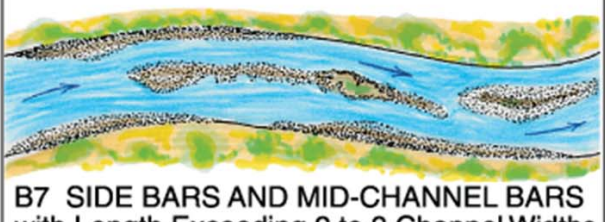

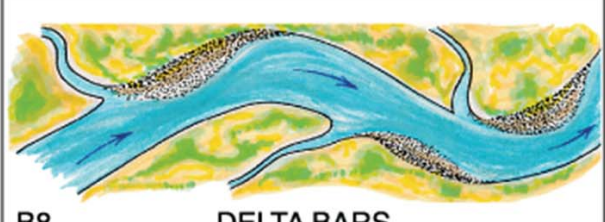
Worksheet 5-10. Depositional patterns.

## Depositional Patterns

Stream: **Trail Creek, F4b Poor Mainstem Reach**      Location: **Pike National Forest, Colorado**  
 Observers: **Rosgen et al.**      Date: **8/13/2010**

List ALL CATEGORIES that APPLY	<b>B4</b>				
--------------------------------	-----------	--	--	--	--

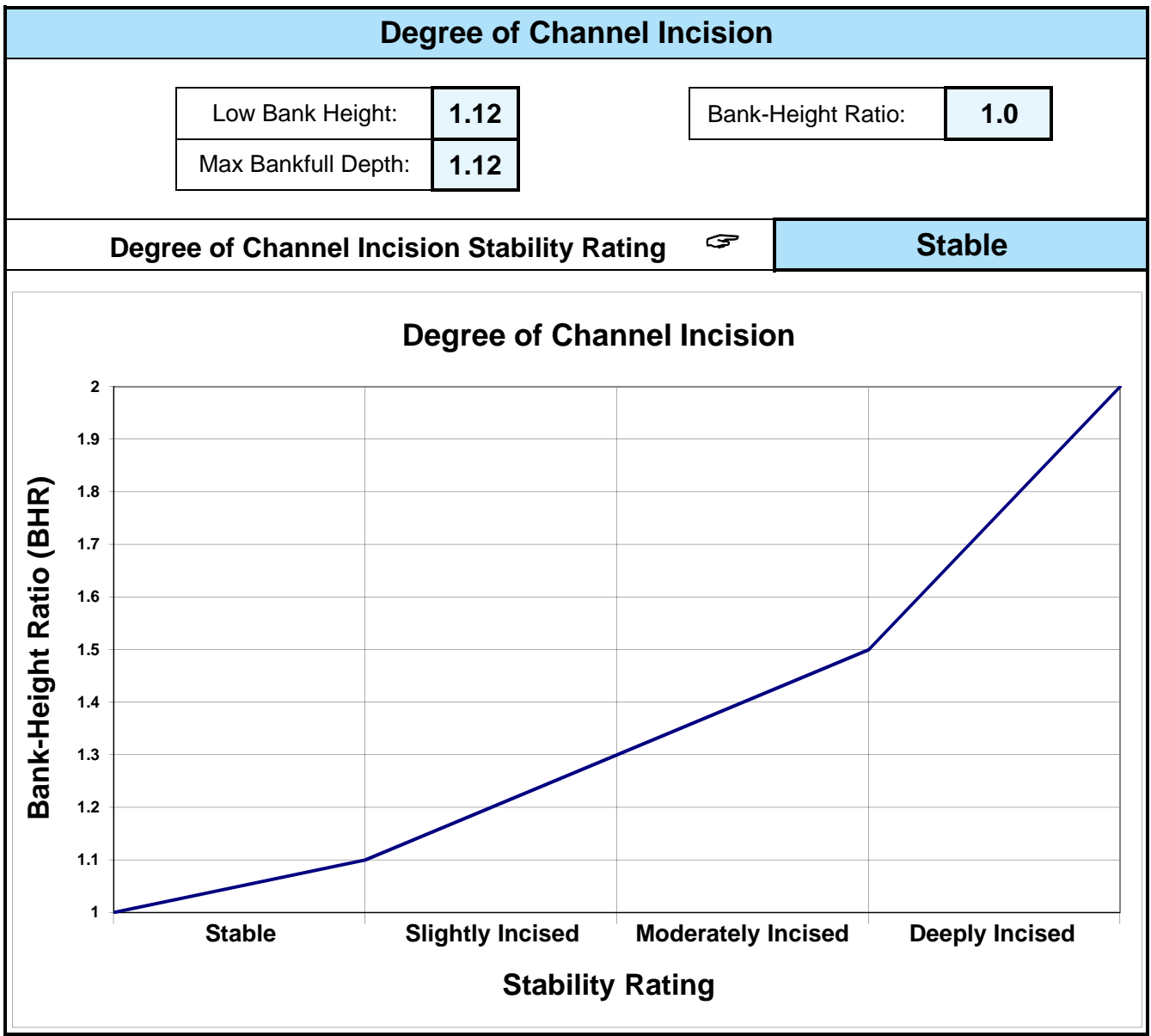
*Various Depositional Features modified from Galay et al. (1973)*

 <p><b>B1</b>      <b>POINT BARS</b></p>	 <p><b>B5</b>      <b>DIAGONAL BARS</b></p>
 <p><b>B2</b>      <b>POINT BARS with Few MID-CHANNEL BARS</b></p>	 <p><b>B6</b>      <b>Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</b></p>
 <p><b>B3</b>      <b>NUMEROUS MID-CHANNEL BARS</b></p>	 <p><b>B7</b>      <b>SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</b></p>
 <p><b>B4</b>      <b>SIDE BARS</b></p>	 <p><b>B8</b>      <b>DELTA BARS</b></p>

## Worksheet 5-11. Channel blockages.


Channel Blockages		
Stream: <b>Trail Creek, F4b Poor Mainstem Reach</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>Rosgen <i>et al.</i></b>		Date: <b>8/13/2010</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input checked="" type="checkbox"/>
<b>D4</b> Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

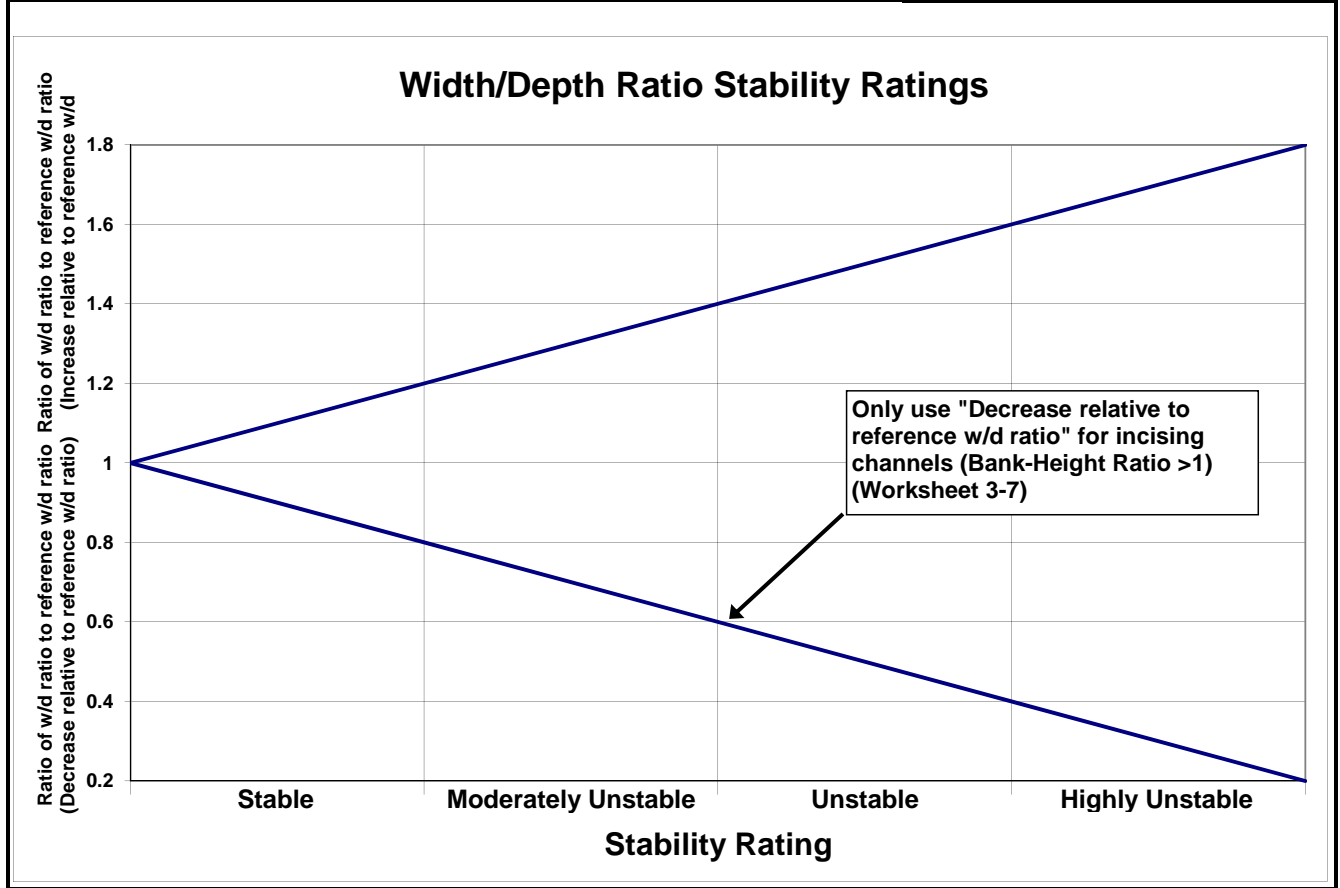
**Worksheet 5-12.** Degree of channel incision.



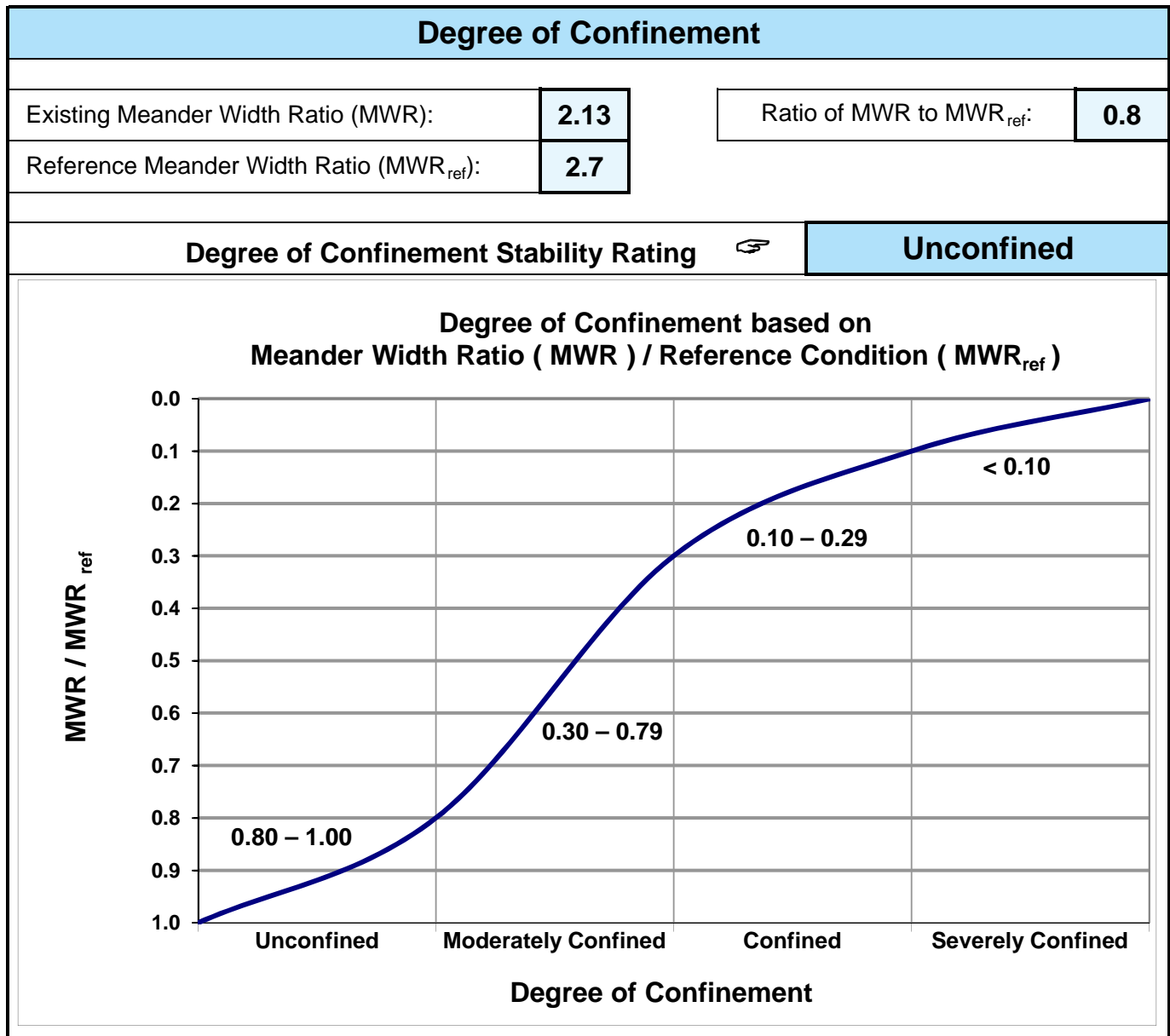


**Worksheet 5-13.** Width/depth ratio state.

Width/Depth Ratio State			
Existing Width/Depth Ratio:	<b>32.36</b>	Ratio of existing W/d to reference W/d:	<b>2.57</b>
Reference Width/Depth Ratio:	<b>12.6</b>		
Width/Depth Ratio State Stability Rating 			<b>Highly Unstable</b>



**Worksheet 5-14.** Degree of channel confinement (lateral containment).



Worksheet 5-15. Pfankuch channel stability rating.

Stream: Trail Creek, F4b Poor Mainstem		Location: Pike National Forest, CO			Valley Type: VIII			Observers: Rosgen et al.			Date: 8/13/2010														
Local- tion	Key Category	Excellent Description	Rating	Good Description	Rating	Fair Description	Rating	Poor Description	Rating																
Upper banks	1	Landform slope	2	Bank slope gradient <30%.	4	Bank slope gradient 40-60%.	6	Bank slope gradient > 60%.	8																
	2	Mass erosion	3	No evidence of past or future mass erosion.	6	Frequent or large, causing sediment nearly yearlong.	9	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.	12																
	3	Debris jam potential	2	Essentially absent from immediate channel area.	3	Present, but mostly small twigs and limbs.	6	Moderate to heavy amounts, mostly larger sizes.	8																
	4	Vegetative bank protection	3	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	6	70-90% density. Fewer species or less vigor suggest less dense or deep root mass.	9	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.	12																
Lower banks	5	Channel capacity	1	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0.	2	Bankfull stage is contained within banks. Width/depth ratio departure from reference width/depth ratio = 1.2-1.4. Bank-Height Ratio (BHR) = 1.1-1.3.	3	Bankfull stage is not contained; over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.	4																
	6	Bank rock content	2	> 65% with large angular boulders. 12"+ common.	4	40-65%. Mostly boulders and small cobbles 6-12".	6	20-40%. Most in the 3-6" diameter class.	8																
	7	Obstructions to flow	2	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	5	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	6	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	8																
	8	Cutting	4	Little or none. Infrequent raw banks <6".	6	Some, intermittently at outcrops and constrictions. Raw banks may be up to 12".	12	Significant. Cuts 12-24" high. Root mat overhangs and sloughing evident.	16																
	9	Deposition	4	Little or no enlargement of channel or point bars.	8	Some new bar increase, mostly from coarse gravel.	10	Moderate deposition of new gravel and coarse sand on old and some new bars.	16																
Bottom	10	Rock angularity	1	Sharp edges and corners. Plane surfaces rough.	2	Rounded corners and edges. Surfaces smooth and flat.	3	Corners and edges well rounded in 2 dimensions.	4																
	11	Brightness	1	Surfaces dull, dark or stained. Generally not bright.	2	Mostly dull, but may have <35% bright surfaces.	3	Mixture dull and bright, i.e., 35-65% mixture range.	4																
	12	Consolidation of particles	2	Assorted sizes tightly packed or overlapping.	4	Moderately packed with some overlapping.	6	Mostly loose assortment with no apparent overlap.	8																
	13	Bottom size distribution	4	No size change evident. Stable material 80-100%.	8	Distribution shift light. Stable material 50-80%.	14	Moderate change in sizes. Stable materials 20-50%.	16																
	14	Scouring and deposition	6	<5% of bottom affected by scour or deposition.	12	5-30% affected. Scour at constrictions and where grades steepen. Some deposition in pools.	18	30-50% affected. Deposits and scour at obstructions, constrictions and bends. Some filling of pools.	24																
	15	Aquatic vegetation	1	Abundant growth moss-like, dark green perennial. In swift water too.	2	Common. Algae forms in low velocity and pool areas. Moss here too.	3	Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick.	4																
			<b>Excellent total = 0</b>	<b>Good total = 8</b>			<b>Fair total = 30</b>			<b>Poor total = 96</b>															
<b>Stream type</b>	<b>A1</b>	<b>A2</b>	<b>A3</b>	<b>A4</b>	<b>A5</b>	<b>A6</b>	<b>B1</b>	<b>B2</b>	<b>B3</b>	<b>B4</b>	<b>B5</b>	<b>B6</b>	<b>C1</b>	<b>C2</b>	<b>C3</b>	<b>C4</b>	<b>C5</b>	<b>C6</b>	<b>D3</b>	<b>D4</b>	<b>D5</b>	<b>D6</b>	<b>Grand total = 134</b>		
Good (Stable)	38-43	38-43	54-90	60-95	60-95	50-80	38-45	38-45	40-60	40-64	48-68	40-60	38-50	38-50	60-85	70-90	60-85	60-85	85-107	85-107	85-107	85-107	85-107	67-98	
Fair (Mod. unstable)	44-47	44-47	91-129	96-132	96-142	81-110	46-58	46-58	61-78	65-84	69-88	61-78	51-61	51-61	86-105	91-110	86-105	86-105	108-132	108-132	108-132	108-132	108-132	99-125	
Poor (Unstable)	48+	48+	130+	133+	143+	111+	59+	59+	79+	85+	89+	79+	62+	62+	106+	111+	106+	106+	133+	133+	133+	133+	126+	F4b	
<b>Stream type</b>	<b>DA3</b>	<b>DA4</b>	<b>DA5</b>	<b>DA6</b>	<b>E3</b>	<b>E4</b>	<b>E5</b>	<b>E6</b>	<b>F1</b>	<b>F2</b>	<b>F3</b>	<b>F4</b>	<b>F5</b>	<b>F6</b>	<b>G1</b>	<b>G2</b>	<b>G3</b>	<b>G4</b>	<b>G5</b>	<b>G6</b>				<b>*Potential stream type = B4</b>	
Good (Stable)	40-63	40-63	40-63	40-63	50-75	50-75	50-75	40-63	80-85	85-110	85-110	90-115	80-95	80-95	40-60	40-60	85-107	85-107	90-112	90-112	85-107				<b>Modified channel stability rating =</b>
Fair (Mod. unstable)	64-86	64-86	64-86	64-86	76-96	76-96	76-96	64-86	86-105	86-105	111-125	111-125	116-130	96-110	61-78	61-78	108-120	108-120	113-125	113-125	108-120				<b>16</b>
Poor (Unstable)	87+	87+	87+	87+	97+	97+	97+	87+	106+	106+	126+	126+	131+	111+	79+	79+	121+	121+	126+	126+	121+				<b>4</b>

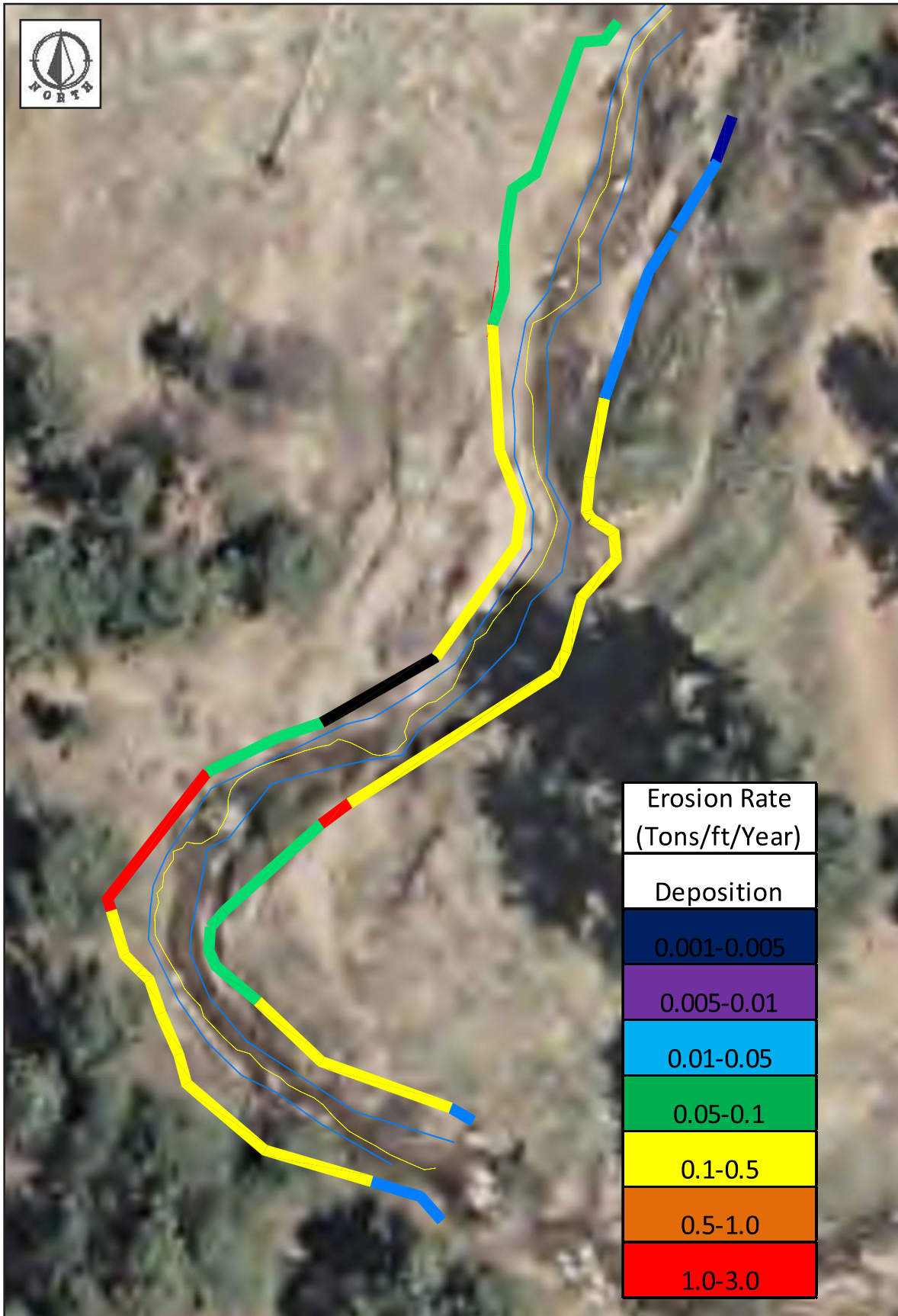
\*Rating is adjusted to potential stream type, not existing.

## BANCS Model – Streambank Erosion

**Worksheet 5-18.** Annual streambank erosion estimates.

Stream: <b>Trail Creek, F4b Poor Mainstem Reach</b>				Location: <b>Pike National Forest, Colorado</b>			
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>322</b>		Date: <b>8/13/2010</b>			
Observers: <b>Rosgen et al.</b>		Valley Type: <b>VIII</b>		Stream Type: <b>F4b</b>			
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 5-16) (adjective)	NBS rating (Worksheet 5-17) (adjective)	Bank erosion rate (Figure 5-34 or 5-35) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [[4]x(5)x(6)] (ft <sup>3</sup> /yr)	Erosion Rate {[(7)/27] × 1.3 / (5)}
1. 0+00L	High	Low	0.25042	7.0	4.1	7.19	0.04944
2. 0+05R	High	Low	0.25042	5.0	4.5	5.63	0.05426
3. 0+21L	High	Low	0.25042	14.0	4.5	15.78	0.05426
4. 0+45R	High	High	0.57533	40.0	4.5	103.56	0.12466
5. 0+78L	Very High	Low	0.25042	33.0	8.0	66.11	0.09646
6. 0+97L	High	High	0.57533	19.0	4.0	43.73	0.11080
7. 0+75R	Very High	Low	0.25042	30.0	4.0	30.05	0.04823
8 1+32L	Extreme	Very High	7.02692	35.0	8.0	1967.54	2.70666
9 1+29R	Very High	Low	0.25042	29.0	4.5	32.68	0.05426
10 1+49L	Moderate	High	0.42031	17.0	3.5	25.01	0.07083
11 1+62L	High	High	0.57533	13.0	2.0	14.96	0.05540
12 1+40R	Extreme	Extreme	2.76027	11.0	6.0	182.18	0.79741
13 1+90R	Extreme	Low	0.41998	50.0	7.0	146.99	0.14155
14 2+87L	Extreme	Low	0.41998	105.0	8.0	352.78	0.16177
15 2+07R	Moderate	Very High	0.69693	17.0	6.0	71.09	0.20133
16 2+32R	Low	Low	0.03566	25.0	1.4	1.25	0.00240
17 2+40R	Extreme	High	2.74738	8.0	1.4	30.77	0.18519
18 2+57R	Low	Low	0.03566	17.0	1.4	0.85	0.00240
19 3+34L	High	Low	0.25042	47.0	5.0	58.85	0.06029
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					Total Erosion (ft <sup>3</sup> /yr)	<b>3156.98</b>	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					Total Erosion (yds <sup>3</sup> /yr)	<b>116.93</b>	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					Total Erosion (tons/yr)	<b>152.00</b>	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					Total Erosion (tons/yr/ft)	<b>0.4721</b>	

Streambank Erosion Map



## FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Equation Type		Equation Source				Equation		Bankfull Discharge (cfs)			Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)	
1. Bedload Sediment		"Good/Fair" Pagosa				$y = -0.0113 + 1.0139x^{2.1929}$		35.85			0.0177		28.94	
2. Suspended Sediment		"Good/Fair" Pagosa				$y = 0.0636 + 0.9326x^{2.4085}$								
From Dimensional Flow-Duration Curve														
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	Calculate		Calculate Sediment Yield	
Percentage of Time	Daily Mean Discharge (cfs)	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimension- less Streamflow	Dimension- less Suspended Sediment Discharge	Suspended Sediment Discharge	Dimension- less Bedload Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow [(5)×(6)]	Suspended Sediment [(5)×(9)]	Bedload Sediment [(5)×(11)]	Suspended Sediment + Bedload Sediment [(13)+ (14)]
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>bed</sub> )	(S/S <sub>bed</sub> )	(tons/day)	(b <sub>f</sub> /b <sub>bed</sub> )	(tons/day)	(cfs)	(tons)	(tons)	(tons)
0%	91.2													
0.10%	78.2	0.05%	0.09%	0.34	84.7	2.363	7.461	49.39	6.670	11.24	29.1	16.94	3.86	20.80
0.25%	67.7	0.08%	0.15%	0.55	73.0	2.036	5.232	29.84	4.809	8.10	40.0	16.34	4.44	20.77
0.50%	58.5	0.13%	0.25%	0.91	63.1	1.761	3.706	18.28	3.494	5.89	57.6	16.68	5.37	22.05
0.75%	50.0	0.13%	0.25%	0.91	54.2	1.513	2.592	10.98	2.502	4.22	49.5	10.02	3.85	13.87
1%	43.2	0.13%	0.25%	0.91	46.6	1.300	1.817	6.62	1.790	3.02	42.5	6.04	2.75	8.79
1.5%	37.1	0.25%	0.50%	1.83	40.2	1.120	1.289	4.05	1.289	2.17	73.3	7.38	3.96	11.35
2%	31.0	0.25%	0.50%	1.83	34.0	0.949	0.886	2.35	0.893	1.50	62.1	4.30	2.74	7.04
3%	26.0	0.50%	1.00%	3.65	28.5	0.795	0.600	1.34	0.602	1.01	104.0	4.88	3.70	8.58
4%	22.3	0.50%	1.00%	3.65	24.2	0.674	0.424	0.80	0.415	0.70	88.2	2.92	2.55	5.48
5%	19.8	0.50%	1.00%	3.65	21.0	0.587	0.322	0.53	0.304	0.51	76.8	1.93	1.87	3.80
10%	12.5	2.50%	5.00%	18.25	16.1	0.450	0.200	0.25	0.165	0.28	294.5	4.60	5.07	9.67
20%	6.8	5.00%	10.00%	36.50	9.6	0.269	0.103	0.08	0.045	0.08	351.4	2.83	2.79	5.62
30%	4.5	5.00%	10.00%	36.50	5.7	0.158	0.075	0.03	0.006	0.01	206.7	1.20	0.39	1.60
40%	3.2	5.00%	10.00%	36.50	3.9	0.108	0.068	0.02	0.000	0.00	141.2	0.75	0.00	0.75
50%	2.5	5.00%	10.00%	36.50	2.8	0.079	0.066	0.01	0.000	0.00	103.3	0.53	0.00	0.53
60%	1.9	5.00%	10.00%	36.50	2.2	0.061	0.065	0.01	0.000	0.00	79.2	0.40	0.00	0.40
70%	1.5	5.00%	10.00%	36.50	1.7	0.047	0.064	0.01	0.000	0.00	62.0	0.31	0.00	0.31
80%	1.3	5.00%	10.00%	36.50	1.4	0.039	0.064	0.01	0.000	0.00	51.7	0.26	0.00	0.26
90%	0.9	5.00%	10.00%	36.50	1.1	0.032	0.064	0.01	0.000	0.00	41.3	0.21	0.00	0.21
100%	0.2	5.00%	10.00%	36.50	0.6	0.016	0.064	0.00	0.000	0.00	20.7	0.10	0.00	0.10
<b>Annual Totals:</b>											1,975.0 (cfs)	98.6 (tons/yr)	43.4 (tons/yr)	142.0 (tons/yr)
											3,917.5 (acre-ft)			

**Worksheet 19b.** Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Equation Type		Equation Source				Equation		Bankfull Discharge (cfs)		Bankfull Bedload Sediment (kg/s)	Bankfull Suspended Sediment (mg/l)			
1. Bedload Sediment		"Poor" Pagosa				$Y = 0.07176 + 1.02176x^{2.3772}$		35.85		0.4367	219.74			
2. Suspended Sediment		"Poor" Pagosa				$Y = 0.0989 + 0.9213x^{3.659}$								
		From Dimensional Flow-Duration Curve				From Sediment Rating Curves				Calculate		Calculate Sediment Yield		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Percentage of Time	Daily Mean Discharge	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Suspended Sediment Discharge	Suspended Sediment Discharge	Dimensionless Bedload Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow	Suspended Sediment	Bedload Sediment	Suspended Sediment + Bedload Sediment
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>bed</sub> )	(S/S <sub>bed</sub> )	(tons/day)	(b <sub>y</sub> /b <sub>bed</sub> )	(tons/day)	[(5)×(6)]	[(5)×(9)]	[(5)×(11)]	[(13)×(14)]
								(cfs)	(tons/day)	(tons/day)	(cfs)	(tons)	(tons)	(tons)
0%	121.4													
0.10%	108.5	0.05%	0.09%	0.34	114.9	3.206	65.506	4466.63	16.367	681.02	39.4	1532.50	233.66	1766.16
0.25%	97.9	0.08%	0.15%	0.55	103.2	2.879	44.227	2708.12	12.691	528.04	56.5	1482.69	289.10	1771.80
0.50%	88.7	0.13%	0.25%	0.91	93.3	2.604	30.649	1697.29	10.009	416.46	85.2	1548.78	380.02	1928.80
0.75%	80.2	0.13%	0.25%	0.91	84.5	2.356	21.290	1066.85	7.907	329.01	77.1	973.50	300.22	1273.72
1%	73.4	0.13%	0.25%	0.91	76.8	2.143	15.075	687.05	6.325	263.18	70.1	626.93	240.16	867.08
1.5%	66.9	0.25%	0.50%	1.83	70.2	1.957	10.851	451.69	5.114	212.78	128.1	824.33	388.33	1212.65
2%	60.3	0.25%	0.50%	1.83	63.6	1.774	7.606	287.01	4.064	169.11	116.1	523.79	308.63	832.42
3%	55.4	0.50%	1.00%	3.65	57.9	1.614	5.412	185.80	3.261	135.69	211.2	678.18	495.28	1173.46
4%	49.3	0.50%	1.00%	3.65	52.3	1.460	3.776	117.24	2.583	107.48	191.0	427.94	392.29	820.23
5%	43.6	0.50%	1.00%	3.65	46.4	1.294	2.467	67.91	1.958	81.49	169.4	247.87	297.43	545.29
10%	27.1	2.50%	5.00%	18.25	35.3	0.986	0.974	20.42	1.060	44.10	645.1	372.68	804.74	1177.42
20%	9.4	5.00%	10.00%	36.50	18.2	0.509	0.177	1.91	0.277	11.52	666.1	69.86	420.66	490.52
30%	4.7	5.00%	10.00%	36.50	7.0	0.196	0.101	0.42	0.093	3.87	256.5	15.41	141.24	156.66
40%	3.2	5.00%	10.00%	36.50	4.0	0.110	0.099	0.23	0.077	3.21	144.3	8.49	117.20	125.70
50%	2.5	5.00%	10.00%	36.50	2.8	0.079	0.099	0.17	0.074	3.09	103.3	6.07	112.70	118.77
60%	1.9	5.00%	10.00%	36.50	2.2	0.061	0.099	0.13	0.073	3.04	79.2	4.65	110.96	115.61
70%	1.5	5.00%	10.00%	36.50	1.7	0.047	0.099	0.10	0.072	3.02	62.0	3.64	110.09	113.72
80%	1.3	5.00%	10.00%	36.50	1.4	0.039	0.099	0.08	0.072	3.01	51.7	3.03	109.70	112.73
90%	0.9	5.00%	10.00%	36.50	1.1	0.032	0.099	0.07	0.072	3.00	41.3	2.43	109.40	111.83
100%	0.2	5.00%	10.00%	36.50	0.6	0.016	0.099	0.03	0.072	2.99	20.7	1.21	109.06	110.28
<b>Annual Totals:</b>											3,214.3 (cfs)	9,354.0 (tons/yr)	5,470.9 (tons/yr)	14,824.8 (tons/yr)
											6,375.5 (acre-ft)			

# POWERSED Model – Sediment Transport Capacity

**Worksheet 20a.** Sediment transport prediction representing the upstream supply up to bankfull for bedload and suspended sand sediment.

Stream: Trail Creek, Upstream Existing Sediment Supply		Location: Pike National Forest, Colorado		Valley Type: VIII		Stream Type: F4b		Gage Station #: Used Post-Fire Dimensionless F-D C.		Date: 08/14/10											
Observers: S=028, Q=36, 28, Bed.=9608, S.Sand=109.87		Stream Type: F4b		Valley Type: VIII		Stream Type: F4b		Gage Station #: Used Post-Fire Dimensionless F-D C.		Date: 08/14/10											
Flow-duration curve			Calculate				Measure					Hydraulic geometry					Calculate				
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)				
Percentage of time	Daily mean discharge	Mil-ordinate stream-flow	Area	Width	Depth	Velocity	Slope	Shear stress	Stream power	Unit power	Time increment	Time increment	Daily mean bedload transport	Daily mean suspended sand transport	Time adjusted bedload transport	Time adjusted suspended sand transport	Time adjusted total transport				
(%)	(cfs)	(cfs)	(ft <sup>2</sup> )	(ft)	(ft)	(ft/s)	(ft/ft)	(lb/ft <sup>2</sup> )	(lb/s)	(lb/ft/s)	(%)	(days)	(tons/day)	(tons/day)	[(13)x(14)]	[(13)x(15)]	[(16)+*(17)]				
100.00%	0.19										0%			0.00	0.00	0.00	0.00				
90.00%	0.94	0.57	0.54	5.18	0.10	0.95	0.0280	0.18	1.00	0.19	10%	36.50	2.98	0.02	108.77	0.73	109.50				
80.00%	1.32	1.13	0.88	6.02	0.15	1.24	0.0280	0.25	1.97	0.33	10%	36.50	2.98	0.03	108.77	1.09	109.86				
70.00%	1.51	1.42	1.02	6.24	0.16	1.33	0.0280	0.28	2.48	0.40	10%	36.50	2.98	0.04	108.77	1.46	110.23				
60.00%	1.89	1.70	1.16	6.45	0.18	1.42	0.0280	0.31	2.97	0.46	10%	36.50	3.02	0.05	110.23	1.83	112.06				
50.00%	2.45	2.17	1.39	6.79	0.20	1.56	0.0280	0.36	3.79	0.56	10%	36.50	3.02	0.06	110.23	2.19	112.42				
40.00%	3.21	2.83	1.64	7.02	0.23	1.69	0.0280	0.41	4.94	0.70	10%	36.50	3.07	0.08	112.05	2.92	114.97				
30.00%	4.70	3.96	2.06	7.40	0.28	1.91	0.0280	0.48	6.92	0.94	10%	36.50	3.20	0.12	116.80	4.38	121.18				
20.00%	9.36	7.03	3.01	8.02	0.38	2.32	0.0280	0.65	12.28	1.53	10%	36.50	3.84	0.21	140.16	7.67	147.83				
10.00%	27.14	18.25	5.74	9.50	0.60	3.17	0.0280	1.03	31.89	3.36	10%	36.50	11.40	0.95	416.10	34.67	450.77				
5.00%	43.55	35.35	11.78	21.41	0.55	2.99	0.0280	0.94	61.76	2.88	5%	18.25	43.59	10.08	795.52	183.96	979.48				
4.00%	49.25	46.40																			
3.00%	55.41	52.33																			
2.00%	60.32	57.87																			
1.50%	66.88	63.60																			
1.00%	73.44	70.16																			
0.75%	80.19	76.82																			
0.50%	88.73	84.46																			
0.25%	97.95	93.34																			
0.10%	108.47	103.21																			
0.0060%	121.38	114.93																			
Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr):															2127.4	240.9	2368.3				



**Worksheet 20b.** Sediment transport prediction for the existing condition reach compared to the upstream sediment supply to assess bed stability.

Stream: Trail Creek, F4b Poor Mainstem, Rifle XS 3+75													Location: Pike National Forest, Colorado (Used "POOR" Curves)			Date: 08/14/10	
Observers: S=028, Q=36, 28, Bed.=9608, S.Sand=109.87													Stream Type: F4b			Gage Station #: Used Post-Fire Dimensionless F-D C.	
Valley Type: VIII													Calculate				
Flow-duration curve			Hydraulic geometry				Measure			Calculate							
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
Percentage of time	Daily mean discharge	Mid-ordinate stream-flow	Area	Width	Depth	Velocity	Slope	Shear stress	Stream power	Unit power	Time increment	Time increment	Daily mean bedload transport	Daily mean suspended sand transport	Time adjusted bedload transport [(13)×(14)]	Time adjusted suspended sand transport [(13)×(15)]	Time adjusted total transport [(16)×(17)]
(%)	(cfs)	(cfs)	(ft <sup>2</sup> )	(ft)	(ft)	(ft/s)	(ft/ft)	(lb/ft <sup>2</sup> )	(lb/s)	(lb/ft/s)	(%)	(days)	(tons/day)	(tons/day)	(tons)	(tons)	(tons)
100.00%	0.19										0%			0.00	0.00	0.00	0.00
90.00%	0.94	0.57	0.43	4.45	0.10	1.19	0.0280	0.17	1.00	0.22	10%	36.50	2.98	0.02	108.77	0.73	109.50
80.00%	1.32	1.13	0.73	5.65	0.13	1.51	0.0280	0.22	1.97	0.35	10%	36.50	2.98	0.03	108.77	1.09	109.86
70.00%	1.51	1.42	0.85	5.97	0.14	1.59	0.0280	0.24	2.48	0.42	10%	36.50	2.98	0.04	108.77	1.46	110.23
60.00%	1.89	1.70	0.97	6.28	0.15	1.68	0.0280	0.26	2.97	0.47	10%	36.50	3.02	0.05	110.23	1.83	112.06
50.00%	2.45	2.17	1.17	6.81	0.17	1.82	0.0280	0.29	3.79	0.56	10%	36.50	3.02	0.06	110.23	2.19	112.42
40.00%	3.21	2.83	1.39	7.17	0.19	1.99	0.0280	0.33	4.94	0.69	10%	36.50	3.07	0.08	112.05	2.92	114.97
30.00%	4.70	3.96	1.71	7.31	0.23	2.25	0.0280	0.40	6.92	0.95	10%	36.50	3.20	0.12	116.80	4.38	121.18
20.00%	9.36	7.03	2.49	7.71	0.32	2.79	0.0280	0.55	12.28	1.59	10%	36.50	4.10	0.22	149.65	8.03	157.68
10.00%	27.14	18.25	5.28	11.92	0.44	3.44	0.0280	0.75	31.89	2.68	10%	36.50	8.60	0.80	313.90	29.20	343.10
5.00%	43.55	35.35															
4.00%	49.25	46.40															
3.00%	55.41	52.33															
2.00%	60.32	57.87															
1.50%	66.88	63.60															
1.00%	73.44	70.16															
0.75%	80.19	76.82															
0.50%	88.73	84.46															
0.25%	97.95	93.34															
0.10%	108.47	103.21															
0.0060%	121.38	114.93															

Notes:		Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr):	1239.2	51.8	1291.0
		Upstream total annual sediment supply (tons/yr) (Worksheet 5-12a):	2127.4	240.9	2368.3
		Difference in sediment transport capacity (tons/yr) (+ or -):	-888.2	-189.1	-1077.3
		Stability evaluation: Aggradation, Degradation or Stable:	Aggradation, > 45% Reduction in Transport		

## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>Trail Creek, F4b Poor Mainstem</b>		Stream Type: <b>F4b</b>	
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>	
Observers: <b>Rosgen et al.</b>		Date: <b>8/13/2010</b>	
<b>Enter Required Information for Existing Condition</b>			
13.5	$D_{50}$	Riffle bed material $D_{50}$ (mm)	
50.6	$D_{50}^{\wedge}$	Bar sample $D_{50}$ (mm)	
0.36	$D_{max}$	Largest particle from bar sample (ft)	110 (mm) 304.8 mm/ft
0.028	S	Existing bankfull water surface slope (ft/ft)	
0.53	d	Existing bankfull mean depth (ft)	
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment	
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>			
0.27	$D_{50}/D_{50}^{\wedge}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 ( D_{50}/D_{50}^{\wedge} )^{-0.872}$
8.15	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 ( D_{max}/D_{50} )^{-0.887}$
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED: 1
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>			
N/A	d	Required bankfull mean depth (ft)	$d = \frac{\tau^*(\gamma_s - 1)D_{max}}{S}$ (use $D_{max}$ in ft)
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>			
N/A	S	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^*(\gamma_s - 1)D_{max}}{d}$ (use $D_{max}$ in ft)
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading			
<b>Sediment Competence Using Dimensional Shear Stress</b>			
0.926	Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d ) $\gamma = 62.4$ , d = existing depth, S = existing slope		
Shields 65	CO 150	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ (Figure 5-49)	
Shields 1.2	CO 0.65	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) (Figure 5-49)	
Shields 0.69	CO 0.37	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm) $\tau =$ predicted shear stress, $\gamma = 62.4$ , S = existing slope	$d = \frac{\tau}{\gamma S}$
Shields 0.0363	CO 0.0197	Predicted slope required to initiate movement of measured $D_{max}$ (mm) $\tau =$ predicted shear stress, $\gamma = 62.4$ , d = existing depth	$S = \frac{\tau}{\gamma d}$
Check: <input checked="" type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading			

## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>Trail Creek, F4b Poor Mainstem</b>	Stream Type: <b>F4b</b>
Location: <b>Pike National Forest, CO</b>	Valley Type: <b>VIII</b>
Observers: <b>Rosgen et al.</b>	Date: <b>8/13/2010</b>
<b>Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)</b>	<b>Stability Rating (Check Appropriate Rating)</b>
Stream Type at potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	<input type="checkbox"/> Stable
(E→C), (C→High W/d C)	<input type="checkbox"/> Moderately Unstable
(G→F), (F→D), (C→F)	<input checked="" type="checkbox"/> Unstable
(C→D), (B→G), (D→G), (C→G), (E→G)	<input type="checkbox"/> Highly Unstable

**Worksheet 5-25.** Lateral stability.

Stream: <b>Trail Creek, F4b Poor Mainstem Reach</b>		Stream Type: <b>F4b</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>Rosgen et al.</b>		Date: <b>8/13/2010</b>			
Lateral stability criteria (choose one stability category for each criterion 1-5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	8
	(2)	(4)	(6)	2.6 (8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	2
	(1)	B4 (2)	(3)	(4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		1
	M3 (1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	8
	(2)	(4)	(6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	1
	0.8 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>20</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input type="checkbox"/>	<i>Unstable</i> 13 – 21 <input checked="" type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	

**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>Trail Creek, F4b Poor Mainstem Reach</b>		Stream Type: <b>F4b</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>Rosgen et al.</b>		Date: <b>8/13/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
1 <b>Sediment competence</b> (Worksheet 5-22)	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope—slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	1
	(1)	(4)	(6)	(8)	
2 <b>Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	6
	(2)	(4)	≈ 18% (6)	(8)	
3 <b>W/d Ratio State</b> (Worksheet 5-13)	1.0 – 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	8
	(2)	(4)	(6)	2.6 (8)	
4 <b>Stream Succession States</b> (Worksheet 5-24)	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	6
	(2)	(4)	(6)	(8)	
5 <b>Depositional Patterns</b> (Worksheet 5-10)	B1	B2, B4	B3, B5	B6, B7, B8	2
	(1)	B4 (2)	(3)	(4)	
6 <b>Debris / Blockages</b> (Worksheet 5-11)	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	1
	D3 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>24</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
Vertical Stability for Excess Deposition / Aggradation (use total points and check stability rating)	<i>No Deposition</i> 10 – 14 <input type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input checked="" type="checkbox"/>	<i>Aggradation</i> > 30 <input type="checkbox"/>	

**Worksheet 5-27.** Vertical stability – degradation.

Stream: <b>Trail Creek, F4b Poor Mainstem Reach</b>		Stream Type: <b>F4b</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>Rosgen et al.</b>		Date: <b>8/13/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>1 Sediment Competence</b> (Worksheet 5-22)	Does not indicate excess competence	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed	$D_{100}$ of bed moved	Particles much larger than $D_{100}$ of bed moved	2
	(2)	(4)	(6)	(8)	
<b>2 Sediment Capacity</b> (POWERSED) (Worksheet 5-20)	Does not indicate excess capacity	Slight excess energy: up to 10% increase above reference	Excess energy sufficient to increase load up to 50% of annual load	Excess energy transporting more than 50% of annual load	2
	(2)	(4)	(6)	(8)	
<b>3 Degree of Channel Incision (BHR)</b> (Worksheet 5-12)	1.00 – 1.10	1.11 – 1.30	1.31 – 1.50	> 1.50	2
	(2)	(4)	(6)	(8)	
<b>4 Stream Succession States</b> (Worksheets 5-12 and 5-24)	Does not indicate incision or degradation	If BHR > 1.1 and stream type has W/d between 5–10	If BHR > 1.1 and stream type has W/d less than 5	(B→G), (C→G), (E→G), (D→G)	2
	(2)	(4)	(6)	(8)	
<b>5 Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.80 – 1.00	0.30 – 0.79	0.10 – 0.29	< 0.10	1
	0.80	(1)	(2)	(3)	
<b>Total Points</b>					<b>9</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation</b> (use total points and check stability rating)	<i>Not Incised</i> 9 – 11 <input checked="" type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input type="checkbox"/>	<i>Degradation</i> > 27 <input type="checkbox"/>	

Worksheet 5-28. Channel enlargement.

Stream: <b>Trail Creek, F4b Poor Mainstem Reach</b>		Stream Type: <b>F4b</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>Rosgen et al.</b>		Date: <b>8/13/2010</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1-4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	6
	(2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	6
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	6
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	2
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>20</b>
<b>Category Point Range</b>					
<b>Channel Enlargement Prediction (use total points and check stability rating)</b>	<i>No Increase</i> 8 – 10 <input type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input checked="" type="checkbox"/>	<i>Extensive</i> > 24 <input type="checkbox"/>	

Worksheet 5-29. Overall sediment supply.

Stream: <b>Trail Creek, F4b Poor Mainstem Reach</b>		Stream Type: <b>F4b</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>		
Observers: <b>Rosgen et al.</b>		Date: <b>8/13/2010</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1-5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	3	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	3	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	1	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	3	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	4	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>14</b>	
<b>Category Point Range</b>				
Overall Sediment Supply Rating (use total points and check stability rating)	<i>Low</i> 5 <input type="checkbox"/>	<i>Moderate</i> 6 – 10 <input type="checkbox"/>	<i>High</i> 11 – 15 <input checked="" type="checkbox"/>	<i>Very High</i> 16 – 20 <input type="checkbox"/>



Worksheet 5-32. Summary of stability condition categories.

Stream: <b>Trail Creek, F4b Poor Mainstem Reach</b>		Location: <b>Pike National Forest, Colorado</b>	
Observers: <b>Rosgen et al.</b>		Stream Type: <b>F4b</b> Valley Type: <b>VIII</b>	
Date: <b>8/13/2010</b>		Width of Flood-Prone Area (ft): <b>24.04</b> Entrenchment Ratio: <b>1.4</b>	
Channel Dimension (Rifle XS 3+75)	Mean Bankfull Depth (ft): <b>0.53</b>	Cross-Sectional Area (ft <sup>2</sup> ): <b>17.15</b>	
Channel Pattern	Mean: $\lambda_r/W_{bkf}$ : <b>9.9</b> Range: <b>7.7-11.8</b>	$R_c/W_{bkf}$ : <b>10.7</b> <b>7.9-12.8</b>	MWR: <b>1.99</b> <b>1.17-2.82</b> Sinuosity: <b>1.25</b>
River Profile & Bed Features	<input checked="" type="checkbox"/> Riffle/Pool <input type="checkbox"/> Step/Pool <input type="checkbox"/> Plane Bed <input type="checkbox"/> Convergence/Divergence <input type="checkbox"/> Dunes/Antidunes/Smooth Bed	Rifle Pool	Pool-to-Pool Ratio
	Max Bankfull Depth (ft): <b>1.49</b>	Depth Ratio (max to mean): <b>1.987</b>	Pool Spacing: <b>1.51</b> Valley: <b>0.035</b> Water Surface: <b>0.028</b>
Riparian Current Composition/Density: <b>Willow, C-wd., c-junc/High</b>		Remarks: Condition, Vigor & Usage of Existing Reach:	
Vegetation <b>Alder, Willow, Forbs/Mod.</b>		<b>Active bank erosion precludes colonization.</b>	
Flow Regime: <b>P1, Stream Size S-4(3)</b>		Depositional Patterns: <b>B4</b> Debris/Channel Blockages: <b>D3</b>	
Degree of Incision (Bank-Height Ratio): <b>1.0</b>		Modified Pfankuch Stability Rating (Numeric & Adjective Rating): <b>134 (Poor)</b>	
Level III Stream Stability Indices	Width/depth Ratio (W/d): <b>32.4</b>	Width/Depth Ratio State (W/d) / (W/d <sub>ref</sub> ): <b>12.6</b>	W/d Ratio State Stability Rating: <b>Highly Unstable</b>
	Meander Width Ratio (MWR): <b>2.13</b>	Reference MWR <sub>ref</sub> : <b>2.7</b>	MWR / MWR <sub>ref</sub> Stability Rating: <b>Unconfined</b>
Bank Erosion Summary	Length of Reach Studied (ft): <b>322</b>	Annual Streambank Erosion Rate: <b>152</b> (tons/yr) <b>0.4721</b> (tons/yrft)	Curve Used: <b>Colorado</b> Remarks:
Sediment Capacity (POWERSED)	<input checked="" type="checkbox"/> Sufficient Capacity <input type="checkbox"/> Insufficient Capacity <input type="checkbox"/> Excess Capacity	Remarks: <b>&gt;18% Reduction in Transport</b>	
Entrainment/Competence	Largest Particle from Bar Sample (mm): <b>B → G → F → B → A</b>	$\tau = 2.2$ $\tau^* = N/A$ Existing Depth: <b>1.3</b>	Required Depth: <b>0.75</b> Existing Slope: <b>0.03</b> Required Slope: <b>0.02</b>
Successional Stage Shift	<b>B → G → F → B → A</b>	Existing Stream State (Type): <b>F4b</b>	Potential Stream State (Type): <b>B4</b>
Lateral Stability	<input type="checkbox"/> Stable <input type="checkbox"/> Mod. Unstable <input checked="" type="checkbox"/> Unstable	Remarks/causes: <b>Fire and flood effects</b>	
Vertical Stability (Aggradation)	<input type="checkbox"/> No Deposition <input type="checkbox"/> Mod. Deposition <input checked="" type="checkbox"/> Ex. Deposition <input type="checkbox"/> Aggradation	Remarks/causes: <b>Fire and flood effects</b>	
Vertical Stability (Degradation)	<input checked="" type="checkbox"/> Not Incised <input type="checkbox"/> Slightly Incised <input type="checkbox"/> Mod. Incised <input type="checkbox"/> Degradation	Remarks/causes: <b>Fire and flood effects</b>	
Channel Enlargement	<input type="checkbox"/> No Increase <input type="checkbox"/> Slight Increase <input checked="" type="checkbox"/> Mod. Increase <input type="checkbox"/> Extensive	Remarks/causes: <b>Fire and flood effects</b>	
Sediment Supply (Channel Source)	<input type="checkbox"/> Low <input type="checkbox"/> Moderate <input checked="" type="checkbox"/> High <input type="checkbox"/> Very High	Remarks/causes: <b>Fire and flood effects</b>	



# *Appendix C14*

## **F4b Stream Type** *Poor Stability Trib. Reach*



# Table of Contents

## Appendix C14: F4b Poor Trib. Reach

<b>Reach Location &amp; Overview.....</b>	<b>C14-2</b>
<b>Survey Summary.....</b>	<b>C14-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C14-7</b>
<b>Velocity, Classification &amp; Morphological Relations.....</b>	<b>C14-7</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b>Stability Indices.....</b>	<b>C14-11</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b>BANCS Model – Streambank Erosion.....</b>	<b>C14-21</b>
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b>FLOWSED Model – Total Annual Sediment Yield.....</b>	<b>C14-23</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b>POWERSED Model– Sediment Transport Capacity to Assess Bed Stability.....</b>	<b>C14-25</b>
Worksheet 5-20a. Sediment transport prediction for the upstream condition.	
Worksheet 5-20b. Sediment transport prediction for the existing condition.	
<b>Sediment Competence/Entrainment.....</b>	<b>C14-27</b>
Worksheet 5-22. Sediment competence calculations.	
<b>Channel Stability Ratings.....</b>	<b>C14-28</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b>Summary.....</b>	<b>C14-34</b>
Worksheet 5-32. Summary of stability condition categories.	

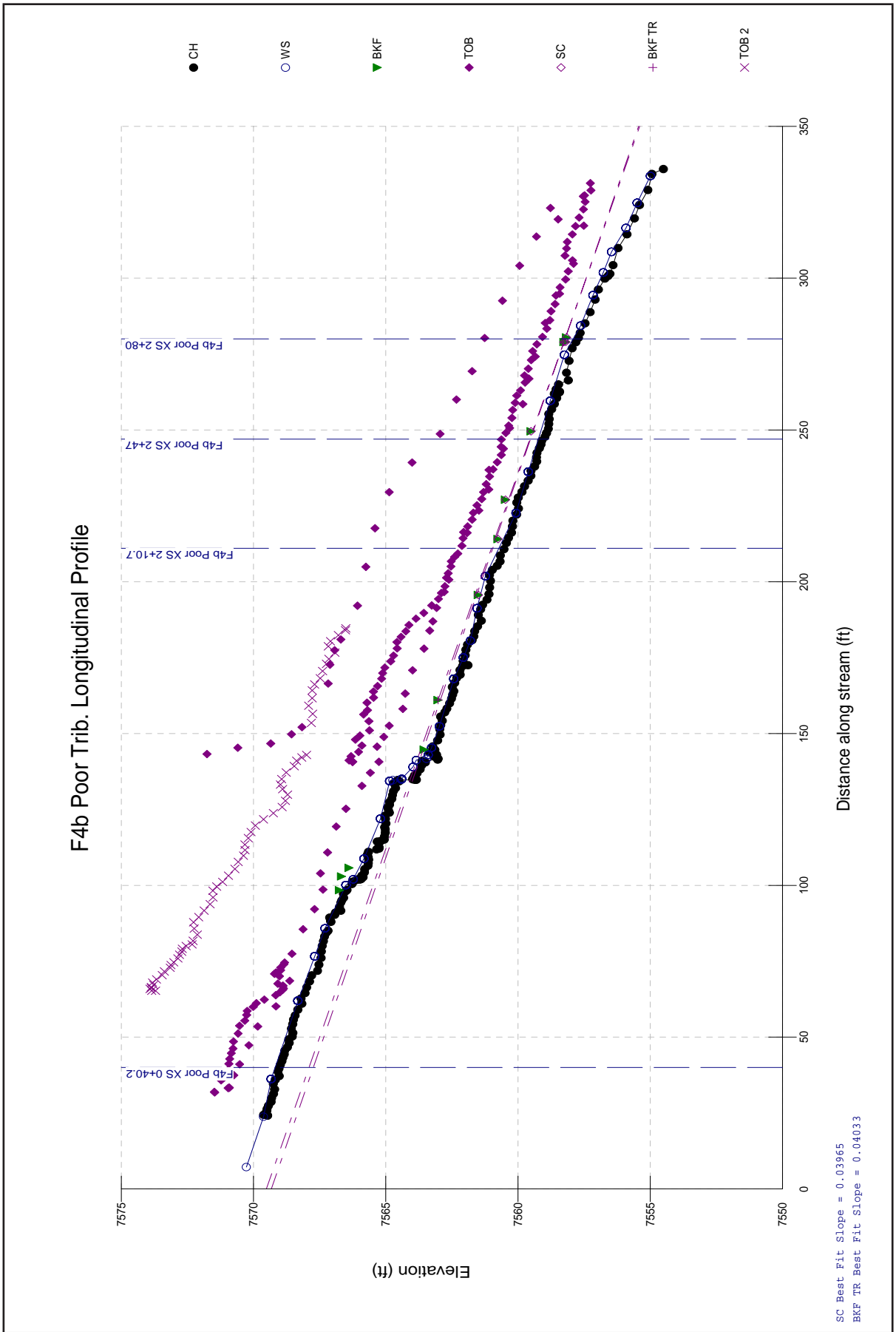
## F4b Poor Trib. Reach Location & Overview

The F4b Poor tributary representative reach is a perennial, relatively steep gradient, entrenched stream located in the upper Trail Creek Watershed (see location map **Figure C-2**). This channel had previously been a D4 stream type on an active alluvial fan (Valley Type IIIa), then shifted to a G4 stream type, and over time has widened to the current F4b stream type. The stable potential stream type is a B4 stream type as the stream is apparently trying to recover from past floods and high sediment supply impacts. The width/depth ratio of 47 is very high and will continue to promote excess deposition and high streambank erosion. The stream is still enlarging due to the high peak flows following the fire. A POWERSED run was made to determine streambed stability, which approximated 129 tons/yr of deposition. The stability rating is “Poor” due to a Pfankuch stability rating of 144 (“Poor”) and the high streambank erosion rate of 0.39 tons/yr/ft. This rate is nearly two orders of magnitude larger than the B4 reference rate of 0.0048 tons/yr/ft. The sediment supply rating is *Very High*, typical of an F4b stream type, due to the high banks on both sides and sediment deposition in the bed. The “Poor” stability rating indicates a higher potential accelerated increase in flow-related sediment compared to the same-sized B4 reference stream type. The WRENSS model indicated that the water yield due to the fire increased from 921 acre-ft to 1,179 acre-ft, representing a total increase of 258 acre-ft. The corresponding bedload increased from 23 tons/yr to 709 tons/yr, and suspended sediment increased from 3.3 tons/yr to 558 tons/yr, representing a total increase in sediment of 1,240 tons/yr. This sediment yield increase is extremely high for a stream with a bankfull discharge of 8.4 cfs. The increased sediment supply is due to the very unstable banks and high width/depth ratio that encourages increased sediment deposition in the streambed. This increased sediment loading is equivalent to 95 ten-yard, end dump truck loads per year.

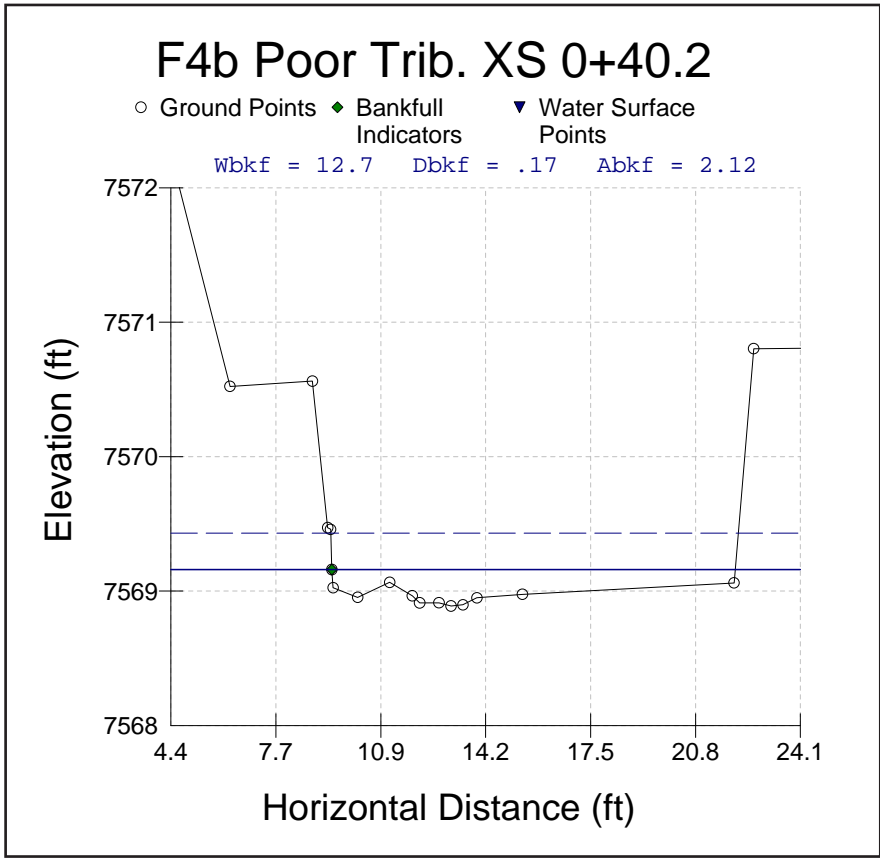
The photograph depicts the typical character of this representative F4b Poor stream type. The following graphs and summary worksheets provide the detail of the morphology, hydraulics, streambank erosion rates, and stability conditions responsible for the overall “Poor” rating.



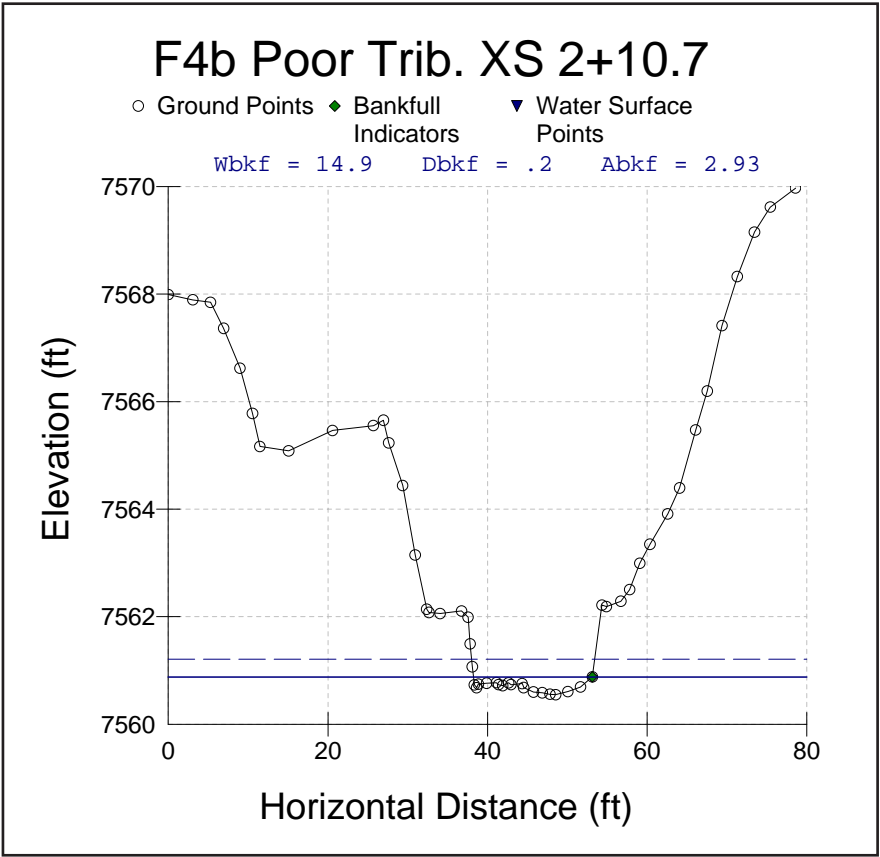
# Survey Summary



Longitudinal Profile (graph generated from RIVERMorph™)

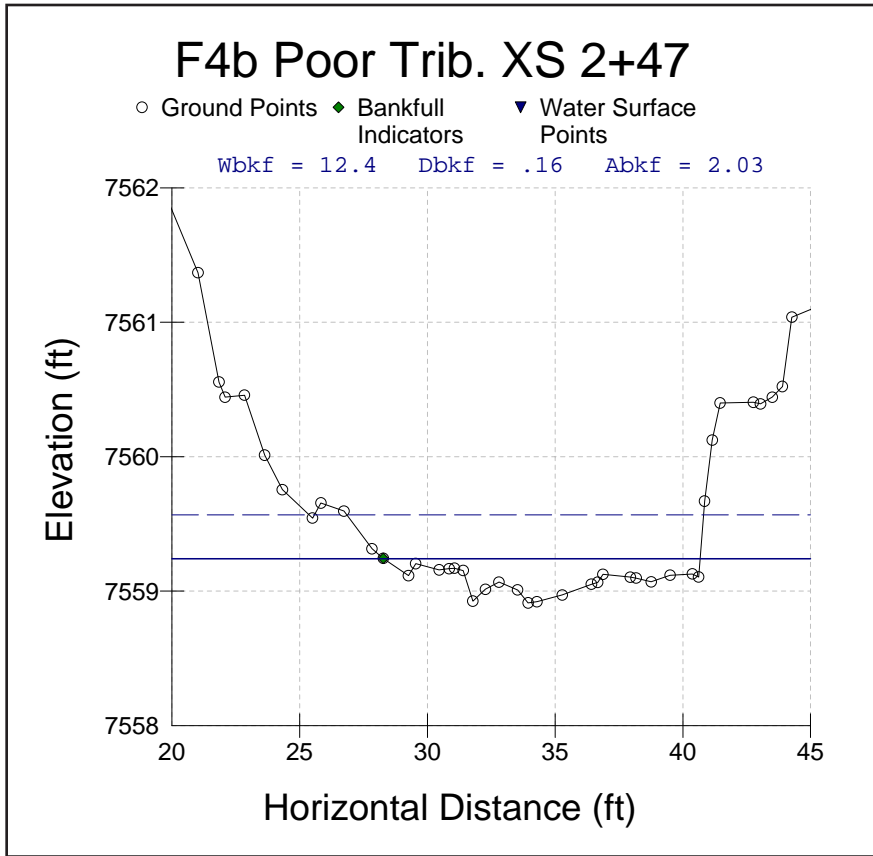


Riffle Cross-section 0+40.2 (graph generated from RIVERMorph™)

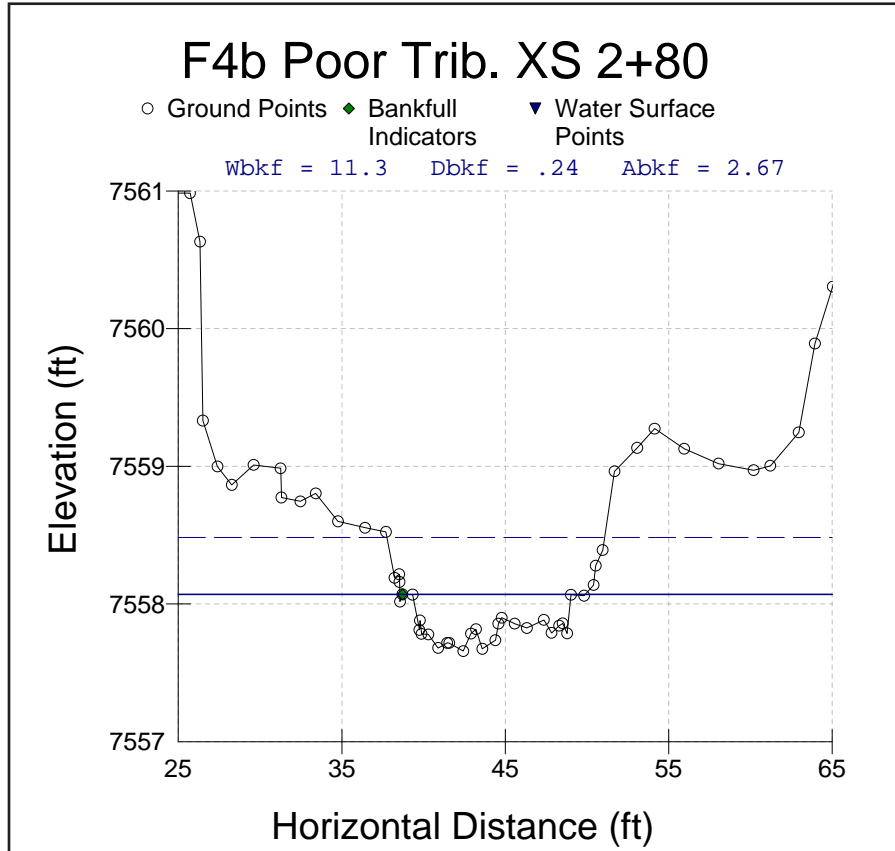


Riffle Cross-section 2+10.7 (graph generated from RIVERMorph™)

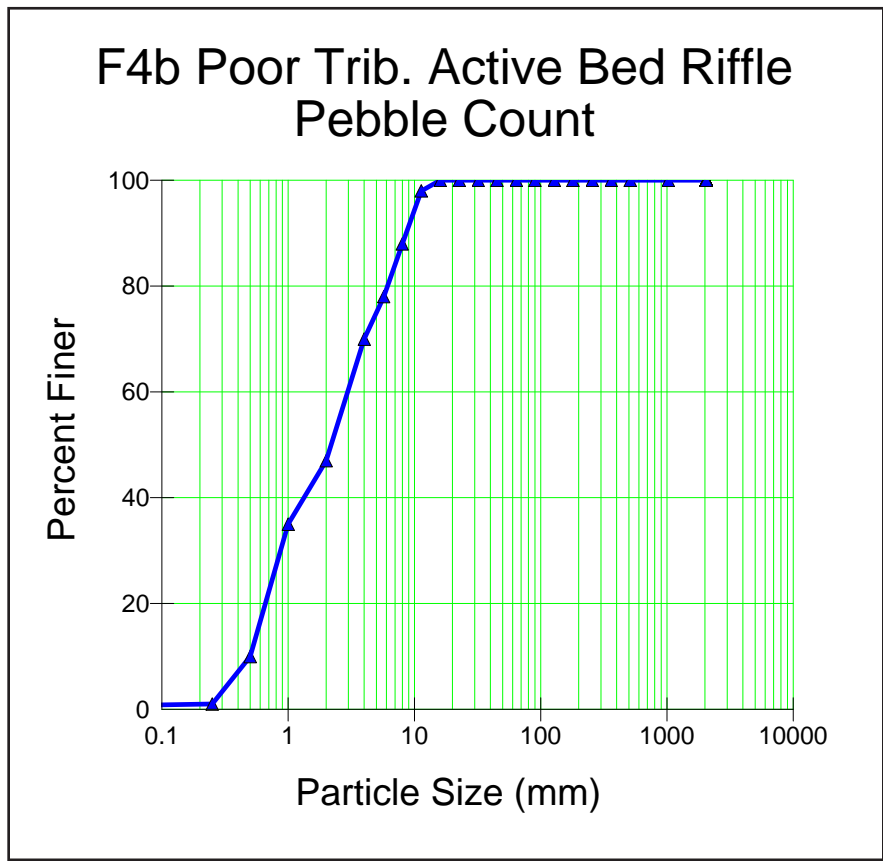




Riffle Cross-section 2+47 (graph generated from RIVERMorph™)



Representative Riffle Cross-Section 2+80 (graph generated from RIVERMorph™)



Active Bed Riffle Pebble Count (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates							
Stream:	Trail Creek, F4b Poor Trib. Reach			Location:	XS 2+80, Pike N.F., Colorado		
Date:	8/17/2010	Stream Type:	F4b	Valley Type:	III		
Observers:	Rosgen <i>et al.</i>			HUC:	-- -- -- -- -- -- -- -- -- --		
INPUT VARIABLES				OUTPUT VARIABLES			
Bankfull Riffle Cross-Sectional AREA	2.67	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.24	$d_{bkf}$ (ft)		
Bankfull Riffle WIDTH	11.35	$W_{bkf}$ (ft)	Wetted PERIMETER ~ (2 * $d_{bkf}$ ) + $W_{bkf}$	11.82	$W_p$ (ft)		
$D_{84}$ at Riffle	7.1	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.02	$D_{84}$ (ft)		
Bankfull SLOPE	0.04	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	0.23	R (ft)		
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R(ft) / $D_{84}$ (ft)	9.72	R / $D_{84}$		
Drainage Area	1.5	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.539	$u^*$ (ft/sec)		
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE	
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$				4.54	ft / sec	12.13	cfs
2. Roughness Coefficient: a) Manning's n from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.035$				3.16	ft / sec	8.43	cfs
2. Roughness Coefficient: b) Manning's n from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.041$				2.70	ft / sec	7.20	cfs
2. Roughness Coefficient: c) Manning's n from Jarrett (USGS): $n = 0.39 * S^{0.38} * R^{-0.16}$ Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for Stream Types A1, A2, A3, B1, B2, B3, C2 & E3 $n = 0.146$				0.76	ft / sec	2.03	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)					ft / sec		cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)					ft / sec		cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q =$ <input type="text"/> year $u = Q / A$					ft / sec		cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation (R/ $D_{84}$ ) – Estimation Method 1							
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.							
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.							
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.							
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.							

**Worksheet 5-3.** Level II stream classification.

Stream: <b>Trail Creek, F4b Poor Trib. Reach</b>	
Basin:	Drainage Area: <b>960</b> acres <b>1.5</b> mi <sup>2</sup>
Location: <b>Pike National Forest, Colorado</b>	
Twp.&Rge:	Sec.&Qtr.:
Cross-Section Monuments (Lat./Long.): <b>XS 2+80</b>	Date: <b>08/17/2010</b>
Observers: <b>Rosgen et al.</b>	Valley Type: <b>III</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>11.35</b> ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>0.24</b> ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>2.67</b> ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>47.29</b> ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>0.41</b> ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>13.31</b> ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>1.17</b> ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>2</b> mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.04</b> ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>1.04</b>

<b>Stream Type</b>	<b>F4b</b>	(See Figure 2-14)
--------------------	------------	-------------------

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, F4b Poor Trib. Reach</b>				Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>Rosgen et al.</b>				Date: <b>8/17/2010</b>		Valley Type: <b>III</b>		Stream Type: <b>F4b</b>	
<b>River Reach Dimension Summary Data.....1</b>									
<b>Riffle Dimensions* ** ***</b>	<b>Riffle Dimensions* ** ***</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Width ( $W_{bkt}$ )	12.83	11.35	14.89	ft	Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	2.44	2.03	2.93
	Mean Riffle Depth ( $d_{bkt}$ )	0.19	0.16	0.24	ft	Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	68.43	47.29	77.38
	Maximum Riffle Depth ( $d_{max}$ )	0.34	0.27	0.41	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max}/d_{bkt}$ )	1.75	1.59	2.06
	Width of Flood-Prone Area ( $W_{fpa}$ )	13.94	12.81	15.44	ft	Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )	1.09	1.01	1.17
	Riffle Inner Berm Width ( $W_{ib}$ )	5.65	5.59	5.70	ft	Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )	0.44	0.44	0.44
	Riffle Inner Berm Depth ( $d_{ib}$ )	0.09	0.08	0.09	ft	Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )	0.44	0.42	0.47
	Riffle Inner Berm Area ( $A_{ib}$ )	0.48	0.45	0.51	ft <sup>2</sup>	Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )	0.20	0.18	0.21
	Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )	66.61	63.33	69.88					
<b>Pool Dimensions* ** ***</b>	<b>Pool Dimensions* ** ***</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Pool Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Pool Width ( $W_{bkfp}$ )				ft	Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )			
	Mean Pool Depth ( $d_{bkfp}$ )				ft	Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )			
	Pool Cross-Sectional Area ( $A_{bkfp}$ )				ft	Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )			
	Maximum Pool Depth ( $d_{maxp}$ )				ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )			
	Pool Inner Berm Width ( $W_{ibp}$ )				ft	Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )			
	Pool Inner Berm Depth ( $d_{ibp}$ )				ft	Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )			
	Pool Inner Berm Area ( $A_{ibp}$ )				ft <sup>2</sup>	Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )			
Point Bar Slope ( $S_{pb}$ )				ft/ft	Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )				
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Run Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Run Width ( $W_{bkfr}$ )				ft	Run Width to Riffle Width ( $W_{bkfr} / W_{bkt}$ )			
	Mean Run Depth ( $d_{bkfr}$ )				ft	Mean Run Depth to Mean Riffle Depth ( $d_{bkfr} / d_{bkt}$ )			
	Run Cross-Sectional Area ( $A_{bkfr}$ )				ft	Run Area to Riffle Area ( $A_{bkfr} / A_{bkt}$ )			
	Maximum Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )			
Run Width/Depth Ratio ( $W_{bkfr} / d_{bkfr}$ )				ft					
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Glide Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Glide Width ( $W_{bkfg}$ )				ft	Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )			
	Mean Glide Depth ( $d_{bkfg}$ )				ft	Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )			
	Glide Cross-Sectional Area ( $A_{bkfg}$ )				ft	Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )			
	Maximum Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )			
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )				ft/ft	Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )			
	Glide Inner Berm Width ( $W_{ibg}$ )				ft	Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )			
	Glide Inner Berm Depth ( $d_{ibg}$ )				ft	Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )			
Glide Inner Berm Area ( $A_{ibg}$ )				ft <sup>2</sup>	Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )				
<b>Step**</b>	<b>Step Dimensions**</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Step Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Step Width ( $W_{bkfs}$ )				ft	Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )			
	Mean Step Depth ( $d_{bkfs}$ )				ft	Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )			
	Step Cross-Sectional Area ( $A_{bkfs}$ )				ft	Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )			
	Maximum Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )									

**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, F4b Poor Trib. Reach</b>		Location: <b>Pike National Forest, Colorado</b>												
Observers: <b>Rosgen et al.</b>		Date: <b>8/17/2010</b>	Valley Type: <b>III</b>											
		Stream Type: <b>F4b</b>												
<b>Hydraulics</b>	<b>River Reach Summary Data.....2</b>													
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )	<b>3.16</b>	ft/sec	Estimation Method	<b>"n" from FF/RR</b>									
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )	<b>8.43</b>	cfs	Drainage Area	<b>1.5</b> mi <sup>2</sup>									
<b>Channel Pattern</b>	<b>Geometry</b>			<b>Dimensionless Geometry Ratios</b>										
	Linear Wavelength ( $\lambda$ )			ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )									
	Stream Meander Length ( $L_m$ )			ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )									
	Radius of Curvature ( $R_c$ )			ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )									
	Belt Width ( $W_{bit}$ )	<b>18.3</b>	<b>14.0</b>	<b>27.4</b>	ft	Meander Width Ratio ( $W_{bit} / W_{bkt}$ )	<b>1.43</b>	<b>1.09</b>						
	Arc Length ( $L_a$ )				ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )								
	Riffle Length ( $L_r$ )				ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )								
	Individual Pool Length ( $L_p$ )				ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )								
Pool to Pool Spacing ( $P_s$ )				ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )									
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )	<b>0.0425</b>		ft/ft	Average Water Surface Slope ( $S$ )	<b>0.0410</b>		ft/ft	Sinuosity ( $S_{val} / S$ )	<b>1.04</b>				
	Stream Length (SL)	<b>304.3</b>		ft	Valley Length (VL)	<b>293.4</b>		ft	Sinuosity (SL / VL)	<b>1.04</b>				
	Low Bank Height (LBH)	start: <b>1.56</b>	ft	end: <b>1.32</b>	ft	Max Bankfull Depth ( $d_{max}$ )	start: <b>0.56</b>	ft	end: <b>0.45</b>	ft	Bank-Height Ratio (BHR) (LBH / $d_{max}$ )	start: <b>2.8</b>	end: <b>2.9</b>	
	<b>Facet Slopes</b>				<b>Dimensionless Facet Slope Ratios</b>									
	Riffle Slope ( $S_{rif}$ )	<b>0.0690</b>	<b>0.0280</b>	<b>0.0880</b>	ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.6829</b>	<b>0.6829</b>	<b>2.1463</b>					
	Run Slope ( $S_{run}$ )				ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )								
	Pool Slope ( $S_p$ )				ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )								
	Glide Slope ( $S_g$ )				ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )								
	Step Slope ( $S_s$ )				ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )								
	<b>Max Depths<sup>a</sup></b>				<b>Dimensionless Depth Ratios</b>									
	Max Riffle Depth ( $d_{max}$ )	<b>0.34</b>	<b>0.27</b>	<b>0.41</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>1.740</b>	<b>1.403</b>	<b>2.130</b>					
	Max Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )								
	Max Pool Depth ( $d_{maxp}$ )				ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )								
	Max Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )								
Max Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )									
<b>Channel Materials</b>	<b>Reach<sup>b</sup></b>		<b>Riffle<sup>c</sup></b>		<b>Bar</b>		<b>Reach<sup>b</sup></b>		<b>Riffle<sup>c</sup></b>		<b>Bar</b>		<b>Protrusion Height<sup>d</sup></b>	
	% Silt/Clay			<b>0</b>			$D_{16}$		<b>0.62</b>					mm
	% Sand			<b>47</b>			$D_{35}$		<b>1.00</b>					mm
	% Gravel			<b>53</b>			$D_{50}$		<b>2.26</b>					mm
	% Cobble			<b>0</b>			$D_{84}$		<b>7.08</b>					mm
	% Boulder			<b>0</b>			$D_{95}$		<b>10.31</b>					mm
	% Bedrock			<b>0</b>			$D_{100}$		<b>16.00</b>					mm

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.  
<sup>b</sup> Composite sample of riffles and pools within the designated reach.      <sup>c</sup> Active bed of a riffle.      <sup>d</sup> Height of roughness feature above bed.

## Stability Indices

**Worksheet 5-6.** Riparian vegetation.


Riparian Vegetation					
Stream: <b>Trail Creek, F4b Poor Trib. Reach</b>		Location: <b>Pike National Forest, Colorado</b>			
Observers: <b>Rosgen et al.</b>		Reference reach <input type="checkbox"/>	Disturbed (impacted reach) <input checked="" type="checkbox"/>	Date: <b>8/16/2010</b>	
Existing species composition: <b>Ponderosa Pine - 5% Burnt, Annual Grass/Forb, Cheatgrass</b>		Potential species composition: <b>Willow, Alder, Grass, Aspen</b>			
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition
<b>1. Overstory</b>	Canopy layer	<b>5%</b>	<b>&lt;1%</b>	<b>Ponderosa Pine</b>	<b>100%</b>
					<b>100%</b>
<b>2. Understory</b>	Shrub layer		<b>0%</b>		
					<b>100%</b>
<b>3. Ground level</b>	Herbaceous		<b>5%</b>	<b>Mullen Cheatgrass Ag Spic Annual grass Forbs</b>	
	Leaf or needle litter		<b>5%</b>	<b>Remarks:</b> Condition, vigor and/or usage of existing reach:	<b>100%</b>
	Bare ground		<b>90%</b>		
*Based on crown closure. **Based on basal area to surface area.			<b>Column total = 100%</b>		

**Worksheet 5-7.** Flow regime.

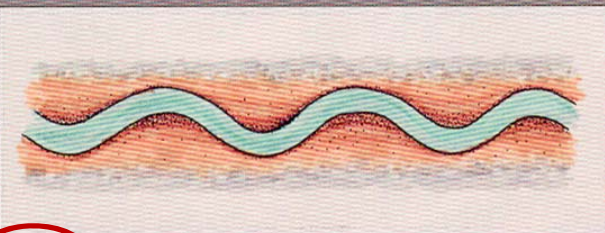



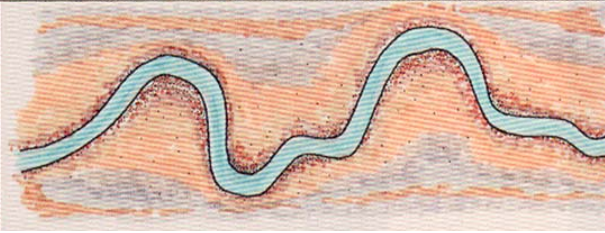
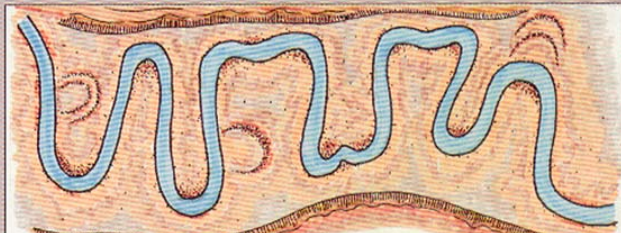
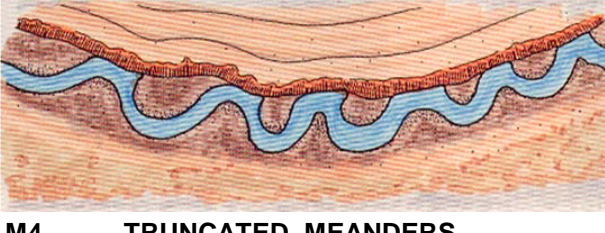

<b>FLOW REGIME</b>								
Stream: <b>Trail Creek, F4b Poor Trib.</b>			Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>Rosgen et al.</b>						Date: <b>8/16/2010</b>		
List ALL COMBINATIONS that APPLY.....			<b>E2</b>	<b>E8</b>	<b>S2</b>	<b>S8</b>		
<b>General Category</b>								
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation							
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
<b>P</b>	Perennial stream channels: Surface water persists yearlong.							
<b>Specific Category</b>								
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
<b>4</b>	Streamflow regulated by glacial melt.							
<b>5</b>	Ice flows/ice torrents from ice dam breaches.							
<b>6</b>	Alternating flow/backwater due to tidal influence.							
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.							
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
<b>9</b>	Rain-on-snow generated runoff.							



**Worksheet 5-8.** Stream order & stream size.

Stream Size and Order			
Stream:	Trail Creek, F4b Poor Trib. Reach		
Location:	Pike National Forest, Colorado		
Observers:	Rosgen <i>et al.</i>		
Date:	8/16/2010		
Stream Size Category and Order 			S-3(4)
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0.305	<1	<input type="checkbox"/>
S-2	0.3 – 1.5	1 – 5	<input type="checkbox"/>
<b>S-3</b>	<b>1.5 – 4.6</b>	<b>5 – 15</b>	<input checked="" type="checkbox"/>
S-4	4.6 – 9	15 – 30	<input type="checkbox"/>
S-5	9 – 15	30 – 50	<input type="checkbox"/>
S-6	15 – 22.8	50 – 75	<input type="checkbox"/>
S-7	22.8 – 30.5	75 – 100	<input type="checkbox"/>
S-8	30.5 – 46	100 – 150	<input type="checkbox"/>
S-9	46 – 76	150 – 250	<input type="checkbox"/>
S-10	76 – 107	250 – 350	<input type="checkbox"/>
S-11	107 – 150	350 – 500	<input type="checkbox"/>
S-12	150 – 305	500 – 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
Stream Order			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			

Worksheet 5-9. Meander patterns.

<b>Meander Patterns</b>					
Stream: <b>Trail Creek, F4b Poor Trib. Reach</b>		Location: <b>Pike National Forest, CO</b>			
Observers: <b>Rosgen et al.</b>		Date: <b>8/16/2010</b>			
List ALL CATEGORIES that APPLY	<b>M1</b>				
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>					
 <b>M1</b> <b>REGULAR MEANDERS</b>	 <b>M5</b> <b>UNCONFINED MEANDER SCROLLS</b>				
 <b>M2</b> <b>TORTUOUS MEANDERS</b>	 <b>M6</b> <b>CONFINED MEANDER SCROLLS</b>				
 <b>M3</b> <b>IRREGULAR MEANDERS</b>	 <b>M7</b> <b>DISTORTED MEANDER LOOPS</b>				
 <b>M4</b> <b>TRUNCATED MEANDERS</b>	 <b>M8</b> <b>IRREGULAR MEANDERS with oxbows and</b>				

**Worksheet 5-10.** Depositional patterns.

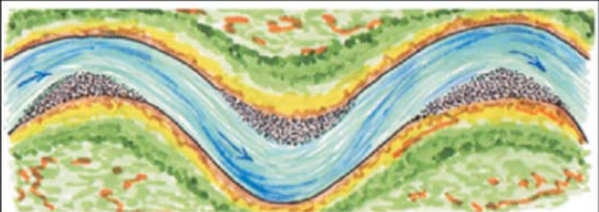


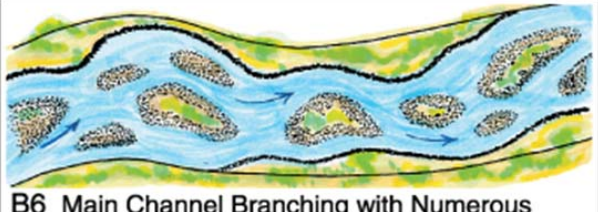
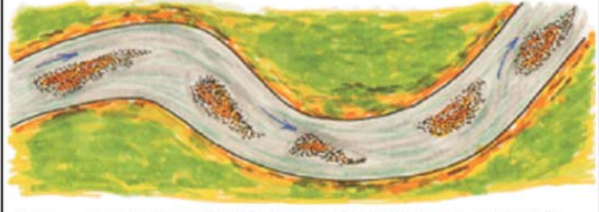
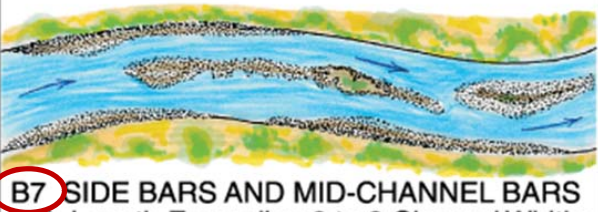


**Depositional Patterns**

Stream: **Trail Creek, F4b Poor Trib. Reach**                      Location: **Pike National Forest, Colorado**

Observers: **Rosgen et al.**    Date: **8/16/2010**

List ALL CATEGORIES that APPLY	<b>B5</b>	<b>B7</b>			
--------------------------------	-----------	-----------	--	--	--

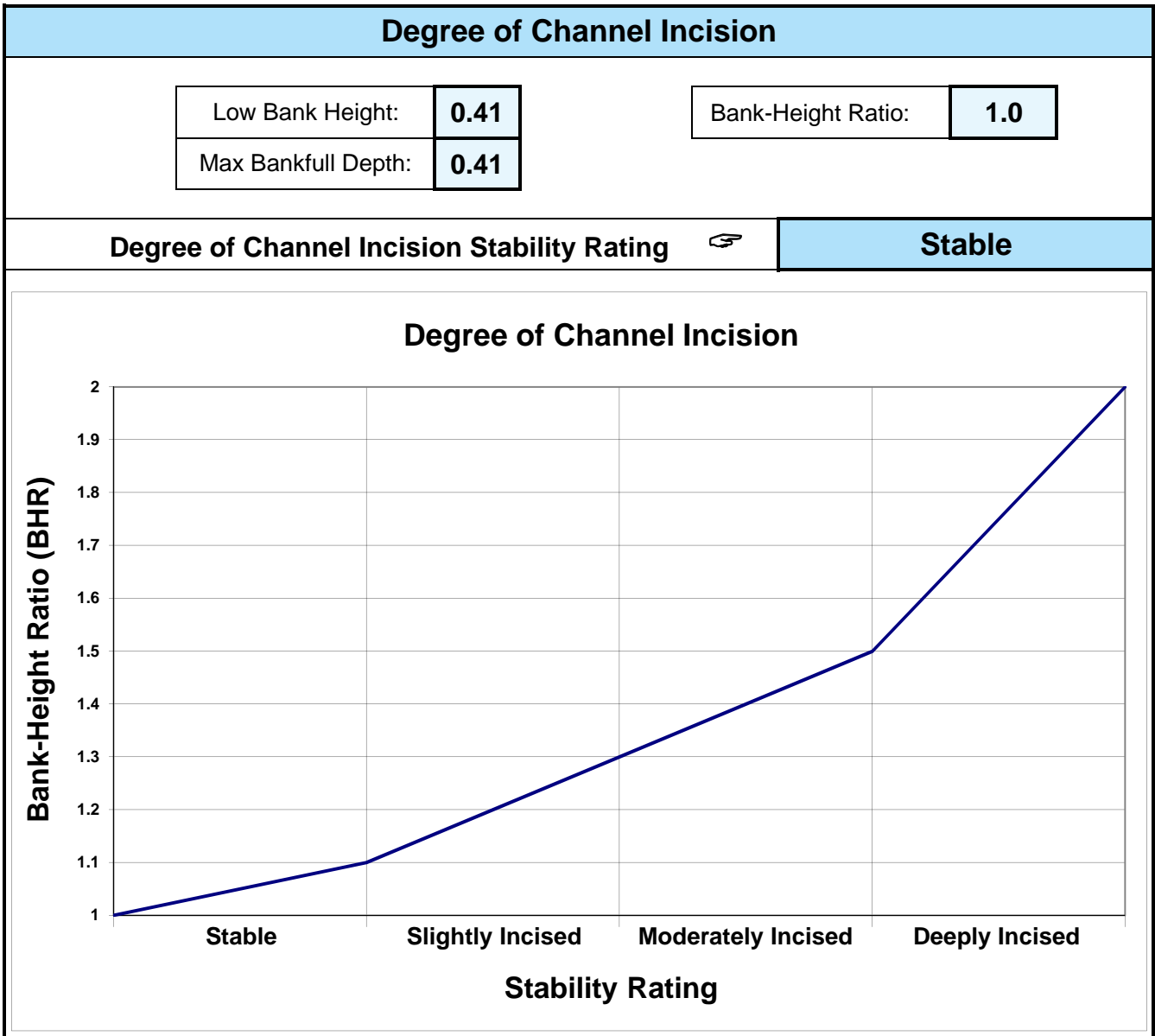
*Various Depositional Features modified from Galay et al. (1973)*

 <p><b>B1</b>                      <b>POINT BARS</b></p>	 <p><b>B5</b>                      <b>DIAGONAL BARS</b></p>
 <p><b>B2</b>    <b>POINT BARS with Few MID-CHANNEL BARS</b></p>	 <p><b>B6</b> <b>Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</b></p>
 <p><b>B3</b>    <b>NUMEROUS MID-CHANNEL BARS</b></p>	 <p><b>B7</b> <b>SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</b></p>
 <p><b>B4</b>                      <b>SIDE BARS</b></p>	 <p><b>B8</b>                      <b>DELTA BARS</b></p>

**Worksheet 5-11.** Channel blockages.

Channel Blockages		
Stream: <b>Trail Creek, F4b Poor Trib. Reach</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>Rosgen et al.</b>		Date: <b>8/16/2010</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input checked="" type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input type="checkbox"/>
<b>D4</b> Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

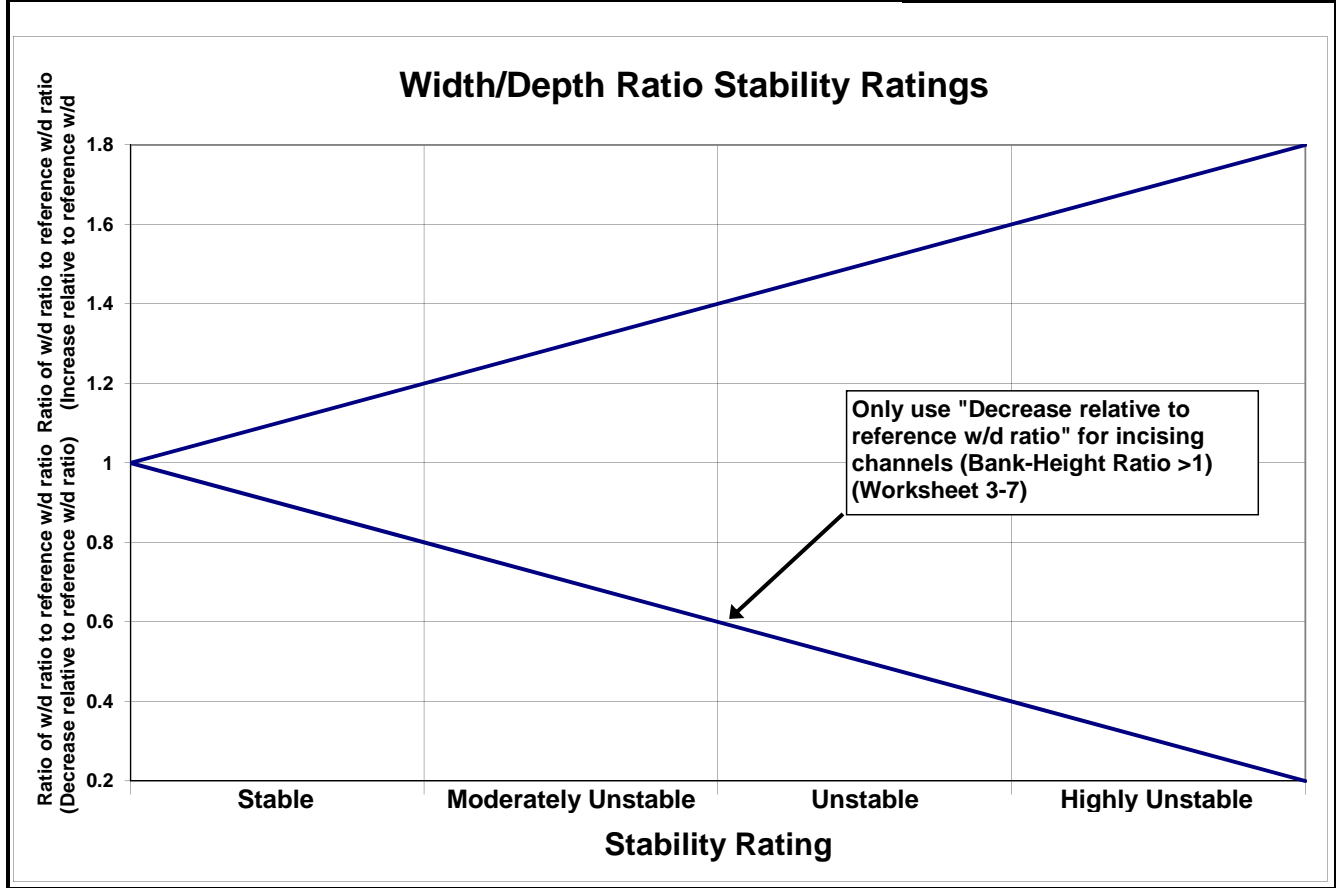
Worksheet 5-12. Degree of channel incision.



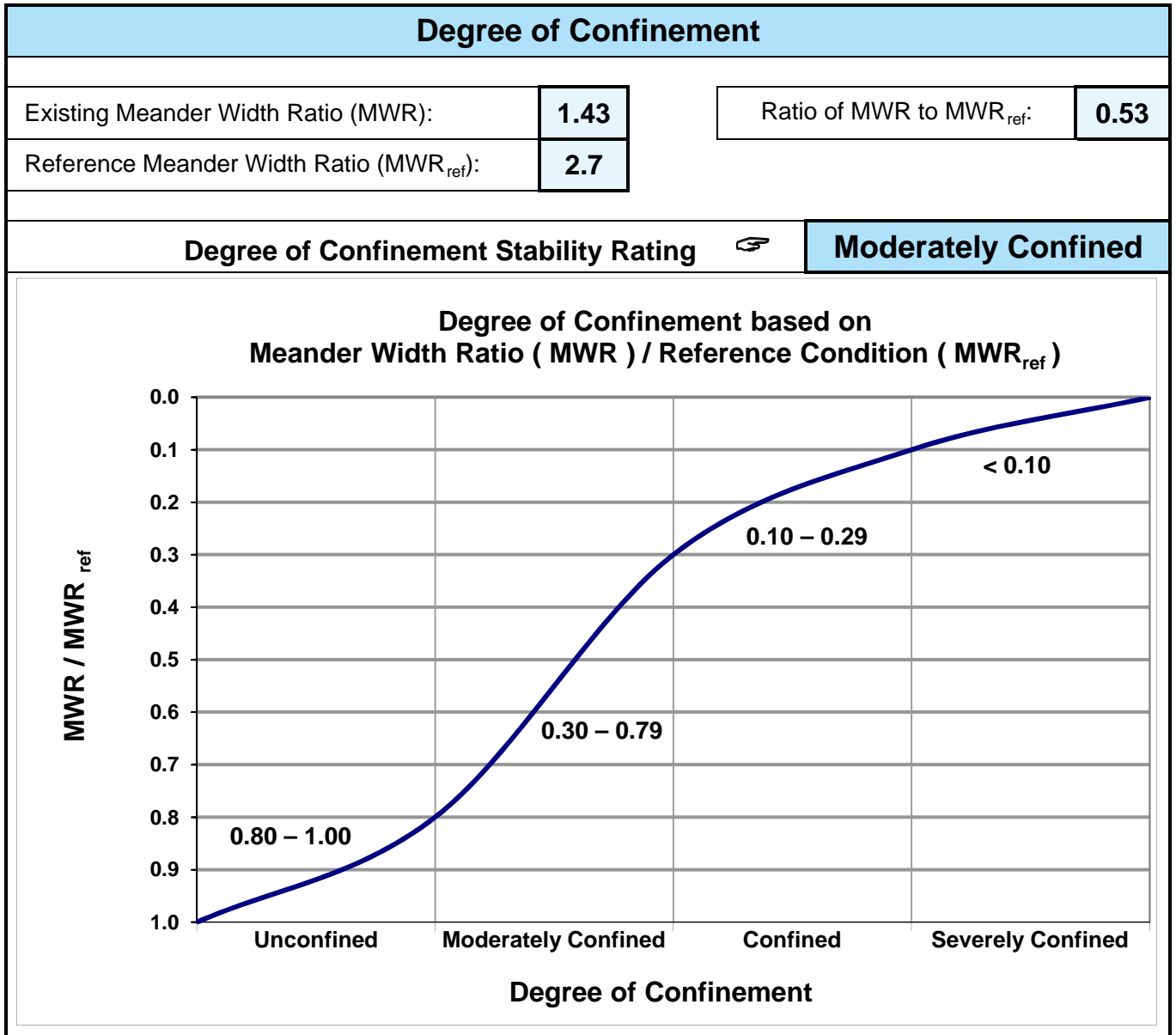
**Worksheet 5-13.** Width/depth ratio state.

Width/Depth Ratio State			
Existing Width/Depth Ratio:	<b>47.29</b>	Ratio of existing W/d to reference W/d:	<b>3.76</b>
Reference Width/Depth Ratio:	<b>12.57</b>		

<b>Width/Depth Ratio State Stability Rating</b>	<b>Highly Unstable</b>
---	------------------------



**Worksheet 5-14.** Degree of channel confinement (lateral containment).



Worksheet 5-15. Pflankuch channel stability rating.

Stream: Trail Creek, F4b Poor Trib. Reach		Location: Pike National Forest, CO			Valley Type: III			Observers: Rosgen et al.			Date: 8/17/2010																																																																																																																																																																																																												
Loca-tion	Key	Category	Excellent	Good	Fair	Poor	Rating	Description	Rating	Description	Rating	Overall																																																																																																																																																																																																											
			Description	Description	Description	Description																																																																																																																																																																																																																	
Upper banks	1	Landform slope	Bank slope gradient <30%.	Bank slope gradient 30–40%.	Bank slope gradient 40–60%.	Bank slope gradient > 60%.	4		6		8	8																																																																																																																																																																																																											
	2	Mass erosion	No evidence of past or future mass erosion.	Infrequent. Mostly healed over. Low future potential.	Frequent or large, causing sediment nearly yearlong.	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.	3		9		12	12																																																																																																																																																																																																											
	3	Debris jam potential	Essentially absent from immediate channel area.	Present, but mostly small twigs and limbs.	Moderate to heavy amounts, mostly larger sizes.	Moderate to heavy amounts, predominantly larger sizes.	2		6		8	8																																																																																																																																																																																																											
	4	Vegetative bank protection	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	70–90% density. Fewer species or less vigor suggest less dense or deep root mass.	50–70% density. Lower vigor and fewer species from a shallow, discontinuous root mass.	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.	3		9		12	12																																																																																																																																																																																																											
Lower banks	5	Channel capacity	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0.	Bankfull stage is contained within banks. Width/depth ratio departure from reference width/depth ratio = 1.0–1.2. Bank-Height Ratio (BHR) = 1.0–1.1.	Bankfull stage is not contained. Width/depth ratio departure from reference width/depth ratio = 1.2–1.4. Bank-Height Ratio (BHR) = 1.1–1.3.	Bankfull stage is not contained; over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.	1		2		3	4																																																																																																																																																																																																											
	6	Bank rock content	> 65% with large angular boulders. 12"+ common.	40–65%. Mostly boulders and small cobbles 6–12".	20–40%. Most in the 3–6" diameter class.	<20% rock fragments of gravel sizes. 1–3" or less.	2		4		6	8																																																																																																																																																																																																											
	7	Obstructions to flow	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	Frequent obstructions and deflectors cause bank erosion yearlong. Sediment traps full, channel migration occurring.	2		4		6	8																																																																																																																																																																																																											
	8	Cutting	Little or none. Infrequent raw banks <6".	Some, intermittently at outcrops and constrictions. Raw banks may be up to 12".	Significant. Cuts 12–24" high. Root mat overhangs and sloughing evident.	Almost continuous cuts, some over 24" high. Failure of overhangs frequent.	4		6		12	16																																																																																																																																																																																																											
Bottom	9	Deposition	Little or no enlargement of channel or point bars.	Some new bar increase, mostly from coarse gravel.	Moderate deposition of new gravel and coarse sand on old and some new bars.	Extensive deposit of predominantly fine particles. Accelerated bar development.	4		8		12	16																																																																																																																																																																																																											
	10	Rock angularity	Sharp edges and corners. Plane surfaces rough.	Rounded corners and edges. Surfaces smooth and flat.	Surfaces smooth and rounded in 2 dimensions.	Well rounded in all dimensions, surfaces smooth.	1		2		3	4																																																																																																																																																																																																											
	11	Brightness	Surfaces dull, dark or stained. Generally not bright.	Mostly dull, but may have <35% bright surfaces.	Mixture dull and bright, i.e., 35–65% mixture range.	Predominantly bright, > 65%, exposed or scoured surfaces.	1		2		3	4																																																																																																																																																																																																											
	12	Consolidation of particles	Assorted sizes tightly packed or overlapping.	Moderately packed with some overlapping.	Mostly loose assortment with no apparent overlap.	No packing evident. Loose assortment, easily moved.	2		4		6	8																																																																																																																																																																																																											
	13	Bottom size distribution	No size change evident. Stable material 80–100%.	Distribution shift light. Stable material 50–80%.	Moderate change in sizes. Stable materials 20–50%.	Marked distribution change. Stable materials 0–20%.	4		8		12	16																																																																																																																																																																																																											
	14	Scouring and deposition	<5% of bottom affected by scour or deposition.	5–30% affected. Scour at constrictions and where grades steepen. Some deposition in pools.	30–50% affected. Deposits and scour at obstructions, constrictions and bends. Some filling of pools.	More than 50% of the bottom in a state of flux or change nearly yearlong.	6		12		18	24																																																																																																																																																																																																											
	15	Aquatic vegetation	Abundant growth moss-like, dark green perennial. In swift water too.	Common. Algae forms in low velocity and pool areas. Moss here too.	Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick.	Perennial types scarce or absent. Yellow-green, short-term bloom may be present.	1		2		3	4																																																																																																																																																																																																											
<b>Excellent total = 0</b>							<b>Good total = 8</b>	<b>Fair total = 0</b>			<b>Poor total = 136</b>																																																																																																																																																																																																												
<table border="1"> <thead> <tr> <th>Stream type</th> <th>A1</th> <th>A2</th> <th>A3</th> <th>A4</th> <th>A5</th> <th>A6</th> <th>A7</th> <th>B1</th> <th>B2</th> <th>B3</th> <th>B4</th> <th>B5</th> <th>B6</th> <th>C1</th> <th>C2</th> <th>C3</th> <th>C4</th> <th>C5</th> <th>C6</th> <th>D3</th> <th>D4</th> <th>D5</th> <th>D6</th> <th>Grand total =</th> </tr> </thead> <tbody> <tr> <td>Good (Stable)</td> <td>38-43</td> <td>38-43</td> <td>54-90</td> <td>60-95</td> <td>60-95</td> <td>50-80</td> <td>38-45</td> <td>38-45</td> <td>38-45</td> <td>40-60</td> <td>40-64</td> <td>48-68</td> <td>40-60</td> <td>38-50</td> <td>38-50</td> <td>60-85</td> <td>70-90</td> <td>70-90</td> <td>60-85</td> <td>85-107</td> <td>85-107</td> <td>85-107</td> <td>85-107</td> <td>67-98</td> <td>144</td> </tr> <tr> <td>Fair (Mod. unstable)</td> <td>44-47</td> <td>44-47</td> <td>91-129</td> <td>96-132</td> <td>96-142</td> <td>81-110</td> <td>46-58</td> <td>46-58</td> <td>46-58</td> <td>61-78</td> <td>65-84</td> <td>69-88</td> <td>61-78</td> <td>51-61</td> <td>51-61</td> <td>86-105</td> <td>91-110</td> <td>91-110</td> <td>86-105</td> <td>108-132</td> <td>108-132</td> <td>108-132</td> <td>108-132</td> <td>99-125</td> <td>F4b</td> </tr> <tr> <td>Poor (Unstable)</td> <td>48+</td> <td>48+</td> <td>130+</td> <td>133+</td> <td>143+</td> <td>111+</td> <td>59+</td> <td>59+</td> <td>59+</td> <td>79+</td> <td>85+</td> <td>89+</td> <td>79+</td> <td>62+</td> <td>62+</td> <td>106+</td> <td>111+</td> <td>111+</td> <td>106+</td> <td>133+</td> <td>133+</td> <td>133+</td> <td>133+</td> <td>126+</td> <td>B4</td> </tr> <tr> <td>Stream type</td> <td>DA3</td> <td>DA4</td> <td>DA5</td> <td>DA6</td> <td>DA7</td> <td>EA</td> <td>E4</td> <td>E5</td> <td>E6</td> <td>F1</td> <td>F2</td> <td>F3</td> <td>F4</td> <td>F5</td> <td>F6</td> <td>G1</td> <td>G2</td> <td>G3</td> <td>G4</td> <td>G5</td> <td>G6</td> <td>G6</td> <td>G6</td> <td>Modified channel stability rating =</td> </tr> <tr> <td>Good (Stable)</td> <td>40-63</td> <td>40-63</td> <td>40-63</td> <td>40-63</td> <td>40-63</td> <td>50-75</td> <td>50-75</td> <td>40-63</td> <td>40-63</td> <td>60-85</td> <td>60-85</td> <td>85-110</td> <td>85-110</td> <td>90-115</td> <td>80-95</td> <td>40-60</td> <td>40-60</td> <td>85-107</td> <td>85-107</td> <td>108-120</td> <td>108-120</td> <td>108-120</td> <td>108-120</td> <td>B4</td> </tr> <tr> <td>Fair (Mod. unstable)</td> <td>64-86</td> <td>64-86</td> <td>64-86</td> <td>64-86</td> <td>64-86</td> <td>76-96</td> <td>76-96</td> <td>64-86</td> <td>64-86</td> <td>86-105</td> <td>86-105</td> <td>111-125</td> <td>111-125</td> <td>116-130</td> <td>96-110</td> <td>61-78</td> <td>61-78</td> <td>108-120</td> <td>108-120</td> <td>113-125</td> <td>108-120</td> <td>108-120</td> <td>108-120</td> <td>Poor</td> </tr> <tr> <td>Poor (Unstable)</td> <td>87+</td> <td>87+</td> <td>87+</td> <td>87+</td> <td>87+</td> <td>97+</td> <td>97+</td> <td>87+</td> <td>87+</td> <td>106+</td> <td>106+</td> <td>126+</td> <td>126+</td> <td>131+</td> <td>111+</td> <td>79+</td> <td>79+</td> <td>121+</td> <td>121+</td> <td>126+</td> <td>126+</td> <td>121+</td> <td>121+</td> <td></td> </tr> </tbody> </table>													Stream type	A1	A2	A3	A4	A5	A6	A7	B1	B2	B3	B4	B5	B6	C1	C2	C3	C4	C5	C6	D3	D4	D5	D6	Grand total =	Good (Stable)	38-43	38-43	54-90	60-95	60-95	50-80	38-45	38-45	38-45	40-60	40-64	48-68	40-60	38-50	38-50	60-85	70-90	70-90	60-85	85-107	85-107	85-107	85-107	67-98	144	Fair (Mod. unstable)	44-47	44-47	91-129	96-132	96-142	81-110	46-58	46-58	46-58	61-78	65-84	69-88	61-78	51-61	51-61	86-105	91-110	91-110	86-105	108-132	108-132	108-132	108-132	99-125	F4b	Poor (Unstable)	48+	48+	130+	133+	143+	111+	59+	59+	59+	79+	85+	89+	79+	62+	62+	106+	111+	111+	106+	133+	133+	133+	133+	126+	B4	Stream type	DA3	DA4	DA5	DA6	DA7	EA	E4	E5	E6	F1	F2	F3	F4	F5	F6	G1	G2	G3	G4	G5	G6	G6	G6	Modified channel stability rating =	Good (Stable)	40-63	40-63	40-63	40-63	40-63	50-75	50-75	40-63	40-63	60-85	60-85	85-110	85-110	90-115	80-95	40-60	40-60	85-107	85-107	108-120	108-120	108-120	108-120	B4	Fair (Mod. unstable)	64-86	64-86	64-86	64-86	64-86	76-96	76-96	64-86	64-86	86-105	86-105	111-125	111-125	116-130	96-110	61-78	61-78	108-120	108-120	113-125	108-120	108-120	108-120	Poor	Poor (Unstable)	87+	87+	87+	87+	87+	97+	97+	87+	87+	106+	106+	126+	126+	131+	111+	79+	79+	121+	121+	126+	126+	121+	121+	
Stream type	A1	A2	A3	A4	A5	A6	A7	B1	B2	B3	B4	B5	B6	C1	C2	C3	C4	C5	C6	D3	D4	D5	D6	Grand total =																																																																																																																																																																																															
Good (Stable)	38-43	38-43	54-90	60-95	60-95	50-80	38-45	38-45	38-45	40-60	40-64	48-68	40-60	38-50	38-50	60-85	70-90	70-90	60-85	85-107	85-107	85-107	85-107	67-98	144																																																																																																																																																																																														
Fair (Mod. unstable)	44-47	44-47	91-129	96-132	96-142	81-110	46-58	46-58	46-58	61-78	65-84	69-88	61-78	51-61	51-61	86-105	91-110	91-110	86-105	108-132	108-132	108-132	108-132	99-125	F4b																																																																																																																																																																																														
Poor (Unstable)	48+	48+	130+	133+	143+	111+	59+	59+	59+	79+	85+	89+	79+	62+	62+	106+	111+	111+	106+	133+	133+	133+	133+	126+	B4																																																																																																																																																																																														
Stream type	DA3	DA4	DA5	DA6	DA7	EA	E4	E5	E6	F1	F2	F3	F4	F5	F6	G1	G2	G3	G4	G5	G6	G6	G6	Modified channel stability rating =																																																																																																																																																																																															
Good (Stable)	40-63	40-63	40-63	40-63	40-63	50-75	50-75	40-63	40-63	60-85	60-85	85-110	85-110	90-115	80-95	40-60	40-60	85-107	85-107	108-120	108-120	108-120	108-120	B4																																																																																																																																																																																															
Fair (Mod. unstable)	64-86	64-86	64-86	64-86	64-86	76-96	76-96	64-86	64-86	86-105	86-105	111-125	111-125	116-130	96-110	61-78	61-78	108-120	108-120	113-125	108-120	108-120	108-120	Poor																																																																																																																																																																																															
Poor (Unstable)	87+	87+	87+	87+	87+	97+	97+	87+	87+	106+	106+	126+	126+	131+	111+	79+	79+	121+	121+	126+	126+	121+	121+																																																																																																																																																																																																

\*Rating is adjusted to potential stream type, not existing.

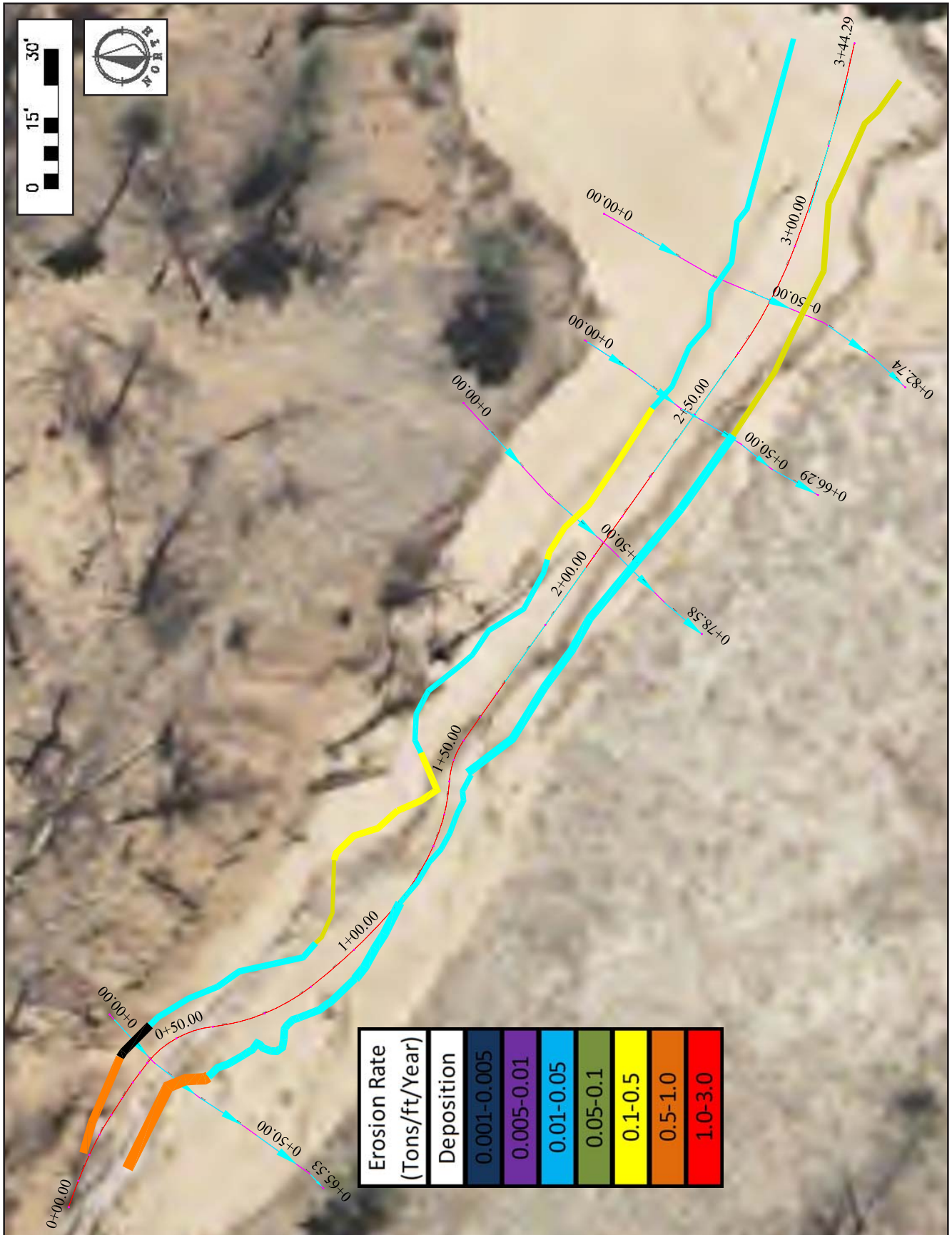


## BANCS Model – Streambank Erosion

**Worksheet 5-18.** Annual streambank erosion estimates.

Stream: <b>Trail Creek, F4b Poor Trib. Reach</b>		Location: <b>Pike National Forest, Colorado</b>					
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>337</b>			Date: <b>8/16/2010</b>		
Observers: <b>Rosgen et al.</b>		Valley Type: <b>III</b>			Stream Type: <b>F4b</b>		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 5-16) (adjective)	NBS rating (Worksheet 5-17) (adjective)	Bank erosion rate (Figure 5-34 or 5-35) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal $[(4) \times (5) \times (6)]$ (ft <sup>3</sup> /yr)	Erosion Rate $\{[(7)/27] \times 1.3 / (5)\}$
1. 0+10 - 0+62 R	Extreme	Very High	7.02692	52.0	2.7	986.58	0.91350
2. 0+10 - 0+43 L	Extreme	Very High	7.02692	33.0	2.0	463.78	0.67667
3. 0+63 - 0+90 L	Extreme	Low	0.41998	27.0	1.5	17.01	0.03033
4. 0+62 - 0+93 R	Extreme	Low	0.41998	31.0	1.8	23.43	0.03640
5. 0+93 - 0+118 R	Extreme	Low	0.41998	25.0	2.2	23.10	0.04449
6. 0+90 - 0+118 L	Extreme	Moderate	1.07417	28.0	1.0	30.08	0.05172
7. 0+118 - 0+157 L	Extreme	Very High	7.02692	39.0	1.6	438.48	0.54133
8. 0+118 - 0+157 R	Extreme	Low	0.41998	39.0	1.3	21.29	0.02629
9. 0+174 - 0+253 R	Extreme	Low	0.41998	59.0	2.0	49.56	0.04044
10. 0+174 - 0+198 L	Extreme	Low	0.41998	24.0	1.3	13.10	0.02629
11. 0+198 - 0+245 L	Extreme	Very High	7.02692	47.0	1.5	495.40	0.50750
12. 0+253 - 0+344 R	Extreme	Moderate	1.07417	89.0	1.4	133.84	0.07241
13. 0+245 - 0+344 L	Extreme	Low	0.41998	99.0	1.3	54.05	0.02629
14.							
15.							
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					Total Erosion (ft <sup>3</sup> /yr)	<b>2749.70</b>	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					Total Erosion (yds <sup>3</sup> /yr)	<b>101.84</b>	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					Total Erosion (tons/yr)	<b>132.39</b>	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					Total Erosion (tons/yr/ft)	<b>0.3929</b>	

Streambank Erosion Map



## FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Equation Type		Equation Source				Equation		Bankfull Discharge (cfs)		Bankfull Bedload Sediment (kg/s)	Bankfull Suspended Sediment (mg/l)			
1. Bedload Sediment		"Good/Fair" Pagosa				$y = -0.0113x + 1.0139x^{2.1929}$		8.43		0.0092	4.17			
2. Suspended Sediment		"Good/Fair" Pagosa				$y = 0.0636 + 0.9326x^{2.4085}$								
From Dimensional Flow-Duration Curve														
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Percentage of Time	Daily Mean Discharge	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimension-less Streamflow	Dimension-less Suspended Sediment Discharge	Suspended Sediment Discharge	Dimension-less Bedload Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow	Suspended Sediment	Bedload Sediment	Suspended + Bedload Sediment
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>bed</sub> )	(S/S <sub>bed</sub> )	(tons/day)	(b <sub>g</sub> /b <sub>bed</sub> )	(tons/day)	(cfs)	(tons)	(tons)	(tons)
0%	21.4													
0.10%	18.4	0.05%	0.09%	0.34	19.9	2.363	7.461	1.67	6.670	5.86	6.8	0.57	2.01	2.58
0.25%	15.9	0.08%	0.15%	0.55	17.2	2.036	5.232	1.01	4.809	4.22	9.4	0.55	2.31	2.87
0.50%	13.8	0.13%	0.25%	0.91	14.8	1.761	3.706	0.62	3.494	3.07	13.5	0.56	2.80	3.36
0.75%	11.7	0.13%	0.25%	0.91	12.8	1.513	2.592	0.37	2.502	2.20	11.6	0.34	2.01	2.34
1%	10.2	0.13%	0.25%	0.91	11.0	1.300	1.817	0.22	1.790	1.57	10.0	0.20	1.43	1.64
1.5%	8.7	0.25%	0.50%	1.83	9.4	1.120	1.289	0.14	1.289	1.13	17.2	0.25	2.07	2.32
2%	7.3	0.25%	0.50%	1.83	8.0	0.949	0.886	0.08	0.893	0.78	14.6	0.15	1.43	1.58
3%	6.1	0.50%	1.00%	3.65	6.7	0.795	0.600	0.05	0.602	0.53	24.5	0.17	1.93	2.09
4%	5.2	0.50%	1.00%	3.65	5.7	0.674	0.424	0.03	0.415	0.36	20.7	0.10	1.33	1.43
5%	4.7	0.50%	1.00%	3.65	4.9	0.587	0.322	0.02	0.304	0.27	18.1	0.07	0.97	1.04
10%	2.9	2.50%	5.00%	18.25	3.8	0.450	0.200	0.01	0.165	0.14	69.3	0.16	2.64	2.80
20%	1.6	5.00%	10.00%	36.50	2.3	0.269	0.103	0.00	0.045	0.04	82.6	0.10	1.46	1.55
30%	1.1	5.00%	10.00%	36.50	1.3	0.158	0.075	0.00	0.006	0.01	48.6	0.04	0.21	0.25
40%	0.8	5.00%	10.00%	36.50	0.9	0.108	0.068	0.00	0.000	0.00	33.2	0.03	0.00	0.03
50%	0.6	5.00%	10.00%	36.50	0.7	0.079	0.066	0.00	0.000	0.00	24.3	0.02	0.00	0.02
60%	0.4	5.00%	10.00%	36.50	0.5	0.061	0.065	0.00	0.000	0.00	18.6	0.01	0.00	0.01
70%	0.4	5.00%	10.00%	36.50	0.4	0.047	0.064	0.00	0.000	0.00	14.6	0.01	0.00	0.01
80%	0.3	5.00%	10.00%	36.50	0.3	0.039	0.064	0.00	0.000	0.00	12.1	0.01	0.00	0.01
90%	0.2	5.00%	10.00%	36.50	0.3	0.032	0.064	0.00	0.000	0.00	9.7	0.01	0.00	0.01
100%	0.0	5.00%	10.00%	36.50	0.1	0.016	0.064	0.00	0.000	0.00	4.9	0.00	0.00	0.00
<b>Annual Totals:</b>										464.4 (cfs)	3.3 (tons/yr)	22.6 (tons/yr)	25.9 (tons/yr)	
<b>Annual Totals:</b>										921.2 (acre-ft)				

**Worksheet 19b.** Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Equation Type		Equation Source		Equation		Bankfull Discharge (cfs)		Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)	
1. Bedload Sediment		"Poor" Pagosa		$y = 0.07176 + 1.02176x^{2.3772}$		8.43		0.0923		153.71	
2. Suspended Sediment		"Poor" Pagosa		$y = 0.0989 + 0.9213x^{3.659}$							
From Dimensional Flow-Duration Curve											
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)
Percentage of Time	Daily Mean Discharge	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Suspended Sediment Discharge	Suspended Sediment Discharge	Dimensionless Bedload Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>bed</sub> )	(S/S <sub>bed</sub> )	(tons/day)	(b <sub>p</sub> /b <sub>bed</sub> )	(tons/day)	(cfs)
0%	24.6										
0.10%	21.6	0.05%	0.09%	0.34	23.1	2.739	36.866	353.25	11.280	99.20	7.9
0.25%	19.1	0.08%	0.15%	0.55	20.3	2.412	23.192	195.70	8.357	73.49	11.1
0.50%	16.9	0.13%	0.25%	0.91	18.0	2.137	14.921	111.54	6.283	55.26	16.4
0.75%	14.9	0.13%	0.25%	0.91	15.9	1.889	9.542	63.06	4.706	41.39	14.5
1%	13.3	0.13%	0.25%	0.91	14.1	1.676	6.191	36.30	3.558	31.29	12.9
1.5%	11.8	0.25%	0.50%	1.83	12.6	1.494	4.097	21.41	2.723	23.95	23.0
2%	10.4	0.25%	0.50%	1.83	11.1	1.317	2.623	12.09	2.038	17.92	20.3
3%	9.2	0.50%	1.00%	3.65	9.8	1.160	1.687	6.85	1.527	13.43	35.7
4%	8.1	0.50%	1.00%	3.65	8.6	1.024	1.105	3.96	1.154	10.15	31.5
5%	7.1	0.50%	1.00%	3.65	7.6	0.903	0.732	2.31	0.872	7.67	27.8
10%	4.5	2.50%	5.00%	18.25	5.8	0.689	0.335	0.81	0.493	4.34	106.0
20%	1.9	5.00%	10.00%	36.50	3.2	0.376	0.125	0.16	0.172	1.51	115.6
30%	1.1	5.00%	10.00%	36.50	1.5	0.175	0.100	0.06	0.088	0.77	53.8
40%	0.8	5.00%	10.00%	36.50	0.9	0.109	0.099	0.04	0.077	0.68	33.5
50%	0.6	5.00%	10.00%	36.50	0.7	0.079	0.099	0.03	0.074	0.65	24.3
60%	0.4	5.00%	10.00%	36.50	0.5	0.061	0.099	0.02	0.073	0.64	18.6
70%	0.4	5.00%	10.00%	36.50	0.4	0.047	0.099	0.02	0.072	0.64	14.6
80%	0.3	5.00%	10.00%	36.50	0.3	0.039	0.099	0.01	0.072	0.64	12.1
90%	0.2	5.00%	10.00%	36.50	0.3	0.032	0.099	0.01	0.072	0.63	9.7
100%	0.0	5.00%	10.00%	36.50	0.1	0.016	0.099	0.01	0.072	0.63	4.9
<b>Annual Totals:</b>											
											594.4 (cfs)
											1,179.0 (acre-ft)
											557.6 (tons/yr)
											708.6 (tons/yr)
											1,266.2 (tons/yr)

# POWERSED Model – Sediment Transport Capacity

**Worksheet 20a.** Sediment transport prediction representing the upstream supply up to bankfull for bedload and suspended sand sediment.

Stream: Trail Creek, Upstream Existing Sediment Supply		Location: Pike National Forest, Colorado		Gage Station #: Used Post-Fire Dimensionless F-D C.		Date: 08/14/10												
Observers: S=04, Q=8, Bed.=2031, S.Sand=76.85		Stream Type: F4b		Valley Type: VIII		Used "POOR" Curves												
Calculate				Measure														
Flow-duration curve				Hydraulic geometry														
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	
Percentage of time	Daily mean discharge (cfs)	Mid-ordinate stream-flow (cfs)	Area (ft <sup>2</sup> )	Width (ft)	Depth (ft)	Velocity (ft/s)	Slope (ft/ft)	Shear stress (lb/ft <sup>2</sup> )	Stream power (lb/s)	Unit power (lb/ft/s)	Time increment (%)	Time increment (days)	Daily mean bedload transport (tons/day)	Daily mean suspended sand transport [(13)x(14)] (tons/day)	Time adjusted bedload transport [(13)x(14)] (tons)	Time adjusted suspended sand transport [(16)x(17)] (tons)	Time adjusted total transport [(16)+(17)] (tons)	
100.00%	0.04										0%				0.00	0.00	0.00	
90.00%	0.22	0.13	0.18	3.01	0.06	0.83	0.0400	0.15	0.32	0.11	10%	36.50	0.65	0.00	23.73	0.00	23.73	
80.00%	0.31	0.27	0.25	3.20	0.08	0.96	0.0400	0.19	0.67	0.21	10%	36.50	0.65	0.01	23.73	0.36	24.09	
70.00%	0.35	0.33	0.29	3.28	0.09	1.02	0.0400	0.22	0.82	0.25	10%	36.50	0.65	0.01	23.73	0.36	24.09	
60.00%	0.44	0.40	0.33	3.37	0.10	1.08	0.0400	0.24	1.00	0.30	10%	36.50	0.65	0.01	23.73	0.36	24.09	
50.00%	0.58	0.51	0.39	3.51	0.11	1.18	0.0400	0.28	1.27	0.36	10%	36.50	0.65	0.01	23.73	0.36	24.09	
40.00%	0.75	0.67	0.48	3.72	0.13	1.33	0.0400	0.32	1.67	0.45	10%	36.50	0.65	0.01	23.73	0.36	24.09	
30.00%	1.08	0.92	0.60	3.96	0.15	1.51	0.0400	0.38	2.30	0.58	10%	36.50	0.69	0.02	25.18	0.73	25.91	
20.00%	1.87	1.48	0.81	4.21	0.19	1.76	0.0400	0.47	3.69	0.88	10%	36.50	0.78	0.03	28.47	1.09	29.56	
10.00%	4.47	3.17	1.37	4.80	0.29	2.30	0.0400	0.70	7.91	1.65	10%	36.50	1.64	0.09	59.86	3.28	63.14	
5.00%	7.15	5.81	2.07	5.39	0.38	2.79	0.0400	0.93	14.50	2.69	5%	18.25	4.84	0.46	88.33	8.39	96.72	
4.00%	8.07	7.61																
3.00%	9.20	8.64																
2.00%	10.36	9.78																
1.50%	11.84	11.10																
1.00%	13.33	12.59																
0.75%	14.92	14.13																
0.50%	16.93	15.93																
0.25%	19.09	18.01																
0.10%	21.56	20.33																
0.0060%	24.60	23.08																
														Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr):		344.2	15.3	359.5

**Worksheet 20b.** Sediment transport prediction for the existing condition reach compared to the upstream sediment supply to assess bed stability.

Stream: Trail Creek, F4b Poor Trib, XS 2+80													Location: Pike National Forest, Colorado (Used "POOR" Curves)			Date: 08/14/10	
Observers: S=04, Q=8, Bed.=.2031, S.Sand=76.85													Valley Type: VIII			Gage Station #: Used Post-Fire Dimensionless F-D C.	
Stream Type: F4b													Stream Type: VIII			Valley Type: VIII	
Flow-duration curve			Calculate				Hydraulic geometry				Measure		Calculate				
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
Percentage of time	Daily mean discharge	Mid-ordinate stream-flow	Area	Width	Depth	Velocity	Slope	Shear stress	Stream power	Unit power	Time increment	Time increment	Daily mean bedload transport	Daily mean suspended sand transport	Time adjusted bedload transport	Time adjusted suspended sand transport	Time adjusted total transport
(%)	(cfs)	(cfs)	(ft <sup>2</sup> )	(ft)	(ft)	(ft/s)	(ft/ft)	(lb/ft <sup>2</sup> )	(lb/s)	(lb/ft/s)	(%)	(days)	(tons/day)	(tons/day)	[(13)×(14)]	[(13)×(15)]	[(16)+(17)]
100.00%	0.04										0%				0.00	0.00	0.00
90.00%	0.22	0.13	0.14	3.07	0.05	1.07	0.0400	0.11	0.32	0.10	10%	36.50	0.00	0.00	0.00	0.00	0.00
80.00%	0.31	0.27	0.22	3.73	0.06	1.15	0.0400	0.14	0.67	0.18	10%	36.50	0.65	0.01	23.73	0.36	24.09
70.00%	0.35	0.33	0.26	4.02	0.06	1.18	0.0400	0.16	0.82	0.20	10%	36.50	0.65	0.01	23.73	0.36	24.09
60.00%	0.44	0.40	0.30	4.35	0.07	1.21	0.0400	0.17	1.00	0.23	10%	36.50	0.65	0.01	23.73	0.36	24.09
50.00%	0.58	0.51	0.36	4.87	0.07	1.27	0.0400	0.18	1.27	0.26	10%	36.50	0.65	0.01	23.73	0.36	24.09
40.00%	0.75	0.67	0.45	5.62	0.08	1.35	0.0400	0.19	1.67	0.30	10%	36.50	0.65	0.01	23.73	0.36	24.09
30.00%	1.08	0.92	0.60	6.80	0.09	1.48	0.0400	0.21	2.30	0.34	10%	36.50	0.65	0.02	23.73	0.73	24.46
20.00%	1.87	1.48	0.83	7.84	0.11	1.68	0.0400	0.26	3.69	0.47	10%	36.50	0.65	0.03	23.73	1.09	24.82
10.00%	4.47	3.17	1.40	9.03	0.16	2.18	0.0400	0.37	7.91	0.88	10%	36.50	0.78	0.07	28.47	2.56	31.03
5.00%	7.15	5.81	2.07	9.60	0.22	2.72	0.0400	0.52	14.50	1.51	5%	18.25	1.47	0.15	26.83	2.74	29.57
4.00%	8.07	7.61															
3.00%	9.20	8.64															
2.00%	10.36	9.78															
1.50%	11.84	11.10															
1.00%	13.33	12.59															
0.75%	14.92	14.13															
0.50%	16.93	15.93															
0.25%	19.09	18.01															
0.10%	21.56	20.33															
0.0060%	24.60	23.08															
Notes:													Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr):				
													221.4				
													Upstream total annual sediment supply (tons/yr) (Worksheet 5-20a):				
													344.2				
													Difference in sediment transport capacity (tons/yr) (+ or -):				
													-122.8				
													Stability evaluation: Aggradation, Degradation or Stable:				
													Aggradation, > 35% Reduction in Transport				

## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>Trail Creek, F4b Poor Trib. Reach</b>		Stream Type: <b>F4b</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>III</b>			
Observers: <b>Rosgen et al.</b>		Date: <b>8/16/2010</b>			
<b>Enter Required Information for Existing Condition</b>					
2.3	$D_{50}$	Riffle bed material $D_{50}$ (mm)			
	$\hat{D}_{50}$	Bar sample $D_{50}$ (mm)			
0.05	$D_{max}$	Largest particle from <b>Bed Material</b> (ft)	16	(mm)	304.8 mm/ft
0.04	<b>S</b>	Existing bankfull water surface slope (ft/ft)			
0.24	<b>d</b>	Existing bankfull mean depth (ft)			
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment			
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>					
N/A	$D_{50}/\hat{D}_{50}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 (D_{50}/\hat{D}_{50})^{-0.872}$		
N/A	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 (D_{max}/D_{50})^{-0.887}$		
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED:		
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	<b>d</b>	Required bankfull mean depth (ft)	$d = \frac{\tau^* (\gamma_s - 1) D_{max}}{S}$ (use $D_{max}$ in ft)		
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	<b>S</b>	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^* (\gamma_s - 1) D_{max}}{d}$ (use $D_{max}$ in ft)		
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					
<b>Sediment Competence Using Dimensional Shear Stress</b>					
0.599	Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d) $\gamma = 62.4$ , d = existing depth, S = existing slope				
Shields 43	CO 105	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ (Figure 5-49)			
Shields 0.21	CO 0.043	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) (Figure 5-49)			
Shields 0.08	CO 0.02	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm) $\tau =$ predicted shear stress, $\gamma = 62.4$ , S = existing slope $d = \frac{\tau}{\gamma S}$			
Shields 0.0140	CO 0.0029	Predicted slope required to initiate movement of measured $D_{max}$ (mm) $\tau =$ predicted shear stress, $\gamma = 62.4$ , d = existing depth $S = \frac{\tau}{\gamma d}$			
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input checked="" type="checkbox"/> Degrading					

## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>Trail Creek, F4b Poor Trib.</b>	Stream Type: <b>F4b</b>
Location: <b>Pike National Forest, CO</b>	Valley Type: <b>III</b>
Observers: <b>Rosgen et al.</b>	Date: <b>8/16/2010</b>
Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)	Stability Rating (Check Appropriate Rating)
Stream Type at potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	<input type="checkbox"/> Stable
(E→C), (C→High W/d C)	<input type="checkbox"/> Moderately Unstable
(G→F), (F→D), (C→F)	<input checked="" type="checkbox"/> Unstable
(C→D), (B→G), (D→G), (C→G), (E→G)	<input type="checkbox"/> Highly Unstable



Worksheet 5-25. Lateral stability.

Stream: <b>Trail Creek, F4b Poor Trib. Reach</b>		Stream Type: <b>F4b</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>III</b>			
Observers: <b>Rosgen et al.</b>		Date: <b>8/16/2010</b>			
Lateral stability criteria (choose one stability category for each criterion 1–5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	8
	(2)	(4)	(6)	3.76 (8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	4
	(1)	(2)	(3)	B5, B7 (4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		1
	M1 (1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	8
	(2)	(4)	(6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	2
	(1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>23</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input type="checkbox"/>	<i>Unstable</i> 13 – 21 <input type="checkbox"/>	<i>Highly Unstable</i> > 21 <input checked="" type="checkbox"/>	

**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>Trail Creek, F4b Poor Trib. Reach</b>		Stream Type: <b>F4b</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>III</b>			
Observers: <b>Rosgen et al.</b>		Date: <b>8/16/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	No Deposition	Moderate Deposition	Excess Deposition	Aggradation	
1 <b>Sediment competence</b> (Worksheet 5-22)	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope-slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	2
	(2)	(4)	(6)	(8)	
2 <b>Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	8
	(2)	(4)	(6)	≈ 40% (8)	
3 <b>W/d Ratio State</b> (Worksheet 5-13)	1.0 – 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	8
	(2)	(4)	(6)	3.8 (8)	
4 <b>Stream Succession States</b> (Worksheet 5-24)	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	6
	(2)	(4)	G to F (6)	(8)	
5 <b>Depositional Patterns</b> (Worksheet 5-10)	B1	B2, B4	B3, B5	B6, B7, B8	4
	(1)	(2)	(3)	B5, B7 (4)	
6 <b>Debris / Blockages</b> (Worksheet 5-11)	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	1
	D2 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>29</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
Vertical Stability for Excess Deposition / Aggradation (use total points and check stability rating)	<b>No Deposition</b> 10 – 14 <input type="checkbox"/>	<b>Moderate Deposition</b> 15 – 20 <input type="checkbox"/>	<b>Excess Deposition</b> 21 – 30 <input checked="" type="checkbox"/>	<b>Aggradation</b> > 30 <input type="checkbox"/>	

Worksheet 5-27. Vertical stability – degradation.

Stream: <b>Trail Creek, F4b Poor Trib. Reach</b>		Stream Type: <b>F4b</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>III</b>			
Observers: <b>Rosgen et al.</b>		Date: <b>8/16/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>1 Sediment Competence</b> (Worksheet 5-22)	Does not indicate excess competence	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed	$D_{100}$ of bed moved	Particles much larger than $D_{100}$ of bed moved	<b>8</b>
	(2)	(4)	(6)	(8)	
<b>2 Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Does not indicate excess capacity	Slight excess energy: up to 10% increase above reference	Excess energy sufficient to increase load up to 50% of annual load	Excess energy transporting more than 50% of annual load	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>3 Degree of Channel Incision (BHR)</b> (Worksheet 5-12)	1.00 – 1.10	1.11 – 1.30	1.31 – 1.50	> 1.50	<b>1</b>
	1.00 (2)	(4)	(6)	(8)	
<b>4 Stream Succession States</b> (Worksheets 5-12 and 5-24)	Does not indicate incision or degradation	If BHR > 1.1 and stream type has W/d between 5–10	If BHR > 1.1 and stream type has W/d less than 5	(B→G), (C→G), (E→G), (D→G)	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>5 Confinement (MWR / MWR<sub>ref</sub>)</b> (Worksheet 5-14)	0.80 – 1.00	0.30 – 0.79	0.10 – 0.29	< 0.10	<b>2</b>
	(1)	0.53 (2)	(3)	(4)	
<b>Total Points</b>					<b>15</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation</b> (use total points and check stability rating)	<i>Not Incised</i> 9 – 11 <input type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input checked="" type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input type="checkbox"/>	<i>Degradation</i> > 27 <input type="checkbox"/>	

**Worksheet 5-28.** Channel enlargement.

Stream: <b>Trail Creek, F4b Poor Trib. Reach</b>		Stream Type: <b>F4b</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>III</b>			
Observers: <b>Rosgen et al.</b>		Date: <b>8/16/2010</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1-4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	6
	(2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	8
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	6
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	4
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>24</b>
<b>Category Point Range</b>					
<b>Channel Enlargement Prediction (use total points and check stability rating)</b>	<b>No Increase</b> 8 – 10 <input type="checkbox"/>	<b>Slight Increase</b> 11 – 16 <input type="checkbox"/>	<b>Moderate Increase</b> 17 – 24 <input type="checkbox"/>	<b>Extensive</b> > 24 <input checked="" type="checkbox"/>	

Worksheet 5-29. Overall sediment supply.

Stream: <b>Trail Creek, F4b Poor Trib. Reach</b>		Stream Type: <b>F4b</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>III</b>		
Observers: <b>Rosgen et al.</b>		Date: <b>8/16/2010</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1–5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	4	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	3	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	2	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	4.0	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	4.0	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>17</b>	
<b>Category Point Range</b>				
Overall Sediment Supply Rating (use total points and check stability rating)	<i>Low</i> 5 <input type="checkbox"/>	<i>Moderate</i> 6 – 10 <input type="checkbox"/>	<i>High</i> 11 – 15 <input type="checkbox"/>	<i>Very High</i> 16 – 20 <input checked="" type="checkbox"/>

Worksheet 5-32. Summary of stability condition categories.

Stream: <b>Trail Creek, F4b Poor Trib. Reach</b>		Location: <b>Pike National Forest, Colorado</b>	
Observers: <b>Rosgen et al.</b>		Valley Type: <b>III</b>	
Date: <b>8/16/2010</b>		Stream Type: <b>F4b</b>	
<b>Channel Dimension (XS 2+80)</b>	Mean Bankfull Depth (ft): <b>0.24</b>	Cross-Sectional Area (ft <sup>2</sup> ): <b>2.67</b>	Width of Flood-Prone Area (ft): <b>13.31</b>
<b>Channel Pattern</b>	Bankfull Width (ft): <b>11.35</b>	Entrenchment Ratio: <b>1.17</b>	
<b>River Profile &amp; Bed Features</b>	Mean: $\lambda/W_{bkt}$ : <b>1.43</b>	$R_c/W_{bkt}$ : <b>1.09-2.14</b>	Sinuosity: <b>1.04</b>
<b>Level III Stream Stability Indices</b>	Check: <input checked="" type="checkbox"/> Riffle/Pool <input type="checkbox"/> Step/Pool <input type="checkbox"/> Plane Bed <input type="checkbox"/> Convergence/Divergence <input type="checkbox"/> Dunes/Antidunes/Smooth Bed	Pool Spacing: <b>N/A</b>	Pool-to-Pool Ratio: <b>N/A</b>
<b>Bank Erosion Summary</b>	Max Bankfull Depth (ft): <b>0.57</b>	Riffle Depth Ratio (max to mean): <b>1.31</b>	Valley: <b>0.0425</b>
<b>Sediment Capacity (POWERSED)</b>	Riparian Vegetation: <b>5% p. pine, burnt, annual grass</b>	Potential Composition/Density: <b>willow, alder, grass, aspen</b>	Remarks: Condition, Vigor & Usage of Existing Reach: <b>burned area that has not fully recovered</b>
<b>Entrainment/Competence</b>	Flow Regime: <b>S2, S8 &amp; Order: S-3(4)</b>	Meander Patterns: <b>M1</b>	Debris/Channel Blockages: <b>B5, B7</b>
<b>Successional Stage Shift</b>	Degree of Incision (Bank-Height Ratio): <b>1.0</b>	Stability Rating: <b>Stable</b>	Modified Plankuch Stability Rating (Numeric & Adjective Rating): <b>144 (Poor)</b>
<b>Lateral Stability</b>	Width/depth Ratio (W/d): <b>47.3</b>	Reference W/d Ratio (W/d <sub>ref</sub> ): <b>12.6</b>	W/d Ratio State Stability Rating: <b>Highly Unstable</b>
<b>Vertical Stability (Aggradation)</b>	Meander Width Ratio (MWR): <b>1.43</b>	Reference MWR <sub>ref</sub> : <b>2.7</b>	MWR / MWR <sub>ref</sub> Stability Rating: <b>Moderately Confined</b>
<b>Vertical Stability (Degradation)</b>	Length of Reach Studied (ft): <b>337</b>	Annual Streambank Erosion Rate: (tons/yr) <b>0.39</b>	Curve Used: <b>Colorado</b>
<b>Channel Enlargement</b>	<input type="checkbox"/> Sufficient Capacity <input checked="" type="checkbox"/> Insufficient Capacity <input type="checkbox"/> Excess Capacity	Remarks: <b>Remarks: ≈ 40% Reduction in Transport</b>	Remarks: <b>F cutting through an alluvial fan</b>
<b>Sediment Supply (Channel Source)</b>	Largest Particle from Bed Material (mm): <b>16</b>	Existing Depth: <b>0.24</b>	Required Depth: <b>0.08</b>
	D → G → <b>F</b> → B →	Existing Stream State (Type): <b>F4b</b>	Potential Stream State (Type): <b>B4</b>
	<input type="checkbox"/> Stable <input type="checkbox"/> Mod. Unstable <input type="checkbox"/> Unstable <input checked="" type="checkbox"/> Highly Unstable	Remarks/causes: <b>High Banks, Poor Veg.</b>	
	<input type="checkbox"/> No Deposition <input type="checkbox"/> Mod. Deposition <input checked="" type="checkbox"/> Ex. Deposition <input type="checkbox"/> Aggradation	Remarks/causes: <b>High W/d Ratio</b>	
	<input type="checkbox"/> Not Incised <input checked="" type="checkbox"/> Slightly Incised <input type="checkbox"/> Mod. Incised <input type="checkbox"/> Degradation	Remarks/causes: <b>Highly Mobile Bed</b>	
	<input type="checkbox"/> No Increase <input type="checkbox"/> Slight Increase <input type="checkbox"/> Mod. Increase <input checked="" type="checkbox"/> Extensive	Remarks/causes: <b>Both Banks Eroding</b>	
	<input type="checkbox"/> Low <input type="checkbox"/> Moderate <input type="checkbox"/> High <input checked="" type="checkbox"/> Very High	Remarks/causes: <b>Hayman Fire - unveg banks, pikes peak granite - highly erosive, F cutting through an alluvial fan</b>	

# *Appendix C15*

## **G4 Stream Type** *Poor Stability Reach*





# Table of Contents

## *Appendix C15: G5 Poor Reach*

<b>Reach Location &amp; Overview.....</b>	<b>C15-2</b>
<b>Survey Summary.....</b>	<b>C15-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C15-10</b>
<b><i>Velocity, Classification &amp; Morphological Relations.....</i></b>	<b>C15-10</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b><i>Stability Indices.....</i></b>	<b>C15-14</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b><i>BANCS Model – Streambank Erosion.....</i></b>	<b>C15-24</b>
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b><i>FLOWSED Model – Total Annual Sediment Yield.....</i></b>	<b>C15-26</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b><i>POWERSED Model– Sediment Transport Capacity to Assess Bed Stability.....</i></b>	<b>C15-28</b>
Worksheet 5-20a. Sediment transport prediction for the upstream condition.	
Worksheet 5-20b. Sediment transport prediction for the existing condition.	
<b><i>Sediment Competence/Entrainment.....</i></b>	<b>C15-30</b>
Worksheet 5-22. Sediment competence calculations.	
<b><i>Channel Stability Ratings.....</i></b>	<b>C15-31</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b><i>Summary.....</i></b>	<b>C15-37</b>
Worksheet 5-32. Summary of stability condition categories.	

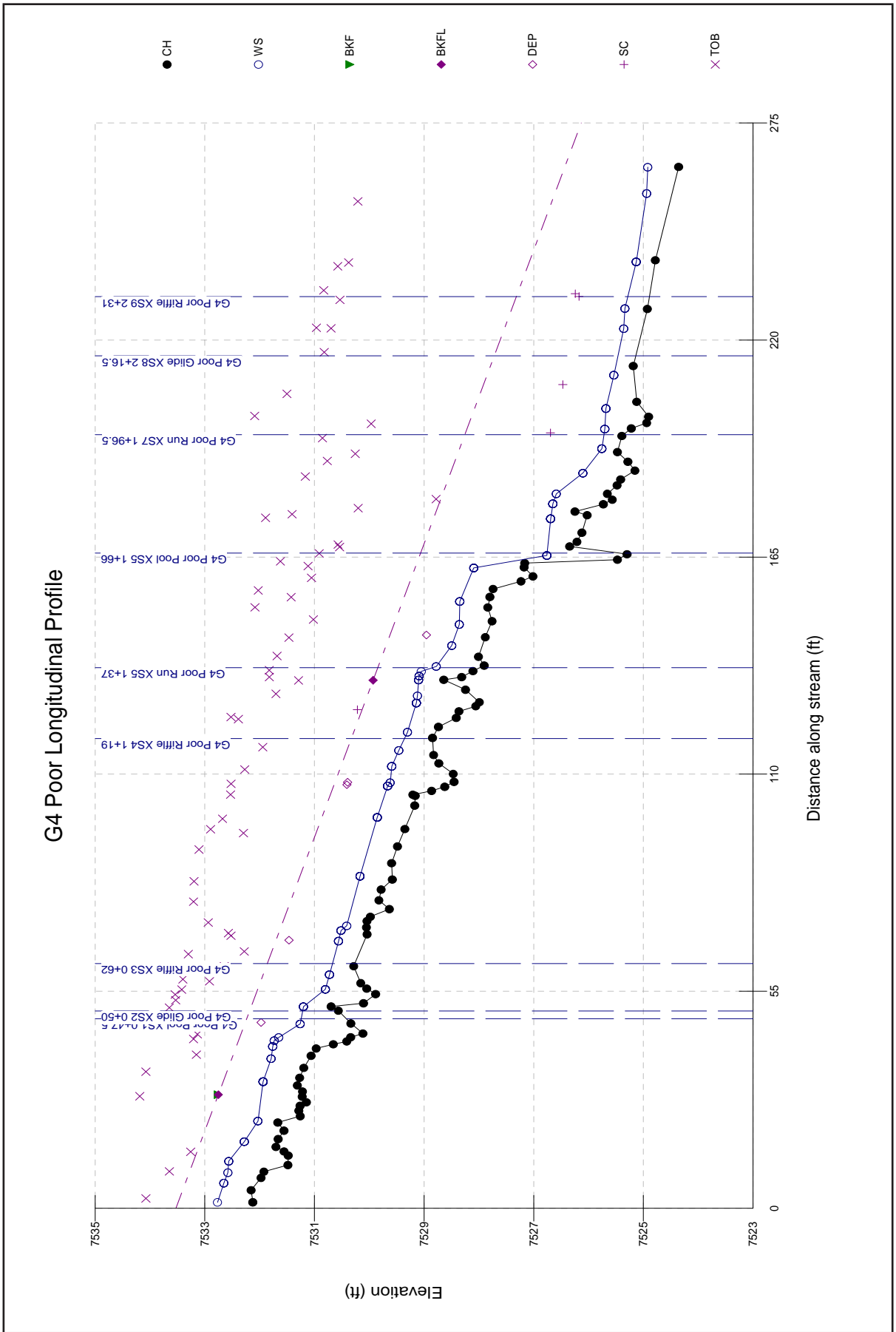
## G4 Poor Reach Location & Overview

The G4 Poor representative reach is a perennial stream located in the upper Trail Creek Watershed (Figure C-2). The stream is entrenched with evident bank erosion and is actively downcutting in previously deposited sediment as depicted in the photograph. This channel had previously been a more stable C4 stream type in this terraced, alluvial Valley Type VIIIc. However, excess sediment deposition and subsequent downcutting converted this stream type to a G4. The stream has apparently not recovered from past floods and high sediment supply impacts. The width/depth ratio is trending to shift to an F4 stream type indicated by the width/depth ratio of 13.9 due to channel enlargement. This reach has a poor recovery potential if left in its present state. The potential stable stream type in the current valley type is a B4; thus POWERSED was used to determine streambed stability. The results approximated severe degradation rates of 17,922 *tons/yr* of downcutting through previously deposited material. The stability rating is “Poor” due to a Pfankuch stability rating of 138 (“Poor”) and the extreme streambank erosion rate of 0.658 *tons/yr/ft* compared to the B4 reference rate of 0.0048 *tons/yr/ft* (an increase of two orders of magnitude). The sediment supply rating is *Very High* due to the excess streambank erosion rates compared to the B4 reference and the channel degradation. The “Poor” rating indicates an extremely high potential increase in flow-related sediment compared to the same sized-B4 stream type reference. The WRENSS model resulted in a water yield increase due to the fire from 3,333 *acre-ft* to 6,066 *acre-ft*, representing a total increase of 2,733 *acre-ft*. The corresponding bedload increased from 45 *tons/yr* to 7,562 *tons/yr* and the suspended sediment increased from 92 *tons/yr* to 13,373 *tons/yr*, representing a total increase in sediment of 20,799 *tons/yr*. This enormous and disproportionate sediment yield reflects the sediment yield increases due to the increased flows in a severely unstable reach.

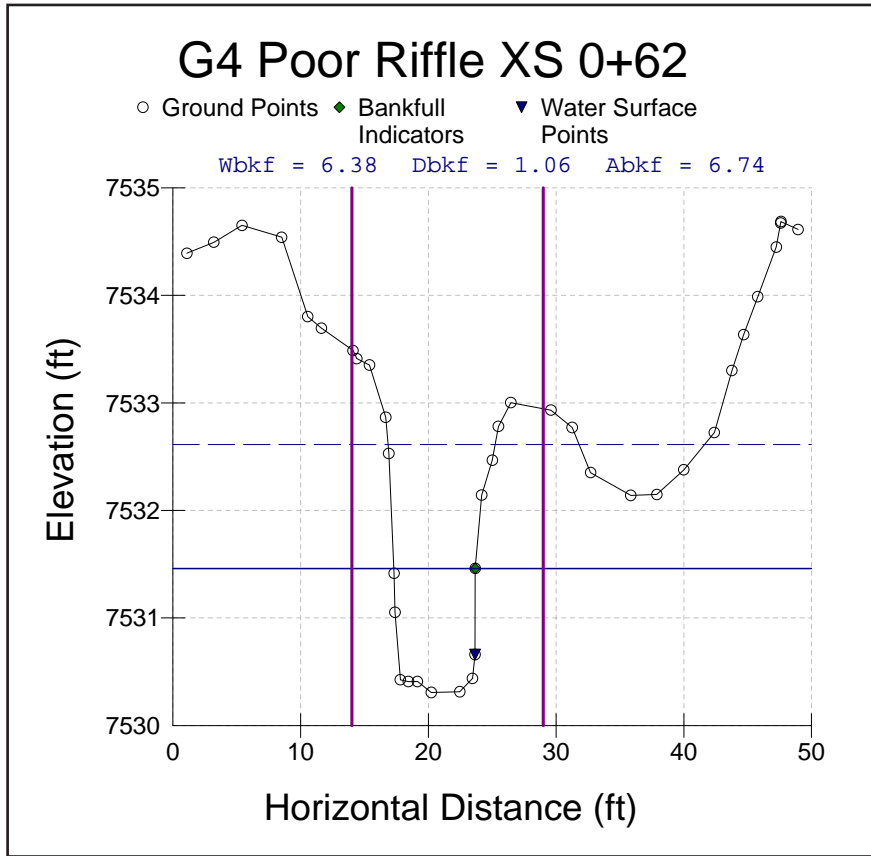
The following graphs and summary worksheets provide the detail of the morphology, hydraulics, streambank erosion rates, and stability conditions responsible for the overall “Poor” rating.



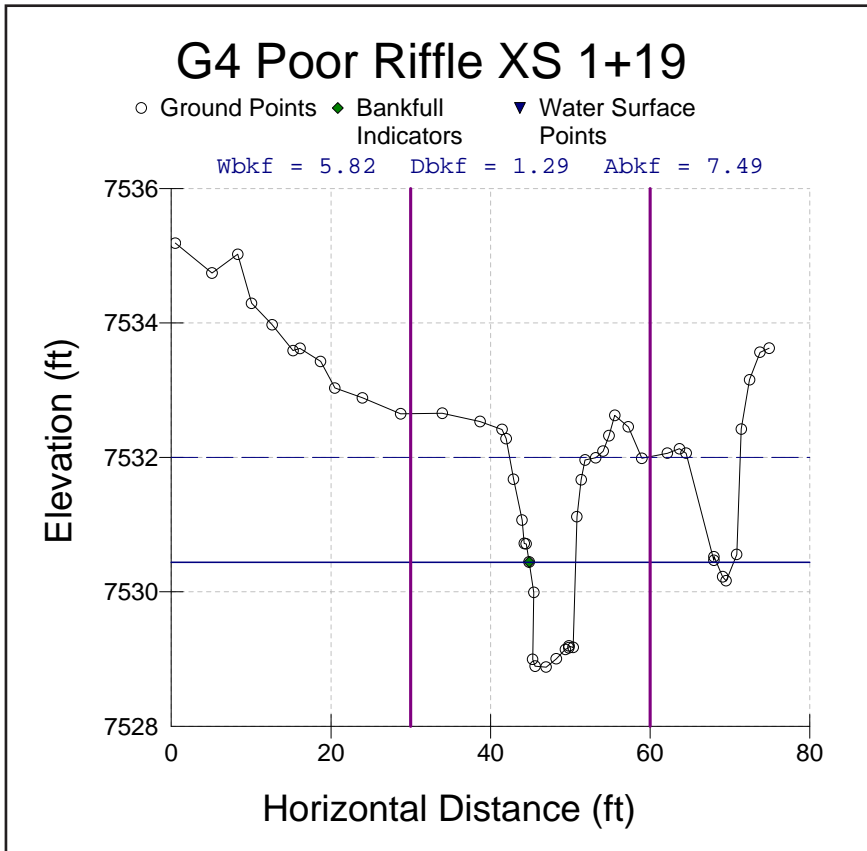
# Survey Summary



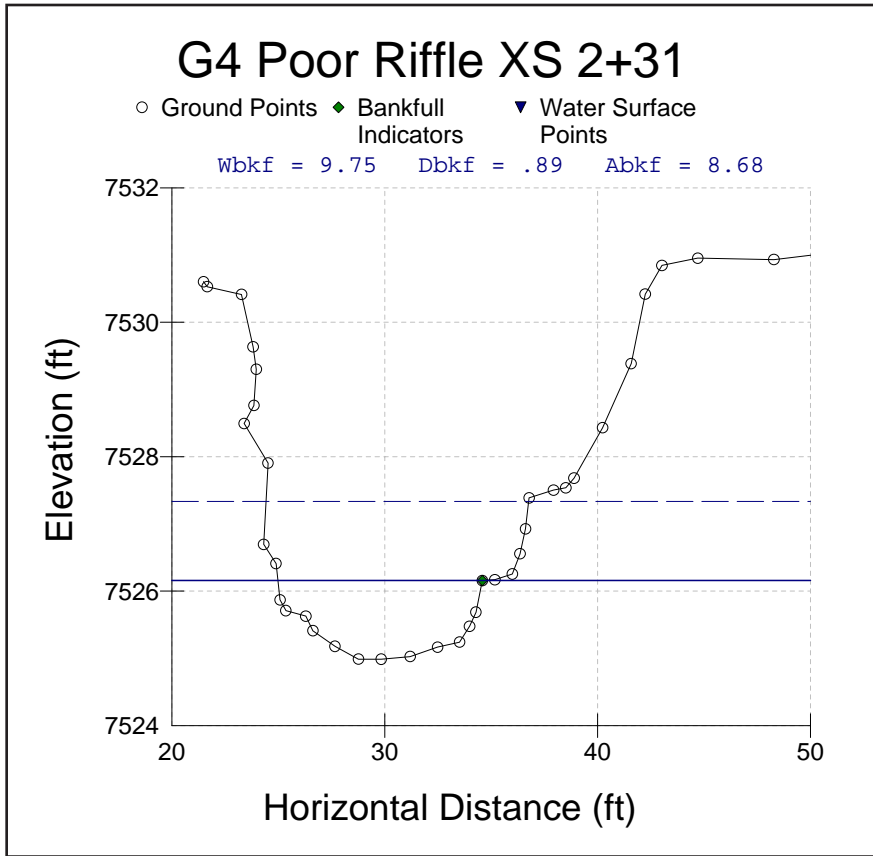
Longitudinal Profile (graph generated from RIVERMorph™)



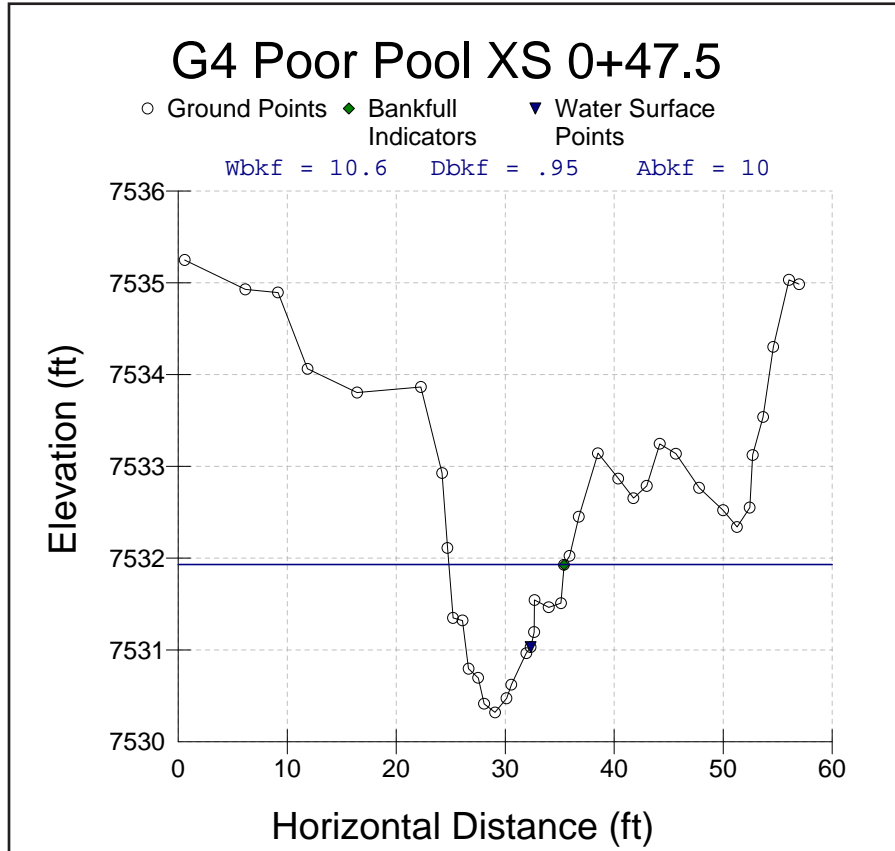
Riffle Cross-section 0+62 (graph generated from RIVERMorph™)



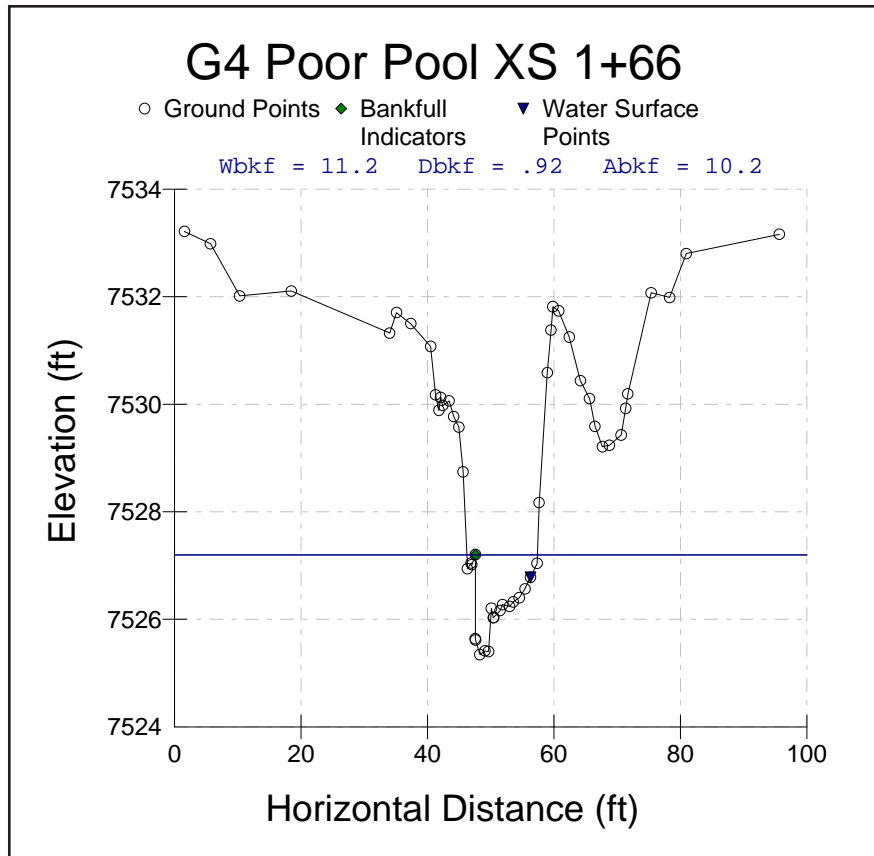
Riffle Cross-section 1+19 (graph generated from RIVERMorph™)



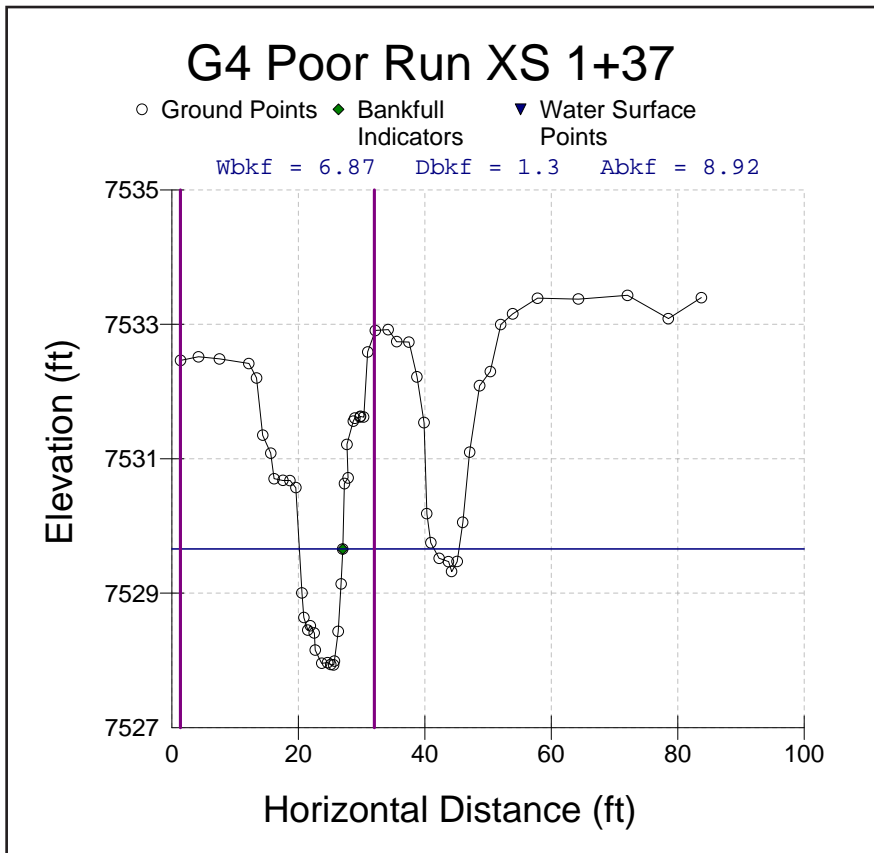
Riffle Cross-section 2+31 (graph generated from RIVERMorph™)



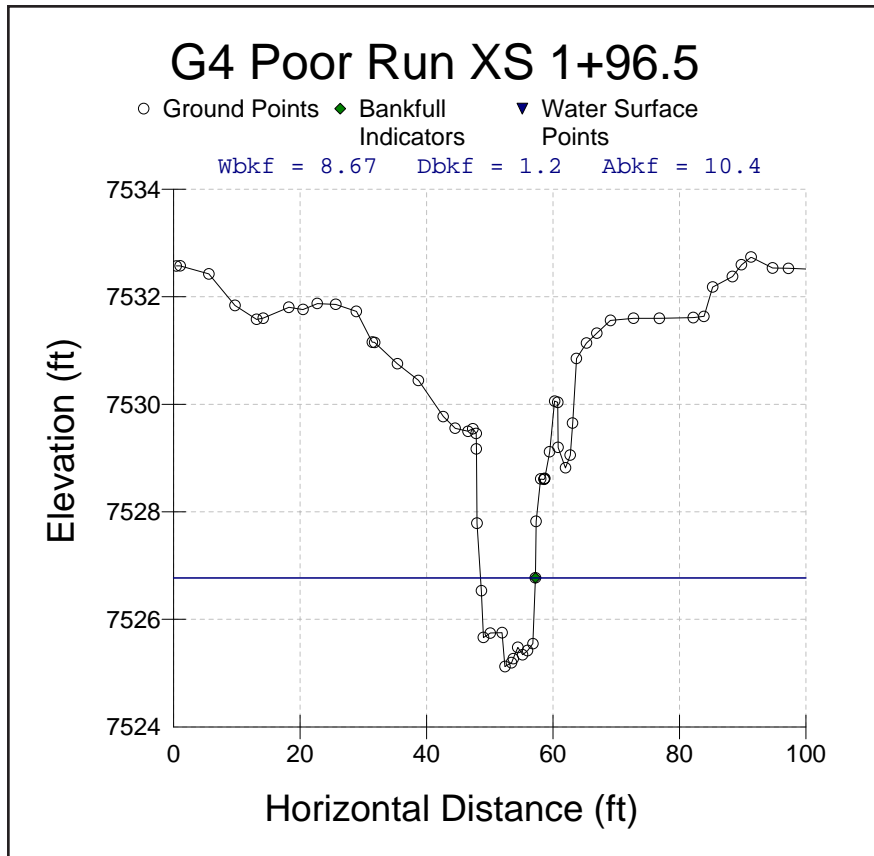
Pool Cross-Section 0+47.5 (graph generated from RIVERMorph™)



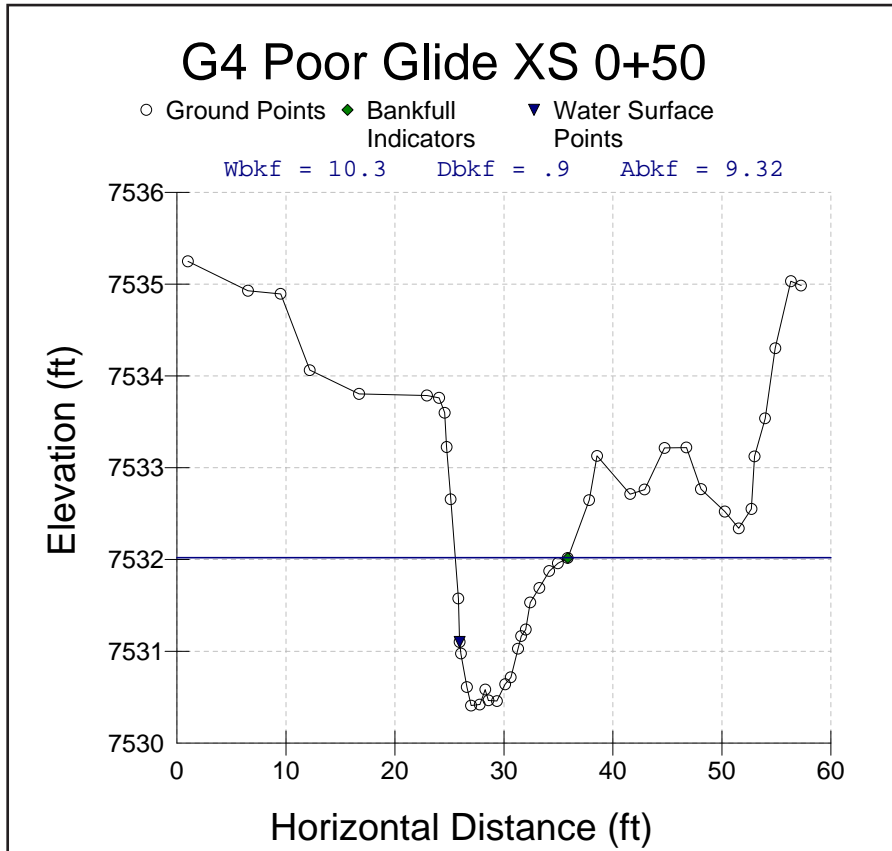
Pool Cross-section 1+66 (graph generated from RIVERMorph™)



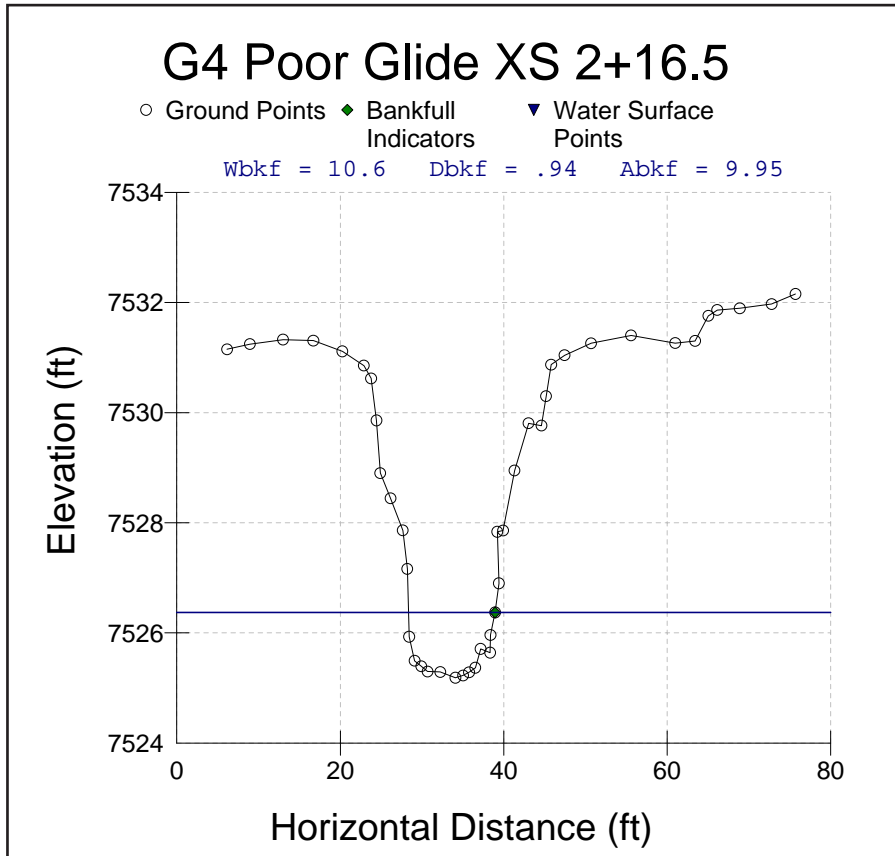
Run Cross-section 1+37 (graph generated from RIVERMorph™)



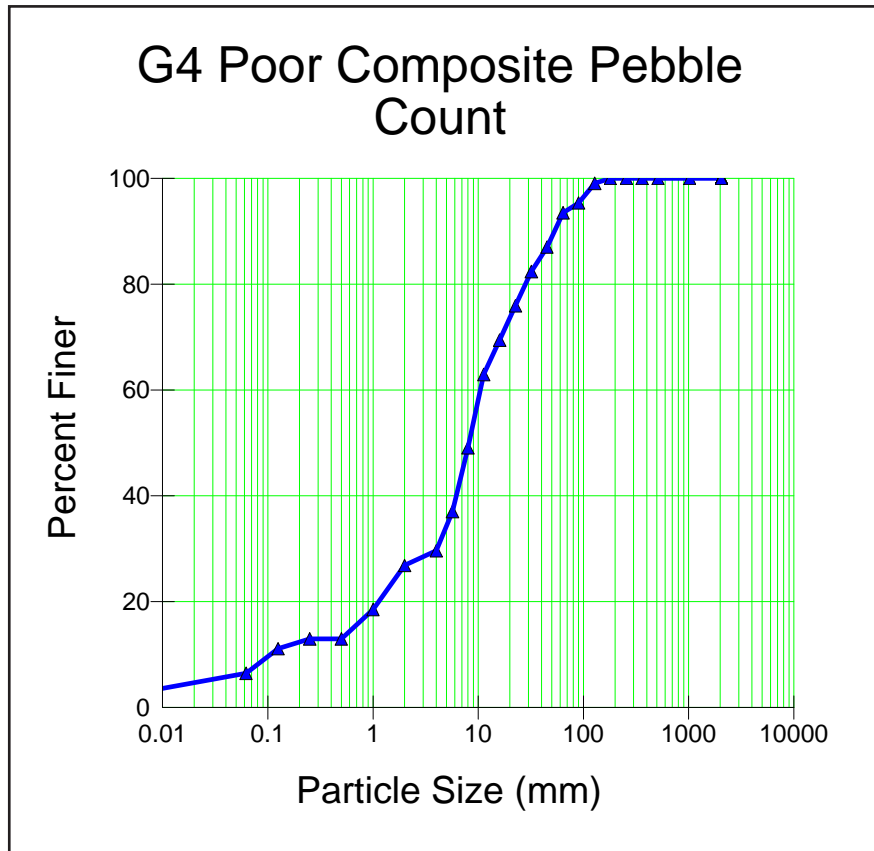
Run Cross-section 1+96.5 (graph generated from RIVERMorph™)



Glide Cross-Section 0+50 (graph generated from RIVERMorph™)

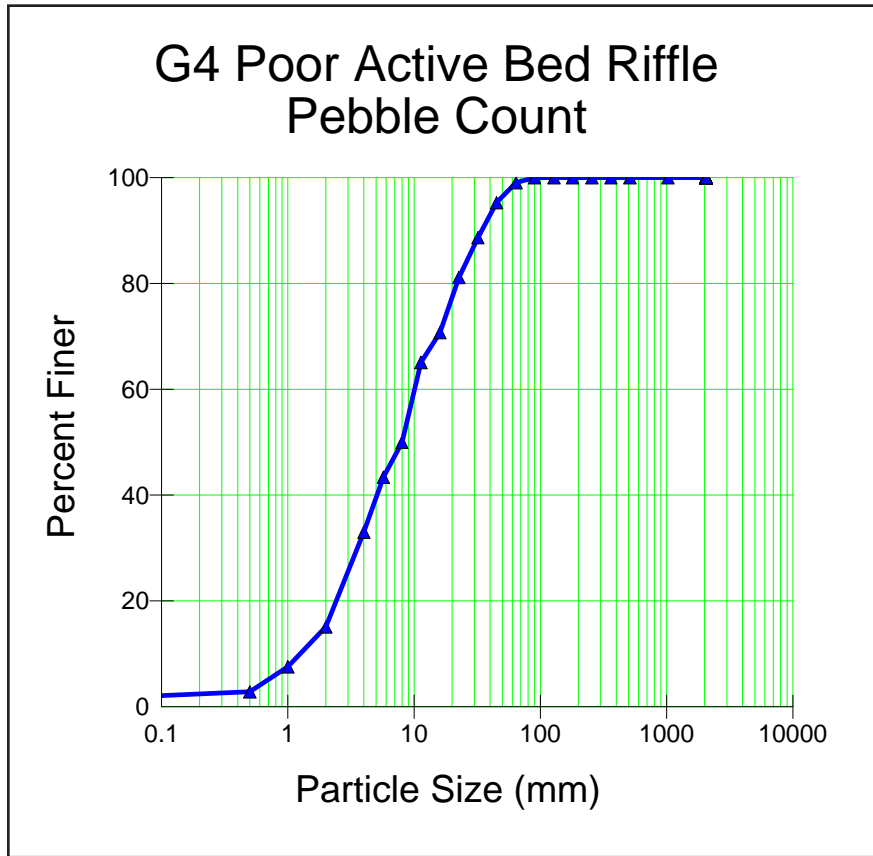


Glide Cross-Section 2+16.5 (graph generated from RIVERMorph™)

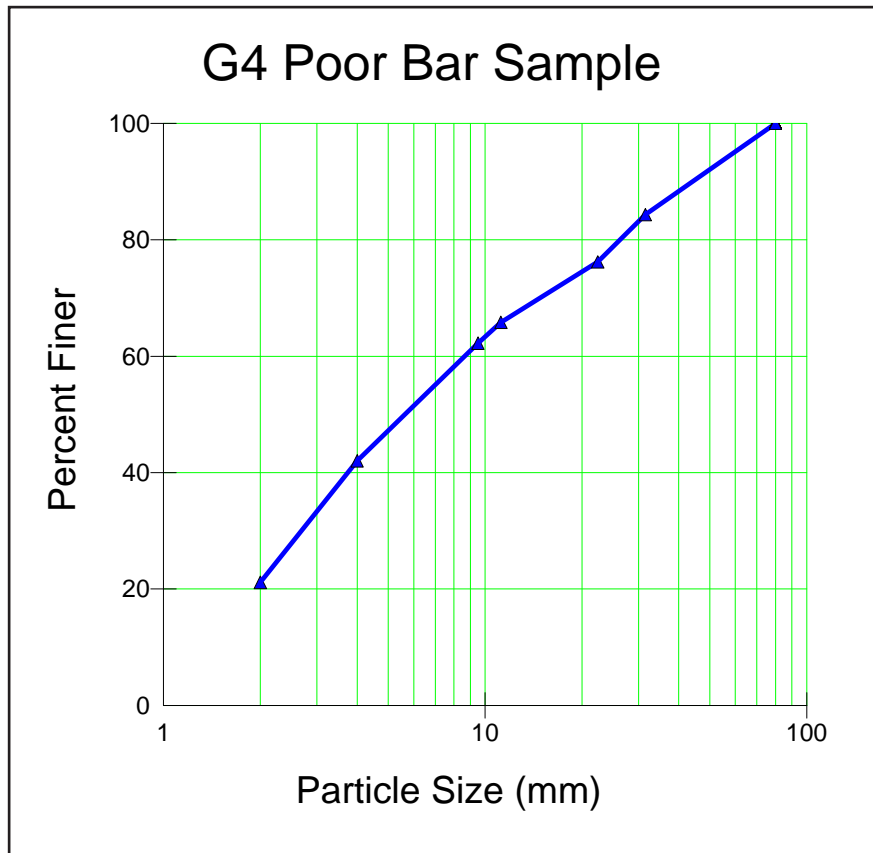


Composite Pebble Count (graph generated from RIVERMorph™)





Active Bed Riffle Pebble Count (graph generated from RIVERMorph™)



Bar Sample (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates					
Stream:	Trail Creek, G4 Poor Reach			Location:	Riffle XS 2+31, Pike N.F., Colorado
Date:	8/18/2010	Stream Type:	G4	Valley Type:	VIII
Observers:	B. Kasun <i>et al.</i>			HUC:	___-___-___-___-___-___-___-___-___-___
INPUT VARIABLES			OUTPUT VARIABLES		
Bankfull Riffle Cross-Sectional AREA	8.68	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.89	$d_{bkf}$ (ft)
Bankfull Riffle WIDTH	9.75	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim (2 * d_{bkf}) + W_{bkf}$	10.50	$W_p$ (ft)
$D_{84}$ at Riffle	26.2	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.09	$D_{84}$ (ft)
Bankfull SLOPE	0.0258	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	0.83	R (ft)
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness $R(ft) / D_{84}(ft)$	9.62	$R / D_{84}$
Drainage Area	15.9	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.829	$u^*$ (ft/sec)
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$			6.96	ft / sec	60.38 cfs
2. Roughness Coefficient: a) Manning's <i>n</i> from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.035$			6.02	ft / sec	52.28 cfs
2. Roughness Coefficient: b) Manning's <i>n</i> from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.06$			3.51	ft / sec	30.50 cfs
2. Roughness Coefficient: c) Manning's <i>n</i> from Jarrett (USGS): $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ <small>Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for Stream Types A1, A2, A3, B1, B2, B3, C2 &amp; E3</small> $n = 0.100$			2.10	ft / sec	18.27 cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)				ft / sec	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)				ft / sec	cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q =$ <input type="text"/> year $u = Q / A$				ft / sec	cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$				ft / sec	cfs
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation ( $R/D_{84}$ ) – Estimation Method 1					
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.					
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.					
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.					
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.					

**Worksheet 5-3.** Level II stream classification.

Stream: <b>Trail Creek, G4 Poor Reach</b>	
Basin:	Drainage Area: <b>10176</b> acres <b>15.9</b> mi <sup>2</sup>
Location: <b>XS 2+31, Pike National Forest, Colorado</b>	
Twp.&Rge:	Sec.&Qtr.:
Cross-Section Monuments (Lat./Long.): <b>Lat =39.13425 Long=105.16711</b> Date: <b>8/18/2010</b>	
Observers: <b>B. Kasun et al.</b>	Valley Type: <b>VIII</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>9.75</b> ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A_{bkf} / W_{bkf}$ ).	<b>0.89</b> ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>8.68</b> ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>10.95</b> ft/ft
<b>Maximum DEPTH (<math>d_{max}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>1.17</b> ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{max}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>12.35</b> ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>1.17</b> ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the median or dominant diameter of channel materials, as sampled proportionately from the channel surface, between the bankfull stage and Thalweg elevations.	<b>8</b> mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.0258</b> ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope ( $S_{val} / S$ ).	<b>1.05</b>

<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>Stream Type</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: #e0f0ff;"> <b>G4</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>See Classification Key (Figure 2-14)</b> </div>
---	---	--

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, G4 Poor Reach</b>		Location: <b>Pike National Forest, Colorado</b>							
Observers: <b>B. Kasun et al.</b>		Date: <b>8/18/2010</b>		Valley Type: <b>VIII</b>		Stream Type: <b>G4</b>			
<b>River Reach Dimension Summary Data.....1</b>									
<b>Riffle Dimensions*</b> , **, ***	<b>Riffle Dimensions*</b> ****, ***	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Width ( $W_{bkt}$ )	<b>6.38</b>	<b>5.82</b>	<b>9.75</b>	ft	Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	<b>7.64</b>	<b>6.74</b>	<b>8.68</b>
	Mean Riffle Depth ( $d_{bkt}$ )	<b>1.08</b>	<b>0.89</b>	<b>1.29</b>	ft	Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	<b>7.16</b>	<b>4.51</b>	<b>10.96</b>
	Maximum Riffle Depth ( $d_{max}$ )	<b>1.29</b>	<b>1.15</b>	<b>1.56</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>1.203</b>	<b>1.085</b>	<b>1.315</b>
	Width of Flood-Prone Area ( $W_{fpa}$ )	<b>10.03</b>	<b>8.41</b>	<b>12.35</b>	ft	Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )	<b>1.36</b>	<b>1.17</b>	<b>1.32</b>
	Riffle Inner Berm Width ( $W_{ib}$ )				ft	Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )			
	Riffle Inner Berm Depth ( $d_{ib}$ )				ft	Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )			
	Riffle Inner Berm Area ( $A_{ib}$ )				ft <sup>2</sup>	Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )			
	Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )								
<b>Pool Dimensions*</b> , **, ***	<b>Pool Dimensions*</b> ****, ***	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Pool Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Pool Width ( $W_{bkfp}$ )	<b>9.6</b>	<b>8.6</b>	<b>10.6</b>	ft	Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )	<b>1.500</b>	<b>1.340</b>	<b>1.660</b>
	Mean Pool Depth ( $d_{bkfp}$ )	<b>0.81</b>	<b>0.67</b>	<b>0.95</b>	ft	Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )	<b>0.750</b>	<b>0.620</b>	<b>0.880</b>
	Pool Cross-Sectional Area ( $A_{bkfp}$ )	<b>7.9</b>	<b>5.7</b>	<b>10.0</b>	ft	Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )	<b>1.031</b>	<b>0.749</b>	<b>1.313</b>
	Maximum Pool Depth ( $d_{maxp}$ )	<b>1.51</b>	<b>1.40</b>	<b>1.61</b>	ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	<b>1.398</b>	<b>1.296</b>	<b>1.491</b>
	Pool Inner Berm Width ( $W_{ibp}$ )				ft	Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )			
	Pool Inner Berm Depth ( $d_{ibp}$ )				ft	Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )			
	Pool Inner Berm Area ( $A_{ibp}$ )				ft <sup>2</sup>	Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )			
	Point Bar Slope ( $S_{pb}$ )				ft/ft	Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )			
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Run Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Run Width ( $W_{bkfr}$ )	<b>9.7</b>	<b>8.7</b>	<b>10.8</b>	ft	Run Width to Riffle Width ( $W_{bkfr} / W_{bkt}$ )	<b>1.527</b>	<b>1.359</b>	<b>1.694</b>
	Mean Run Depth ( $d_{bkfr}$ )	<b>1.69</b>	<b>1.65</b>	<b>1.73</b>	ft	Mean Run Depth to Mean Riffle Depth ( $d_{bkfr} / d_{bkt}$ )	<b>1.565</b>	<b>1.528</b>	<b>1.602</b>
	Run Cross-Sectional Area ( $A_{bkfr}$ )	<b>10.0</b>	<b>9.6</b>	<b>10.4</b>	ft	Run Area to Riffle Area ( $A_{bkfr} / A_{bkt}$ )	<b>1.313</b>	<b>1.259</b>	<b>1.366</b>
	Maximum Run Depth ( $d_{maxr}$ )	<b>1.69</b>	<b>1.65</b>	<b>1.73</b>	ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )	<b>1.565</b>	<b>1.528</b>	<b>1.602</b>
	Run Width/Depth Ratio ( $W_{bkfr} / d_{bkfr}$ )	<b>5.7</b>	<b>5.3</b>	<b>6.2</b>	ft				
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Glide Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Glide Width ( $W_{bkfg}$ )	<b>10.5</b>	<b>10.3</b>	<b>10.6</b>	ft	Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )	<b>1.639</b>	<b>1.621</b>	<b>1.658</b>
	Mean Glide Depth ( $d_{bkfg}$ )	<b>1.40</b>	<b>1.18</b>	<b>1.61</b>	ft	Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )	<b>1.296</b>	<b>1.093</b>	<b>1.491</b>
	Glide Cross-Sectional Area ( $A_{bkfg}$ )	<b>9.6</b>	<b>9.3</b>	<b>10.0</b>	ft	Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )	<b>1.262</b>	<b>1.217</b>	<b>1.302</b>
	Maximum Glide Depth ( $d_{maxg}$ )	<b>1.40</b>	<b>1.18</b>	<b>1.61</b>	ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )	<b>1.296</b>	<b>1.093</b>	<b>1.491</b>
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )	<b>7.5</b>	<b>8.7</b>	<b>6.6</b>	ft/ft	Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )			
	Glide Inner Berm Width ( $W_{ibg}$ )				ft	Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )			
	Glide Inner Berm Depth ( $d_{ibg}$ )				ft	Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )			
Glide Inner Berm Area ( $A_{ibg}$ )				ft <sup>2</sup>	Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )				
<b>Step**</b>	<b>Step Dimensions**</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Step Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Step Width ( $W_{bkfs}$ )				ft	Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )			
	Mean Step Depth ( $d_{bkfs}$ )				ft	Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )			
	Step Cross-Sectional Area ( $A_{bkfs}$ )				ft	Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )			
	Maximum Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )									

**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, G4 Poor Reach</b>		Location: <b>Pike National Forest, Colorado</b>											
Observers: <b>B. Kasun et al.</b>		Date: <b>8/18/2010</b>		Valley Type: <b>VIII</b>		Stream Type: <b>G4</b>							
<b>Hydraulics</b>	<b>River Reach Summary Data.....2</b>												
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )		<b>3.5</b>		ft/sec		Estimation Method	<b>"n" by Stream Type</b>					
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )		<b>30.3</b>		cfs		Drainage Area	<b>15.9</b> mi <sup>2</sup>					
<b>Channel Pattern</b>	<b>Geometry</b>			<b>Dimensionless Geometry Ratios</b>									
	Linear Wavelength ( $\lambda$ )			ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )								
	Stream Meander Length ( $L_m$ )			ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )								
	Radius of Curvature ( $R_c$ )			ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )								
	Belt Width ( $W_{bit}$ )	<b>14.6</b>		ft	Meander Width Ratio ( $W_{bit} / W_{bkt}$ )	<b>2.29</b>							
	Arc Length ( $L_a$ )			ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )								
	Riffle Length ( $L_r$ )	<b>4.6</b>	<b>1.3</b>	<b>9.1</b>	ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )	<b>0.72</b>	<b>0.20</b>	<b>1.43</b>				
	Individual Pool Length ( $L_p$ )	<b>7.8</b>	<b>4.1</b>	<b>11.4</b>	ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )	<b>1.22</b>	<b>0.64</b>	<b>1.79</b>				
Pool to Pool Spacing ( $P_s$ )	<b>163.0</b>	<b>7.6</b>	<b>24.2</b>	ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )	<b>25.55</b>	<b>1.19</b>	<b>3.79</b>					
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )	<b>0.0270</b>		ft/ft	Average Water Surface Slope (S)	<b>0.0258</b>		ft/ft	Sinuosity ( $S_{val} / S$ )	<b>1.05</b>			
	Stream Length (SL)	<b>232.0</b>		ft	Valley Length (VL)	<b>222.0</b>		ft	Sinuosity (SL / VL)	<b>1.05</b>			
	Low Bank Height (LBH)	start: <b>2.00</b>	ft	end: <b>2.50</b>	ft	Max Bankfull Depth ( $d_{max}$ )	start: <b>1.10</b>	ft	end: <b>1.10</b>	ft	Bank-Height Ratio (BHR) (LBH / $d_{max}$ )	start: <b>1.8</b>	end: <b>2.3</b>
	<b>Facet Slopes</b>			<b>Dimensionless Facet Slope Ratios</b>									
	Riffle Slope ( $S_{rif}$ )	<b>0.0240</b>	<b>0.0150</b>	<b>0.0370</b>	ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rif} / S$ )	<b>0.9302</b>	<b>0.5814</b>	<b>1.4341</b>				
	Run Slope ( $S_{run}$ )	<b>0.0690</b>	<b>0.0180</b>	<b>0.1110</b>	ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )	<b>2.6744</b>	<b>0.6977</b>	<b>4.3023</b>				
	Pool Slope ( $S_p$ )	<b>0.0130</b>	<b>0.0060</b>	<b>0.0200</b>	ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )	<b>0.5039</b>	<b>0.2326</b>	<b>0.7752</b>				
	Glide Slope ( $S_g$ )	<b>0.0240</b>	<b>0.0060</b>	<b>0.0620</b>	ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )	<b>0.9302</b>	<b>0.2326</b>	<b>2.4031</b>				
	Step Slope ( $S_s$ )				ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )							
	<b>Max Depths<sup>a</sup></b>			<b>Dimensionless Depth Ratios</b>									
	Max Riffle Depth ( $d_{max}$ )	<b>1.29</b>	<b>1.15</b>	<b>1.56</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>1.194</b>	<b>1.065</b>	<b>1.444</b>				
	Max Run Depth ( $d_{maxr}$ )	<b>1.73</b>	<b>1.65</b>	<b>1.96</b>	ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )	<b>1.602</b>	<b>1.528</b>	<b>1.815</b>				
	Max Pool Depth ( $d_{maxp}$ )	<b>1.51</b>	<b>1.40</b>	<b>1.61</b>	ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	<b>1.398</b>	<b>1.296</b>	<b>1.491</b>				
	Max Glide Depth ( $d_{maxg}$ )	<b>1.40</b>	<b>1.18</b>	<b>1.61</b>	ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )	<b>1.296</b>	<b>1.093</b>	<b>1.491</b>				
	Max Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )							
<b>Channel Materials</b>		<b>Reach<sup>b</sup></b>	<b>Riffle<sup>c</sup></b>	<b>Bar</b>		<b>Reach<sup>b</sup></b>	<b>Riffle<sup>c</sup></b>	<b>Bar</b>	<b>Protrusion Height<sup>d</sup></b>				
	% Silt/Clay	<b>6</b>	<b>0</b>	<b>0</b>	$D_{16}$	<b>1.0</b>	<b>2.0</b>	<b>0.0</b>	mm				
	% Sand	<b>20</b>	<b>15</b>	<b>21</b>	$D_{35}$	<b>5.0</b>	<b>4.0</b>	<b>3.0</b>	mm				
	% Gravel	<b>67</b>	<b>84</b>	<b>75</b>	$D_{50}$	<b>8.0</b>	<b>8.0</b>	<b>6.0</b>	mm				
	% Cobble	<b>6</b>	<b>1</b>	<b>4</b>	$D_{84}$	<b>36.0</b>	<b>26.0</b>	<b>31.0</b>	mm				
	% Boulder				$D_{95}$	<b>85.0</b>	<b>44.0</b>	<b>65.0</b>	mm				
	% Bedrock				$D_{100}$	<b>180.0</b>	<b>90.0</b>	<b>80.0</b>	mm				

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.  
<sup>b</sup> Composite sample of riffles and pools within the designated reach.      <sup>c</sup> Active bed of a riffle.      <sup>d</sup> Height of roughness feature above bed.

## Stability Indices


**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation					
Stream: <b>Trail Creek, G4 Poor Reach</b>			Location: <b>Pike National Forest, Colorado</b>		
Observers: <b>B. Kasun et al.</b>		Reference reach <input type="checkbox"/>	Disturbed (impacted reach) <input checked="" type="checkbox"/>	Date: <b>8/18/2010</b>	
Existing species composition: <b>Willow</b>			Potential species composition: <b>Willow, Salix, Alder</b>		
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition
<b>1. Overstory</b>	Canopy layer	<b>0%</b>	<b>0%</b>		
					<b>100%</b>
<b>2. Understory</b>	Shrub layer		<b>15%</b>	<b>Willows, 2 BroadleafSp.</b>	<b>100%</b>
					<b>100%</b>
<b>3. Ground level</b>	Herbaceous		<b>35%</b>	<b>Horseweed</b>	<b>65%</b>
				<b>Phacella</b>	<b>5%</b>
				<b>Grasses</b>	<b>20%</b>
				<b>Invasives (Mullen)</b>	<b>10%</b>
				<b>Carex</b>	<b>17%</b>
					<b>100%</b>
	Leaf or needle litter		<b>20%</b>	<b>Remarks:</b> Condition, vigor and/or usage of existing reach:	
	Bare ground		<b>30%</b>		
*Based on crown closure. **Based on basal area to surface area.			<b>Column total = 100%</b>		

**Worksheet 5-7.** Flow regime.

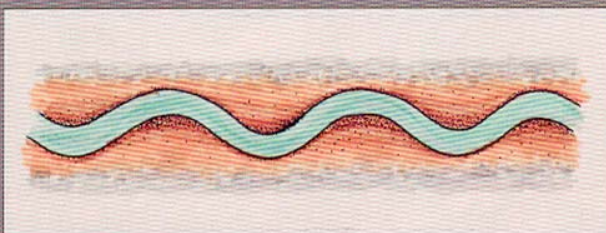




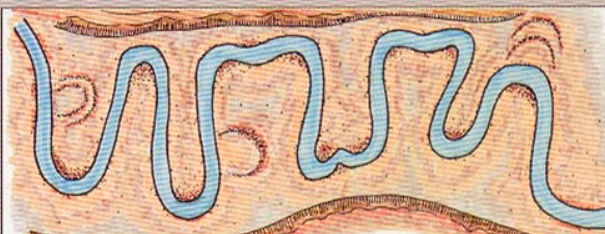
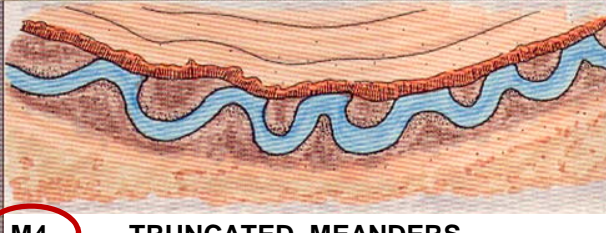
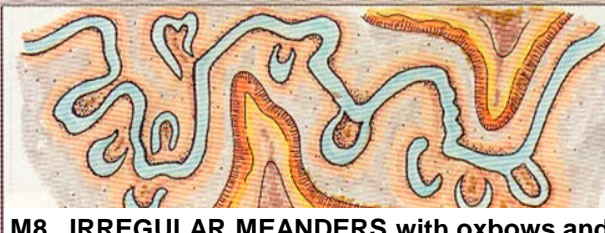
<b>FLOW REGIME</b>								
Stream: <b>Trail Creek, G4 Poor Reach</b>			Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>B. Kasun <i>et al.</i></b>						Date: <b>8/18/2010</b>		
<b>List ALL COMBINATIONS that APPLY.....</b>	<b>P1</b>	<b>P2</b>	<b>P8</b>					
<b>General Category</b>								
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation							
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
<b>P</b>	Perennial stream channels: Surface water persists yearlong.							
<b>Specific Category</b>								
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
<b>4</b>	Streamflow regulated by glacial melt.							
<b>5</b>	Ice flows/ice torrents from ice dam breaches.							
<b>6</b>	Alternating flow/backwater due to tidal influence.							
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.							
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
<b>9</b>	Rain-on-snow generated runoff.							

**Worksheet 5-8.** Stream order & stream size.


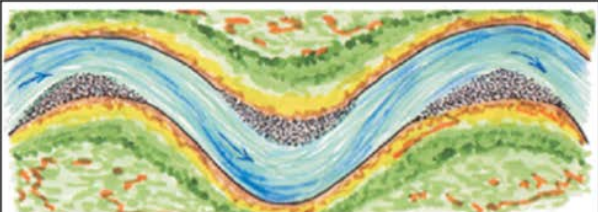


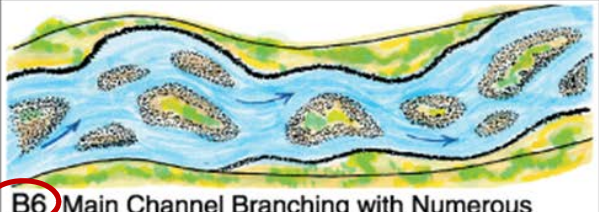




Stream Size and Order			
Stream:	Trail Creek, G4 Poor Reach		
Location:	Pike National Forest, Colorado		
Observers:	B. Kasun <i>et al.</i>		
Date:	8/18/2010		
Stream Size Category and Order 			S-3(4)
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0.305	<1	<input type="checkbox"/>
S-2	0.3 – 1.5	1 – 5	<input type="checkbox"/>
<b>S-3</b>	<b>1.5 – 4.6</b>	<b>5 – 15</b>	<input checked="" type="checkbox"/>
S-4	4.6 – 9	15 – 30	<input type="checkbox"/>
S-5	9 – 15	30 – 50	<input type="checkbox"/>
S-6	15 – 22.8	50 – 75	<input type="checkbox"/>
S-7	22.8 – 30.5	75 – 100	<input type="checkbox"/>
S-8	30.5 – 46	100 – 150	<input type="checkbox"/>
S-9	46 – 76	150 – 250	<input type="checkbox"/>
S-10	76 – 107	250 – 350	<input type="checkbox"/>
S-11	107 – 150	350 – 500	<input type="checkbox"/>
S-12	150 – 305	500 – 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
Stream Order			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			



Worksheet 5-9. Meander patterns.

<b>Meander Patterns</b>					
Stream: <b>Trail Creek, G4 Poor Reach</b>	Location: <b>Pike National Forest, CO</b>				
Observers: <b>B. Kasun et al.</b>	Date: <b>8/18/2010</b>				
List ALL CATEGORIES that APPLY	<b>M3</b>	<b>M4</b>			
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>					
 <b>M1</b> <b>REGULAR MEANDERS</b>	 <b>M5</b> <b>UNCONFINED MEANDER SCROLLS</b>				
 <b>M2</b> <b>TORTUOUS MEANDERS</b>	 <b>M6</b> <b>CONFINED MEANDER SCROLLS</b>				
 <span style="border: 1px solid red; border-radius: 50%; padding: 2px;"><b>M3</b></span> <b>IRREGULAR MEANDERS</b>	 <b>M7</b> <b>DISTORTED MEANDER LOOPS</b>				
 <span style="border: 1px solid red; border-radius: 50%; padding: 2px;"><b>M4</b></span> <b>TRUNCATED MEANDERS</b>	 <b>M8</b> <b>IRREGULAR MEANDERS with oxbows and</b>				

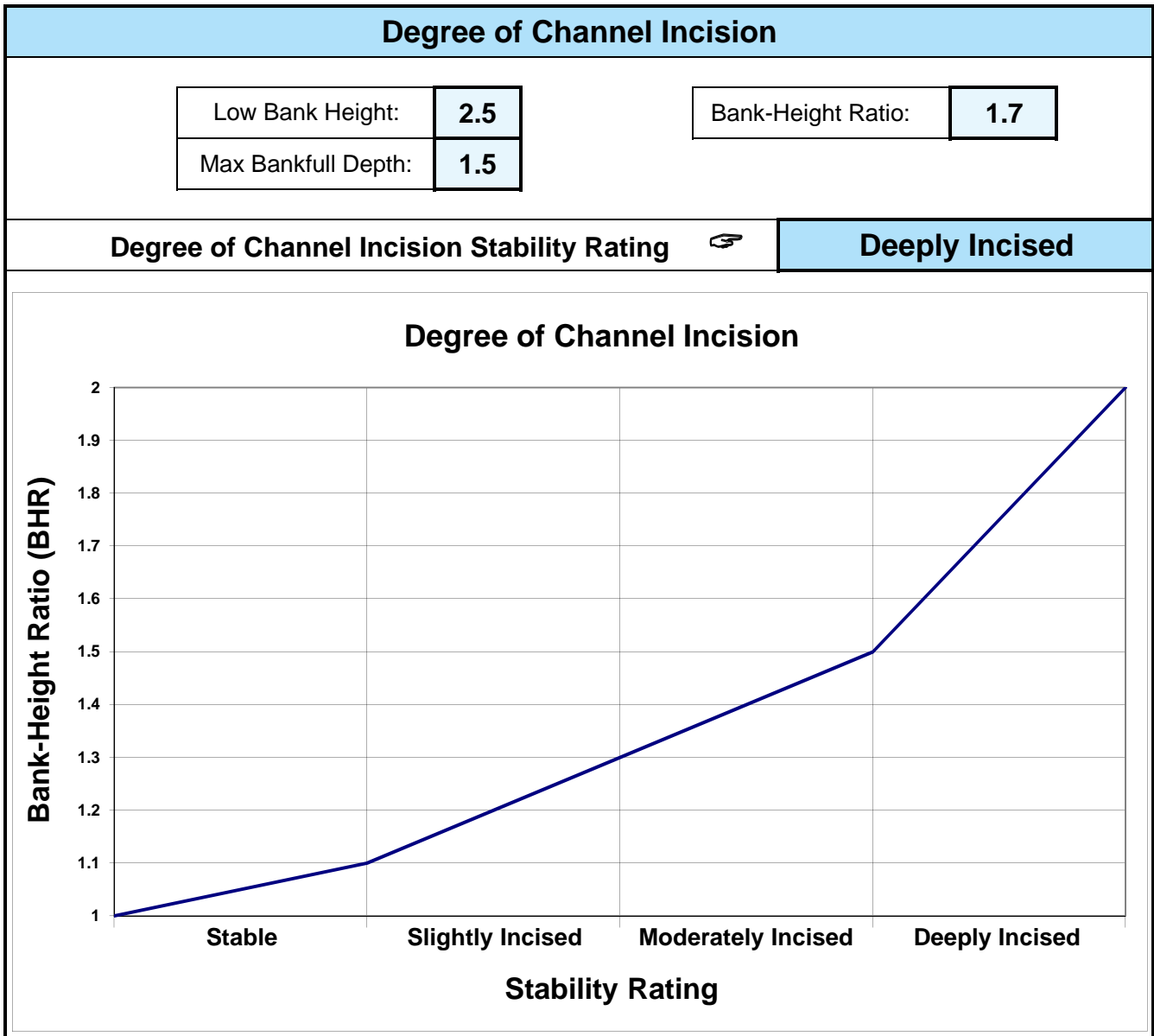
Worksheet 5-10. Depositional patterns.

Depositional Patterns					
Stream: Trail Creek, G4 Poor Reach		Location: Pike National Forest, Colorado			
Observers: B. Kasun et al.		Date: 8/18/2010			
List ALL CATEGORIES that APPLY 	B6	B7			
<i>Various Depositional Features modified from Galay et al. (1973)</i>					
 <p>B1 POINT BARS</p>	 <p>B5 DIAGONAL BARS</p>				
 <p>B2 POINT BARS with Few MID-CHANNEL BARS</p>	 <p><b>B6</b> Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</p>				
 <p>B3 NUMEROUS MID-CHANNEL BARS</p>	 <p><b>B7</b> SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</p>				
 <p>B4 SIDE BARS</p>	 <p>B8 DELTA BARS</p>				

## Worksheet 5-11. Channel blockages.

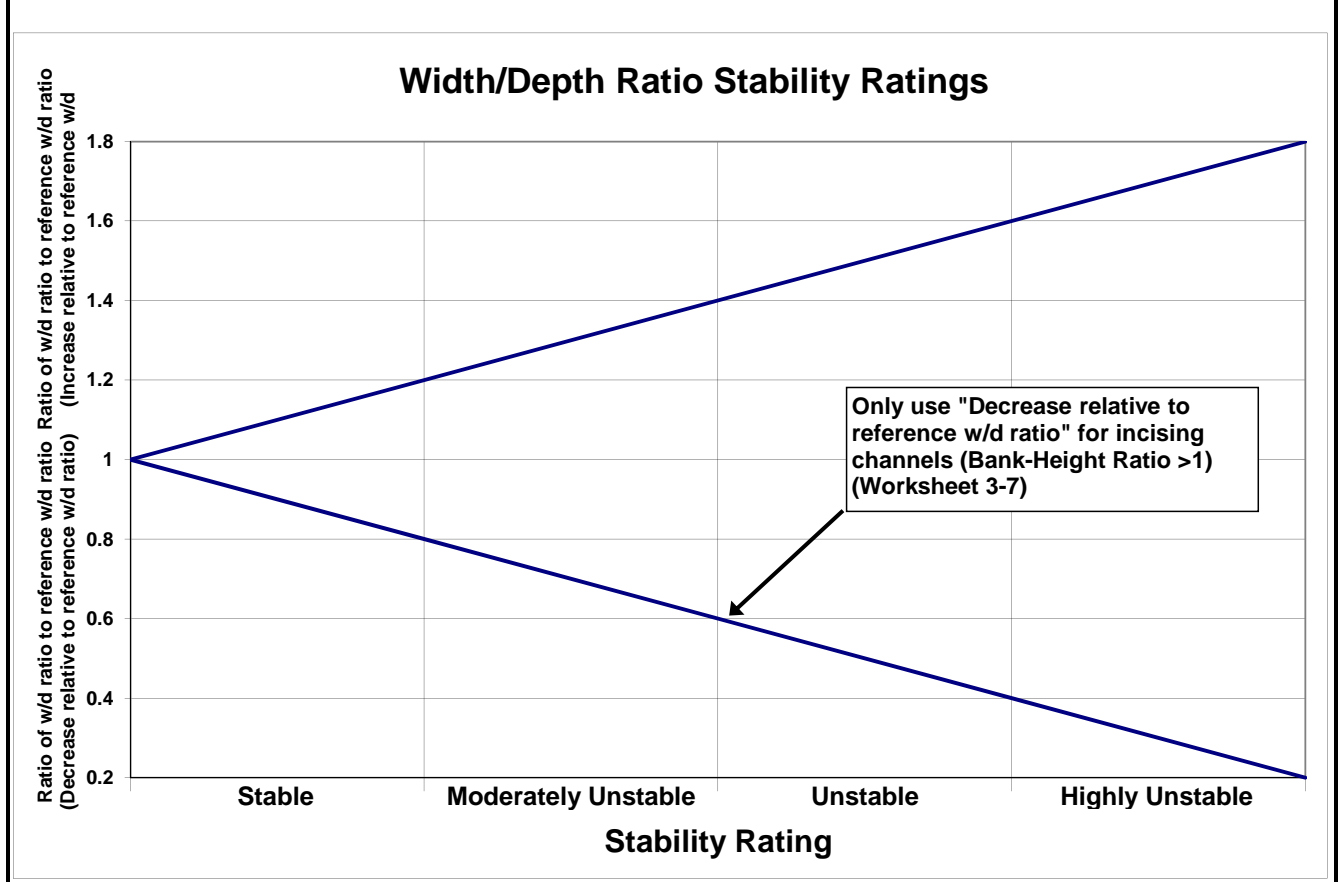
Channel Blockages		
Stream: <b>Trail Creek, G4 Poor Reach</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>B. Kasun et al.</b>		Date: <b>8/18/2010</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input checked="" type="checkbox"/>
<b>D4</b> Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

**Worksheet 5-12.** Degree of channel incision.



**Worksheet 5-13.** Width/depth ratio state.

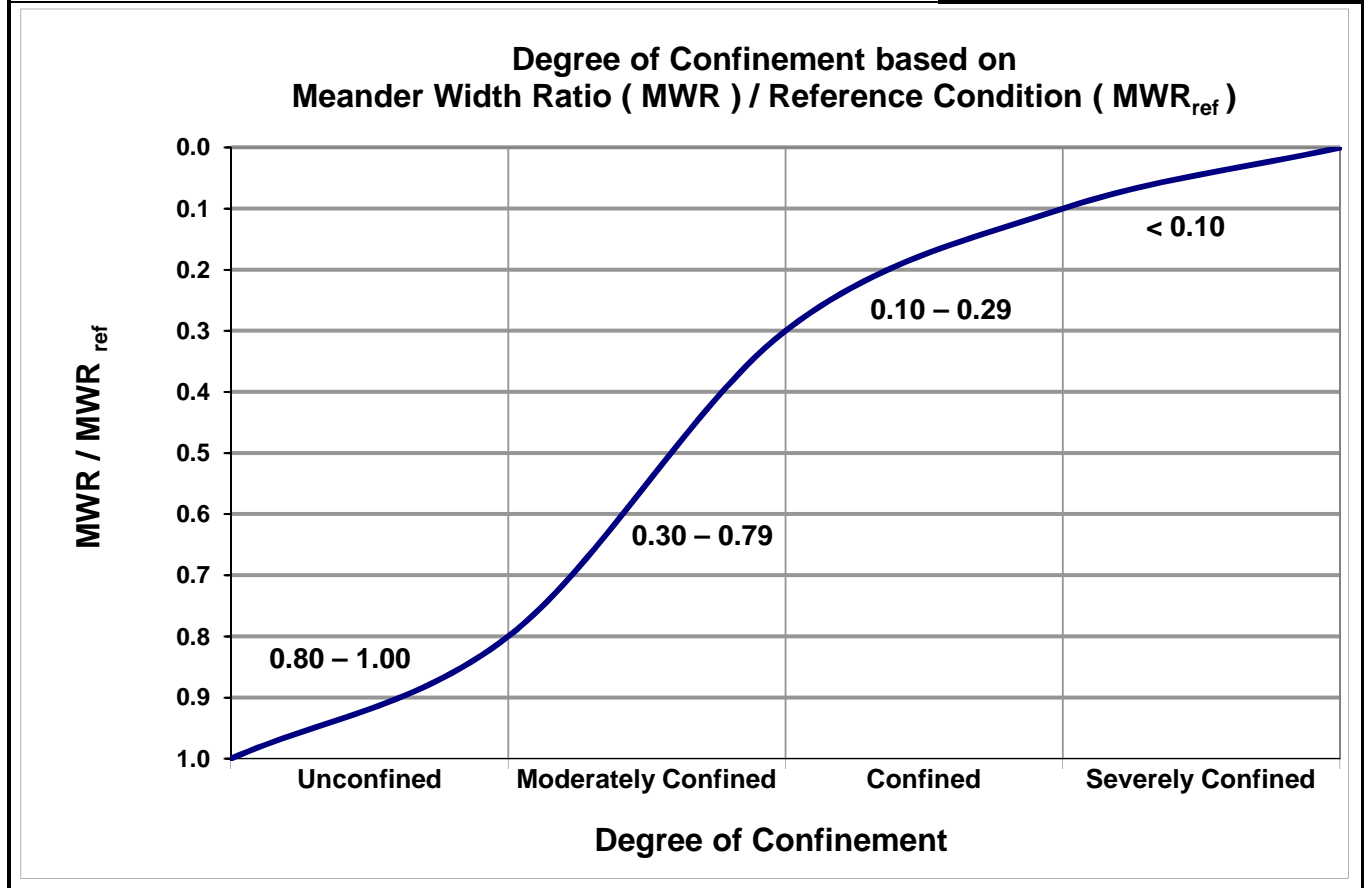
Width/Depth Ratio State			
Existing Width/Depth Ratio:	<b>6*</b>	Ratio of existing W/d to reference W/d:	<b>0.48</b>
Reference Width/Depth Ratio:	<b>12.57</b>	*Riffle XS 0+62	
Width/Depth Ratio State Stability Rating			<b>Unstable</b>



**Worksheet 5-14.** Degree of channel confinement (lateral containment).

Degree of Confinement			
Existing Meander Width Ratio (MWR):	<b>1.8</b>	Ratio of MWR to $MWR_{ref}$ :	<b>0.49</b>
Reference Meander Width Ratio ( $MWR_{ref}$ ):	<b>3.7</b>		

<b>Degree of Confinement Stability Rating</b>	<b>Mod. Confined</b>
---	----------------------



Worksheet 5-15. Pfankuch channel stability rating.

Stream: Trail Creek, G4 Poor Reach		Location: Pike National Forest, CO			Valley Type: VIII			Observers: B. Kasun et al.			Date: 8/18/2010													
Local- tion	Key Category	Excellent	Good	Fair	Poor	Rating	Rating	Rating	Rating	Description	Rating													
Upper banks	1 Landform slope	Bank slope gradient <30%.	Bank slope gradient 30–40%.	Bank slope gradient 40–60%.	Bank slope gradient > 60%.	2	4	6	6	Bank slope gradient > 60%.	8													
	2 Mass erosion	No evidence of past or future mass erosion.	In frequent. Mostly healed over. Low future potential.	Frequent or large, causing sediment nearly yearlong.	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.	3	6	9	9	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.	12													
	3 Debris jam potential	Essentially absent from immediate channel area.	Present, but mostly small twigs and limbs.	Moderate to heavy amounts, mostly larger sizes.	Moderate to heavy amounts, mostly larger sizes.	2	4	6	6	Moderate to heavy amounts, predominantly larger sizes.	8													
	4 Vegetative bank protection	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	70–90% density. Fewer species or less vigor suggest less dense or deep root mass.	50–70% density. Lower vigor and fewer species from a shallow, discontinuous root mass.	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.	3	6	9	9	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.	12													
Lower banks	5 Channel capacity	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0.	Bankfull stage is contained within banks. Width/depth ratio departure from reference width/depth ratio = 1.0–1.2. Bank-Height Ratio (BHR) = 1.0–1.1.	Bankfull stage is not contained. Width/depth ratio departure from reference width/depth ratio = 1.2–1.4. Bank-Height Ratio (BHR) = 1.1–1.3.	Bankfull stage is not contained; over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.	1	2	3	3	Bankfull stage is not contained; over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.	4													
	6 Bank rock content	> 65% with large angular boulders. 12"+ common.	40–65%. Mostly boulders and small cobbles 6–12".	20–40%. Most in the 3–6" diameter class.	<20% rock fragments of gravel sizes, 1–3" or less.	2	4	6	6	<20% rock fragments of gravel sizes, 1–3" or less.	8													
	7 Obstructions to flow	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	Frequent obstructions and deflectors cause bank erosion yearlong. Sediment traps full, channel migration occurring.	2	4	6	6	Frequent obstructions and deflectors cause bank erosion yearlong. Sediment traps full, channel migration occurring.	8													
	8 Cutting	Little or none. Infrequent raw banks <6".	Some, intermittently at outcrops and constrictions. Raw banks may be up to 12".	Significant. Cuts 12–24" high. Root mat overhangs and sloughing evident.	Almost continuous cuts, some over 24" high. Failure of overhangs frequent.	4	6	12	12	Almost continuous cuts, some over 24" high. Failure of overhangs frequent.	16													
	9 Deposition	Little or no enlargement of channel or point bars.	Some new bar increase, mostly from coarse gravel.	Moderate deposition of new gravel and coarse sand on old and some new bars.	Extensive deposit of predominantly fine particles. Accelerated bar development.	4	8	12	12	Extensive deposit of predominantly fine particles. Accelerated bar development.	16													
Bottom	10 Rock angularity	Sharp edges and corners. Plane surfaces rough.	Rounded corners and edges. Surfaces smooth and flat.	Comers and edges well rounded in 2 dimensions.	Well rounded in all dimensions, surfaces smooth.	1	2	3	3	Well rounded in all dimensions, surfaces smooth.	4													
	11 Brightness	Surfaces dull, dark or stained. Generally not bright.	Mostly dull, but may have <35% bright surfaces.	Mixture dull and bright, i.e., 35–65% mixture range.	Predominantly bright, > 65%, exposed or scoured surfaces.	1	2	3	3	Predominantly bright, > 65%, exposed or scoured surfaces.	4													
	12 Consolidation of particles	Assorted sizes tightly packed or overlapping.	Moderately packed with some overlapping.	Mostly loose assortment with no apparent overlap.	No packing evident. Loose assortment, easily moved.	2	4	6	6	No packing evident. Loose assortment, easily moved.	8													
	13 Bottom size distribution	No size change evident. Stable material 80–100%.	Distribution shift light. Stable material 50–80%.	Moderate change in sizes. Stable materials 20–50%.	Marked distribution change. Stable materials 0–20%.	4	8	12	12	Marked distribution change. Stable materials 0–20%.	16													
	14 Scouring and deposition	<5% of bottom affected by scour or deposition.	5–30% affected. Scour at constrictions and where grades steepen. Some deposition in pools.	30–50% affected. Deposits and scour at obstructions, constrictions and bends. Some filling of pools.	More than 50% of the bottom in a state of flux or change nearly yearlong.	6	12	18	18	More than 50% of the bottom in a state of flux or change nearly yearlong.	24													
	15 Aquatic vegetation	Abundant growth moss-like, dark green perennial. In swift water too.	Common. Algae forms in low velocity and pool areas. Moss here too.	Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick.	Perennial types scarce or absent. Yellow-green, short-term bloom may be present.	1	2	3	3	Perennial types scarce or absent. Yellow-green, short-term bloom may be present.	4													
<b>Excellent total = 1</b>						<b>Good total = 4</b>	<b>Fair total = 21</b>	<b>Poor total = 112</b>																
<b>Stream type</b>	<b>A1</b>	<b>A2</b>	<b>A3</b>	<b>A4</b>	<b>A5</b>	<b>A6</b>	<b>B1</b>	<b>B2</b>	<b>B3</b>	<b>B4</b>	<b>B5</b>	<b>B6</b>	<b>C1</b>	<b>C2</b>	<b>C3</b>	<b>C4</b>	<b>C5</b>	<b>C6</b>	<b>D3</b>	<b>D4</b>	<b>D5</b>	<b>D6</b>	<b>Grand total = 138</b>	
Good (Stable)	38-43	38-43	54-90	60-95	60-95	50-80	38-45	38-45	40-60	40-64	48-68	40-60	38-50	38-50	60-85	70-90	70-90	60-85	85-107	85-107	85-107	85-107	85-107	67-98
Fair (Mod. unstable)	44-47	44-47	91-129	96-132	96-142	81-110	46-58	46-58	69-88	61-78	65-84	61-78	51-61	51-61	86-105	91-110	91-110	86-105	108-132	108-132	108-132	108-132	108-132	99-125
Poor (Unstable)	48+	48+	130+	133+	143+	111+	59+	59+	79+	85+	89+	79+	62+	62+	106+	111+	111+	106+	133+	133+	133+	133+	133+	126+
<b>Stream type</b>	<b>DA3</b>	<b>DA4</b>	<b>DA5</b>	<b>DA6</b>	<b>E3</b>	<b>E4</b>	<b>E5</b>	<b>E6</b>	<b>F1</b>	<b>F2</b>	<b>F3</b>	<b>F4</b>	<b>F5</b>	<b>F6</b>	<b>G1</b>	<b>G2</b>	<b>G3</b>	<b>G4</b>	<b>G5</b>	<b>G6</b>				<b>Grand total = 138</b>
Good (Stable)	40-63	40-63	40-63	40-63	50-75	50-75	50-75	40-63	60-85	61-110	85-110	85-110	90-115	80-95	40-60	40-60	85-107	85-107	90-112	85-107				<b>Existing stream type = G4</b>
Fair (Mod. unstable)	64-86	64-86	64-86	64-86	76-96	76-96	76-96	64-86	86-105	86-105	111-125	111-125	116-130	96-110	61-78	61-78	108-120	108-120	113-125	108-120				<b>*Potential stream type = B4</b>
Poor (Unstable)	87+	87+	87+	87+	97+	97+	97+	87+	106+	106+	126+	126+	131+	111+	79+	79+	121+	121+	126+	121+				<b>Modified channel stability rating = Poor</b>

\*Rating is adjusted to potential stream type, not existing.

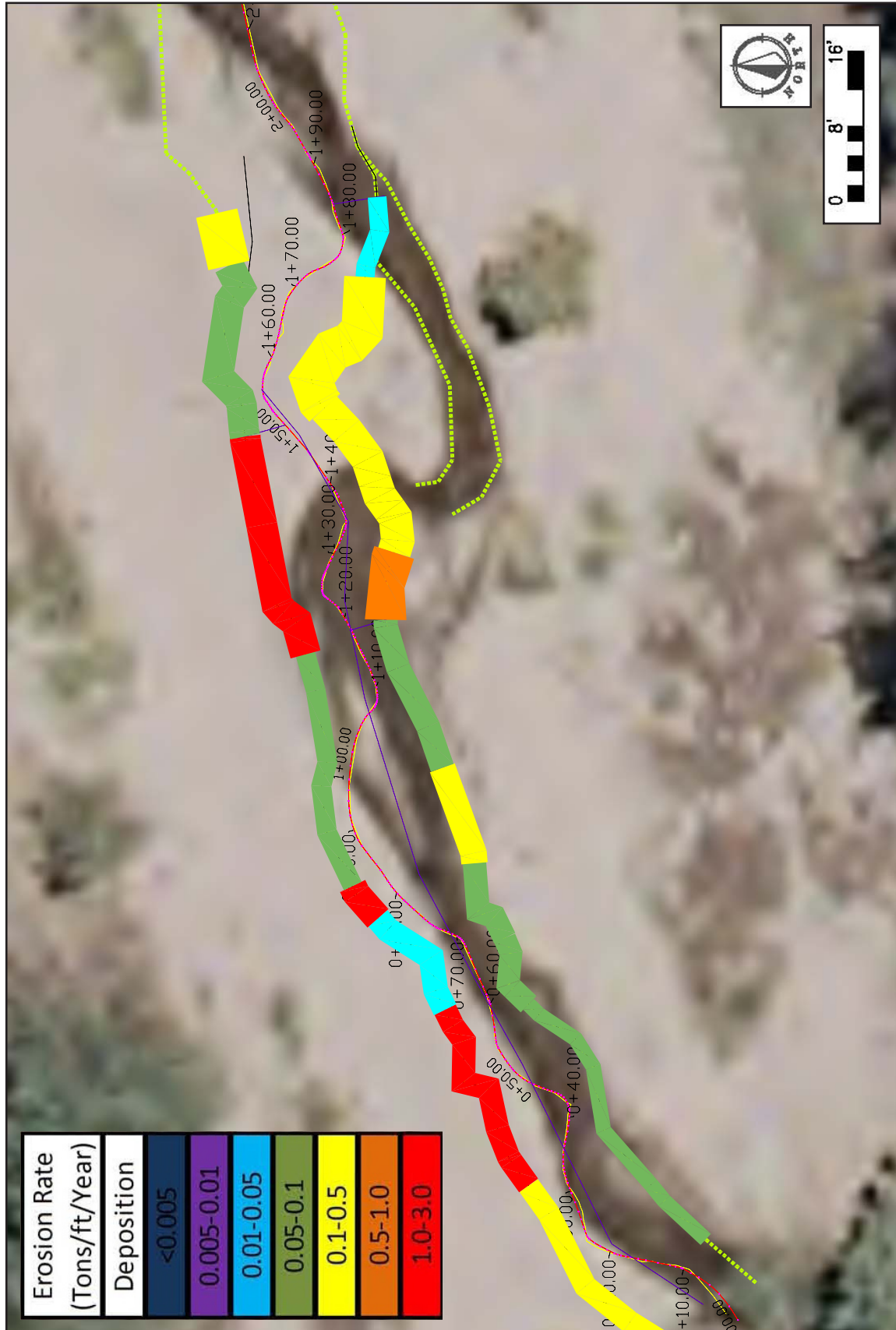
## BANCS Model – Streambank Erosion

**Worksheet 5-18.** Annual streambank erosion estimates.

Stream: <b>Trail Creek, G4 Poor Reach</b>				Location: <b>Pike National Forest, Colorado</b>			
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>184</b>		Date: <b>8/18/2010</b>			
Observers: <b>B. Kasun et al.</b>		Valley Type: <b>VIII</b>		Stream Type: <b>G4</b>			
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 5-16) (adjective)	NBS rating (Worksheet 5-17) (adjective)	Bank erosion rate (Figure 5-34 or 5- 35) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [[ <b>(4)</b> ] <b>×</b> <b>(5)</b> ] <b>×</b> <b>(6)</b> ] (ft <sup>3</sup> /yr)	Erosion Rate (tons/yr/ft) { <b>[(7)/27]</b> <b>×</b> <b>1.3 / (5)</b> }
1. 0+00-57R	High	High	0.57533	57.0	2.0	65.59	0.05540
2. 0+00-34L	Very High	Very High	0.87205	34.0	3.0	88.95	0.12596
3. 0+34-63L	Extreme	Very High	7.02692	29.0	3.1	631.72	1.04883
4. 0+63-80L	Moderate	Low	0.15287	17.0	3.3	8.58	0.02429
5. 0+80-84L	Extreme	Very High	7.02692	4.0	3.7	104.00	1.25183
6. 0+57-67R	Moderate	High	0.42031	10.0	3.0	12.61	0.06071
7. 0+67-78R	Moderate	High	0.42031	11.0	3.1	14.33	0.06273
8. 0+84-118L	Very High	High	0.57533	34.0	2.6	50.86	0.07202
9. 0+78-93R	Extreme	Extreme	2.76027	15.0	3.5	144.91	0.46516
10. 0+93-118R	High	Moderate	0.37957	25.0	3.2	30.37	0.05848
11. 118-150L	Extreme	Very High	7.02692	32.0	4.1	921.93	1.38717
12. 118-131R	Extreme	Extreme	2.76027	13.0	4.5	161.48	0.59806
13. 131-150R	High	Very High	0.87205	19.0	4.4	72.90	0.18475
14. 150-174R	Extreme	Moderate	1.07417	24.0	5.5	141.79	0.28446
15. 150-174L	High	Moderate	0.37957	24.0	4.0	36.44	0.07310
16. 174-184L	Extreme	Low	0.41998	10.0	5.6	23.52	0.11324
17. 174-184R	Very High	Low	0.25042	10.0	2.5	6.26	0.03014
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					Total Erosion (ft <sup>3</sup> /yr)	<b>2516.23</b>	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					Total Erosion (yds <sup>3</sup> /yr)	<b>93.19</b>	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					Total Erosion (tons/yr)	<b>121.15</b>	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					Total Erosion (tons/yr/ft)	<b>0.6584</b>	



### Streambank Erosion Map



## FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Equation Type		Equation Source				Equation		Bankfull Discharge (cfs)			Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)			
1. Bedload Sediment		"Good/Fair" Pagosa				$y = -0.0113 + 1.0139x^{2.1929}$		30.5			0.0182		31.70			
2. Suspended Sediment		"Good/Fair" Pagosa				$y = 0.0636 + 0.9326x^{2.4085}$										
From Dimensional Flow-Duration Curve																
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)		
Percentage of Time	Daily Mean Discharge	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Suspended Sediment Discharge	Suspended Sediment Discharge	Dimensionless Bedload Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow [(5)×(6)]	Suspended Sediment [(5)×(9)]	Bedload Sediment [(5)×(11)]	Suspended Bedload Sediment [(13)+(14)]		
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>bed</sub> )	(S/S <sub>bed</sub> )	(tons/day)	(b <sub>y</sub> /b <sub>bed</sub> )	(tons/day)	(cfs)	(tons)	(tons)	(tons)		
0%	77.6															
0.10%	66.6	0.05%	0.09%	0.34	72.1	2.363	7.461	46.03	6.670	11.59	24.7	15.79	3.98	19.77		
0.25%	57.6	0.08%	0.15%	0.55	62.1	2.036	5.232	27.81	4.809	8.35	34.0	15.22	4.57	19.80		
0.50%	49.8	0.13%	0.25%	0.91	53.7	1.761	3.706	17.04	3.494	6.07	49.0	15.54	5.54	21.08		
0.75%	42.5	0.13%	0.25%	0.91	46.1	1.513	2.592	10.24	2.502	4.35	42.1	9.34	3.97	13.31		
1%	36.8	0.13%	0.25%	0.91	39.6	1.300	1.817	6.17	1.790	3.11	36.2	5.63	2.84	8.46		
1.5%	31.6	0.25%	0.50%	1.83	34.2	1.120	1.289	3.77	1.289	2.24	62.3	6.88	4.09	10.97		
2%	26.3	0.25%	0.50%	1.83	28.9	0.949	0.886	2.19	0.893	1.55	52.8	4.01	2.83	6.84		
3%	22.2	0.50%	1.00%	3.65	24.2	0.795	0.600	1.25	0.602	1.05	88.5	4.55	3.82	8.36		
4%	18.9	0.50%	1.00%	3.65	20.6	0.674	0.424	0.75	0.415	0.72	75.0	2.72	2.63	5.36		
5%	16.9	0.50%	1.00%	3.65	17.9	0.587	0.322	0.49	0.304	0.53	65.4	1.80	1.93	3.73		
10%	10.6	2.50%	5.00%	18.25	13.7	0.450	0.200	0.24	0.165	0.29	250.6	4.29	5.23	9.52		
20%	5.8	5.00%	10.00%	36.50	8.2	0.269	0.103	0.07	0.045	0.08	298.9	2.63	2.88	5.51		
30%	3.9	5.00%	10.00%	36.50	4.8	0.158	0.075	0.03	0.006	0.01	175.8	1.12	0.41	1.53		
40%	2.7	5.00%	10.00%	36.50	3.3	0.108	0.068	0.02	0.000	0.00	120.2	0.70	0.00	0.70		
50%	2.1	5.00%	10.00%	36.50	2.4	0.079	0.066	0.01	0.000	0.00	87.9	0.49	0.00	0.49		
60%	1.6	5.00%	10.00%	36.50	1.8	0.061	0.065	0.01	0.000	0.00	67.4	0.37	0.00	0.37		
70%	1.3	5.00%	10.00%	36.50	1.4	0.047	0.064	0.01	0.000	0.00	52.8	0.29	0.00	0.29		
80%	1.1	5.00%	10.00%	36.50	1.2	0.039	0.064	0.01	0.000	0.00	44.0	0.24	0.00	0.24		
90%	0.8	5.00%	10.00%	36.50	1.0	0.032	0.064	0.01	0.000	0.00	35.2	0.19	0.00	0.19		
100%	0.2	5.00%	10.00%	36.50	0.5	0.016	0.064	0.00	0.000	0.00	17.6	0.10	0.00	0.10		
<b>Annual Totals:</b>											<b>1,680.3</b> (cfs)		<b>91.9</b> (tons/yr)		<b>136.6</b> (tons/yr)	
											<b>3,332.9</b> (acre-ft)					

**Worksheet 19b.** Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Equation Type		Equation Source				Equation		Bankfull Discharge (cfs)			Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)	
		"Poor" Pagosa				$y = 0.07176 + 1.02176x^{2.3772}$		30.5			0.4699		223.46	
		"Poor" Pagosa				$y = 0.0989 + 0.9213x^{3.659}$								
		From Dimensional Flow-Duration Curve				From Sediment Rating Curves				Calculate		Calculate Sediment Yield		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Percentage of Time	Daily Mean Discharge	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Suspended Sediment Discharge $(S/S_{crit})$	Suspended Sediment Discharge	Dimensionless Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow $[(5) \times (6)]$	Suspended Sediment $[(5) \times (9)]$	Bedload Sediment $[(5) \times (11)]$	Suspended + Bedload Sediment $[(13) + (14)]$
(%)	(cfs)	(%)	(%)	(days)	(cfs)	$(Q/Q_{crit})$	$(S/S_{crit})$	(tons/day)	$(b_j/b_{crit})$	(tons/day)	(cfs)	(tons)	(tons)	(tons)
0%	111.2													
0.10%	100.2	0.05%	0.09%	0.34	105.7	3.465	86.989	5546.02	19.669	880.48	36.3	1902.84	302.09	2204.93
0.25%	91.2	0.08%	0.15%	0.55	95.7	3.138	60.560	3496.68	15.555	696.33	52.4	1914.43	381.24	2295.67
0.50%	83.4	0.13%	0.25%	0.91	87.3	2.862	43.307	2281.18	12.519	560.42	79.7	2081.58	511.38	2592.96
0.75%	76.1	0.13%	0.25%	0.91	79.7	2.615	31.126	1497.67	10.110	452.55	72.8	1366.62	412.95	1779.57
1%	70.4	0.13%	0.25%	0.91	73.2	2.401	22.827	1008.77	8.272	370.28	66.8	920.51	337.88	1258.39
1.5%	64.7	0.25%	0.50%	1.83	67.5	2.214	16.983	691.95	6.832	305.82	123.2	1262.80	558.12	1820.92
2%	59.0	0.25%	0.50%	1.83	61.8	2.027	12.331	460.06	5.555	248.65	112.9	839.62	453.79	1293.41
3%	54.8	0.50%	1.00%	3.65	56.9	1.866	9.122	313.18	4.571	204.63	207.7	1143.10	746.90	1890.00
4%	48.9	0.50%	1.00%	3.65	51.9	1.701	6.534	204.51	3.684	164.91	189.4	746.46	601.91	1348.38
5%	43.3	0.50%	1.00%	3.65	46.1	1.511	4.275	118.89	2.799	125.31	168.3	433.96	457.38	891.34
10%	26.9	2.50%	5.00%	18.25	35.1	1.150	1.637	34.66	1.497	67.03	640.4	632.60	1223.33	1855.93
20%	8.6	5.00%	10.00%	36.50	17.8	0.583	0.227	2.43	0.355	15.89	648.9	88.76	579.91	668.67
30%	4.0	5.00%	10.00%	36.50	6.3	0.208	0.102	0.39	0.096	4.30	231.3	14.21	157.08	171.29
40%	2.7	5.00%	10.00%	36.50	3.4	0.111	0.099	0.20	0.077	3.46	123.6	7.40	126.23	133.63
50%	2.1	5.00%	10.00%	36.50	2.4	0.079	0.099	0.14	0.074	3.32	87.9	5.25	121.25	126.50
60%	1.6	5.00%	10.00%	36.50	1.8	0.061	0.099	0.11	0.073	3.27	67.4	4.02	119.37	123.40
70%	1.3	5.00%	10.00%	36.50	1.4	0.047	0.099	0.09	0.072	3.24	52.8	3.15	118.44	121.58
80%	1.1	5.00%	10.00%	36.50	1.2	0.039	0.099	0.07	0.072	3.23	44.0	2.62	118.02	120.64
90%	0.8	5.00%	10.00%	36.50	1.0	0.032	0.099	0.06	0.072	3.22	35.2	2.10	117.70	119.80
100%	0.2	5.00%	10.00%	36.50	0.5	0.016	0.099	0.03	0.072	3.21	17.6	1.05	117.34	118.39
<b>Annual Totals:</b>											3,058.2	13,373	7,562	20,935
											(cfs)	(tons/yr)	(tons/yr)	(tons/yr)
											6,066.0			
											(acre-ft)			

# POWERSED Model – Sediment Transport Capacity

**Worksheet 20a.** Sediment transport prediction representing the upstream supply up to bankfull for bedload and suspended sand sediment.

Stream: Trail Creek, Upstream Existing Sediment Supply		Location: Pike National Forest, Colorado (Used "POOR" Curves)		Valley Type: VIII		Stream Type: G4		Gage Station #: Used Post-Fire Dimensionless F-D C.		Date: 08/14/10								
Observers: S=0258, Q=31, 24.25, Bed.=1.0337, S.Sands=111.73		Hydraulic geometry		Measure		Calculate												
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	
Percentage of time	Daily mean discharge	Mil-ordinate stream-flow	Area	Width	Depth	Velocity	Slope	Shear stress	Stream power	Unit power	Time increment	Time increment	Daily mean bedload transport	Daily mean suspended sand transport	Time adjusted bedload transport	Time adjusted suspended sand transport	Time adjusted total transport	
(%)	(cfs)	(cfs)	(ft <sup>2</sup> )	(ft)	(ft)	(ft/s)	(ft/ft)	(lb/ft <sup>2</sup> )	(lb/s)	(lb/ft/s)	(%)	(days)	(tons/day)	(tons/day)	[(13)x(14)]	[(13)x(15)]	[(16)+(17)]	
100.00%	0.16										0%			0.00	0.00	0.00	0.00	
90.00%	0.80	0.48	0.38	4.37	0.09	1.08	0.0258	0.14	0.77	0.18	10%	36.50	3.20	0.01	116.80	0.36	117.16	
80.00%	1.12	0.96	0.64	5.09	0.13	1.44	0.0258	0.20	1.55	0.30	10%	36.50	3.20	0.03	116.80	1.09	117.89	
70.00%	1.28	1.20	0.75	5.32	0.14	1.56	0.0258	0.23	1.93	0.36	10%	36.50	3.24	0.04	118.26	1.46	119.72	
60.00%	1.61	1.45	0.84	5.45	0.15	1.65	0.0258	0.25	2.33	0.43	10%	36.50	3.24	0.04	118.26	1.46	119.72	
50.00%	2.09	1.85	0.99	5.67	0.17	1.79	0.0258	0.28	2.98	0.53	10%	36.50	3.24	0.06	118.26	2.19	120.45	
40.00%	2.73	2.41	1.20	5.98	0.20	1.98	0.0258	0.32	3.88	0.65	10%	36.50	3.33	0.07	121.55	2.56	124.11	
30.00%	4.04	3.39	1.50	6.27	0.24	2.21	0.0258	0.38	5.46	0.87	10%	36.50	3.46	0.10	126.29	3.65	129.94	
20.00%	8.63	6.34	2.28	6.90	0.33	2.75	0.0258	0.52	10.21	1.48	10%	36.50	4.23	0.19	154.40	6.94	161.34	
10.00%	26.93	17.78	4.60	8.30	0.55	3.85	0.0258	0.87	28.62	3.45	10%	36.50	15.38	1.18	561.37	43.07	604.44	
5.00%	43.25	35.09	9.48	18.37	0.52	3.69	0.0258	0.81	56.49	3.08	5%	18.25	64.45	16.40	1176.21	299.30	1475.51	
4.00%	48.95	46.10																
3.00%	54.82	51.89																
2.00%	58.99	56.91																
1.50%	64.69	61.84																
1.00%	70.38	67.54																
0.75%	76.12	73.25																
0.50%	83.39	79.76																
0.25%	91.23	87.31																
0.10%	100.18	95.71																
0.0060%	111.17	105.68																
														Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr):		2728.2	362.1	3090.3

**Worksheet 20b.** Sediment transport prediction for the existing condition reach compared to the upstream sediment supply to assess bed stability.

Stream: Trail Creek, G4 Poor, Riffle XS3 0+62																	
Location: Pike National Forest, Colorado (Used "POOR" Curves)																	
Date: 08/14/10																	
Observers: S=0.258, Q=31, 24.25, Bed=1.0337, S.Sand=111.73																	
Gage Station #: Used Post-Fire Dimensionless F-D C.																	
Valley Type: VIII																	
Stream Type: G4																	
Calculate																	
Flow-duration curve			Calculate			Hydraulic geometry			Measure			Calculate					
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
Percentage of time	Daily mean discharge	Mid-ordinate stream-flow	Area	Width	Depth	Velocity	Slope	Shear stress	Stream power	Unit power	Time increment	Time increment	Daily mean bedload transport	Daily mean suspended sand transport	Time adjusted bedload transport [(13)x(14)]	Time adjusted suspended sand transport [(13)x(15)]	Time adjusted total transport [(16)+[17]]
(%)	(cfs)	(cfs)	(ft <sup>2</sup> )	(ft)	(ft)	(ft/s)	(ft/ft)	(lb/ft <sup>2</sup> )	(lb/s)	(lb/ft/s)	(%)	(days)	(tons/day)	(tons/day)	(tons)	(tons)	(tons)
100.00%	0.16										0%			0.00	0.00	0.00	0.00
90.00%	0.80	0.48	0.42	4.40	0.10	1.03	0.0258	0.15	0.77	0.17	10%	36.50	0.00	0.01	0.00	0.36	0.36
80.00%	1.12	0.96	0.70	5.25	0.13	1.29	0.0258	0.21	1.55	0.30	10%	36.50	3.20	0.03	116.80	1.09	117.89
70.00%	1.28	1.20	0.83	5.68	0.15	1.42	0.0258	0.23	1.93	0.34	10%	36.50	3.24	0.04	118.26	1.46	119.72
60.00%	1.61	1.45	0.93	5.78	0.16	1.51	0.0258	0.25	2.33	0.40	10%	36.50	3.24	0.04	118.26	1.46	119.72
50.00%	2.09	1.85	1.08	5.82	0.19	1.65	0.0258	0.29	2.98	0.51	10%	36.50	3.24	0.06	118.26	2.19	120.45
40.00%	2.73	2.41	1.28	5.87	0.22	1.83	0.0258	0.34	3.88	0.66	10%	36.50	3.33	0.07	121.55	2.56	124.11
30.00%	4.04	3.39	1.59	5.94	0.27	2.10	0.0258	0.42	5.46	0.92	10%	36.50	3.50	0.10	127.75	3.65	131.40
20.00%	8.63	6.34	2.37	6.07	0.39	2.65	0.0258	0.59	10.21	1.68	10%	36.50	5.36	0.22	195.64	8.03	203.67
10.00%	26.93	17.78	4.62	6.29	0.73	3.84	0.0258	1.03	28.62	4.55	10%	36.50	164.98	35.31	6021.77	1288.82	7310.59
5.00%	43.25	35.09	7.27	6.47	1.12	4.82	0.0258	1.44	56.49	8.73	5%	18.25	366.55	332.90	6689.54	6075.42	12764.96
4.00%	48.95	46.10															
3.00%	54.82	51.89															
2.00%	58.99	56.91															
1.50%	64.69	61.84															
1.00%	70.38	67.54															
0.75%	76.12	73.25															
0.50%	83.39	79.76															
0.25%	91.23	87.31															
0.10%	100.18	95.71															
0.0060%	111.17	105.68															
Notes:																	
Total annual sediment yield (bedload and suspended sand bed-material load) (tons/yr): 13627.8																	
Upstream total annual sediment supply (tons/yr) (Worksheet 5-20a): 2728.2																	
Difference in sediment transport capacity (tons/yr) (+ or - ): 10899.6																	
Stability evaluation: Aggradation, Degradation or Stable: Degradation, ≈ 72% Increase in Transport																	

## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>Trail Creek, G4 Poor Reach</b>		Stream Type: <b>G4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>B. Kasun et al.</b>		Date: <b>8/18/2010</b>			
<b>Enter Required Information for Existing Condition</b>					
8.0	$D_{50}$	Riffle bed material $D_{50}$ (mm)			
6.0	$D_{50}^{\wedge}$	Bar sample $D_{50}$ (mm)			
0.26	$D_{max}$	Largest particle from bar sample (ft)	80	(mm)	304.8 mm/ft
0.0258	S	Existing bankfull water surface slope (ft/ft)			
0.89	d	Existing bankfull mean depth (ft)			
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment			
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>					
1.33	$D_{50}/D_{50}^{\wedge}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 ( D_{50}/D_{50}^{\wedge} )^{-0.872}$		
10.00	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 ( D_{max}/D_{50} )^{-0.887}$		
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED:		
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	d	Required bankfull mean depth (ft)	$d = \frac{\tau^*(\gamma_s - 1)D_{max}}{S}$ (use $D_{max}$ in ft)		
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	S	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^*(\gamma_s - 1)D_{max}}{d}$ (use $D_{max}$ in ft)		
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input checked="" type="checkbox"/> Degrading					
<b>Sediment Competence Using Dimensional Shear Stress</b>					
1.433	Bankfull shear stress $\tau = \gamma ds$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d ) $\gamma = 62.4$ , d = existing depth, S = existing slope				
Shields 99	CO 190	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ (Figure 5-49)			
Shields 1.01	CO 0.4	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) (Figure 5-49)			
Shields 0.63	CO 0.25	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm)		$d = \frac{\tau}{\gamma S}$	
Shields 0.0182	CO 0.0072	Predicted slope required to initiate movement of measured $D_{max}$ (mm)		$S = \frac{\tau}{\gamma d}$	
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input checked="" type="checkbox"/> Degrading					

## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>Trail Creek, G4 Poor Reach</b>	Stream Type: <b>G4</b>
Location: <b>Pike National Forest, CO</b>	Valley Type: <b>VIII</b>
Observers: <b>B. Kasun et al.</b>	Date: <b>8/18/2010</b>
<b>Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)</b>	<b>Stability Rating (Check Appropriate Rating)</b>
Stream Type at potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	<input type="checkbox"/> Stable
(E→C), (C→High W/d C)	<input type="checkbox"/> Moderately Unstable
(G→F), (F→D), (C→F)	<input type="checkbox"/> Unstable
(C→D), (B→G), (D→G), (C→G), (E→G)	<input checked="" type="checkbox"/> Highly Unstable

**Worksheet 5-25.** Lateral stability.

Stream: <b>Trail Creek, G4 Poor Reach</b>		Stream Type: <b>G4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>B. Kasun et al.</b>		Date: <b>8/18/2010</b>			
Lateral stability criteria (choose one stability category for each criterion 1-5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	2
	(2)	(4)	(6)	(8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	4
	(1)	(2)	(3)	B6, B7 (4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		1
	M3, M4 (1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	8
	(2)	(4)	(6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	2
	(1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>17</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input type="checkbox"/>	<i>Unstable</i> 13 – 21 <input checked="" type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	



**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>Trail Creek, G4 Poor Reach</b>		Stream Type: <b>G4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>B. Kasun et al.</b>		Date: <b>8/18/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
1 <b>Sediment competence</b> (Worksheet 5-22)	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope—slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	2
	(2)	(4)	(6)	(8)	
2 <b>Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	2
	(2)	(4)	(6)	(8)	
3 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	2
	(2)	(4)	(6)	(8)	
4 <b>Stream Succession States</b> (Worksheet 5-24)	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	2
	(2)	(4)	(6)	(8)	
5 <b>Depositional Patterns</b> (Worksheet 5-10)	B1	B2, B4	B3, B5	B6, B7, B8	4
	(1)	(2)	(3)	B6, B7 (4)	
6 <b>Debris / Blockages</b> (Worksheet 5-11)	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	1
	D3 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>13</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
Vertical Stability for Excess Deposition / Aggradation (use total points and check stability rating)	<i>No Deposition</i> 10 – 14 <input checked="" type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input type="checkbox"/>	<i>Aggradation</i> > 30 <input type="checkbox"/>	

**Worksheet 5-27.** Vertical stability – degradation.

Stream: <b>Trail Creek, G4 Poor Reach</b>		Stream Type: <b>G4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>B. Kasun et al.</b>		Date: <b>8/18/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>1 Sediment Competence</b> (Worksheet 5-22)	Does not indicate excess competence  (2)	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed  (4)	$D_{100}$ of bed moved  (6)	Particles much larger than $D_{100}$ of bed moved  (8)	8
<b>2 Sediment Capacity</b> (POWERSED) (Worksheet 5-20)	Does not indicate excess capacity  (2)	Slight excess energy: up to 10% increase above reference  (4)	Excess energy sufficient to increase load up to 50% of annual load  (6)	Excess energy transporting more than 50% of annual load  (8)	8
<b>3 Degree of Channel Incision (BHR)</b> (Worksheet 5-12)	1.00 – 1.10  (2)	1.11 – 1.30  (4)	1.31 – 1.50  (6)	$> 1.50$  (8)	8
<b>4 Stream Succession States</b> (Worksheets 5-12 and 5-24)	Does not indicate incision or degradation  (2)	If BHR $> 1.1$ and stream type has W/d between 5–10  (4)	If BHR $> 1.1$ and stream type has W/d less than 5  (6)	(B→G), (C→G), (E→G), (D→G)  (8)	8
<b>5 Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.80 – 1.00  (1)	0.30 – 0.79  (2)	0.10 – 0.29  (3)	$< 0.10$  (4)	2
<b>Total Points</b>					<b>34</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation</b> (use total points and check stability rating)	<i>Not Incised</i> 9 – 11 <input type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input type="checkbox"/>	<i>Degradation</i> $> 27$ <input checked="" type="checkbox"/>	

Worksheet 5-28. Channel enlargement.

Stream: <b>Trail Creek, G4 Poor Reach</b>		Stream Type: <b>G4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>B. Kasun et al.</b>		Date: <b>8/18/2010</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1-4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	8
	(2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	6
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	2
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	8
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>24</b>
<b>Category Point Range</b>					
<b>Channel Enlargement Prediction (use total points and check stability rating)</b>	<i>No Increase</i> 8 – 10 <input type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input type="checkbox"/>	<i>Extensive</i> > 24 <input checked="" type="checkbox"/>	

Worksheet 5-29. Overall sediment supply.

Stream: <b>Trail Creek, G4 Poor Reach</b>		Stream Type: <b>G4</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>		
Observers: <b>B. Kasun et al.</b>		Date: <b>8/18/2010</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1–5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	3	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	1	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	4	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	4	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	4	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>16</b>	
<b>Category Point Range</b>				
Overall Sediment Supply Rating (use total points and check stability rating)	<b>Low</b> 5 <input type="checkbox"/>	<b>Moderate</b> 6 – 10 <input type="checkbox"/>	<b>High</b> 11 – 15 <input type="checkbox"/>	<b>Very High</b> > 15 <input checked="" type="checkbox"/>

Worksheet 5-32. Summary of stability condition categories.

Stream: <b>Trail Creek, G4 Poor Reach</b>		Location: <b>Pike National Forest, Colorado</b>	
Observers: <b>B. Kasun et al.</b>		Date: <b>8/18/2010</b>	Stream Type: <b>G4</b> Valley Type: <b>VIII</b>
Channel Dimension (Rifle XS 2+31)	Mean Bankfull Depth (ft): <b>0.89</b>	Bankfull Width (ft): <b>9.75</b>	Cross-Sectional Area (ft <sup>2</sup> ): <b>8.68</b>
	Width of Flood-Prone Area (ft): <b>12.35</b>	Entrenchment Ratio: <b>1.27</b>	
Channel Pattern	Mean: $\lambda/W_{bkt}$ : <b>N/A</b>	$R_c/W_{bkt}$ : <b>N/A</b>	MWR: <b>1.82</b>
	Range: $\lambda/W_{bkt}$ : <b>N/A</b>	$R_c/W_{bkt}$ : <b>N/A</b>	Sinuosity: <b>1.05</b>
River Profile & Bed Features	Check: <input type="checkbox"/> Riffle/Pool <input checked="" type="checkbox"/> Step/Pool <input type="checkbox"/> Plane Bed <input type="checkbox"/> Convergence/Divergence <input type="checkbox"/> Dunes/Antidunes/Smooth Bed		
	Max Bankfull Depth (ft): <b>1.29</b>	Riffle Pool: <b>1.32</b>	Pool-to-Ratio: <b>2.03</b>
Level III Stream Stability Indices	Riparian Vegetation: <b>Willow 100% 2 B.leaf Sp.</b>	Potential Composition/Density: <b>Salix, Alder/100%</b>	Remarks: Condition, Vigor & Usage of Existing Reach: <b>Sprouts w/good vigor</b>
	Flow Regime: <b>P1, P2, P8 &amp; Order: S-3(4)</b>	Meander Patterns: <b>M3, M4</b>	Depositional Patterns: <b>B6, B7</b> Channel Blockages: <b>D3</b>
Bank Erosion Summary	Degree of Incision (Bank-Height Ratio): <b>1.7</b>	Degree of Incision Stability Rating: <b>Deeply Incised</b>	Modified Pfankuch Stability Rating: <b>138 (Poor)</b>
	Width/depth Ratio (W/d): <b>6.02</b>	Reference W/d Ratio (W/d <sub>ref</sub> ): <b>12.6</b>	W/d Ratio State Stability Rating: <b>Unstable</b>
Sediment Capacity (POWERSED)	Meander Width Ratio (MWR): <b>1.82</b>	Reference MWR <sub>ref</sub> : <b>3.7</b>	MWR / MWR <sub>ref</sub> Stability Rating: <b>Moderately Confined</b>
	Length of Reach Studied (ft): <b>184</b>	Annual Streambank Erosion Rate: <b>121.15</b> (tons/yr)	Curve Used: <b>Colorado</b> Remarks: <b>Fire effects</b>
Entrainment/Competence	<input type="checkbox"/> Sufficient Capacity <input type="checkbox"/> Insufficient Capacity <input checked="" type="checkbox"/> Excess Capacity	Remarks: <b>Transitioning from F to G to B potential</b>	
	Largest Particle from Bar Sample (mm): <b>80</b>	$\tau = 1.769$	$\tau^* = N/A$
Successional Stage Shift	<b>C</b> → <b>D</b> → <b>G</b> → <b>F</b> → <b>G</b> → <b>B4</b>	Existing Depth: <b>0.89</b>	Required Depth: <b>0.63</b>
	<input type="checkbox"/> Stable <input type="checkbox"/> Mod. Unstable <input checked="" type="checkbox"/> Unstable	Existing Stream State (Type): <b>B4</b>	Required Stream State (Type): <b>G4</b>
Vertical Stability (Aggradation)	<input type="checkbox"/> No Deposition <input type="checkbox"/> Mod. Deposition <input type="checkbox"/> Ex. Deposition <input type="checkbox"/> Aggradation	Remarks/causes: <b>little veg recovery, very erosive soils</b>	
	<input type="checkbox"/> Not Incised <input type="checkbox"/> Slightly Incised <input type="checkbox"/> Mod. Incised <input checked="" type="checkbox"/> Degradation	Remarks/causes: <b>little veg recovery, very erosive soils</b>	
Channel Enlargement	<input type="checkbox"/> No Increase <input type="checkbox"/> Slight Increase <input type="checkbox"/> Mod. Increase <input checked="" type="checkbox"/> Extensive	Remarks/causes: <b>little veg recovery, very erosive soils</b>	
	<input type="checkbox"/> Low <input type="checkbox"/> Moderate <input type="checkbox"/> High <input checked="" type="checkbox"/> Very High	Remarks/causes: <b>little veg recovery, very erosive soils</b>	



## *Appendix C16*

# **A4a+ Stream Type** *Reference Reach*





# Table of Contents

## *Appendix C16: A4a+ Reference Reach*

<b>Reach Location &amp; Overview.....</b>	<b>C16-2</b>
<b>Survey Summary.....</b>	<b>C16-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C16-6</b>
<b><i>Velocity, Classification &amp; Morphological Relations.....</i></b>	<b>C16-6</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b><i>Stability Indices.....</i></b>	<b>C16-10</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b><i>BANCS Model – Streambank Erosion.....</i></b>	<b>C16-20</b>
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b><i>FLOWSED Model – Total Annual Sediment Yield.....</i></b>	<b>C16-22</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b><i>Sediment Competence/Entrainment.....</i></b>	<b>C16-24</b>
Worksheet 5-22. Sediment competence calculations.	
<b><i>Channel Stability Ratings.....</i></b>	<b>C16-25</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b><i>Summary.....</i></b>	<b>C16-31</b>
Worksheet 5-32. Summary of stability condition categories.	

## A4a+ Reference Reach Location & Overview

The A4a+ reference reach is in a Valley Type I and is typical of a channel comprising of gravel-cobble and sand materials. The channel bed and banks are potentially erodible, but due to the vegetation condition, this reference reach shows little sediment yield from this 1<sup>st</sup> order channel. Bed features are generally dominated by step/pool and cascades. The channel is ephemeral and is associated with a stable bed and banks and a high sediment transport capacity. There is little sediment storage and very low to negligible streambank erosion.

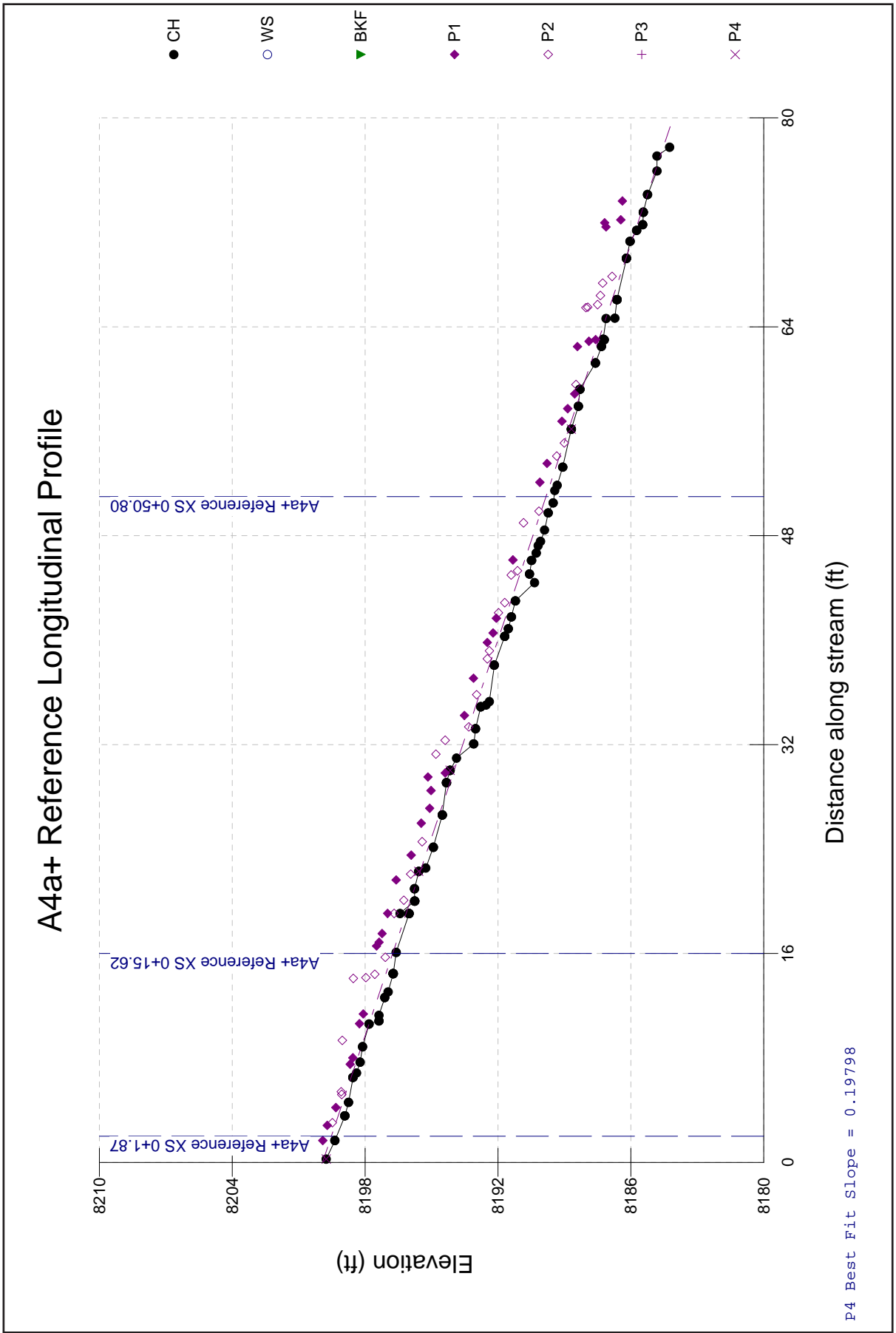
Typical of A4a+ stream types, the channel is entrenched and has a low width/depth ratio with a relatively straight pattern with a sinuosity less than 1.1. The channel is also laterally contained or confined (meander width ratio around 2 or less). Little channel source sediment is generated from this stream type during high runoff events due to the good riparian vegetation. The predicted streambank erosion rate of *0.0017 tons/yr/ft* represents a geologic, yet acceptable rate of erosion for these soil and stream types (**Worksheet 5-18**).

The location of this reach is shown in **Figure C-2**, and the photograph depicts the stable characteristics of this stream type. Although the fire burned the riparian, aspen and perennial bunch grasses are colonizing the site. There is little to no evidence of active channel-source sediment from this stream type. Such stream types are mapped where they occur by sub-watershed as shown in **Appendix D**.

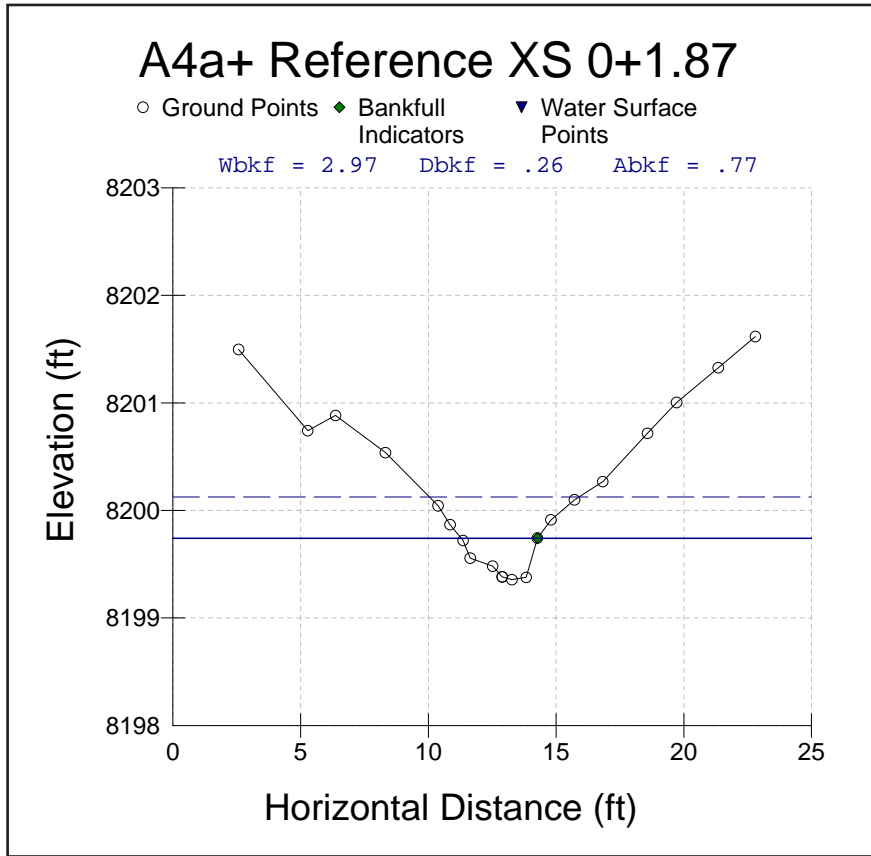
The details of the dimension, pattern, profile and materials are summarized. The POWERSED model was not run on this reference reach as the bed is obviously stable. The following summary worksheets provide the detail of the morphology, hydraulics, stability, and streambank erosion rates for this reference reach. In the situation where impaired A4a+ stream types are located, an alternative for mitigation and sediment reduction is to use the data from the stable form to extrapolate for potential implementation of natural channel design.



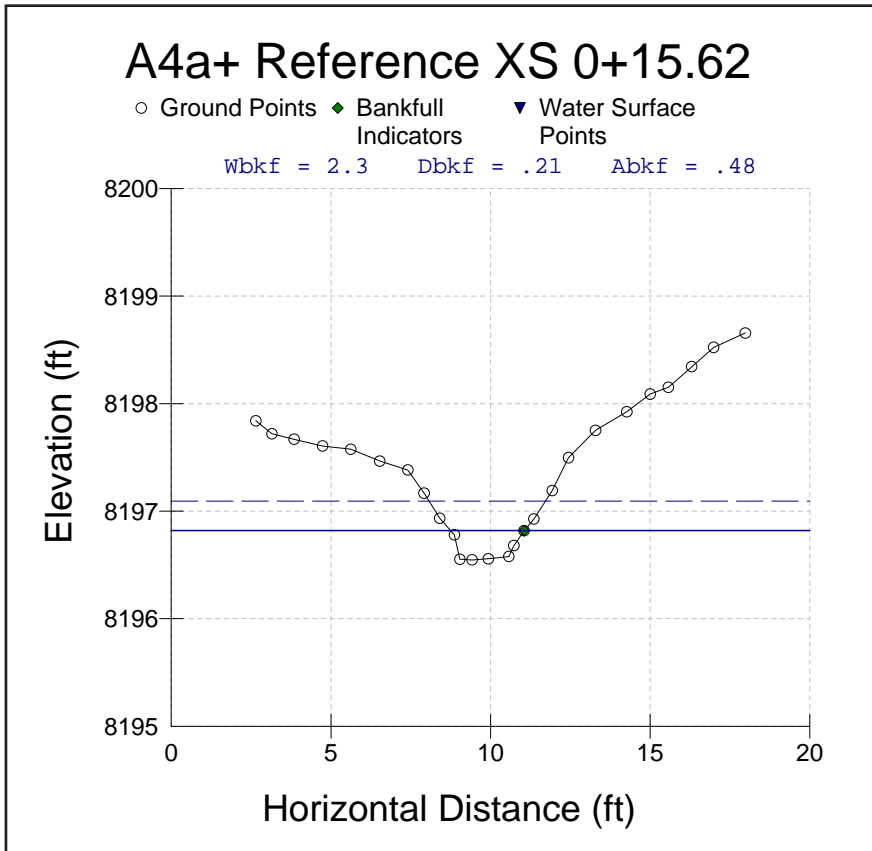
# Survey Summary



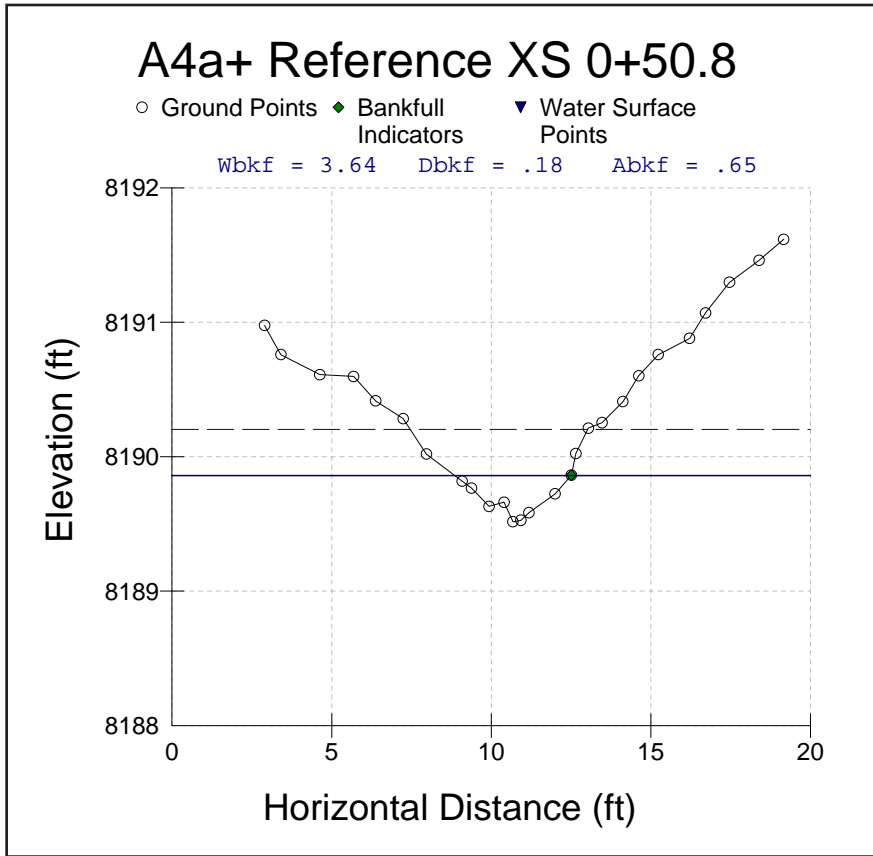
Longitudinal Profile (graph generated from RIVERMorph™)



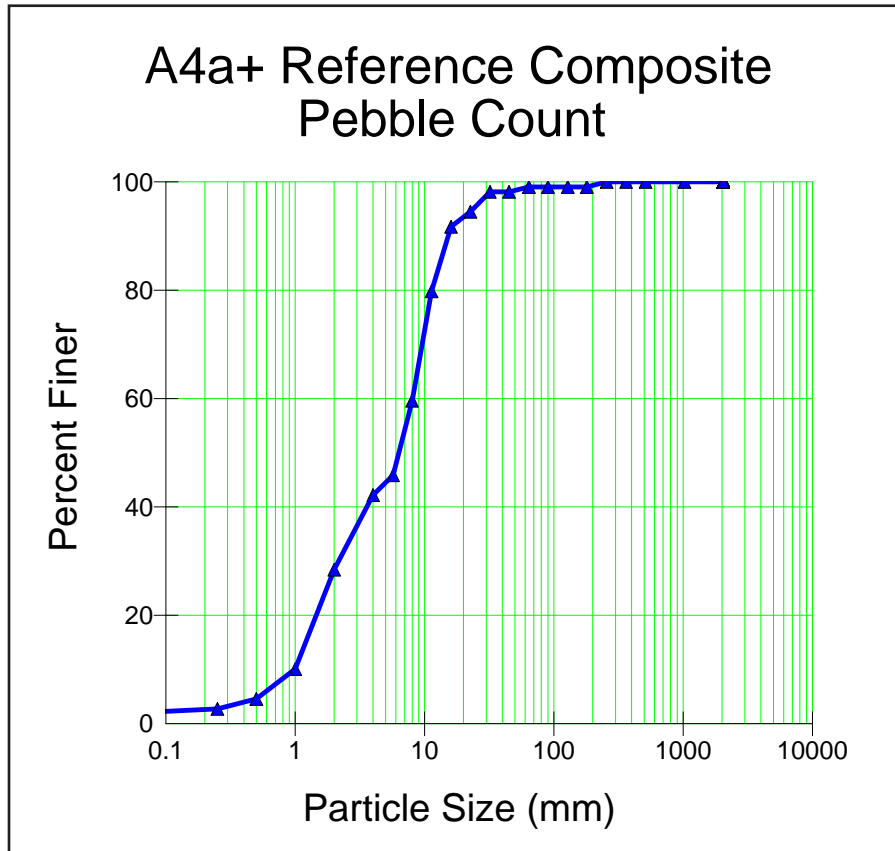
Cross-section 0+1.87 (graph generated from RIVERMorph™)



Representative Cross-section 0+15.62 (graph generated from RIVERMorph™)



**Cross-section 0+50.8** (graph generated from RIVERMorph™)



**Composite Pebble Count** (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates					
Stream:	Trail Creek, A4a+ Reference		Location:	XS 0+15.62, Pike N.F., Colorado	
Date:	9/3/2010	Stream Type:	A4a+	Valley Type:	I
Observers:	Chavez, Kasun & Gallagher		HUC:	___ ___ ___ ___ ___ ___ ___ ___ ___	
INPUT VARIABLES			OUTPUT VARIABLES		
Bankfull Riffle Cross-Sectional AREA	0.48	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.21	$d_{bkf}$ (ft)
Bankfull Riffle WIDTH	2.30	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim (2 * d_{bkf}) + W_{bkf}$	2.72	$W_p$ (ft)
$D_{84}$ at Riffle	13.0	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.04	$D_{84}$ (ft)
Bankfull SLOPE	0.198	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	0.18	R (ft)
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness $R(ft) / D_{84}(ft)$	4.16	$R / D_{84}$
Drainage Area	0.002	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	1.061	$u^*$ (ft/sec)
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$			6.72	ft / sec	3.23 cfs
2. Roughness Coefficient: a) Manning's n from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.0285$			7.32	ft / sec	3.52 cfs
2. Roughness Coefficient: b) Manning's n from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n =$ <input type="text"/>				ft / sec	cfs
2. Roughness Coefficient: c) Manning's n from Jarrett (USGS): $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for Stream Types A1, A2, A3, B1, B2, B3, C2 & E3 $n = 0.278$			0.75	ft / sec	0.36 cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) <input type="text"/>				ft / sec	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) <input type="text"/>				ft / sec	cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q =$ <input type="text"/> year $u = Q / A$				ft / sec	cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$				ft / sec	cfs
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation ( $R/D_{84}$ ) – Estimation Method 1					
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.					
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.					
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.					
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.					

**Worksheet 5-3.** Level II stream classification.

Stream: <b>Trail Creek, A4a+ Reference Reach</b>	
Basin:	Drainage Area: acres <b>0.002</b> mi <sup>2</sup>
Location: <b>Pike National Forest, Colorado</b>	
Twp.&Rge:	Sec.&Qtr.:
Cross-Section Monuments (Lat./Long.): <b>XS 0+15.62</b> Date: <b>09/03/10</b>	
Observers: <b>Chavez, Kasun &amp; Gallagher</b> Valley Type: <b>I</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>2.30</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>0.21</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>0.48</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>10.95</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>0.27</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>3.65</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>1.59</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>6.39</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.198</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>1.11</b>	

<div style="border: 1px solid black; padding: 5px; display: inline-block;">Stream Type</div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: #e0f0ff;"><b>A4a+</b></div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;">(See Figure 2-14)</div>
--	---	--

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, A4a+ Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>								
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/3/2010</b>		Valley Type: <b>I</b>		Stream Type: <b>A4a+</b>				
<b>River Reach Dimension Summary Data.....1</b>										
<b>Riffle Dimensions*</b> , **, ***	<b>Riffle Dimensions*</b> , **, ***		<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Width ( $W_{bkt}$ )		<b>3.0</b>	<b>2.3</b>	<b>3.6</b>	ft	Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	<b>0.6</b>	<b>0.5</b>	<b>0.8</b>
	Mean Riffle Depth ( $d_{bkt}$ )		<b>0.22</b>	<b>0.18</b>	<b>0.26</b>	ft	Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	<b>11.19</b>	<b>10.95</b>	<b>11.42</b>
	Maximum Riffle Depth ( $d_{max}$ )		<b>0.33</b>	<b>0.27</b>	<b>0.39</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>1.558</b>	<b>1.286</b>	<b>1.889</b>
	Width of Flood-Prone Area ( $W_{fpa}$ )		<b>5.0</b>	<b>3.7</b>	<b>5.9</b>	ft	Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )	<b>1.55</b>	<b>1.53</b>	<b>1.6</b>
	Riffle Inner Berm Width ( $W_{ib}$ )					ft	Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )			
	Riffle Inner Berm Depth ( $d_{ib}$ )					ft	Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )			
	Riffle Inner Berm Area ( $A_{ib}$ )					ft <sup>2</sup>	Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )			
	Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )									
<b>Pool Dimensions*</b> , **, ***	<b>Pool Dimensions*</b> , **, ***		<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Pool Dimensions &amp; Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Pool Width ( $W_{bkfp}$ )					ft	Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )			
	Mean Pool Depth ( $d_{bkfp}$ )					ft	Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )			
	Pool Cross-Sectional Area ( $A_{bkfp}$ )					ft	Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )			
	Maximum Pool Depth ( $d_{maxp}$ )					ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )			
	Pool Inner Berm Width ( $W_{ibp}$ )					ft	Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )			
	Pool Inner Berm Depth ( $d_{ibp}$ )					ft	Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )			
	Pool Inner Berm Area ( $A_{ibp}$ )					ft <sup>2</sup>	Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )			
	Point Bar Slope ( $S_{pb}$ )					ft/ft	Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )			
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Run Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Run Width ( $W_{bkfr}$ )					ft	Run Width to Riffle Width ( $W_{bkfr} / W_{bkt}$ )			
	Mean Run Depth ( $d_{bkfr}$ )					ft	Mean Run Depth to Mean Riffle Depth ( $d_{bkfr} / d_{bkt}$ )			
	Run Cross-Sectional Area ( $A_{bkfr}$ )					ft	Run Area to Riffle Area ( $A_{bkfr} / A_{bkt}$ )			
	Maximum Run Depth ( $d_{maxr}$ )					ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )			
	Run Width/Depth Ratio ( $W_{bkfr} / d_{bkfr}$ )					ft				
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Glide Dimensions &amp; Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Glide Width ( $W_{bkfg}$ )					ft	Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )			
	Mean Glide Depth ( $d_{bkfg}$ )					ft	Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )			
	Glide Cross-Sectional Area ( $A_{bkfg}$ )					ft	Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )			
	Maximum Glide Depth ( $d_{maxg}$ )					ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )			
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )					ft/ft	Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )			
	Glide Inner Berm Width ( $W_{ibg}$ )					ft	Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )			
	Glide Inner Berm Depth ( $d_{ibg}$ )					ft	Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )			
	Glide Inner Berm Area ( $A_{ibg}$ )					ft <sup>2</sup>	Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )			
<b>Step*</b>	<b>Step Dimensions**</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Step Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Step Width ( $W_{bkfs}$ )					ft	Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )			
	Mean Step Depth ( $d_{bkfs}$ )					ft	Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )			
	Step Cross-Sectional Area ( $A_{bkfs}$ )					ft	Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )			
	Maximum Step Depth ( $d_{maxs}$ )					ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
	Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )									



**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, A4a+ Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>							
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/3/2010</b>		Valley Type: <b>I</b>		Stream Type: <b>A4a+</b>			
<b>River Reach Summary Data.....2</b>									
<b>Hydraulics</b>	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )		<b>0.75</b>	ft/sec	Estimation Method		<b>Manning's n from Jarrett</b>		
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )		<b>0.36</b>	cfs	Drainage Area		<b>0.002</b> mi <sup>2</sup>		
<b>Channel Pattern</b>	<b>Geometry</b>			<b>Dimensionless Geometry Ratios</b>					
	Linear Wavelength ( $\lambda$ )	Mean	Min	Max	ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )	Mean		
	Stream Meander Length ( $L_m$ )				ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )	Min		
	Radius of Curvature ( $R_c$ )				ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )	Max		
	Belt Width ( $W_{bit}$ )	<b>4.5</b>			ft	Meander Width Ratio ( $W_{bit} / W_{bkt}$ )	<b>1.52</b>		
	Arc Length ( $L_a$ )				ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )			
	Riffle Length ( $L_r$ )				ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )			
	Individual Pool Length ( $L_p$ )				ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )			
Pool to Pool Spacing ( $P_s$ )				ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )				
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )	<b>0.220</b>	ft/ft	Average Water Surface Slope (S)	<b>0.198</b>	ft/ft	Sinuosity ( $S_{val} / S$ )	<b>1.11</b>	
	Stream Length (SL)		ft	Valley Length (VL)		ft	Sinuosity (SL / VL)		
	Low Bank Height (LBH)	start: _____ ft end: _____ ft		Max Bankfull Depth ( $d_{max}$ )	start: _____ ft end: _____ ft		Bank-Height Ratio (BHR) ( $LBH / d_{max}$ )	start: _____ end: _____	
	<b>Facet Slopes</b>			<b>Dimensionless Facet Slope Ratios</b>					
	Riffle Slope ( $S_{rif}$ )	<b>0.1980</b>		ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0000</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )				
	Step Slope ( $S_s$ )			ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )				
	<b>Max Depths<sup>a</sup></b>			<b>Dimensionless Depth Ratios</b>					
	Max Riffle Depth ( $d_{max}$ )	<b>0.38</b>	<b>0.27</b>	<b>0.49</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>1.520</b>	<b>1.080</b>	<b>1.960</b>
	Max Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )			
	Max Pool Depth ( $d_{maxp}$ )				ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )			
	Max Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )			
	Max Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
<b>Channel Materials</b>	<b>Reach<sup>b</sup></b>		<b>Riffle<sup>c</sup></b>		<b>Bar</b>		<b>Protrusion Height<sup>d</sup></b>		
	% Silt/Clay	<b>0</b>			$D_{16}$	<b>1.32</b>		mm	
	% Sand	<b>28.44</b>			$D_{35}$	<b>2.95</b>		mm	
	% Gravel	<b>70.64</b>			$D_{50}$	<b>6.39</b>		mm	
	% Cobble	<b>0.92</b>			$D_{84}$	<b>12.95</b>		mm	
	% Boulder	<b>0</b>			$D_{95}$	<b>23.88</b>		mm	
	% Bedrock	<b>0</b>			$D_{100}$	<b>255.99</b>		mm	

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.  
<sup>b</sup> Composite sample of riffles and pools within the designated reach.      <sup>c</sup> Active bed of a riffle.      <sup>d</sup> Height of roughness feature above bed.

## Stability Indices


**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation							
Stream: <b>Trail Creek, A4a+ Reference Reach</b>		Location: <b>Pike NF</b>					
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Reference reach <input checked="" type="checkbox"/>	Disturbed (impacted reach) <input type="checkbox"/>	Date: <b>9/3/2010</b>			
Existing species composition: <b>Aspen, Forb/Grass</b>		Potential species composition: <b>Same but without Invasive Species &amp; with Ponderosa Pine</b>					
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition		
<b>1. Overstory</b>	Canopy layer	<b>25%</b>	<b>25%</b>	<b>Aspen</b>	<b>100%</b>		
					<b>100%</b>		
<b>2. Understory</b>	Shrub layer		<b>15%</b>	<b>Raspberry</b>	<b>80%</b>		
				<b>Rose</b>	<b>10%</b>		
				<b>Ribes</b>	<b>10%</b>		
				<b>100%</b>			
<b>3. Ground level</b>	Herbaceous		<b>25%</b>	<b>Forbs (senecio, aster, scarlet gilia, mullen)</b>	<b>65%</b>		
					<b>35%</b>		
					<b>100%</b>		
Leaf or needle litter			<b>5%</b>	<b>Remarks:</b> Condition, vigor and/or usage of existing reach: <b>Sediment from hillslope delivery - lots of rilling on south aspect</b>			
Bare ground			<b>30%</b>				
		<b>Column total = 100%</b>					
*Based on crown closure.							
**Based on basal area to surface area.							

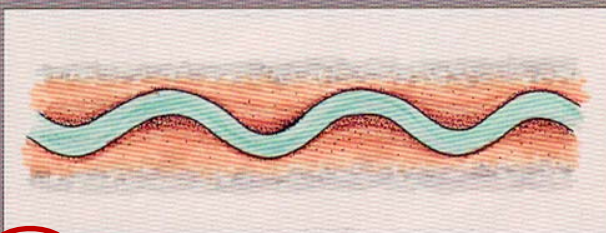


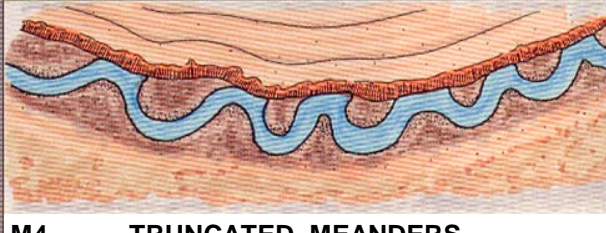


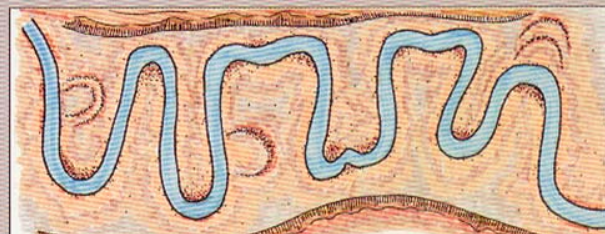
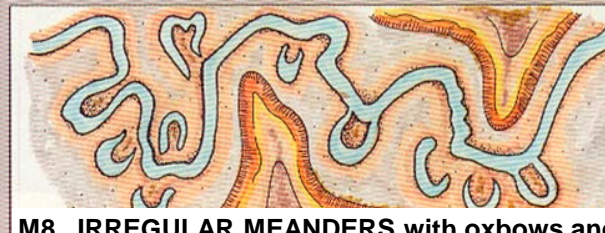
**Worksheet 5-7.** Flow regime.

<b>FLOW REGIME</b>								
Stream: <b>Trail Creek, A4a+ Reference</b>			Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>Chavez, Kasun &amp; Gallagher</b>						Date: <b>9/3/2010</b>		
<b>List ALL COMBINATIONS that APPLY.....</b>	<b>E1</b>	<b>E2</b>	<b>E8</b>					
<b>General Category</b>								
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation							
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
<b>P</b>	Perennial stream channels: Surface water persists yearlong.							
<b>Specific Category</b>								
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
<b>4</b>	Streamflow regulated by glacial melt.							
<b>5</b>	Ice flows/ice torrents from ice dam breaches.							
<b>6</b>	Alternating flow/backwater due to tidal influence.							
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.							
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
<b>9</b>	Rain-on-snow generated runoff.							

**Worksheet 5-8.** Stream order & stream size.

<b>Stream Size and Order</b>			
Stream:	<b>Trail Creek, A4a+ Reference Reach</b>		
Location:	<b>Pike National Forest, Colorado</b>		
Observers:	<b>Chavez, Kasun &amp; Gallagher</b>		
Date:	<b>9/3/2010</b>		
<b>Stream Size Category and Order</b> 			<b>S-2(1)</b>
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0 - 305	<1	<input type="checkbox"/>
<b>S-2</b>	<b>0.3 - 1.5</b>	<b>1 - 5</b>	<input checked="" type="checkbox"/>
S-3	1.5 - 4.6	5 - 15	<input type="checkbox"/>
S-4	4.6 - 9	15 - 30	<input type="checkbox"/>
S-5	9 - 15	30 - 50	<input type="checkbox"/>
S-6	15 - 22.8	50 - 75	<input type="checkbox"/>
S-7	22.8 - 30.5	75 - 100	<input type="checkbox"/>
S-8	30.5 - 46	100 - 150	<input type="checkbox"/>
S-9	46 - 76	150 - 250	<input type="checkbox"/>
S-10	76 - 107	250 - 350	<input type="checkbox"/>
S-11	107 - 150	350 - 500	<input type="checkbox"/>
S-12	150 - 305	500 - 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
<b>Stream Order</b>			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			

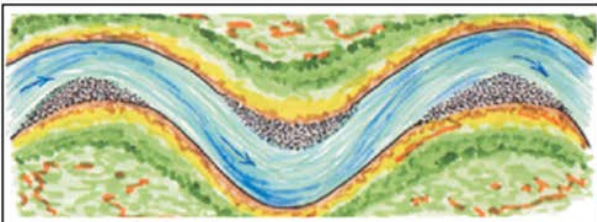
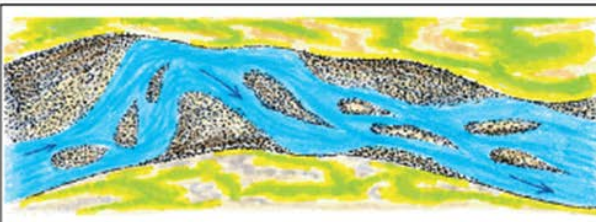

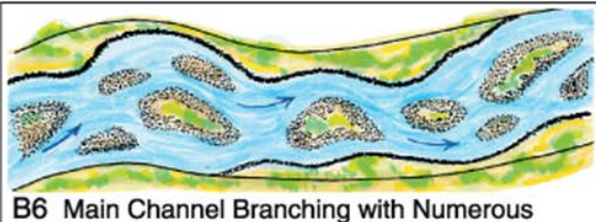
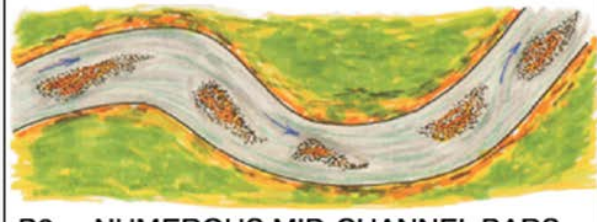
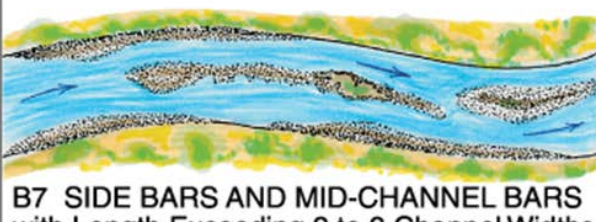

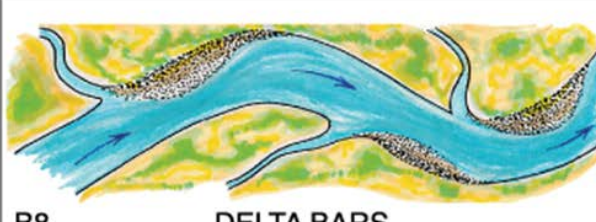
Worksheet 5-9. Meander patterns.

<b>Meander Patterns</b>					
Stream:	Trail Creek, A4a+ Reference Reach	Location:	Pike National Forest, CO		
Observers:	Chavez, Kasun & Gallagher		Date:	9/3/2010	
List ALL CATEGORIES that APPLY	<b>M1</b>				
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>					
	<b>M1 REGULAR MEANDERS</b>				
	<b>M2 TORTUOUS MEANDERS</b>				
	<b>M3 IRREGULAR MEANDERS</b>				
	<b>M4 TRUNCATED MEANDERS</b>				
	<b>M5 UNCONFINED MEANDER SCROLLS</b>				
	<b>M6 CONFINED MEANDER SCROLLS</b>				
	<b>M7 DISTORTED MEANDER LOOPS</b>				
	<b>M8 IRREGULAR MEANDERS with oxbows and</b>				

**Worksheet 5-10.** Depositional patterns.

<b>Depositional Patterns</b>					
Stream:	Trail Creek, A4a+ Reference Reach	Location:	Pike National Forest, Colorado		
Observers:	Chavez, Kasun & Gallagher	Date:	9/3/2010		
List ALL CATEGORIES that APPLY	None				

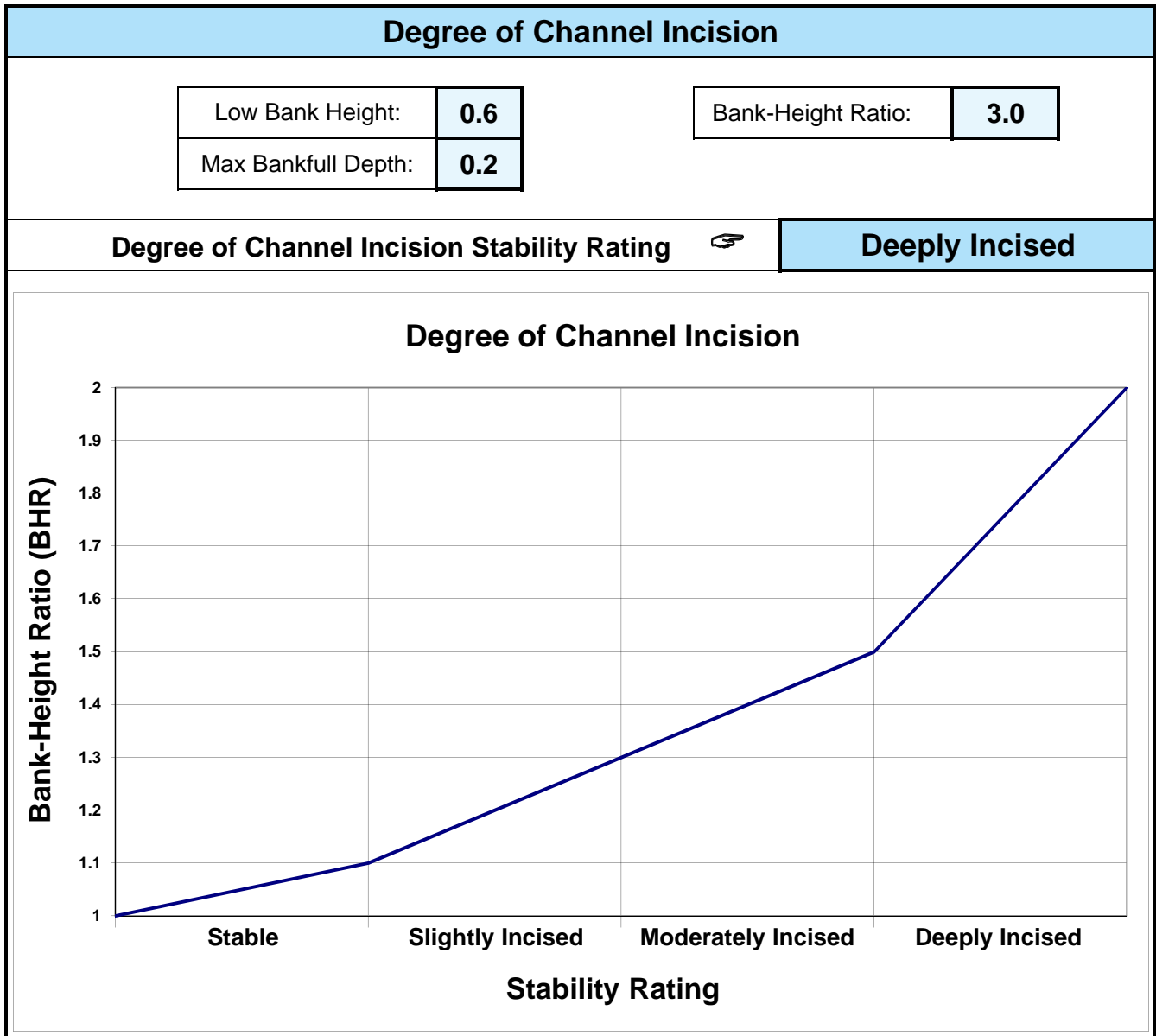
*Various Depositional Features modified from Galay et al. (1973)*

 <p><b>B1</b> POINT BARS</p>	 <p><b>B5</b> DIAGONAL BARS</p>
 <p><b>B2</b> POINT BARS with Few MID-CHANNEL BARS</p>	 <p><b>B6</b> Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</p>
 <p><b>B3</b> NUMEROUS MID-CHANNEL BARS</p>	 <p><b>B7</b> SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</p>
 <p><b>B4</b> SIDE BARS</p>	 <p><b>B8</b> DELTA BARS</p>

## Worksheet 5-11. Channel blockages.

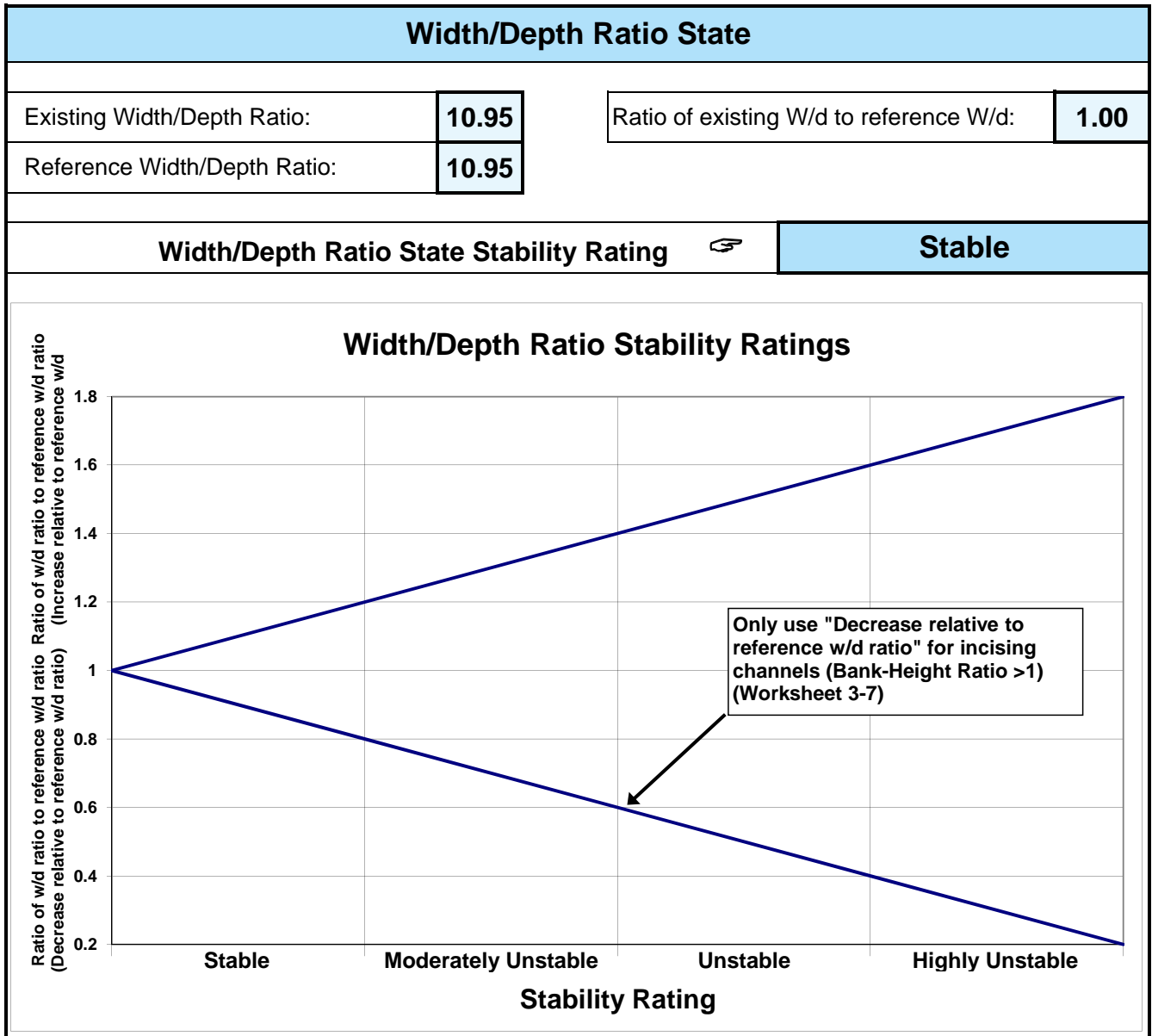
Channel Blockages		
Stream: <b>Trail Creek, A4a+ Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/3/2010</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input checked="" type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input type="checkbox"/>
<b>D4</b> Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

**Worksheet 5-12.** Degree of channel incision.

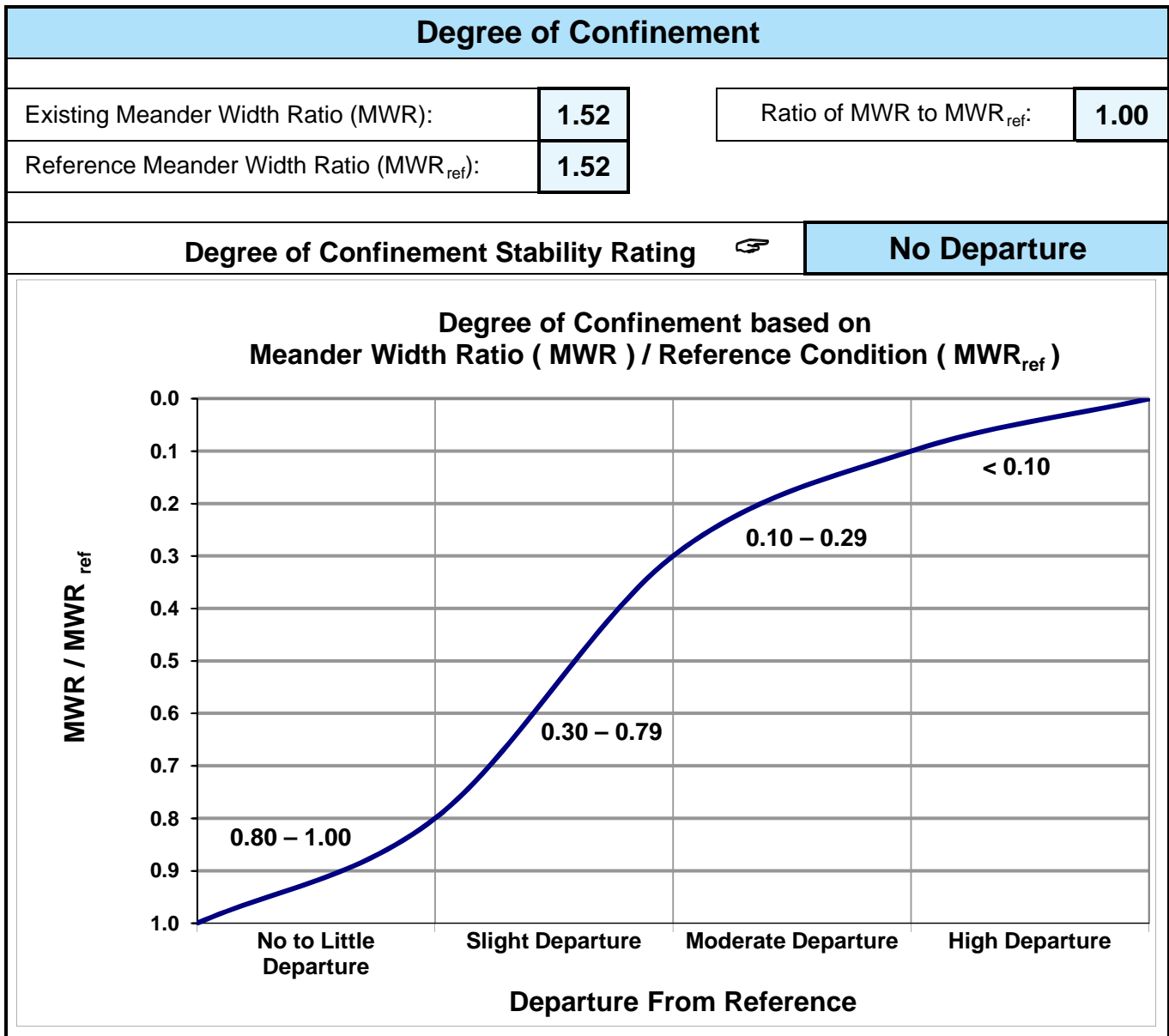




**Worksheet 5-13.** Width/depth ratio state.



**Worksheet 5-14.** Degree of channel confinement (lateral containment).



**Worksheet 5-15. Pfankuch channel stability rating.**

Stream: Trail Creek, A4a+ Reference		Location: Pike National Forest			Valley Type: I			Observers: Chavez, Kasun & Gallagher			Date: 9/3/2010														
Loca- tion	Key	Excellent			Good			Fair			Poor														
		Category	Description	Rating	Category	Description	Rating	Category	Description	Rating	Category	Description	Rating												
Upper banks	1	Landform slope	Bank slope gradient <30%.	2	Bank slope gradient 30–40%.	4	Bank slope gradient 40–60%.	6	Bank slope gradient > 60%.	8															
	2	Mass erosion	No evidence of past or future mass erosion.	3	Infrequent. Mostly healed over. Low future potential.	6	Frequent or large, causing sediment nearly yearlong.	9	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.	12															
	3	Debris jam potential	Essentially absent from immediate channel area.	2	Present, but mostly small twigs and limbs.	4	Moderate to heavy amounts, mostly larger sizes.	6	Moderate to heavy amounts, predominantly larger sizes.	8															
	4	Vegetative bank protection	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	3	70–90% density. Fewer species or less vigor suggest less dense or deep root mass.	6	50–70% density. Lower vigor and fewer species from a shallow, discontinuous root mass.	9	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.	12															
Lower banks	5	Channel capacity	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0.	1	Bankfull stage is contained within banks. Width/depth ratio departure from reference width/depth ratio = 1.0–1.2. Bank-Height Ratio (BHR) = 1.0–1.1.	2	Bankfull stage is not contained. Width/depth ratio departure from reference width/depth ratio = 1.2–1.4. Bank-Height Ratio (BHR) > 1.3.	3	Bankfull stage is not contained; over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.	4															
	6	Bank rock content	> 65% with large angular boulders, 12"+ common.	2	40–65%. Mostly boulders and small cobbles 6–12".	4	20–40%. Most in the 3–6" diameter class.	6	<20% rock fragments of gravel sizes, 1–3" or less.	8															
	7	Obstructions to flow	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	2	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	4	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	6	Frequent obstructions and deflectors cause bank erosion yearlong. Sediment traps full, channel migration occurring.	8															
	8	Cutting	Little or none. Infrequent raw banks <6".	4	Some, intermittently at outcrops and constrictions. Raw banks may be up to 12".	6	Significant. Cuts 12–24" high. Root mat overhangs and sloughing evident.	12	Almost continuous cuts, some over 24" high. Failure of overhangs frequent.	16															
	9	Deposition	Little or no enlargement of channel or point bars.	4	Some new bar increase, mostly from coarse gravel.	8	Moderate deposition of new gravel and coarse sand on old and some new bars.	12	Extensive deposit of predominantly fine particles. Accelerated bar development.	16															
Bottom	10	Rock angularity	Sharp edges and corners. Plane surfaces rough.	1	Rounded corners and edges. Surfaces smooth and flat.	2	Corners and edges well rounded in 2 dimensions.	3	Well rounded in all dimensions, surfaces smooth.	4															
	11	Brightness	Surfaces dull, dark or stained. Generally not bright.	1	Mostly dull, but may have <35% bright surfaces.	2	Mixture dull and bright, i.e., 35–65% mixture range.	3	Predominantly bright, > 65%, exposed or scoured surfaces.	4															
	12	Consolidation of particles	Assorted sizes tightly packed or overlapping.	2	Moderately packed with some overlapping.	4	Mostly loose assortment with no apparent overlap.	6	No packing evident. Loose assortment, easily moved.	8															
	13	Bottom size distribution	No size change evident. Stable material 80–100%.	4	Distribution shift light. Stable material 50–80%.	8	Moderate change in sizes. Stable materials 20–50%.	12	Marked distribution change. Stable materials 0–20%.	16															
	14	Scouring and deposition	<5% of bottom affected by scour or deposition.	6	5–30% affected. Scour at constrictions and where grades steepen. Some deposition in pools.	12	30–50% affected. Deposits and scour at obstructions, constrictions and bends. Some filling of pools.	18	More than 50% of the bottom in a state of flux or change nearly yearlong.	24															
	15	Aquatic vegetation	Abundant growth moss-like, dark green perennial. In swift water too.	1	Common. Algae forms in low velocity and pool areas. Moss here too.	2	Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick.	3	Perennial types scarce or absent. Yellow-green, short-term bloom may be present.	4															
<b>Excellent total = 10</b>				<b>Good total = 30</b>				<b>Fair total = 9</b>				<b>Poor total = 40</b>													
<b>Stream type</b>		A1	A2	A3	A4	A5	A6	B1	B2	B3	B4	B5	B6	C1	C2	C3	C4	C5	C6	D3	D4	D5	D6	<b>Grand total = 89</b>	
Good (Stable)		38-43	38-43	54-90	60-95	60-95	50-80	38-45	38-45	40-60	40-64	48-68	40-60	38-50	38-50	60-85	70-90	70-90	60-85	85-107	85-107	85-107	85-107	67-98	
Fair (Mod. unstable)		44-47	44-47	91-129	96-132	96-142	81-110	46-58	46-58	61-78	65-84	69-88	61-78	51-61	51-61	86-105	91-110	91-110	86-105	108-132	108-132	108-132	108-132	99-125	
Poor (Unstable)		48+	48+	130+	133+	143+	111+	59+	59+	79+	85+	89+	79+	62+	62+	106+	111+	111+	106+	133+	133+	133+	126+		
<b>Stream type</b>		DA3	DA4	DA5	DA6	E3	E4	E5	E6	F1	F2	F3	F4	F5	F6	G1	G2	G3	G4	G5	G6	G7	G8	<b>A4a+</b>	
Good (Stable)		40-63	40-63	40-63	40-63	50-75	50-75	40-63	40-63	60-85	60-85	85-110	85-110	90-115	80-95	40-60	40-60	40-60	85-107	90-112	90-112	85-107	85-107		
Fair (Mod. unstable)		64-86	64-86	64-86	64-86	76-96	76-96	64-86	64-86	86-105	86-105	111-125	111-125	116-130	96-110	61-78	61-78	61-78	108-120	113-125	113-125	108-120	108-120		
Poor (Unstable)		87+	87+	87+	87+	87+	87+	87+	87+	106+	106+	126+	126+	131+	111+	79+	79+	79+	121+	121+	126+	126+	121+		
		<b>Excellent total = 10</b>				<b>Good total = 30</b>				<b>Fair total = 9</b>				<b>Poor total = 40</b>				<b>Grand total = 89</b>							
																		<b>Existing stream type = A4a+</b>							
																		<b>*Potential stream type = A4a+</b>							
																		<b>Modified channel stability rating = Good</b>							

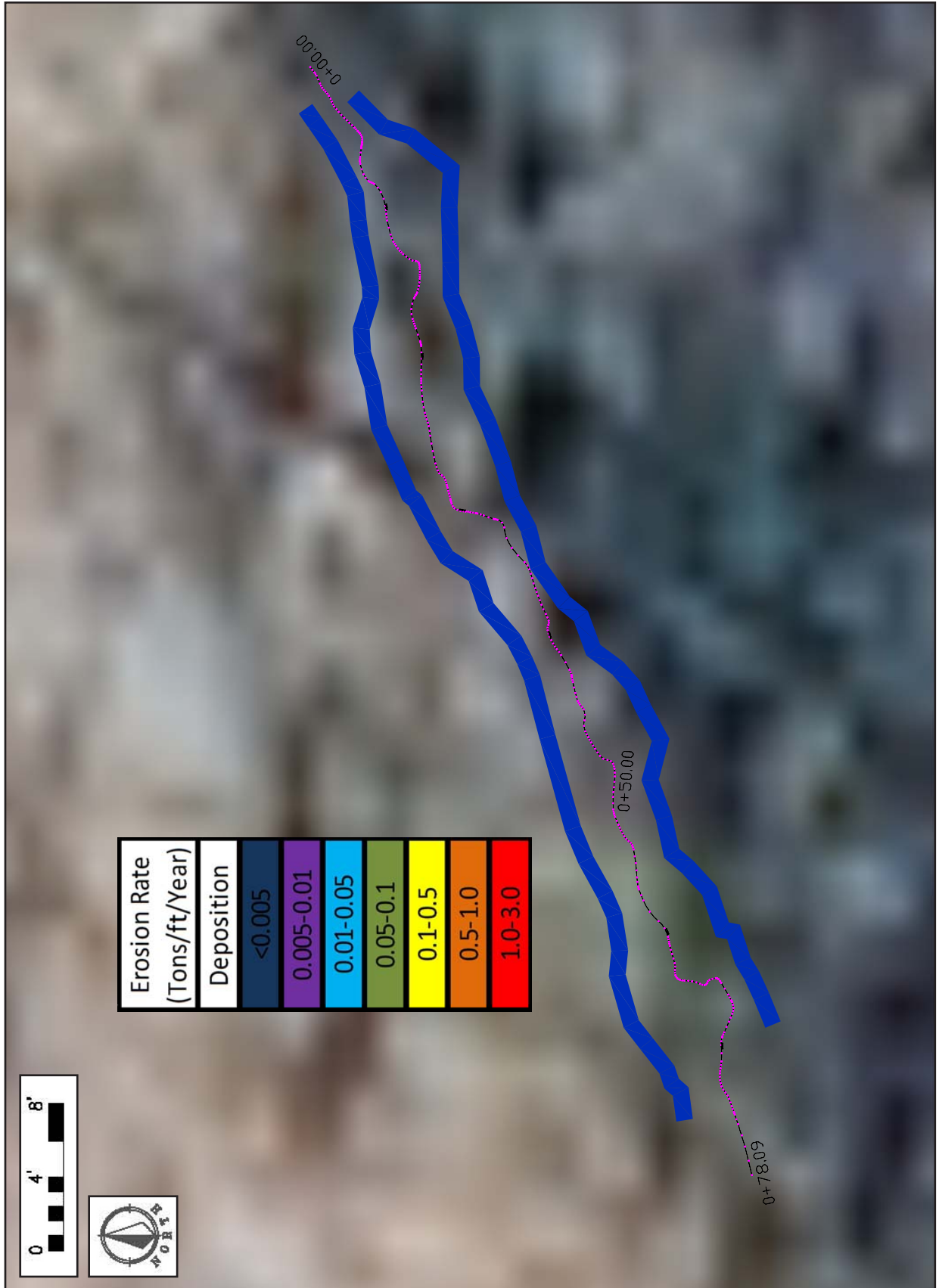
\*Rating is adjusted to potential stream type, not existing.

## BANCS Model – Streambank Erosion

**Worksheet 5-18.** Annual streambank erosion estimates.

Stream: <b>Trail Creek, A4a+ Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>					
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>70</b>				Date: <b>9/3/2010</b>	
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Valley Type: <b>I</b>			Stream Type: <b>A4a+</b>		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 5-16) (adjective)	NBS rating (Worksheet 5-17) (adjective)	Bank erosion rate (Figure 5-34 or 5-35) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [[4]x(5)x(6)] (ft <sup>3</sup> /yr)	Erosion Rate {[(7)/27] × 1.3 / (5)}
1. L 0+00 to 0+70	Low	Low	0.03566	70.0	0.5	1.25	0.00086
2. R 0+00 to 0+70	Low	Low	0.03566	70.0	0.5	1.25	0.00086
3.							
4.							
5.							
6.							
7.							
8.							
9.							
10.							
11.							
12.							
13.							
14.							
15.							
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					Total Erosion (ft <sup>3</sup> /yr)	2.50	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					Total Erosion (yds <sup>3</sup> /yr)	0.09	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					Total Erosion (tons/yr)	0.12	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					Total Erosion (tons/yr/ft)	0.0017	

Streambank Erosion Map



## FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Equation Type		Equation Source				Equation		Bankfull Discharge (cfs)			Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)			
1. Bedload Sediment		"Good/Fair" Pagosa				$Y = -0.0113 + 1.0139x^{2.1929}$		0.36			0.0013617		0.01405947			
2. Suspended Sediment		"Good/Fair" Pagosa				$Y = 0.0636 + 0.9326x^{2.4085}$										
From Dimensional Flow-Duration Curve																
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	Calculate		Calculate Sediment Yield			
Percentage of Time	Daily Mean Discharge (cfs)	Mid-Ordinate (%)	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow (cfs)	Dimensionless Streamflow ( $Q/Q_{bed}$ )	Dimensionless Suspended Sediment Discharge ( $S/S_{bed}$ )	Suspended Sediment Discharge (tons/day)	Dimensionless Bedload Discharge ( $b_b/b_{bed}$ )	Bedload Sediment Discharge (tons/day)	Time Adjusted Streamflow [(5)×(6)]	Suspended Sediment [(5)×(9)]	Bedload Sediment [(5)×(11)]	Suspended Sediment + Bedload Sediment [(13)+(14)]		
(%)	(cfs)	(%)	(%)	(days)	(cfs)	( $Q/Q_{bed}$ )	( $S/S_{bed}$ )	(tons/day)	( $b_b/b_{bed}$ )	(tons/day)	(cfs)	(tons)	(tons)	(tons)		
0%	0.9															
0.10%	0.8	0.05%	0.09%	0.34	0.9	2.363	7.461	0.00	6.670	0.87	0.3	0.00	0.30	0.30		
0.25%	0.7	0.08%	0.15%	0.55	0.7	2.036	5.232	0.00	4.809	0.62	0.4	0.00	0.34	0.34		
0.50%	0.6	0.13%	0.25%	0.91	0.6	1.761	3.706	0.00	3.494	0.45	0.6	0.00	0.41	0.41		
0.75%	0.5	0.13%	0.25%	0.91	0.5	1.513	2.592	0.00	2.502	0.32	0.5	0.00	0.30	0.30		
1%	0.4	0.13%	0.25%	0.91	0.5	1.300	1.817	0.00	1.790	0.23	0.4	0.00	0.21	0.21		
1.5%	0.4	0.25%	0.50%	1.83	0.4	1.120	1.289	0.00	1.289	0.17	0.7	0.00	0.31	0.31		
2%	0.3	0.25%	0.50%	1.83	0.3	0.949	0.886	0.00	0.893	0.12	0.6	0.00	0.21	0.21		
3%	0.3	0.50%	1.00%	3.65	0.3	0.795	0.600	0.00	0.602	0.08	1.0	0.00	0.28	0.28		
4%	0.2	0.50%	1.00%	3.65	0.2	0.674	0.424	0.00	0.415	0.05	0.9	0.00	0.20	0.20		
5%	0.2	0.50%	1.00%	3.65	0.2	0.587	0.322	0.00	0.304	0.04	0.8	0.00	0.14	0.14		
10%	0.1	2.50%	5.00%	18.25	0.2	0.450	0.200	0.00	0.165	0.02	3.0	0.00	0.39	0.39		
20%	0.1	5.00%	10.00%	36.50	0.1	0.269	0.103	0.00	0.045	0.01	3.5	0.00	0.22	0.22		
30%	0.0	5.00%	10.00%	36.50	0.1	0.158	0.075	0.00	0.006	0.00	2.1	0.00	0.03	0.03		
40%	0.0	5.00%	10.00%	36.50	0.0	0.108	0.068	0.00	0.000	0.00	1.4	0.00	0.00	0.00		
50%	0.0	5.00%	10.00%	36.50	0.0	0.079	0.066	0.00	0.000	0.00	1.0	0.00	0.00	0.00		
60%	0.0	5.00%	10.00%	36.50	0.0	0.061	0.065	0.00	0.000	0.00	0.8	0.00	0.00	0.00		
70%	0.0	5.00%	10.00%	36.50	0.0	0.047	0.064	0.00	0.000	0.00	0.6	0.00	0.00	0.00		
80%	0.0	5.00%	10.00%	36.50	0.0	0.039	0.064	0.00	0.000	0.00	0.5	0.00	0.00	0.00		
90%	0.0	5.00%	10.00%	36.50	0.0	0.032	0.064	0.00	0.000	0.00	0.4	0.00	0.00	0.00		
100%	0.0	5.00%	10.00%	36.50	0.0	0.016	0.064	0.00	0.000	0.00	0.2	0.00	0.00	0.00		
<b>Annual Totals:</b>											19.8 (cfs)		0.0 (tons/yr)		3.3 (tons/yr)	
											39.3 (acre-ft)					

Worksheet 19b. Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Equation Type		Equation Source		Equation		Bankfull Discharge (cfs)		Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)				
1. Bedload Sediment		"Good/Fair" Pagosa		$Y = -0.0113 + 1.0139x^{2.1929}$		0.36		0.0013617		0.01405947				
2. Suspended Sediment		"Good/Fair" Pagosa		$Y = 0.0636 + 0.9326x^{2.4085}$										
From Dimensional Flow-Duration Curve														
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Percentage of Time	Daily Mean Discharge (cfs)	Mid-Ordinate (%)	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Suspended Sediment Discharge	Suspended Sediment Discharge (tons/day)	Dimensionless Bedload Discharge	Bedload Sediment Discharge (tons/day)	Time Adjusted Streamflow [(5)×(6)]	Suspended Sediment [(5)×(9)]	Bedload Sediment [(5)×(11)]	Suspended Sediment + Bedload Sediment [(13)+(14)]
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>bed</sub> )	(S/S <sub>bed</sub> )	(tons/day)	(b <sub>g</sub> /b <sub>bed</sub> )	(tons/day)	(cfs)	(tons)	(tons)	(tons)
0%	0.9													
0.10%	0.8	0.05%	0.09%	0.34	0.9	2.383	7.614	0.00	6.796	0.88	0.3	0.00	0.30	0.30
0.25%	0.7	0.08%	0.15%	0.55	0.7	2.056	5.356	0.00	4.914	0.64	0.4	0.00	0.35	0.35
0.50%	0.6	0.13%	0.25%	0.91	0.6	1.781	3.807	0.00	3.582	0.46	0.6	0.00	0.42	0.42
0.75%	0.5	0.13%	0.25%	0.91	0.6	1.533	2.673	0.00	2.576	0.33	0.5	0.00	0.30	0.31
1%	0.4	0.13%	0.25%	0.91	0.5	1.320	1.883	0.00	1.852	0.24	0.4	0.00	0.22	0.22
1.5%	0.4	0.25%	0.50%	1.83	0.4	1.140	1.343	0.00	1.340	0.17	0.7	0.00	0.32	0.32
2%	0.3	0.25%	0.50%	1.83	0.3	0.969	0.927	0.00	0.934	0.12	0.6	0.00	0.22	0.22
3%	0.3	0.50%	1.00%	3.65	0.3	0.815	0.633	0.00	0.635	0.08	1.1	0.00	0.30	0.30
4%	0.2	0.50%	1.00%	3.65	0.2	0.693	0.449	0.00	0.442	0.06	0.9	0.00	0.21	0.21
5%	0.2	0.50%	1.00%	3.65	0.2	0.604	0.340	0.00	0.324	0.04	0.8	0.00	0.15	0.15
10%	0.1	2.50%	5.00%	18.25	0.2	0.463	0.210	0.00	0.176	0.02	3.0	0.00	0.42	0.42
20%	0.1	5.00%	10.00%	36.50	0.1	0.274	0.105	0.00	0.048	0.01	3.6	0.00	0.23	0.23
30%	0.0	5.00%	10.00%	36.50	0.1	0.159	0.075	0.00	0.007	0.00	2.1	0.00	0.03	0.03
40%	0.0	5.00%	10.00%	36.50	0.0	0.108	0.068	0.00	0.000	0.00	1.4	0.00	0.00	0.00
50%	0.0	5.00%	10.00%	36.50	0.0	0.079	0.066	0.00	0.000	0.00	1.0	0.00	0.00	0.00
60%	0.0	5.00%	10.00%	36.50	0.0	0.061	0.065	0.00	0.000	0.00	0.8	0.00	0.00	0.00
70%	0.0	5.00%	10.00%	36.50	0.0	0.047	0.064	0.00	0.000	0.00	0.6	0.00	0.00	0.00
80%	0.0	5.00%	10.00%	36.50	0.0	0.039	0.064	0.00	0.000	0.00	0.5	0.00	0.00	0.00
90%	0.0	5.00%	10.00%	36.50	0.0	0.032	0.064	0.00	0.000	0.00	0.4	0.00	0.00	0.00
100%	0.0	5.00%	10.00%	36.50	0.0	0.016	0.064	0.00	0.000	0.00	0.2	0.00	0.00	0.00
<b>Annual Totals:</b>											20.1 (cfs)	0.0 (tons/yr)	3.5 (tons/yr)	3.5 (tons/yr)
											39.9 (acre-ft)			

## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>Trail Creek, A4a+ Reference Reach</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/3/2010</b>			
<b>Enter Required Information for Existing Condition</b>					
13.0	$D_{50}$	Riffle bed material $D_{50}$ (mm) <b>NOTE: Used <math>D_{84}</math></b>			
N/A	$D_{50}^{\wedge}$	Bar sample $D_{50}$ (mm)			
0.84	$D_{max}$	Largest particle from <b>BED MATERIAL</b> (ft)	256	(mm)	304.8 mm/ft
0.198	$S$	Existing bankfull water surface slope (ft/ft)			
0.21	$d$	Existing bankfull mean depth (ft)			
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment			
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>					
N/A	$D_{50}/D_{50}^{\wedge}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 ( D_{50}/D_{50}^{\wedge} )^{-0.872}$		
19.77	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 ( D_{max}/D_{50} )^{-0.887}$		
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED:		
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	$d$	Required bankfull mean depth (ft)	$d = \frac{\tau^*(\gamma_s - 1)D_{max}}{S}$ (use $D_{max}$ in ft)		
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	$S$	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^*(\gamma_s - 1)D_{max}}{d}$ (use $D_{max}$ in ft)		
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					
<b>Sediment Competence Using Dimensional Shear Stress</b>					
2.595	Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d ) $\gamma = 62.4$ , $d =$ existing depth, $S =$ existing slope				
Shields <b>200</b>	CO <b>300</b>	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ ( <b>Figure 5-49</b> )			
Shields <b>2</b>	CO <b>3.3</b>	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) ( <b>Figure 5-49</b> )			
Shields <b>0.16</b>	CO <b>0.27</b>	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm)		$d = \frac{\tau}{\gamma S}$	
Shields <b>0.1526</b>	CO <b>0.2518</b>	Predicted slope required to initiate movement of measured $D_{max}$ (mm)		$S = \frac{\tau}{\gamma d}$	
Check: <input checked="" type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					



## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>Trail Creek, A4a+ Reference</b>		Stream Type: <b>A4a+</b>
Location: <b>Pike National Forest, CO</b>		Valley Type: <b>I</b>
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/3/2010</b>
<b>Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)</b>		<b>Stability Rating (Check Appropriate Rating)</b>
<b>Stream Type at potential, (C→E),</b> (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)		<input checked="" type="checkbox"/> Stable
(E→C), (C→High W/d C)		<input type="checkbox"/> Moderately Unstable
(G→F), (F→D), (C→F)		<input type="checkbox"/> Unstable
(C→D), (B→G), (D→G), (C→G), (E→G)		<input type="checkbox"/> Highly Unstable

**Worksheet 5-25.** Lateral stability.

Stream: <b>Trail Creek, A4a+ Reference Reach</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/3/2010</b>			
Lateral stability criteria (choose one stability category for each criterion 1-5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	2
	1.0 (2)	(4)	(6)	(8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	0
	None (1)	(2)	(3)	(4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		1
	M1 (1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	2
	L/L (2)	(4)	(6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	1
	1.0 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>6</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input checked="" type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input type="checkbox"/>	<i>Unstable</i> 13 – 21 <input type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	

**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>Trail Creek, A4a+ Reference Reach</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/3/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
1 <b>Sediment Competence</b> (Worksheet 5-22)	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope—slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	2
	(2)	(4)	(6)	(8)	
2 <b>Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	2
	Ref. Reach (2)	(4)	(6)	(8)	
3 <b>W/d Ratio State</b> (Worksheet 5-13)	1.0 – 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	2
	1.0 (2)	(4)	(6)	(8)	
4 <b>Stream Succession States</b> (Worksheet 5-24)	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	2
	at potential (2)	(4)	(6)	(8)	
5 <b>Depositional Patterns</b> (Worksheet 5-10)	B1	B2, B4	B3, B5	B6, B7, B8	0
	None (1)	(2)	(3)	(4)	
6 <b>Debris / Blockages</b> (Worksheet 5-11)	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	1
	D2 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>9</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
Vertical Stability for Excess Deposition / Aggradation (use total points and check stability rating)	<i>No Deposition</i> 10 – 14 <input checked="" type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input type="checkbox"/>	<i>Aggradation</i> > 30 <input type="checkbox"/>	

**Worksheet 5-27.** Vertical stability – degradation.

Stream: <b>Trail Creek, A4a+ Reference Reach</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Chavez, Kasun &amp; Galagher</b>		Date: <b>9/3/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>1 Sediment Competence</b> (Worksheet 5-22)	Does not indicate excess competence	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed	$D_{100}$ of bed moved	Particles much larger than $D_{100}$ of bed moved	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>2 Sediment Capacity</b> (POWERSED) (Worksheet 5-20)	Does not indicate excess capacity	Slight excess energy: up to 10% increase above reference	Excess energy sufficient to increase load up to 50% of annual load	Excess energy transporting more than 50% of annual load	<b>2</b>
	Ref. Reach (2)	(4)	(6)	(8)	
<b>3 Degree of Channel Incision (BHR)</b> (Worksheet 5-12)	1.00 – 1.10	1.11 – 1.30	1.31 – 1.50	> 1.50	<b>8</b>
	(2)	(4)	(6)	<b>3.00</b> (8)	
<b>4 Stream Succession States</b> (Worksheets 5-12 and 5-24)	Does not indicate incision or degradation	If BHR > 1.1 and stream type has W/d between 5–10	If BHR > 1.1 and stream type has W/d less than 5	(B→G), (C→G), (E→G), (D→G)	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>5 Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.80 – 1.00	0.30 – 0.79	0.10 – 0.29	< 0.10	<b>1</b>
	<b>1.00</b> (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>15</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation</b> (use total points and check stability rating)	<i>Not Incised</i> 9 – 11 <input type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input checked="" type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input type="checkbox"/>	<i>Degradation</i> > 27 <input type="checkbox"/>	

Worksheet 5-28. Channel enlargement.

Stream: <b>Trail Creek, A4a+ Reference Reach</b>		Stream Type: <b>A4a+</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>			
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/3/2010</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1–4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	2
	at potential (2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	2
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	2
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	4
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>10</b>
<b>Category Point Range</b>					
Channel Enlargement Prediction (use total points and check stability rating)	<i>No Increase</i> 8 – 10 <input checked="" type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input type="checkbox"/>	<i>Extensive</i> > 24 <input type="checkbox"/>	

Worksheet 5-29. Overall sediment supply.

Stream: <b>Trail Creek, A4a+ Reference Reach</b>		Stream Type: <b>A4a+</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>I</b>		
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Date: <b>9/3/2010</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1-5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	1	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	1	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	2	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	1	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	1	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>6</b>	
<b>Category Point Range</b>				
Overall Sediment Supply Rating (use total points and check stability rating)	<i>Low</i> 5 <input type="checkbox"/>	<i>Moderate</i> 6 – 10 <input checked="" type="checkbox"/>	<i>High</i> 11 – 15 <input type="checkbox"/>	<i>Very High</i> 16 – 20 <input type="checkbox"/>

Worksheet 5-32. Summary of stability condition categories.

Stream: <b>Trail Creek, A4a+ Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>	
Observers: <b>Chavez, Kasun &amp; Gallagher</b>		Stream Type: <b>A4a+</b> Valley Type: <b>I</b>	
Date: <b>9/3/2010</b>		Entrenchment Ratio: <b>1.59</b>	
Channel Dimension (XS 0+15.62)		Width of Flood-Prone Area (ft): <b>0.48</b>	
Mean Bankfull Depth (ft): <b>0.21</b>		Cross-Sectional Area (ft <sup>2</sup> ): <b>2.3</b>	
Channel Pattern		MWR: <b>1.52</b> Sinuosity: <b>1.11</b>	
River Profile & Bed Features		R <sub>c</sub> /W <sub>bkf</sub> : <b>N/A</b>	
Check: <input type="checkbox"/> Riffle/Pool <input type="checkbox"/> Step/Pool <input checked="" type="checkbox"/> Plane Bed <input type="checkbox"/> Convergence/Divergence <input type="checkbox"/> Dunes/Antidunes/Smooth Bed		Pool Spacing: <b>0.220</b> Valley: <b>0.220</b> Water Surface: <b>0.198</b>	
Max Bankfull Depth (ft): <b>0.38</b>		Depth Ratio (max to mean): <b>1.52</b>	
Riparian Vegetation		Potential Composition/Density: <b>Some riling from south aspects</b>	
Flow Regime: <b>E1, E2, E8 &amp; Order: S-2(1)</b>		Meander Patterns: <b>M1</b>	
Degree of Incision (Bank-Height Ratio): <b>3.0</b>		Degree of Incision Stability Rating: <b>Deeply Incised</b>	
Width/depth Ratio (W/d): <b>11</b>		Width/Depth Ratio State (W/d) / (W/d <sub>ref</sub> ): <b>1.0</b>	
Meander Width Ratio (MWR): <b>1.52</b>		Degree of confinement (MWR / MWR <sub>ref</sub> ): <b>1.0</b>	
Length of Reach Studied (ft): <b>70</b>		Annual Streambank Erosion Rate: (tons/yr) <b>0.0017</b> Curve Used: <b>Colorado</b>	
Sediment Capacity (POWERSED)		Remarks: <b>Remarks: Sufficient Capacity <input type="checkbox"/> Insufficient Capacity <input type="checkbox"/> Excess Capacity <input type="checkbox"/></b>	
Entrainment/Competence		Largest Particle from Bed Material (mm): <b>256</b>	
Successional Stage Shift		τ = <b>2.6</b> τ* = <b>N/A</b> Existing Depth: <b>0.21</b> Required Depth: <b>0.16-0.27</b> Existing Slope: <b>0.198</b> Required Slope: <b>0.15-0.25</b>	
Lateral Stability		A4a+ → <b>A4a+</b> → <b>A4a+</b> Existing Stream State (Type): <b>A4a+</b> Potential Stream (Type): <b>A4a+</b>	
Vertical Stability (Aggradation)		<input checked="" type="checkbox"/> Stable <input type="checkbox"/> Mod. Unstable <input type="checkbox"/> Unstable <input type="checkbox"/> Highly Unstable	
Vertical Stability (Degradation)		<input checked="" type="checkbox"/> No Deposition <input type="checkbox"/> Mod. Deposition <input type="checkbox"/> Ex. Deposition <input type="checkbox"/> Aggradation	
Channel Enlargement		<input type="checkbox"/> Not Incised <input checked="" type="checkbox"/> Slightly Incised <input type="checkbox"/> Mod. Incised <input type="checkbox"/> Degradation	
Sediment Supply (Channel Source)		<input checked="" type="checkbox"/> No Increase <input type="checkbox"/> Slight Increase <input type="checkbox"/> Mod. Increase <input type="checkbox"/> Extensive	
		<input type="checkbox"/> Low <input checked="" type="checkbox"/> Moderate <input type="checkbox"/> High <input type="checkbox"/> Very High	
		Remarks/causes: <b>Because of BHR of 3.0</b>	





## *Appendix C17*

# **A4/2 Stream Type** *Reference Reach*



# Table of Contents

## *Appendix C17: A4/2 Reference Reach*

**Reach Location & Overview..... C17-2**

**Survey Summary.....C17-3**  
 Longitudinal Profile  
 Cross-Sections  
 Pebble Counts

**WARSSS Worksheets..... C17-7**

***Velocity, Classification & Morphological Relations..... C17-7***  
 Worksheet 5-2. Computations of velocity and bankfull discharge.  
 Worksheet 5-3. Level II stream classification.  
 Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).

***Stability Indices..... C17-11***  
 Worksheet 5-6. Riparian vegetation.  
 Worksheet 5-7. Flow regime.  
 Worksheet 5-8. Stream order and stream size.  
 Worksheet 5-9. Meander patterns.  
 Worksheet 5-10. Depositional patterns.  
 Worksheet 5-11. Channel blockages.  
 Worksheet 5-12. Degree of channel incision.  
 Worksheet 5-13. Width/depth ratio state.  
 Worksheet 5-14. Degree of channel confinement (lateral containment).  
 Worksheet 5-15. Pfankuch channel stability rating.

***BANCS Model – Streambank Erosion..... C17-21***  
 Worksheet 5-18. Annual streambank erosion estimates.  
 Streambank Erosion Map

***FLOWSED Model – Total Annual Sediment Yield..... C17-23***  
 Worksheet 5-19a. Total annual sediment yield, pre-fire condition.  
 Worksheet 5-19b. Total annual sediment yield, post-fire condition.

***Sediment Competence/Entrainment..... C17-25***  
 Worksheet 5-22. Sediment competence calculations.

***Channel Stability Ratings..... C17-26***  
 Worksheet 5-24. Successional stage shifts.  
 Worksheet 5-25. Lateral stability.  
 Worksheet 5-26. Vertical stability – aggradation.  
 Worksheet 5-27. Vertical stability – degradation.  
 Worksheet 5-28. Channel enlargement.  
 Worksheet 5-29. Overall sediment supply.

***Summary..... C17-32***  
 Worksheet 5-32. Summary of stability condition categories.

## A4/2 Reference Reach Location & Overview

The A4/2 reference reach is in a Valley Type VIIIb located on the mainstem of West Monument Creek (see location map in **Figure C-1**). This reach is dominated by gravel and influenced by boulders. The channel bed and banks show little sediment yield and good stability from abundant vegetation and boulders. Bed features are generally dominated by step/pools. The channel is perennial and streamflow is seasonal by snowmelt and stormflow runoff. Flow is regulated by an upstream dam and is altered due to the Waldo Canyon Fire. The reach is a 4<sup>th</sup> order channel.

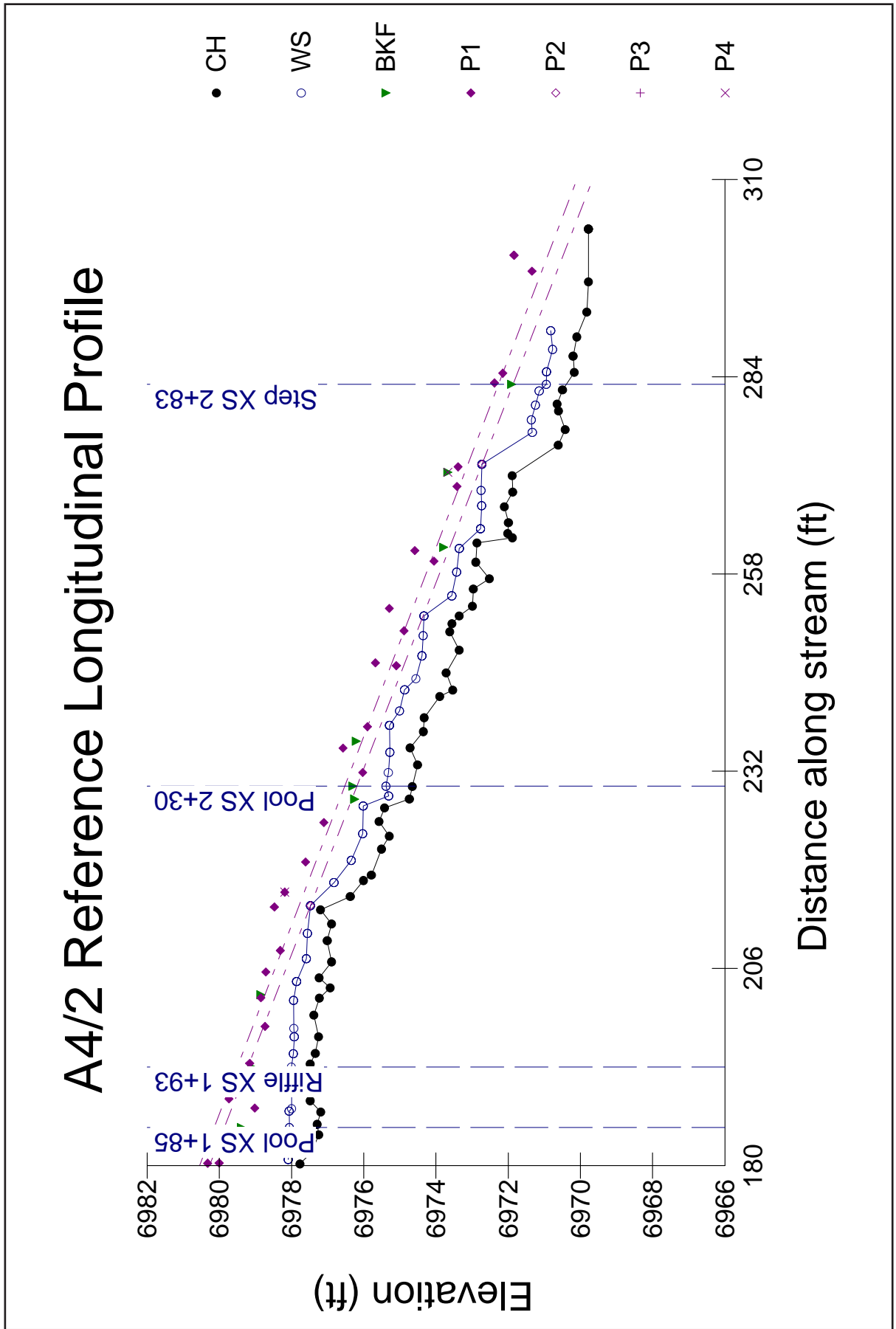
Typical of A stream types, the channel is entrenched and has a low width/depth ratio with a relatively straight pattern having a sinuosity of 1.05. Little channel source sediment is generated from this stream during high runoff events due to good riparian vegetation. The predicted streambank erosion rate of 0.0076 *tons/yr/ft* represents an acceptable geologic rate (**Worksheet 5-18**).

The photograph depicts the stable characteristics of this stream type. Such stream types are mapped where they occur by sub-watershed as shown in **Appendix D**.

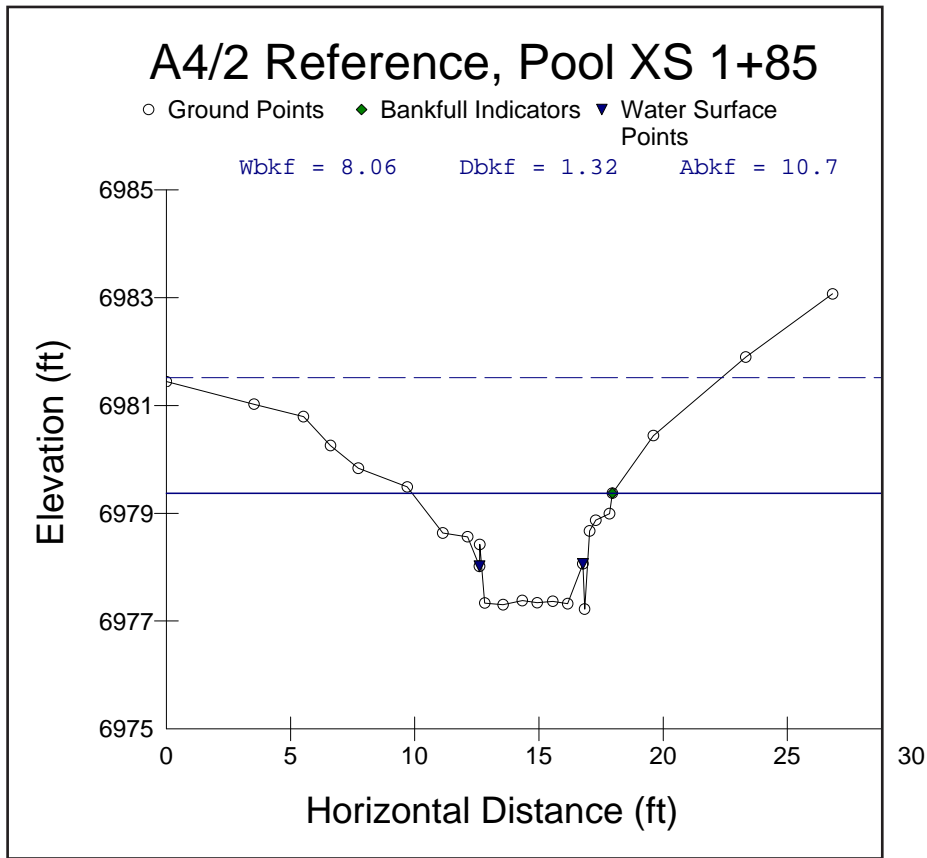
The details of the dimension, pattern, profile, and materials are summarized. The following summary worksheets provide details of the morphology, hydraulics, stability, and streambank erosion rates for this reference reach. In the situation where impaired A4/2 stream types are located, an alternative for mitigation and sediment reduction is to use the data from the stable form to extrapolate for potential implementation of natural channel design.



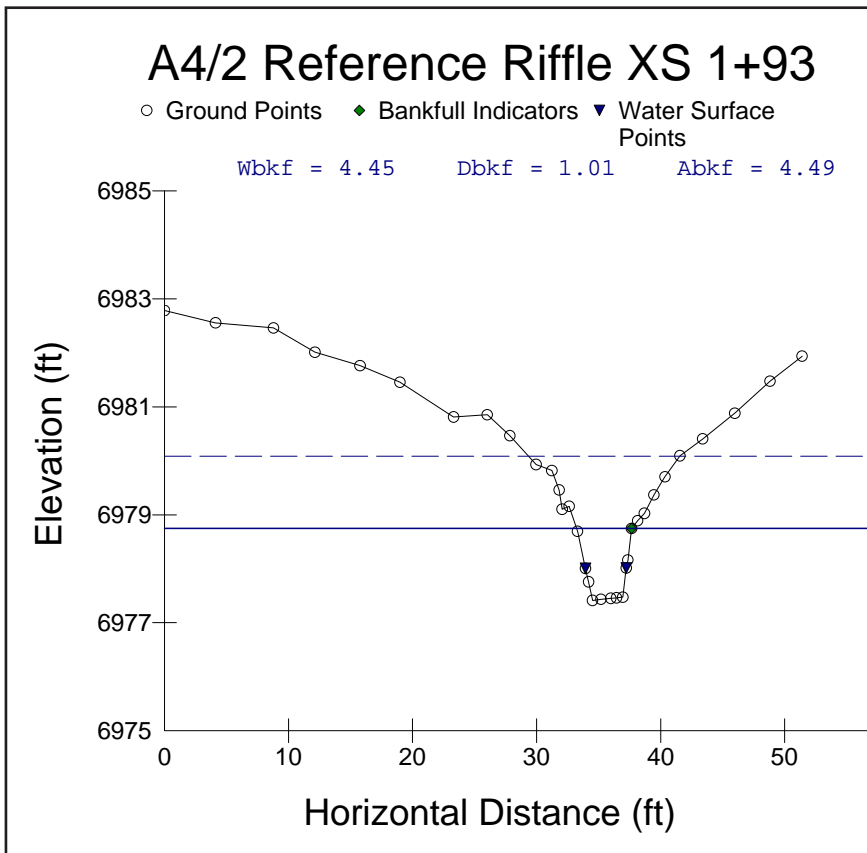
Survey Summary



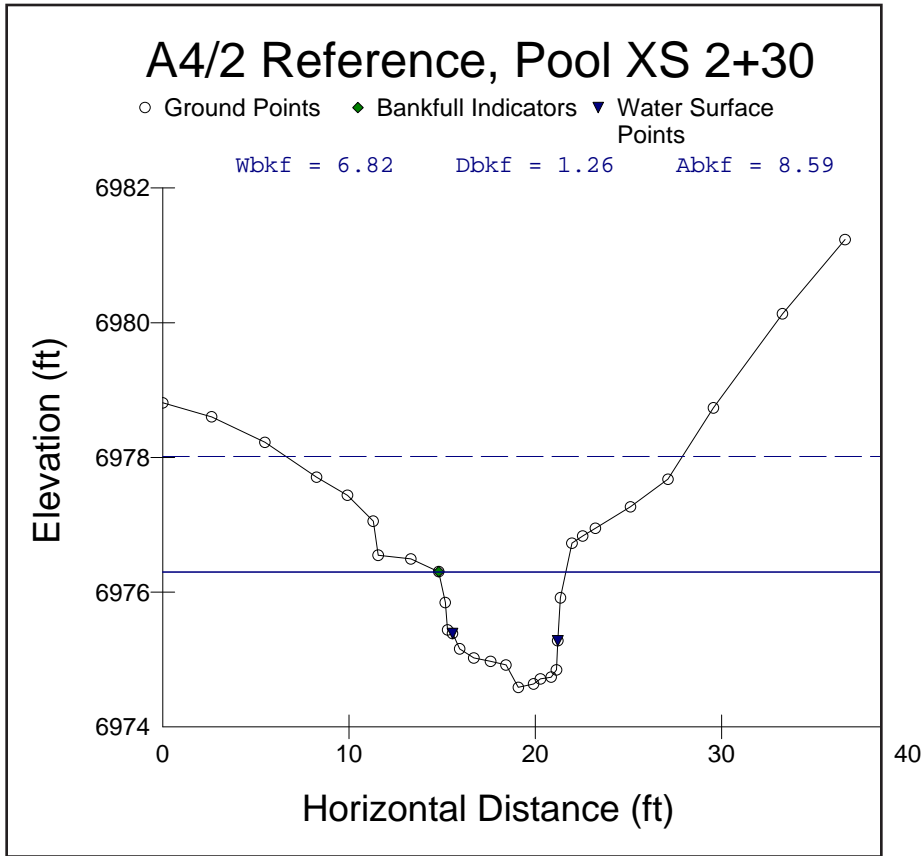
Longitudinal Profile (graph generated from RIVERMorph™)



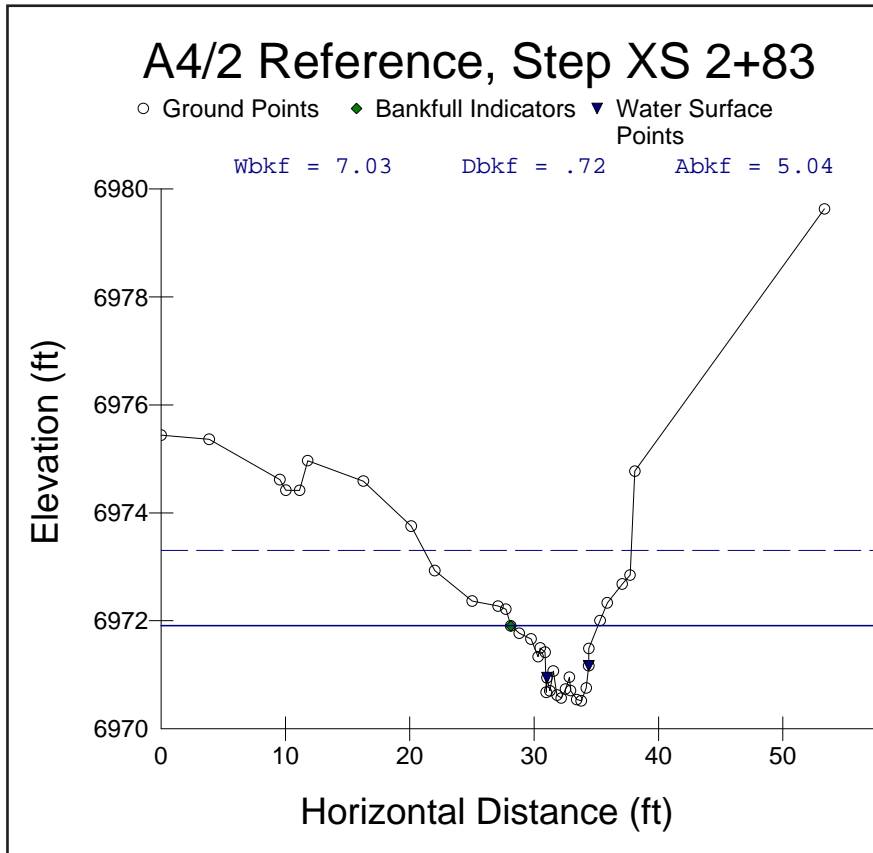
Cross-section 1+85 (graph generated from RIVERMorph™)



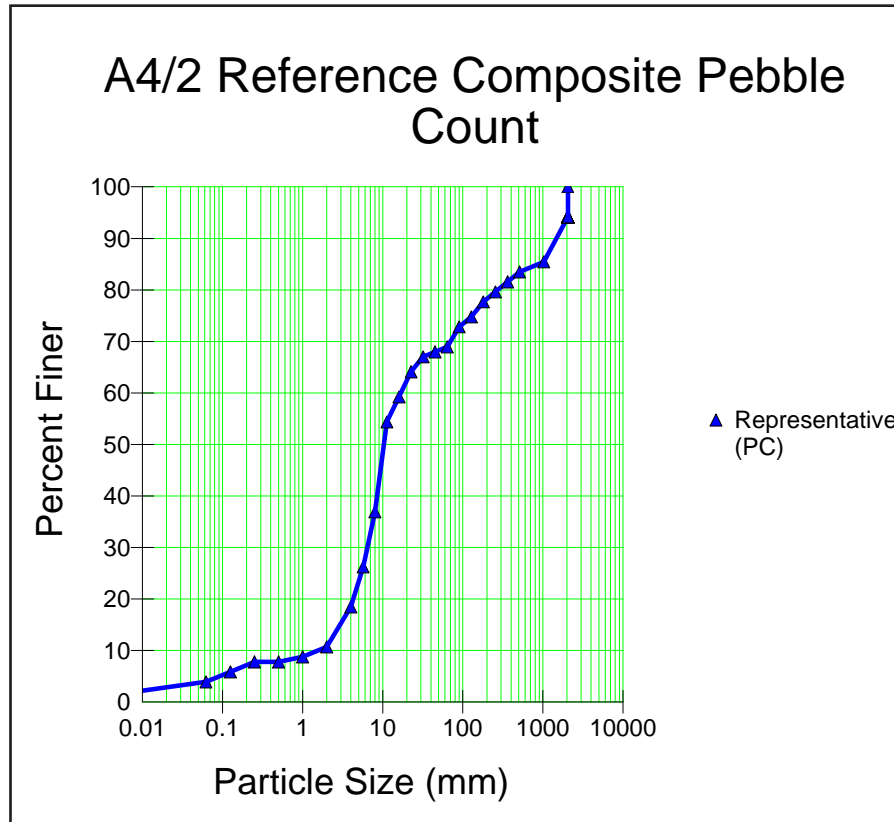
Cross-section 1+93 (graph generated from RIVERMorph™)



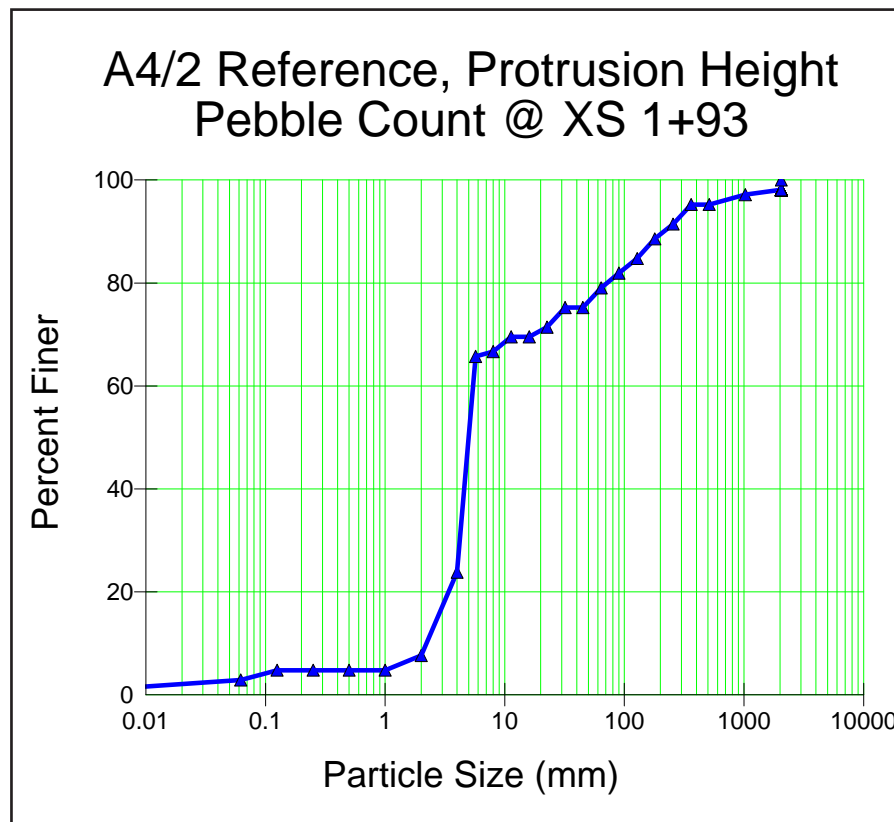
**Cross-section 2+30** (graph generated from RIVERMorph™)



**Representative Cross-section 2+83** (graph generated from RIVERMorph™)



Composite Pebble Count (graph generated from RIVERMorph™)



Protrusion Height Pebble Count (graph generated from RIVERMorph™)



# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates					
Stream:	West Monument A4/2 Reference			Location:	XS 2+83, Pike N.F., Colorado
Date:	11/6/2012	Stream Type:	A4/2	Valley Type:	VIIIb
Observers:	Lee, Sumner, Jara, Leah			HUC:	__ __ __ __ __ __ __ __ __ __
INPUT VARIABLES			OUTPUT VARIABLES		
Bankfull Riffle Cross-Sectional AREA	5.04	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.72	$d_{bkf}$ (ft)
Bankfull Riffle WIDTH	7.0	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim (2 * d_{bkf}) + W_{bkf}$	8.47	$W_p$ (ft)
$D_{84}$ at Riffle	224.9	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.74	$D_{84}$ (ft)
Bankfull SLOPE	0.08	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	0.60	R (ft)
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R(ft) / $D_{84}$ (ft)	0.81	R / $D_{84}$
Drainage Area	10.95	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	1.247	$u^*$ (ft/sec)
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE
1. Friction Factor / Relative Roughness	$u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$		2.31	ft / sec	11.64 cfs
2. Roughness Coefficient: a) Manning's n from Friction Factor / Relative Roughness (Figs. 5-7, 5-8)	$u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.09$		3.05	ft / sec	15.37 cfs
2. Roughness Coefficient: b) Manning's n from Stream Type (Fig. 5-9)	$u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.15$		1.83	ft / sec	9.22 cfs
2. Roughness Coefficient: c) Manning's n from Jarrett (USGS): <small>Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for Stream Types A1, A2, A3, B1, B2, B3, C2 &amp; E3</small>	$u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ $n = 0.167$		1.65	ft / sec	8.32 cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Darcy-Weisbach (Leopold, Wolman and Miller)			3.80	ft / sec	19.2 cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)				ft / sec	cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge	a) Regional Curves $u = Q / A$ Q = _____ year			ft / sec	cfs
4. Continuity Equations: b) USGS Gage Data	b) USGS Gage Data $u = Q / A$			ft / sec	cfs
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation (R/ $D_{84}$ ) – Estimation Method 1					
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.					
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.					
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.					
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.					

**Worksheet 5-3.** Level II stream classification.

Stream: <b>West Monument A4/2 Reference</b>	
Basin:	Drainage Area: <b>7011</b> acres <b>10.95</b> mi <sup>2</sup>
Location: <b>Pike National Forest, Colorado</b>	
Twp.&Rge:	Sec.&Qtr.:
Cross-Section Monuments (Lat./Long.): <b>XS 2+83</b> Date: <b>11/06/2012</b>	
Observers: <b>Lee, Sumner, Jara, Leah</b>	Valley Type: <b>VIIIb</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>7.03</b> ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A_{bkf} / W_{bkf}$ ).	<b>0.72</b> ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>5.04</b> ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>9.76</b> ft/ft
<b>Maximum DEPTH (<math>d_{max}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>1.39</b> ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>16.64</b> ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>2.37</b> ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the median or dominant diameter of channel materials, as sampled proportionately from the channel surface, between the bankfull stage and Thalweg elevations.	<b>10.48</b> mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.08113</b> ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope ( $S_{val} / S$ ).	<b>1.05</b>

<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>Stream Type</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: #e0f0ff;"> <b>A4/2</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>See Classification Key (Figure 2-14)</b> </div>
---	---	--

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>West Monument A4/2 Reference</b>		Location: <b>Pike National Forest, Colorado</b>							
Observers: <b>Lee, Sumner, Jara, Leah</b>		Date: <b>11/06/12</b>		Valley Type: <b>VIIIb</b>		Stream Type: <b>A4/2</b>			
<b>River Reach Dimension Summary Data....1</b>									
<b>Riffle Dimensions*, **, ***</b>	<b>Riffle Dimensions* ** , ***</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Width ( $W_{bkt}$ )	5.7	4.5	7.0	ft	Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	4.8	4.5	5.0
	Mean Riffle Depth ( $d_{bkt}$ )	0.87	0.72	1.01	ft	Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	7.1	4.4	9.8
	Maximum Riffle Depth ( $d_{max}$ )	1.37	1.34	1.39	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	1.629	1.327	1.931
	Width of Flood-Prone Area ( $W_{fpa}$ )	14.4	12.2	16.6	ft	Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )	2.6	2.4	2.7
	Riffle Inner Berm Width ( $W_{ib}$ )				ft	Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )			
	Riffle Inner Berm Depth ( $d_{ib}$ )				ft	Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )			
	Riffle Inner Berm Area ( $A_{ib}$ )				ft <sup>2</sup>	Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )			
Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )									
<b>Pool Dimensions* ** , ***</b>	<b>Pool Dimensions* ** , ***</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Pool Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Pool Width ( $W_{bkfp}$ )	7.4	6.8	8.1	ft	Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )	1.296	1.188	1.404
	Mean Pool Depth ( $d_{bkfp}$ )	1.29	1.26	1.32	ft	Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )	1.483	1.448	1.517
	Pool Cross-Sectional Area ( $A_{bkfp}$ )	9.6	8.6	10.7	ft	Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )	2.019	1.801	2.243
	Maximum Pool Depth ( $d_{maxp}$ )	1.94	1.72	2.15	ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	2.230	1.977	2.471
	Pool Inner Berm Width ( $W_{ibp}$ )				ft	Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )			
	Pool Inner Berm Depth ( $d_{ibp}$ )				ft	Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )			
	Pool Inner Berm Area ( $A_{ibp}$ )				ft <sup>2</sup>	Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )			
Point Bar Slope ( $S_{pb}$ )				ft/ft	Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )				
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Run Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Run Width ( $W_{bkfr}$ )				ft	Run Width to Riffle Width ( $W_{bkfr} / W_{bkt}$ )			
	Mean Run Depth ( $d_{bkfr}$ )				ft	Mean Run Depth to Mean Riffle Depth ( $d_{bkfr} / d_{bkt}$ )			
	Run Cross-Sectional Area ( $A_{bkfr}$ )				ft	Run Area to Riffle Area ( $A_{bkfr} / A_{bkt}$ )			
	Maximum Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )			
Run Width/Depth Ratio ( $W_{bkfr} / d_{bkfr}$ )				ft					
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Glide Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Glide Width ( $W_{bkfg}$ )				ft	Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )			
	Mean Glide Depth ( $d_{bkfg}$ )				ft	Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )			
	Glide Cross-Sectional Area ( $A_{bkfg}$ )				ft	Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )			
	Maximum Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )			
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )				ft/ft	Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )			
	Glide Inner Berm Width ( $W_{ibg}$ )				ft	Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )			
	Glide Inner Berm Depth ( $d_{ibg}$ )				ft	Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )			
Glide Inner Berm Area ( $A_{ibg}$ )				ft <sup>2</sup>	Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )				
<b>Step**</b>	<b>Step Dimensions**</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Step Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Step Width ( $W_{bkfs}$ )				ft	Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )			
	Mean Step Depth ( $d_{bkfs}$ )				ft	Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )			
	Step Cross-Sectional Area ( $A_{bkfs}$ )				ft	Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )			
	Maximum Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )									

**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>West Monument A4/2 Reference</b>		Location: <b>Pike National Forest, Colorado</b>								
Observers: <b>Lee, Sumner, Jara, Leah</b>		Date: <b>11/6/2012</b>		Valley Type: <b>VIIIb</b>		Stream Type: <b>A4/2</b>				
<b>River Reach Summary Data.....2</b>										
<b>Hydraulics</b>	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )		<b>2.31</b> ft/sec		Estimation Method		<b>Friction Factor</b>			
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )		<b>11.64</b> cfs		Drainage Area		<b>10.95</b> mi <sup>2</sup>			
<b>Channel Pattern</b>	<b>Geometry</b>			<b>Dimensionless Geometry Ratios</b>						
	Linear Wavelength ( $\lambda$ )			ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )					
	Stream Meander Length ( $L_m$ )			ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )					
	Radius of Curvature ( $R_c$ )			ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )					
	Belt Width ( $W_{bit}$ )	<b>14.4</b>	<b>12.5</b>	<b>18.1</b>	ft	Meander Width Ratio ( $W_{bit} / W_{bkt}$ )	<b>2.51</b>	<b>2.18</b>	<b>3.15</b>	
	Arc Length ( $L_a$ )				ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )				
	Riffle Length ( $L_r$ )	<b>6.6</b>	<b>4.5</b>	<b>8.7</b>	ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )	<b>1.15</b>	<b>0.78</b>	<b>1.52</b>	
	Individual Pool Length ( $L_p$ )	<b>6.7</b>	<b>3.6</b>	<b>9.2</b>	ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )	<b>1.16</b>	<b>0.62</b>	<b>1.60</b>	
Pool to Pool Spacing ( $P_s$ )	<b>16.0</b>	<b>8.7</b>	<b>26.5</b>	ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )	<b>2.79</b>	<b>1.51</b>	<b>4.62</b>		
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )	<b>0.0852</b>		ft/ft	Average Water Surface Slope ( $S$ )	<b>0.0811</b>		ft/ft	Sinuosity ( $S_{val} / S$ )	<b>1.05</b>
	Stream Length (SL)	<b>172.0</b>		ft	Valley Length (VL)	<b>141.0</b>		ft	Sinuosity (SL / VL)	<b>1.23</b>
	Low Bank Height (LBH)	start: <b>1.58</b> ft end: <b>2.77</b> ft			Max Bankfull Depth ( $d_{max}$ )	start: <b>1.35</b> ft end: <b>1.97</b> ft			Bank-Height Ratio (BHR) ( $LBH / d_{max}$ )	start: <b>1.2</b> end: <b>1.4</b>
	<b>Facet Slopes</b>			<b>Dimensionless Facet Slope Ratios</b>						
	Riffle Slope ( $S_{rif}$ )	<b>0.1180</b>	<b>0.0870</b>	<b>0.1490</b>	ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.4545</b>	<b>1.0724</b>	<b>1.8366</b>	
	Run Slope ( $S_{run}$ )				ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )	<b>0.0080</b>	<b>0.0000</b>	<b>0.0200</b>	ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )	<b>0.0986</b>	<b>0.0000</b>	<b>0.2465</b>	
	Glide Slope ( $S_g$ )				ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )				
	Step Slope ( $S_s$ )	<b>0.3380</b>	<b>0.2300</b>	<b>0.5110</b>	ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )	<b>4.1662</b>	<b>2.8350</b>	<b>6.2985</b>	
	<b>Max Depths<sup>a</sup></b>			<b>Dimensionless Depth Ratios</b>						
	Max Riffle Depth ( $d_{maxr}$ )	<b>2.20</b>	<b>2.16</b>	<b>2.23</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )	<b>2.529</b>	<b>2.483</b>	<b>2.563</b>	
	Max Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )	<b>2.34</b>	<b>2.01</b>	<b>2.75</b>	ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	<b>2.690</b>	<b>2.310</b>	<b>3.161</b>	
	Max Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )				
Max Step Depth ( $d_{maxs}$ )	<b>2.12</b>	<b>1.97</b>	<b>2.33</b>	ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )	<b>2.437</b>	<b>2.264</b>	<b>2.678</b>		
<b>Channel Materials</b>		<b>Reach<sup>b</sup></b>	<b>Riffle<sup>c</sup></b>	<b>Bar</b>		<b>Reach<sup>b</sup></b>	<b>Riffle<sup>c</sup></b>	<b>Bar</b>	<b>Protrusion Height<sup>d</sup></b>	
	% Silt/Clay	<b>3.88</b>	<b>0.00</b>		$D_{16}$	<b>3.37</b>	<b>7.26</b>		mm	
	% Sand	<b>6.80</b>	<b>1.02</b>		$D_{35}$	<b>7.59</b>	<b>32.56</b>		mm	
	% Gravel	<b>58.25</b>	<b>51.02</b>		$D_{50}$	<b>10.48</b>	<b>60.20</b>		mm	
	% Cobble	<b>10.68</b>	<b>35.72</b>		$D_{84}$	<b>6.44</b>	<b>224.91</b>		mm	
	% Boulder	<b>14.56</b>	<b>12.24</b>		$D_{95}$	<b>Bedrock</b>	<b>870.07</b>		mm	
	% Bedrock	<b>5.83</b>	<b>0.00</b>		$D_{100}$	<b>Bedrock</b>	<b>2047.97</b>		mm	

## Stability Indices

**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation					
Stream: <b>West Monument A4/2 Reference</b>		Location: <b>Pike National Forest, Colorado</b>			
Observers: <b>Lee, Sumner, Jara, Leah</b>		Reference reach <input checked="" type="checkbox"/>	Disturbed (impacted reach) <input type="checkbox"/>	Date: <b>11/06/2012</b>	
Existing species composition: <b>Aspen, Spruce, Ponderosa, Willow, Choke Cheery, Dogwood, rose, grass, forb</b>		Potential species composition: <b>Species at Potential</b>			
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition
<b>1. Overstory</b>	Canopy layer	<b>45%</b>	<b>45%</b>	<b>Aspen</b>	<b>45%</b>
				<b>spruce</b>	<b>50%</b>
				<b>ponderosa</b>	<b>5%</b>
					<b>0%</b>
					<b>0%</b>
					<b>100%</b>
<b>2. Understory</b>	Shrub layer	<b>30%</b>	<b>30%</b>	<b>willow</b>	<b>80%</b>
				<b>choke cherry</b>	<b>10%</b>
				<b>dogwood</b>	<b>2%</b>
				<b>rose</b>	<b>8%</b>
					<b>0%</b>
					<b>100%</b>
<b>3. Ground level</b>	Herbaceous	<b>10%</b>	<b>10%</b>	<b>Grass</b>	<b>50%</b>
				<b>forbes</b>	<b>50%</b>
					<b>0%</b>
					<b>0%</b>
					<b>0%</b>
					<b>100%</b>
	Leaf or needle litter	<b>5%</b>		<b>Remarks:</b> Condition, vigor and/or usage of existing reach: <b>vigorous riparian vegetation density</b>	
	Bare ground	<b>10%</b>			
					<b>Column Total = 100%</b>


\*Based on crown closure.

\*\*Based on basal area to surface area.

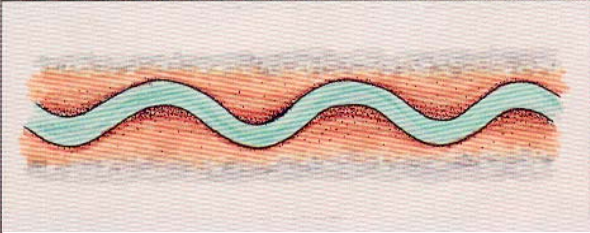

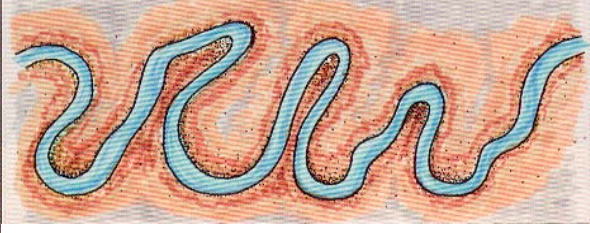
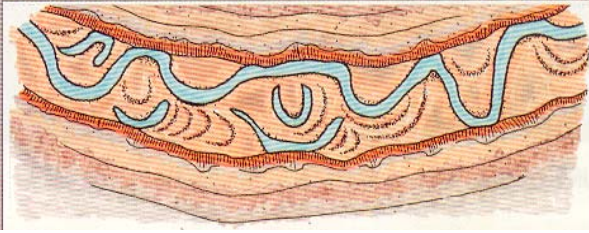
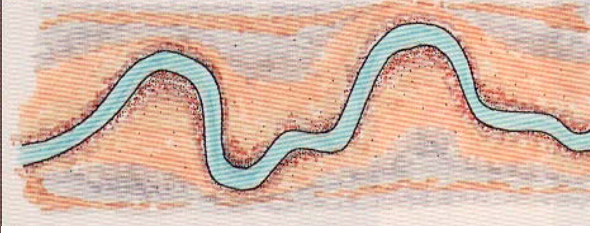
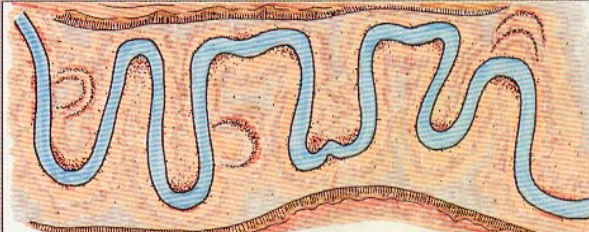
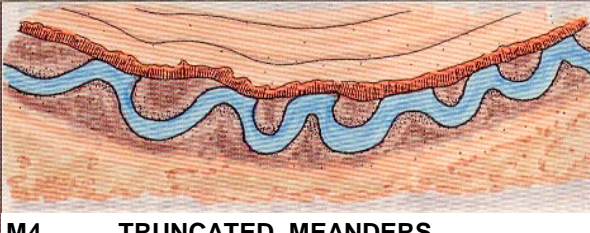
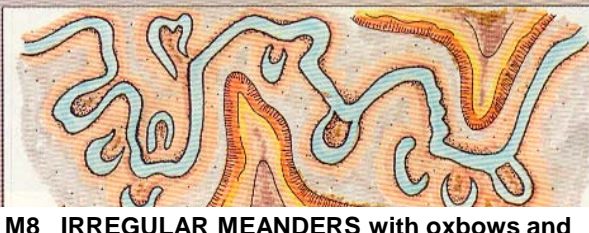
**Worksheet 5-7.** Flow regime.

<b>FLOW REGIME</b>								
Stream: <b>West Monument A4/2 Reference</b> Location: <b>Pike National Forest, Colorado</b>								
Observers: <b>Lee, Sumner, Jara, Leah</b>						Date: <b>11/6/2012</b>		
<b>List ALL COMBINATIONS that APPLY.....</b>	<b>P1</b>	<b>P2</b>	<b>P7</b>	<b>P8</b>				
<b>General Category</b>								
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation							
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
<b>P</b>	Perennial stream channels: Surface water persists yearlong.							
<b>Specific Category</b>								
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
<b>4</b>	Streamflow regulated by glacial melt.							
<b>5</b>	Ice flows/ice torrents from ice dam breaches.							
<b>6</b>	Alternating flow/backwater due to tidal influence.							
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.							
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
<b>9</b>	Rain-on-snow generated runoff.							

**Worksheet 5-8.** Stream order & stream size.

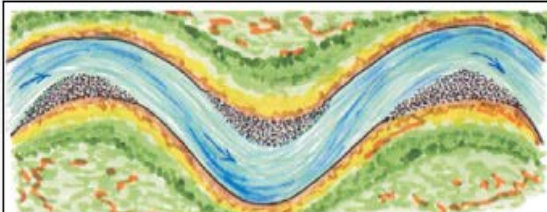


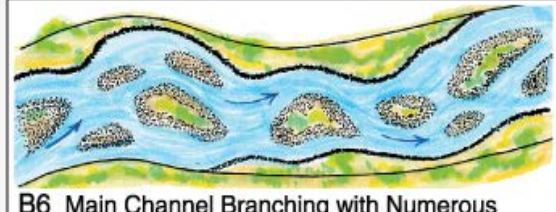

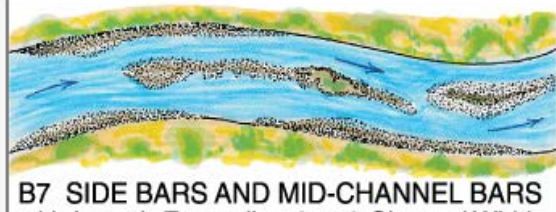

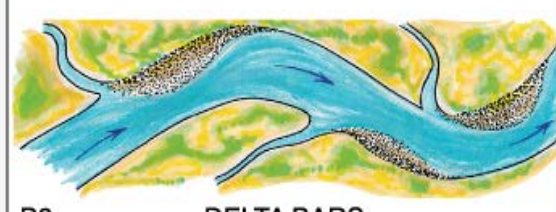
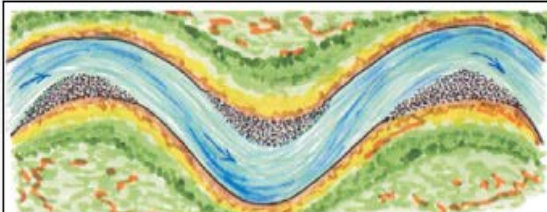


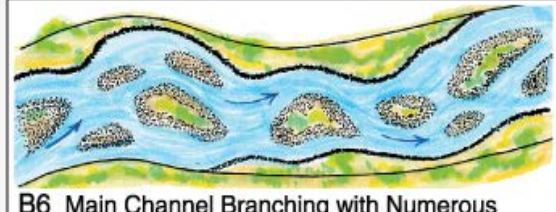

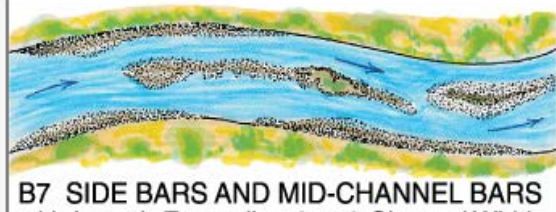

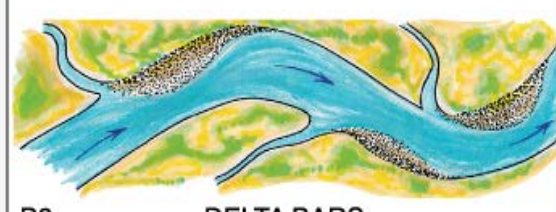
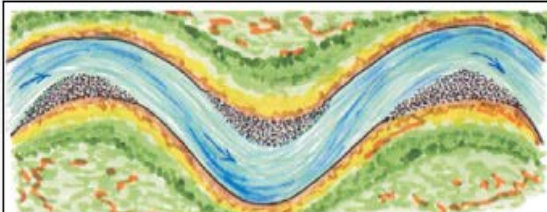


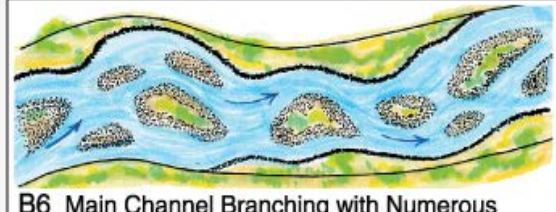

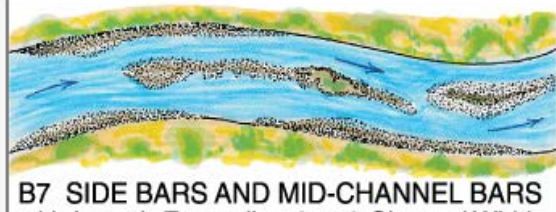

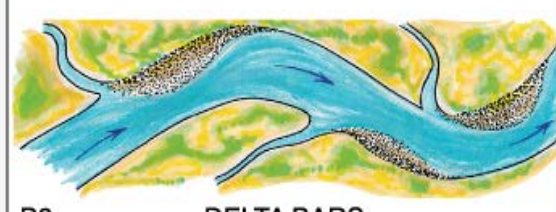
<b>Stream Size and Order</b>			
Stream:	<b>West Monument A4/2 Reference</b>		
Location:	<b>Pike National Forest, Colorado</b>		
Observers:	<b>Lee, Sumner, Jara, Leah</b>		
Date:	<b>11/6/2012</b>		
<b>Stream Size Category and Order</b> 			<b>S-3(4)</b>
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0.305	<1	<input type="checkbox"/>
S-2	0.3 – 1.5	1 – 5	<input type="checkbox"/>
<b>S-3</b>	<b>1.5 – 4.6</b>	<b>5 – 15</b>	<input checked="" type="checkbox"/>
S-4	4.6 – 9	15 – 30	<input type="checkbox"/>
S-5	9 – 15	30 – 50	<input type="checkbox"/>
S-6	15 – 22.8	50 – 75	<input type="checkbox"/>
S-7	22.8 – 30.5	75 – 100	<input type="checkbox"/>
S-8	30.5 – 46	100 – 150	<input type="checkbox"/>
S-9	46 – 76	150 – 250	<input type="checkbox"/>
S-10	76 – 107	250 – 350	<input type="checkbox"/>
S-11	107 – 150	350 – 500	<input type="checkbox"/>
S-12	150 – 305	500 – 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
<b>Stream Order</b>			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			

**Worksheet 5-9.** Meander patterns.

<b>Meander Patterns</b>					
Stream: <b>West Monument A4/2 Reference</b>			Location: <b>Pike National Forest, CO</b>		
Observers: <b>Lee, Sumner, Jara, Leah</b>			Date: <b>11/6/2012</b>		
List ALL CATEGORIES that APPLY ↩		N/A			
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>					
 <b>M1</b> <b>REGULAR MEANDERS</b>	 <b>M5</b> <b>UNCONFINED MEANDER SCROLLS</b>				
 <b>M2</b> <b>TORTUOUS MEANDERS</b>	 <b>M6</b> <b>CONFINED MEANDER SCROLLS</b>				
 <b>M3</b> <b>IRREGULAR MEANDERS</b>	 <b>M7</b> <b>DISTORTED MEANDER LOOPS</b>				
 <b>M4</b> <b>TRUNCATED MEANDERS</b>	 <b>M8</b> <b>IRREGULAR MEANDERS with oxbows and oxbow cutoffs</b>				



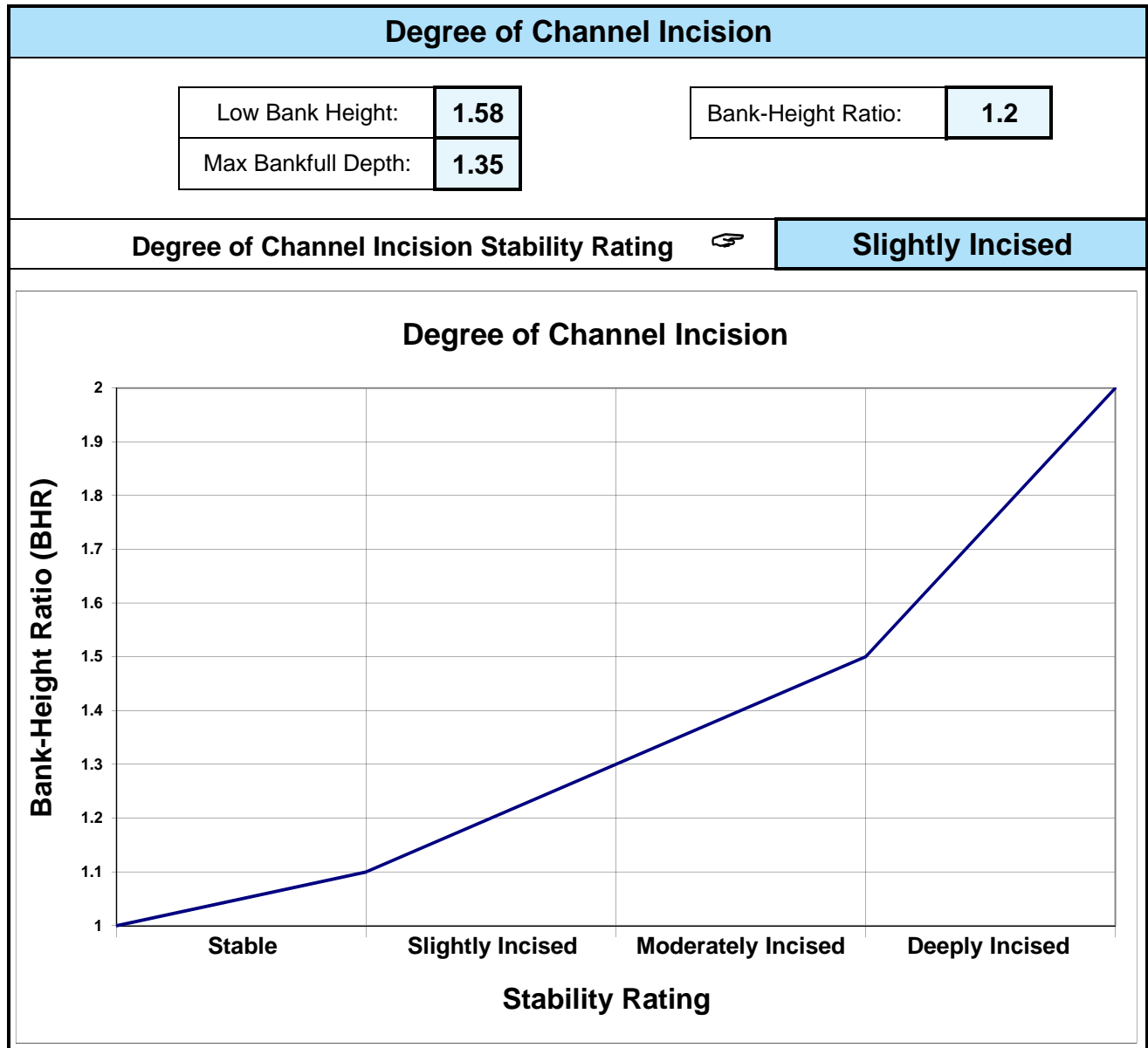
**Worksheet 5-10.** Depositional patterns.

<b>Depositional Patterns</b>													
Stream:	<b>West Monument A4/2 Reference</b>	Location:	<b>Pike National Forest, CO</b>										
Observers:	<b>Lee, Sumner, Jara, Leah</b>	Date:	<b>11/6/2012</b>										
List ALL CATEGORIES that APPLY	<b>NA</b>												
<i>Various Depositional Features modified from Galay et al. (1973)</i>													
<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 50%; padding: 5px; vertical-align: top;">  <p style="text-align: center;"><b>B1 POINT BARS</b></p> </td> <td style="width: 50%; padding: 5px; vertical-align: top;">  <p style="text-align: center;"><b>B5 DIAGONAL BARS</b></p> </td> </tr> <tr> <td style="padding: 5px; vertical-align: top;">  <p style="text-align: center;"><b>B2 POINT BARS with Few MID-CHANNEL BARS</b></p> </td> <td style="padding: 5px; vertical-align: top;">  <p style="text-align: center;"><b>B6 Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</b></p> </td> </tr> <tr> <td style="padding: 5px; vertical-align: top;">  <p style="text-align: center;"><b>B3 NUMEROUS MID-CHANNEL BARS</b></p> </td> <td style="padding: 5px; vertical-align: top;">  <p style="text-align: center;"><b>B7 SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</b></p> </td> </tr> <tr> <td style="padding: 5px; vertical-align: top;">  <p style="text-align: center;"><b>B4 SIDE BARS</b></p> </td> <td style="padding: 5px; vertical-align: top;">  <p style="text-align: center;"><b>B8 DELTA BARS</b></p> </td> </tr> </table>						 <p style="text-align: center;"><b>B1 POINT BARS</b></p>	 <p style="text-align: center;"><b>B5 DIAGONAL BARS</b></p>	 <p style="text-align: center;"><b>B2 POINT BARS with Few MID-CHANNEL BARS</b></p>	 <p style="text-align: center;"><b>B6 Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</b></p>	 <p style="text-align: center;"><b>B3 NUMEROUS MID-CHANNEL BARS</b></p>	 <p style="text-align: center;"><b>B7 SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</b></p>	 <p style="text-align: center;"><b>B4 SIDE BARS</b></p>	 <p style="text-align: center;"><b>B8 DELTA BARS</b></p>
 <p style="text-align: center;"><b>B1 POINT BARS</b></p>	 <p style="text-align: center;"><b>B5 DIAGONAL BARS</b></p>												
 <p style="text-align: center;"><b>B2 POINT BARS with Few MID-CHANNEL BARS</b></p>	 <p style="text-align: center;"><b>B6 Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</b></p>												
 <p style="text-align: center;"><b>B3 NUMEROUS MID-CHANNEL BARS</b></p>	 <p style="text-align: center;"><b>B7 SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</b></p>												
 <p style="text-align: center;"><b>B4 SIDE BARS</b></p>	 <p style="text-align: center;"><b>B8 DELTA BARS</b></p>												

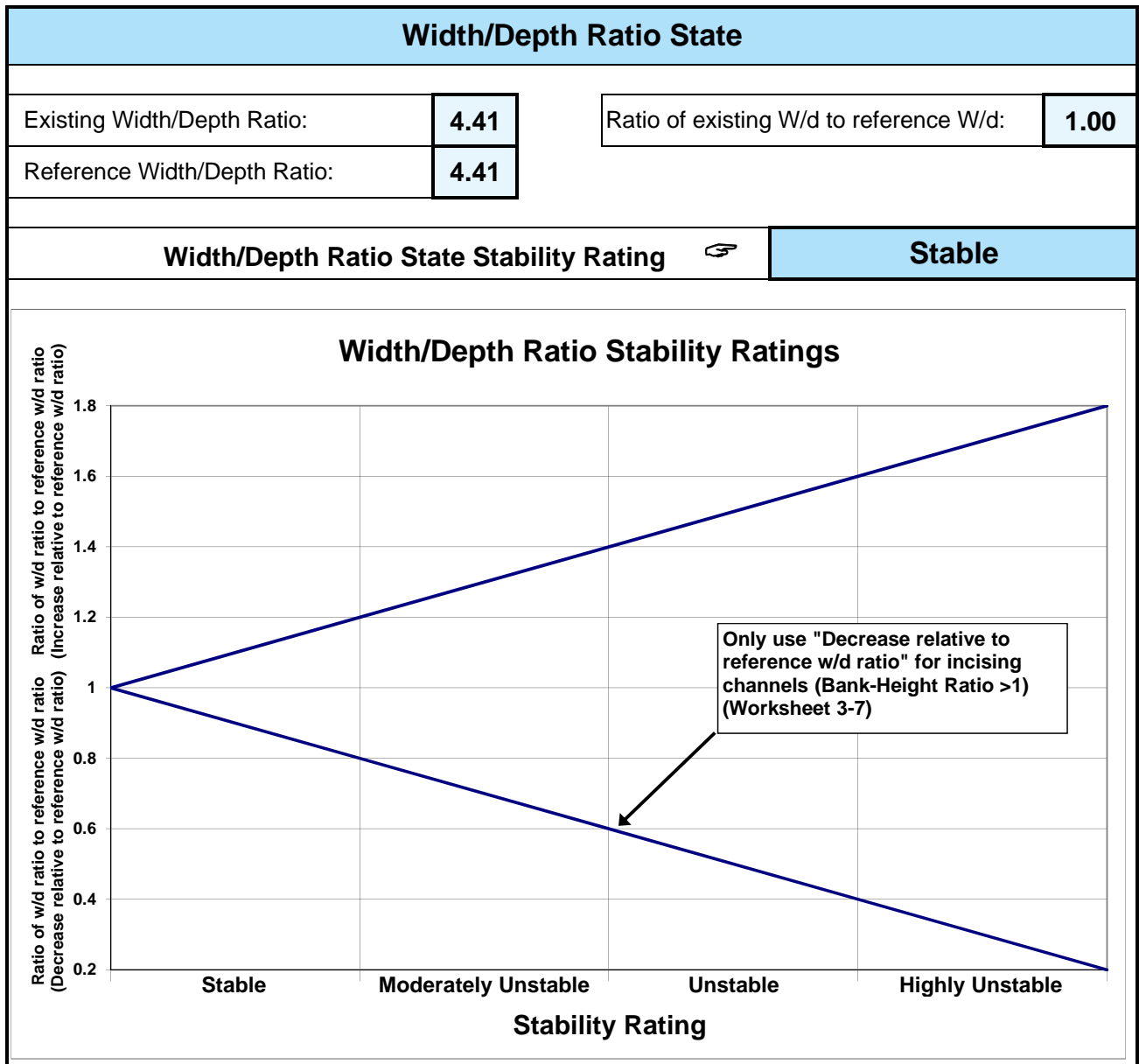
**Worksheet 5-11.** Channel blockages.

Channel Blockages		
Stream: <b>West Monument A4/2 Reference</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>Lee, Sumner, Jara, Leah</b>		Date: <b>11/6/2012</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input checked="" type="checkbox"/>
<b>D4</b> Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

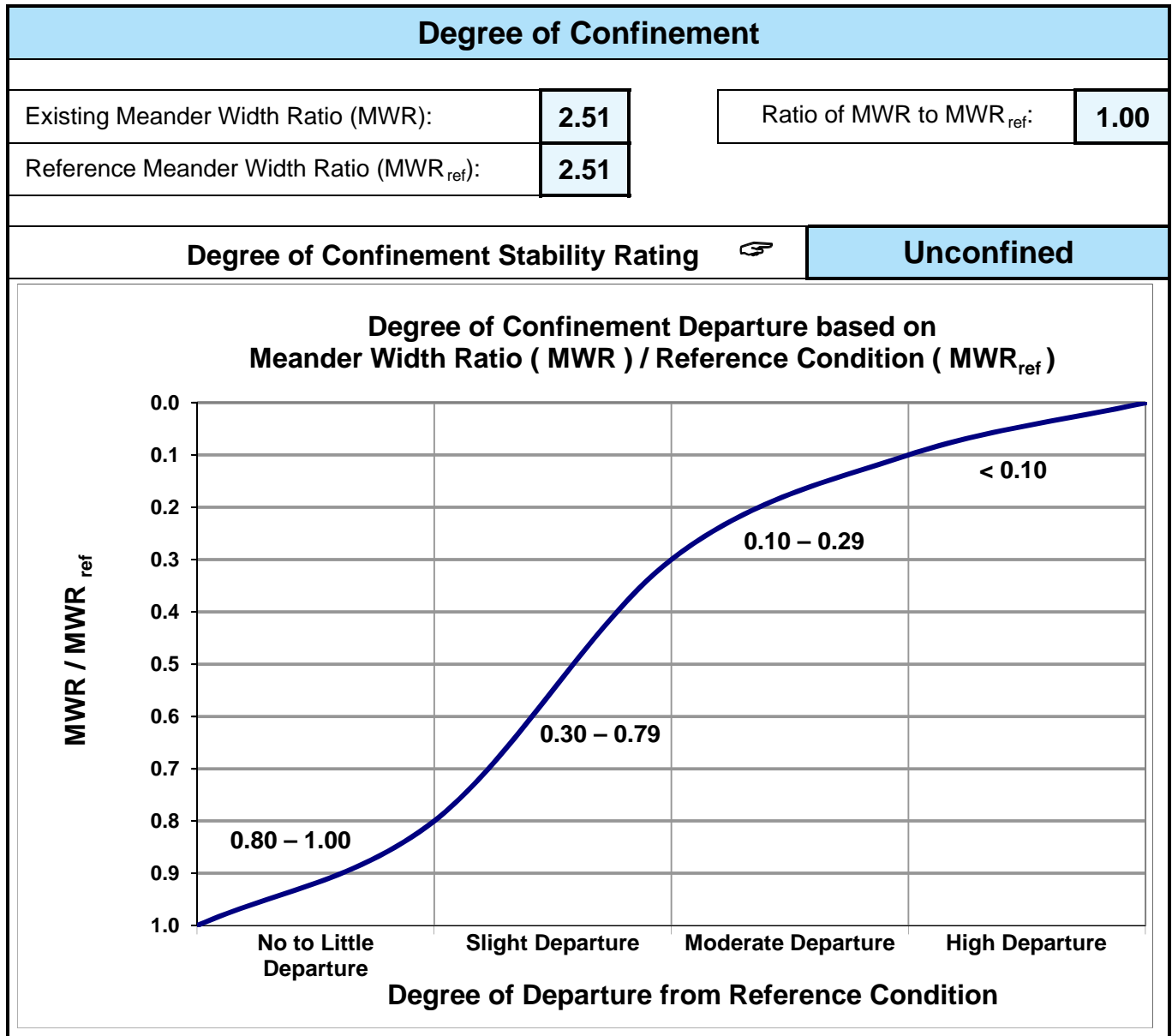
**Worksheet 5-12.** Degree of channel incision.



**Worksheet 5-13.** Width/depth ratio state.



**Worksheet 5-14.** Degree of channel confinement (lateral containment).



Worksheet 5-15. Pfrankuch channel stability rating.

Stream: West Monument A/2		Location: Pike National Forest, CO		Valley Type: VIIIb		Observers: Lee, Summer, Jara, Leah		Date: 11/8/2012																
Loca-tion	Key	Category	Excellent	Good	Fair	Poor	Rating	Description	Rating															
Upper banks	1	Landform slope	Bank slope gradient <30%.	Bank slope gradient 30-40%.	Bank slope gradient 40-60%.	Bank slope gradient > 60%.	4	Bank slope gradient 30-40%.	6	Bank slope gradient > 60%.														
	2	Mass erosion	No evidence of past or future mass erosion.	Infrequent. Mostly healed over. Low future potential.	Frequent or large, causing sediment nearly yearlong.	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.	3	Infrequent. Mostly healed over. Low future potential.	9	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.														
	3	Debris jam potential	Essentially absent from immediate channel area.	Present, but mostly small twigs and limbs.	Moderate to heavy amounts, mostly larger sizes.	Moderate to heavy amounts, predominantly larger sizes.	2	Present, but mostly small twigs and limbs.	4	Moderate to heavy amounts, predominantly larger sizes.														
	4	Vegetative bank protection	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	70-90% density. Fewer species or less vigor suggest less dense or deep root mass.	50-70% density. Lower vigor and fewer species from a shallow, discontinuous root mass.	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.	3	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	6	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.														
Lower banks	5	Channel capacity	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0.	Bankfull stage is contained within banks. Width/depth ratio departure from reference width/depth ratio = 1.0-1.2. Bank-Height Ratio (BHR) = 1.0-1.1.	Bankfull stage is not contained. Width/depth ratio departure from reference width/depth ratio = 1.1-1.3. Bank-Height Ratio (BHR) = 1.1-1.3.	Bankfull stage is not contained; over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.	1	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0.	2	Bankfull stage is not contained; over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.														
	6	Bank rock content	> 65% with large angular boulders. 12"+ common.	40-65%. Mostly boulders and small cobbles 6-12".	20-40%. Most in the 3-6" diameter class.	<20% rock fragments of gravel sizes, 1-3" or less.	2	> 65% with large angular boulders. 12"+ common.	4	20-40%. Most in the 3-6" diameter class.														
	7	Obstructions to flow	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	Frequent obstructions and deflectors cause bank erosion yearlong. Sediment traps full, channel migration occurring.	2	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	4	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.														
	8	Cutting	Little or none. Infrequent raw banks <6".	Some, intermittently at outcurves and constrictions. Raw banks may be up to 12".	Significant. Cuts 12-24" high. Root mat overhangs and sloughing evident.	Almost continuous cuts, some over 24" high. Failure of overhangs frequent.	4	Little or none. Infrequent raw banks <6".	9	Significant. Cuts 12-24" high. Root mat overhangs and sloughing evident.														
Bottom	9	Deposition	Little or no enlargement of channel or point bars.	Some new bar increase, mostly from coarse gravel.	Moderate deposition of new gravel and coarse sand on old and some new bars.	Extensive deposit of predominantly fine particles. Accelerated bar development.	4	Little or no enlargement of channel or point bars.	4	Extensive deposit of predominantly fine particles. Accelerated bar development.														
	10	Rock angularity	Sharp edges and corners. Plane surfaces rough.	Rounded corners and edges. Surfaces smooth and flat.	Comers and edges well rounded in 2 dimensions.	Well rounded in all dimensions, surfaces smooth.	1	Sharp edges and corners. Plane surfaces rough.	1	Rounded corners and edges. Surfaces smooth and flat.														
	11	Brightness	Surfaces dull, dark or stained. Generally not bright.	Mostly dull, but may have <35% bright surfaces.	Mixture dull and bright, i.e., 35-65% mixture range.	Predominantly bright, > 65%, exposed or scoured surfaces.	1	Surfaces dull, dark or stained. Generally not bright.	2	Mixture dull and bright, i.e., 35-65% mixture range.														
	12	Consolidation of particles	Assorted sizes tightly packed or overlapping.	Moderately packed with some overlapping.	Mostly loose assortment with no apparent overlap.	No packing evident. Loose assortment, easily moved.	2	Assorted sizes tightly packed or overlapping.	4	Mostly loose assortment with no apparent overlap.														
Stream type	A1	A2	A3	A4	A5	A6	B1	B2	B3	B4	B5	B6	C1	C2	C3	C4	C5	C6	D3	D4	D5	D6	Grand total =	
	38-43	38-43	54-90	60-95	50-80	50-80	38-45	38-45	40-60	40-64	48-68	40-60	38-50	38-50	60-85	70-90	70-90	60-85	85-107	85-107	85-107	85-107	67-98	74
	44-47	44-47	91-125	96-132	81-110	81-110	46-58	46-58	61-78	65-84	69-88	61-78	51-61	51-61	86-105	91-110	91-110	86-105	108-132	108-132	108-132	108-132	99-125	A2/4
48+	48+	130+	133+	111+	111+	59+	59+	79+	85+	89+	79+	62+	62+	106+	111+	111+	106+	133+	133+	133+	133+	126+	A2/4	
DA3	DA4	DA5	DA6	E3	E4	E5	E6	F1	F2	F3	F4	F5	F6	G1	G2	G3	G4	G5	G6					
40-63	40-63	40-63	40-63	50-75	50-75	40-63	40-63	60-85	60-85	85-110	85-110	90-115	80-95	80-95	40-60	40-60	85-107	90-112	90-112	85-107	85-107	85-107	108-120	A2/4
64-86	64-86	64-86	64-86	76-96	76-96	64-86	64-86	86-105	86-105	111-125	111-125	116-130	96-110	96-110	61-78	108-120	108-120	113-125	108-120	108-120	108-120	108-120	121+	A2/4
87+	87+	87+	87+	97+	97+	87+	87+	106+	106+	126+	126+	131+	111+	111+	79+	79+	121+	121+	126+	126+	126+	126+	121+	Good
Excellent total =			13			Good total =			44			Fair total =			17			Poor total =			0			

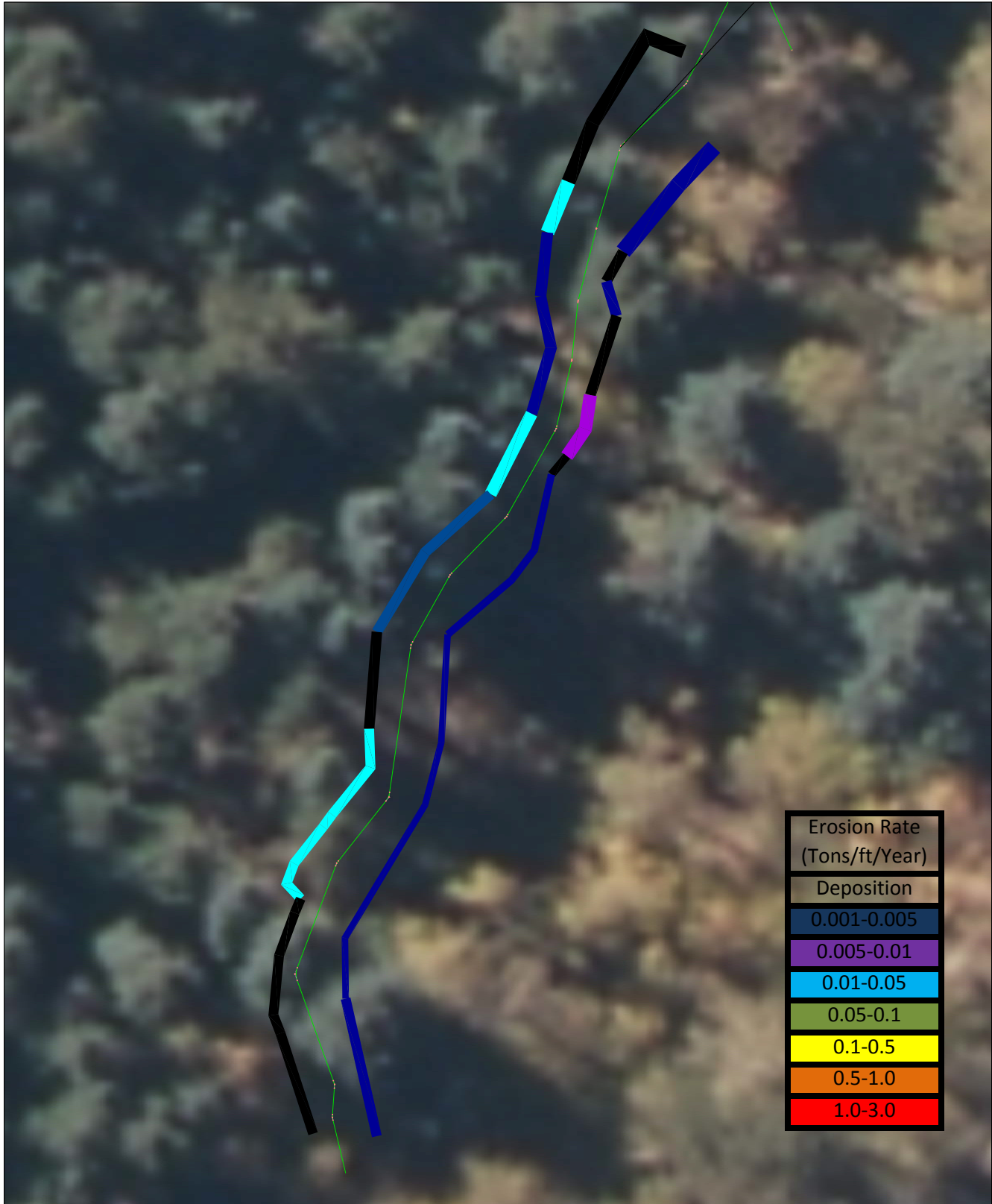
\*Rating is adjusted to potential stream type, not existing.

## BANCS Model – Streambank Erosion

**Worksheet 5-18.** Annual streambank erosion estimates.

Stream: <b>West Monument Creek A4/2 Reference</b>		Location: <b>A4/2 Reference</b>					
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>174</b>				Date: <b>11/6/2012</b>	
Observers: <b>Lee, Sumner, Jara, Leah</b>		Valley Type: <b>VIIIb</b>			Stream Type: <b>A4/2</b>		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 3-11) (adjective)	NBS rating (Worksheet 3-12) (adjective)	Bank erosion rate (Figure 3-9 or 3-10) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [[ $(4) \times (5) \times (6)$ ] (ft <sup>3</sup> /yr)	Erosion Rate {[( $7$ )/ $27$ ] $\times$ $1.3 / (5)$ }
1. R115-123	Very Low	High	0.021	8.0	1.5	0.26	0.00150
2. R128-154	Very Low	High	0.021	26.0	1.7	0.94	0.00170
3. R171-178	Low	Very High	0.323	7.0	1.7	3.84	0.02640
4. R178-183	Low	Low	0.036	5.0	1.4	0.24	0.00230
5. R183-201	Low	Low	0.036	18.0	1.4	0.87	0.00230
6. R201-212	Low	High	0.151	20.0	1.5	4.53	0.01090
7. R212-232	Very Low	Very High	0.050	12.0	1.3	0.78	0.00310
8. R244-266	Low	Very High	0.323	22.0	1.2	8.53	0.01870
9. L289-277	Low	Moderate	0.073	12.0	1.2	1.04	0.00420
10. L229-251	Very Low	Low	0.004	22.0	0.8	0.07	0.00015
11. L207-216	Very Low	High	0.021	9.0	0.9	0.17	0.00090
12. L196-203	Low	Moderate	0.072	7.0	1.6	0.81	0.00560
13. L182-186	Low	Low	0.036	4.0	1.3	0.19	0.00220
14. L161-177	Low	Low	0.036	16.0	2.0	1.12	0.00340
15. L144-154	Low	Very High	0.323	10.0	1.3	4.20	0.02020
16. L134-144	Very Low	Low	0.004	10.0	0.9	0.03	0.00020
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					Total Erosion (ft <sup>3</sup> /yr)	<b>27.63</b>	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					Total Erosion (yds <sup>3</sup> /yr)	<b>1.02</b>	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					Total Erosion (tons/yr)	<b>1.33</b>	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					Unit Erosion Rate (tons/yr/ft)	<b>0.0076</b>	

### Streambank Erosion Map



Waldo Canyon Fire WARSSS  
Typical Reach



Wildland Hydrology  
11210 North County Road 19  
Fort Collins, CO  
80524  
Tel. 970-568-0002  
Fax. 970.568.0014



# FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Equation type		Intercept	Coefficient	Exponent	Form (e.g., linear, non-linear, etc.)		Equation name		Bankfull discharge (cfs)	Bankfull bedload (kg/s)	Bankfull suspended (mg/l)			
1. Bedload (dimensionless)		-0.0113	1.0139	2.1929	Non-Linear		Pagosa Springs Reference Curve		9.19	0.0163	23.015			
2. Suspended sediment (dimensionless)		0.0636	0.9326	2.4085	Non-Linear		Pagosa Springs Reference Curve							
Notes:														
3. User-defined relations (bedload)														
4. User-defined relations (suspended sediment)														
From dimensioned flow-duration curve														
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Flow exceedence	Daily mean discharge (cfs)	Mid-ordinate (%)	Time increment (percent)	Time increment (days)	Mid-ordinate streamflow (cfs)	Dimensionless streamflow (Q/Q <sub>med</sub> )	Dimensionless suspended sediment discharge (S/S <sub>med</sub> )	Suspended sediment discharge (tons/day)	Dimensionless bedload discharge (b <sub>d</sub> /b <sub>med</sub> )	Bedload (tons/day)	Time adjusted streamflow (cfs)	Suspended sediment bedload [(5)×(9)] (tons)	Bedload sediment bedload [(5)×(11)] (tons)	Suspended + bedload [(13)+(14)] (tons)
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>med</sub> )	(S/S <sub>med</sub> )	(tons/day)	(b <sub>d</sub> /b <sub>med</sub> )	(tons/day)	(cfs)	(tons)	(tons)	(tons)
100.000	0.1													
90.000	0.3	95.00	10.00	36.50	0.2	0.02	1.7	0.0	0.0002	0.00	1.80	0.00	0.00	0.00
80.000	0.4	85.00	10.00	36.50	0.4	0.04	2.4	0.0	0.0017	0.00	3.60	0.00	0.00	0.00
70.000	0.5	75.00	10.00	36.50	0.5	0.05	3.1	0.0	0.0031	0.00	4.60	0.00	0.00	0.00
60.000	0.6	65.00	10.00	36.50	0.6	0.06	4.0	0.0	0.0047	0.00	5.50	0.00	0.00	0.00
50.000	0.8	55.00	10.00	36.50	0.7	0.08	5.9	0.0	0.0083	0.00	7.00	0.00	0.00	0.00
40.000	1.0	45.00	10.00	36.50	0.9	0.10	9.8	0.0	0.0151	0.00	9.10	0.00	0.00	0.00
30.000	1.5	35.00	10.00	36.50	1.3	0.14	19.4	0.0	0.0305	0.00	12.50	0.36	0.00	0.36
20.000	2.2	25.00	10.00	36.50	1.8	0.20	34.8	0.0	0.0540	0.00	18.20	0.36	0.00	0.36
10.000	4.0	15.00	10.00	36.50	3.1	0.34	34.8	0.0	0.0540	0.09	31.00	0.73	3.28	4.01
5.000	6.4	7.50	5.00	18.25	5.2	0.57	34.8	0.1	0.0540	0.26	26.05	1.09	4.75	5.84
4.000	7.2	4.50	1.00	3.65	6.8	0.74	34.8	0.1	0.0540	0.48	6.79	0.51	1.75	2.26
3.000	8.4	3.50	1.00	3.65	7.8	0.85	34.8	0.2	0.0540	0.65	7.79	0.73	2.37	3.10
2.000	10.0	2.50	1.00	3.65	9.2	1.00	34.8	0.3	0.0540	0.91	9.19	1.24	3.32	4.56
1.500	11.4	1.75	0.50	1.83	10.7	1.17	34.8	0.6	0.0540	1.30	5.36	1.00	2.37	3.37
1.000	13.9	1.25	0.50	1.83	12.7	1.38	34.8	1.0	0.0540	1.90	6.34	1.75	3.47	5.22
0.900	14.9	0.95	0.10	0.37	14.4	1.57	34.8	1.5	0.0540	2.51	1.44	0.53	0.92	1.45
0.800	15.7	0.85	0.10	0.37	15.3	1.66	34.8	1.8	0.0540	2.85	1.53	0.65	1.04	1.69
0.700	16.6	0.75	0.10	0.37	16.1	1.76	34.8	2.1	0.0540	3.24	1.61	0.78	1.18	1.96
0.600	17.7	0.65	0.10	0.37	17.1	1.86	34.8	2.6	0.0540	3.67	1.71	0.95	1.34	2.29
0.500	18.9	0.55	0.10	0.37	18.3	1.99	34.8	3.2	0.0540	4.23	1.83	1.18	1.54	2.72
0.250	21.9	0.38	0.25	0.91	20.4	2.22	34.8	4.7	0.0540	5.40	5.09	4.24	4.93	9.17
0.100	25.3	0.18	0.15	0.55	23.6	2.56	34.8	7.6	0.0540	7.43	3.53	4.17	4.07	8.24
0.050	27.0	0.08	0.05	0.18	26.1	2.84	34.8	10.8	0.0540	9.33	1.31	1.97	1.70	3.67
0.010	29.4	0.03	0.04	0.15	28.2	3.07	34.8	14.0	0.0540	11.06	1.13	2.05	1.61	3.66
0.005	29.4	0.01	0.01	0.02	29.4	3.20	34.8	16.1	0.0540	12.10	0.15	0.29	0.22	0.51
0.001	29.4	0.00	0.00	0.01	29.4	3.20	34.8	16.1	0.0540	12.10	0.12	0.24	0.18	0.42
Annual totals:											24.8 (tons/yr)	40.0 (tons/yr)	64.8 (tons/yr)	

**Worksheet 19b.** Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Equation type	Intercept	Coefficient	Exponent	Form (e.g., linear, non-linear, etc.)	Equation name		Bankfull discharge (cfs)	Bankfull bedload (kg/s)	Bankfull suspended (mg/l)						
					Pagosa Springs Reference Curve	Pagosa Springs Reference Curve									
1. Bedload (dimensionless)	-0.0113	1.0139	2.1929	Non-Linear			9.19	0.0163	23.02						
2. Suspended sediment (dimensionless)	0.0636	0.9326	2.4085	Non-Linear											
Notes:															
3. User-defined relations (bedload)															
4. User-defined relations (suspended sediment)															
From dimensioned flow-duration curve															
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)		(9)	(10)	(11)	(12)	(13)	(14)	(15)
Flow exceedence	Daily mean discharge	Mid-ordinate	Time increment (percent)	Time increment (days)	Mid-ordinate streamflow	Dimensionless streamflow	Dimensionless suspended sediment discharge	Suspended sediment discharge	Dimensionless bedload discharge	Bedload	Time adjusted streamflow	Suspended sediment	Bedload sediment	Suspended + bedload	
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>med</sub> )	(S/S <sub>med</sub> )	(tons/day)	(b <sub>p</sub> /b <sub>med</sub> )	(tons/day)	(cfs)	(tons)	(tons)	(tons)	(tons)
100.000	0.1														
90.000	0.3	95.00	10.00	36.50	0.2	0.02	1.7	0.0	0.0002	0.00	1.80	0.00	0.00	0.00	0.00
80.000	0.4	85.00	10.00	36.50	0.4	0.04	2.4	0.0	0.0017	0.00	3.60	0.00	0.00	0.00	0.00
70.000	0.5	75.00	10.00	36.50	0.5	0.05	3.1	0.0	0.0031	0.00	4.60	0.00	0.00	0.00	0.00
60.000	0.6	65.00	10.00	36.50	0.6	0.06	4.0	0.0	0.0047	0.00	5.50	0.00	0.00	0.00	0.00
50.000	0.8	55.00	10.00	36.50	0.7	0.08	5.9	0.0	0.0083	0.00	7.00	0.00	0.00	0.00	0.00
40.000	1.0	45.00	10.00	36.50	0.9	0.10	10.0	0.0	0.0154	0.00	9.20	0.00	0.00	0.00	0.00
30.000	1.6	35.00	10.00	36.50	1.3	0.14	22.2	0.0	0.0350	0.00	13.30	0.36	0.00	0.00	0.36
20.000	3.2	25.00	10.00	36.50	2.4	0.26	34.8	0.0	0.0540	0.04	24.20	0.36	1.46	1.46	1.82
10.000	6.6	15.00	10.00	36.50	4.9	0.53	34.8	0.1	0.0540	0.22	49.10	2.19	8.03	10.22	10.22
5.000	9.8	7.50	5.00	18.25	8.2	0.89	34.8	0.2	0.0540	0.73	41.05	4.38	13.32	17.70	17.70
4.000	10.7	4.50	1.00	3.65	10.3	1.12	34.8	0.5	0.0540	1.21	10.29	1.79	4.42	6.21	6.21
3.000	12.2	3.50	1.00	3.65	11.5	1.25	34.8	0.7	0.0540	1.51	11.46	2.52	5.51	8.03	8.03
2.000	13.8	2.50	1.00	3.65	13.0	1.41	34.8	1.0	0.0540	1.99	12.98	3.80	7.26	11.06	11.06
1.500	15.3	1.75	0.50	1.83	14.6	1.58	34.8	1.5	0.0540	2.59	7.28	2.77	4.73	7.50	7.50
1.000	17.8	1.25	0.50	1.83	16.6	1.80	34.8	2.3	0.0540	3.41	8.29	4.25	6.22	10.47	10.47
0.900	18.7	0.95	0.10	0.37	18.3	1.99	34.8	3.2	0.0540	4.23	1.83	1.18	1.54	2.72	2.72
0.800	19.6	0.85	0.10	0.37	19.2	2.08	34.8	3.8	0.0540	4.71	1.92	1.38	1.72	3.10	3.10
0.700	20.4	0.75	0.10	0.37	20.0	2.18	34.8	4.4	0.0540	5.18	2.00	1.61	1.89	3.50	3.50
0.600	21.5	0.65	0.10	0.37	21.0	2.28	34.8	5.2	0.0540	5.75	2.10	1.88	2.10	3.98	3.98
0.500	22.8	0.55	0.10	0.37	22.1	2.41	34.8	6.2	0.0540	6.48	2.21	2.25	2.37	4.62	4.62
0.250	25.7	0.38	0.25	0.91	24.2	2.64	34.8	8.4	0.0540	7.91	6.06	7.66	7.22	14.88	14.88
0.100	29.1	0.18	0.15	0.55	27.4	2.99	34.8	12.8	0.0540	10.41	4.12	6.99	5.70	12.69	12.69
0.050	30.9	0.08	0.05	0.18	30.0	3.27	34.8	17.3	0.0540	12.66	1.50	3.16	2.31	5.47	5.47
0.010	33.3	0.03	0.04	0.15	32.1	3.49	34.8	21.7	0.0540	14.69	1.28	3.17	2.14	5.31	5.31
0.005	33.3	0.01	0.01	0.02	33.3	3.62	34.8	24.6	0.0540	15.90	0.17	0.45	0.29	0.74	0.74
0.001	33.3	0.00	0.00	0.01	33.3	3.62	34.8	24.6	0.0540	15.90	0.13	0.36	0.23	0.59	0.59
Annual totals:											52.5	78.5	131.0		

## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>West Mounment A4/2 Reference</b>		Stream Type: <b>A4/2</b>	
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIIb</b>	
Observers: <b>Lee, Sumner, Jara, Leah</b>		Date: <b>11/06/2012</b>	
<b>Enter Required Information for Existing Condition</b>			
10.5	$D_{50}$	Riffle bed material $D_{50}$ (mm)	
0.0	$\hat{D}_{50}$	Bar sample $D_{50}$ (mm)	
2.113	$D_{max}$	Largest particle from <b>Bed Material</b> (ft)	644 (mm) 304.8 mm/ft
0.08113	$S$	Existing bankfull water surface slope (ft/ft)	
0.72	$d$	Existing bankfull mean depth (ft)	
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment	
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>			
0.00	$D_{50}/\hat{D}_{50}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 ( D_{50}/\hat{D}_{50} )^{-0.872}$
61.45	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 ( D_{max}/D_{50} )^{-0.887}$
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED: <b>2</b>
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>			
N/A	$d$	Required bankfull mean depth (ft)	$d = \frac{\tau^* (\gamma_s - 1) D_{max}}{S}$ (use $D_{max}$ in ft)
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>			
N/A	$S$	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^* (\gamma_s - 1) D_{max}}{d}$ (use $D_{max}$ in ft)
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading			
<b>Sediment Competence Using Dimensional Shear Stress</b>			
3.645	Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d ) $\gamma = 62.4$ , $d =$ existing depth, $S =$ existing slope		
Shields 300.1	CO 393.6	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ (Figure 5-49)	
Shields 7.586	CO 7.12	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) (Figure 5-49)	
Shields 1.50	CO 1.41	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm) $\tau =$ predicted shear stress, $\gamma = 62.4$ , $S =$ existing slope	$d = \frac{\tau}{\gamma S}$
Shields 0.1689	CO 0.1585	Predicted slope required to initiate movement of measured $D_{max}$ (mm) $\tau =$ predicted shear stress, $\gamma = 62.4$ , $d =$ existing depth	$S = \frac{\tau}{\gamma d}$
Check: <input checked="" type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading			

## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>West Monument A4/2 Reference</b> Stream Type: <b>A4/2</b>	
Location: <b>Pike National Forest, CO</b> Valley Type: <b>VIIIb</b>	
Observers: <b>Lee, Sumner, Jara, Leah</b> Date: <b>11/06/2012</b>	
Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)	Stability Rating (Check Appropriate Rating)
Stream Type at potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	<input checked="" type="checkbox"/> Stable
(E→C), (C→High W/d C)	<input type="checkbox"/> Moderately Unstable
(G→F), (F→D), (C→F)	<input type="checkbox"/> Unstable
(C→D), (B→G), (D→G), (C→G), (E→G)	<input type="checkbox"/> Highly Unstable

Worksheet 5-25. Lateral stability.

Stream: <b>West Monument A4/2 Reference</b>		Stream Type: <b>A4/2</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIIb</b>			
Observers: <b>Lee, Sumner, Jara, Leah</b>		Date: <b>11/06/2012</b>			
Lateral stability criteria (choose one stability category for each criterion 1–5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	2
	(2)	(4)	(6)	(8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	N/A
	(1)	(2)	(3)	(4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		N/A
	(1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	2
	(2)	(4)	(6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	1
	(1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>5</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input checked="" type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input type="checkbox"/>	<i>Unstable</i> 13 – 21 <input type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	

**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>West Monument A4/2 Reference</b>		Stream Type: <b>A4/2</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIIb</b>			
Observers: <b>Lee, Sumner, Jara, Leah</b>		Date: <b>11/06/2012</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
1 <b>Sediment competence</b> (Worksheet 5-22)	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope-slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	2
	(2)	(4)	(6)	(8)	
2 <b>Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	2
	(2)	(4)	(6)	(7)	
3 <b>W/d Ratio State</b> (Worksheet 5-13)	1.0 – 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	2
	(2)	(4)	(6)	(8)	
4 <b>Stream Succession States</b> (Worksheet 5-24)	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	2
	(2)	(4)	(6)	(8)	
5 <b>Depositional Patterns</b> (Worksheet 5-10)	B1	B2, B4	B3, B5	B6, B7, B8	1
	(1)	(2)	(3)	(4)	
6 <b>Debris / Blockages</b> (Worksheet 5-11)	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	1
	(1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>10</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
<b>Vertical Stability for Excess Deposition / Aggradation (use total points and check stability rating)</b>	<i>No Deposition</i> 10 – 14 <input checked="" type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input type="checkbox"/>	<i>Aggradation</i> > 30 <input type="checkbox"/>	

Worksheet 5-27. Vertical stability – degradation.

Stream: <b>West Monument A4/2 Reference</b>		Stream Type: <b>A4/2</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIIb</b>			
Observers: <b>Lee, Sumner, Jara, Leah</b>		Date: <b>11/06/2012</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>1 Sediment Competence (Worksheet 5-22)</b>	Does not indicate excess competence <b>(2)</b>	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed <b>(4)</b>	$D_{100}$ of bed moved <b>(6)</b>	Particles much larger than $D_{100}$ of bed moved <b>(8)</b>	<b>2</b>
<b>2 Sediment Capacity (POWERSED) (Worksheet 5-20)</b>	Does not indicate excess capacity <b>(2)</b>	Slight excess energy: up to 10% increase above reference <b>(4)</b>	Excess energy sufficient to increase load up to 50% of annual load <b>(6)</b>	Excess energy transporting more than 50% of annual load <b>(8)</b>	<b>2</b>
<b>3 Degree of Channel Incision (BHR) (Worksheet 5-12)</b>	1.00 – 1.10 <b>(2)</b>	1.11 – 1.30 <b>(4)</b>	1.31 – 1.50 <b>(6)</b>	> 1.50 <b>(8)</b>	<b>2</b>
<b>4 Stream Succession States (Worksheets 5-12 and 5-24)</b>	Does not indicate incision or degradation <b>(2)</b>	If BHR > 1.1 and stream type has W/d between 5–10 <b>(4)</b>	If BHR > 1.1 and stream type has W/d less than 5 <b>(6)</b>	(B→G), (C→G), (E→G), (D→G) <b>(8)</b>	<b>2</b>
<b>5 Confinement (MWR / MWR<sub>ref</sub>) (Worksheet 5-14)</b>	0.80 – 1.00 <b>(1)</b>	0.30 – 0.79 <b>(2)</b>	0.10 – 0.29 <b>(3)</b>	< 0.10 <b>(4)</b>	<b>1</b>
<b>Total Points</b>					<b>9</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation (use total points and check stability rating)</b>	<i>Not Incised</i> 9 – 11 <input checked="" type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input type="checkbox"/>	<i>Degradation</i> > 27 <input type="checkbox"/>	

**Worksheet 5-28.** Channel enlargement.

Stream: <b>West Monument A4/2 Reference</b>		Stream Type: <b>A4/2</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIIb</b>			
Observers: <b>Lee, Sumner, Jara, Leah</b>		Date: <b>11/06/2012</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1-4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	2
	(2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	2
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	2
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	2
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>8</b>
<b>Category Point Range</b>					
<b>Channel Enlargement Prediction (use total points and check stability rating)</b>	<i>No Increase</i> 8 – 10 <input checked="" type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input type="checkbox"/>	<i>Extensive</i> > 24 <input type="checkbox"/>	



Worksheet 5-29. Overall sediment supply.

Stream: <b>West Monument A4/2 Reference</b>		Stream Type: <b>A4/2</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIIb</b>		
Observers: <b>Lee, Sumner, Jara, Leah</b>		Date: <b>11/06/2012</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1–5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	1	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	1	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	1	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	1	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	1	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>5</b>	
<b>Category Point Range</b>				
Overall Sediment Supply Rating (use total points and check stability rating)	<i>Low</i> 5 <input checked="" type="checkbox"/>	<i>Moderate</i> 6 – 10 <input type="checkbox"/>	<i>High</i> 11 – 15 <input type="checkbox"/>	<i>Very High</i> 16 – 20 <input type="checkbox"/>

Worksheet 5-32. Summary of stability condition categories.

Stream: <b>West Monument Creek A4/2 Reference</b>		Location: <b>A4/2 Reference</b>	
Observers: <b>Lee, Sumner, Jara, Leah</b>		Date: <b>11/6/2012</b>	Stream Type: <b>A4/2</b>
Channel Dimension		Bankfull Width (ft): <b>4.45</b>	Width/Depth Ratio: <b>4.41</b>
Channel Pattern		Cross-Sectional Area (ft <sup>2</sup> ): <b>0</b>	Entrenchment Ratio: <b>2.74</b>
River Profile & Bed Features		Mean Bankfull Depth (ft): <b>1.01</b>	MWR: <b>3.23</b>
		Mean: $\lambda/W_{bkt}$ : <b>0.00 - 0.00</b>	Sinuosity: <b>1.05</b>
		Range: $\lambda/W_{bkt}$ : <b>0.00 - 0.00</b>	MWR: <b>2.81 - 4.07</b>
River Profile & Bed Features		Check: <input type="checkbox"/> Riffle/Pool <input checked="" type="checkbox"/> Step/Pool <input type="checkbox"/> Plane Bed <input type="checkbox"/> Convergence/Divergence <input type="checkbox"/> Dunes/Antidunes/Smooth Bed	Slope
		Max Bankfull Depth (ft): <b>1.34</b>	Valley: <b>0.0852</b>
		Depth Ratio (max to mean): <b>1.33</b>	Water Surface: <b>0.08113</b>
Level III Stream Stability Indices		Riparian Vegetation: <b>Aspen, Spruce, Ponderosa, W</b>	Remarks: Condition, Vigor & Usage of Existing Reach:
		Flow Regime: <b>P1, P2</b> Stream Size <b>S-3(4)</b>	Species at Potential
		Meander Patterns: <b>N/A</b>	Debris/Channel Blockages: <b>D3</b>
		Degree of Incision (Bank-Height Ratio): <b>1.2</b>	Modified Pfankuch Stability Rating: <b>74 (Good)</b>
		Stability Rating: <b>Slightly Incised</b>	
		Reference W/d Ratio (W/d <sub>ref</sub> ): <b>4.41</b>	W/d Ratio State: <b>Stable</b>
		Degree of confinement (MWR / MWR <sub>ref</sub> ): <b>2.51</b>	Stability Rating: <b>Stable</b>
Bank Erosion Summary		Annual Streambank Erosion Rate: <b>1.33</b> (tons/yr)	Remarks: <b>Used Yellowstone curve for very low BEHI</b>
Sediment Capacity (POWERSED)		Length of Reach Studied (ft): <b>174</b>	Curve Used: <b>Colorado</b>
Entrainment/Competence		Sufficient Capacity	Excess Capacity
Successional Stage Shift		Insufficient Capacity	Remarks:
Lateral Stability		Stable <input checked="" type="checkbox"/>	Required Depth: <b>1.5</b>
Vertical Stability (Aggradation)		Mod. Unstable <input type="checkbox"/>	Existing Slope: <b>0.081</b>
Vertical Stability (Degradation)		Mod. Deposition <input type="checkbox"/>	Required Slope: <b>0.13</b>
Channel Enlargement		Mod. Incised <input type="checkbox"/>	Potential Stream State (Type): <b>A2/4</b>
Sediment Supply (Channel Source)		Slight Increase <input type="checkbox"/>	Remarks/causes:
		No Increase <input type="checkbox"/>	Remarks/causes:
		Moderate <input type="checkbox"/>	Remarks/causes:
		High <input type="checkbox"/>	Remarks/causes:
		Very High <input type="checkbox"/>	Remarks/causes:
		Low <input checked="" type="checkbox"/>	Stable condition, also had bedrock control associated with the Windy Gap Granite

# *Appendix C18*

## **B4 Stream Type**

### *Reference Reach*



# Table of Contents

## *Appendix C18: B4 Reference Reach*

<b>Reach Location &amp; Overview.....</b>	<b>C18-2</b>
<b>Survey Summary.....</b>	<b>C18-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C18-9</b>
<b><i>Velocity, Classification &amp; Morphological Relations.....</i></b>	<b>C18-9</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b><i>Stability Indices.....</i></b>	<b>C18-13</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b><i>BANCS Model – Streambank Erosion.....</i></b>	<b>C18-23</b>
Worksheet 5-16. Bank Erosion Hazard Index (BEHI) rating.	
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b><i>FLOWSED Model – Total Annual Sediment Yield.....</i></b>	<b>C18-27</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b><i>Sediment Competence/Entrainment.....</i></b>	<b>C18-29</b>
Worksheet 5-22. Sediment competence calculations.	
<b><i>Channel Stability Ratings.....</i></b>	<b>C18-30</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b><i>Summary.....</i></b>	<b>C18-36</b>
Worksheet 5-32. Summary of stability condition categories.	

## B4 Reference Reach Location & Overview

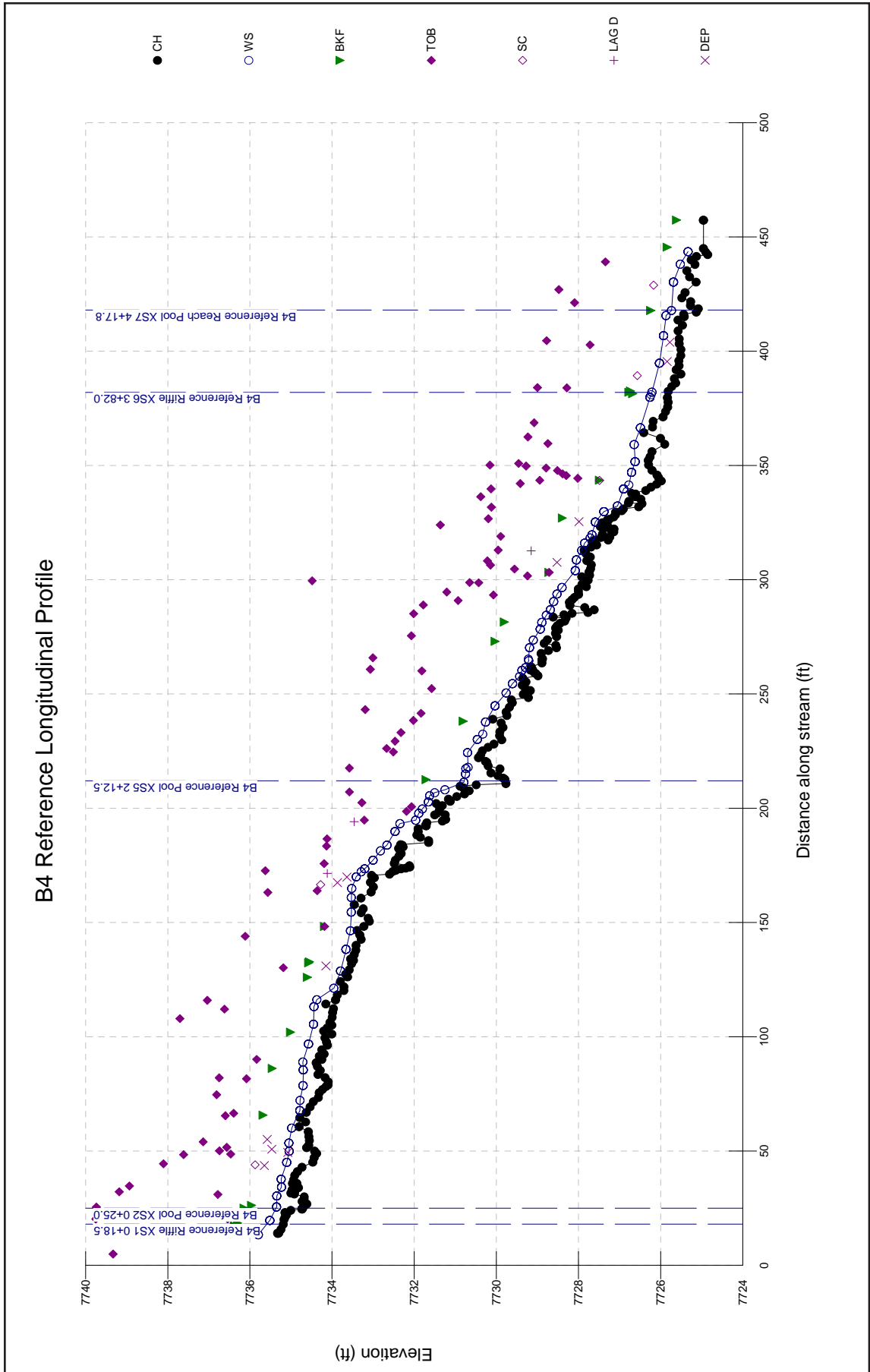
The B4 reference reach exists in a Valley Type VIII and is typical of a gravel-cobble and sand composite channel material. The channel bed and banks are potentially erodible, but due to the vegetation condition, this reference reach shows little sediment yield from this 3<sup>rd</sup> order, perennial channel. Bed features are generally dominated by rapids and pools and some step/pool features. The stream is confined (lateral contained) and as such has evolved from a post-disturbance F4b stream type. This evolution has occurred due to the presence of riparian vegetation that over time reduced the streambank erosion to a condition where the stream changed to a B4 stream type. The stable form for G4 and F4b stream types is the B4 stream type. The morphological data from this reach will be used to develop dimension, pattern and profile data for impaired streams that potentially should be B4 stream types. This reach has little sediment storage and very low streambank erosion rates (*0.0048 tons/yr/ft*, see **Worksheet 5-18**).

The location of this reach is shown in **Figure C-2**, and the photograph depicts the stable characteristics of the B4 stream type. The willow community and the dominating *Carex/Juncus* understory that has occupied the riparian areas are key components responsible for such stable conditions. There is little to no evidence of active channel-source sediment from this stream type. Such stream types are mapped where they occur by sub-watershed as shown in **Appendix D**.

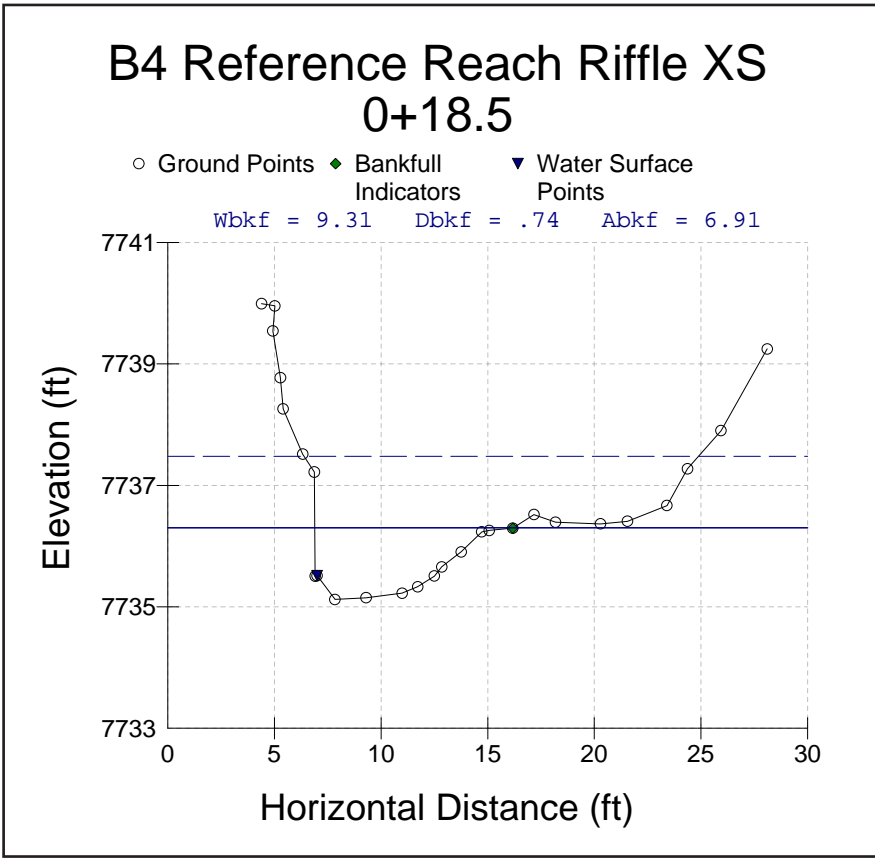
The details of the dimension, pattern, profile, and materials are summarized. The POWERSED model was not run on this reference reach as the bed is obviously stable. The following summary worksheets provide the detail of the morphology, hydraulics, streambank erosion rates, and stability for this stable reach. In the situation where impaired B4, G4 and F4b stream types are located, an alternative for mitigation and sediment reduction from increased flow is to use the data from the stable form to extrapolate for potential implementation of natural channel design.



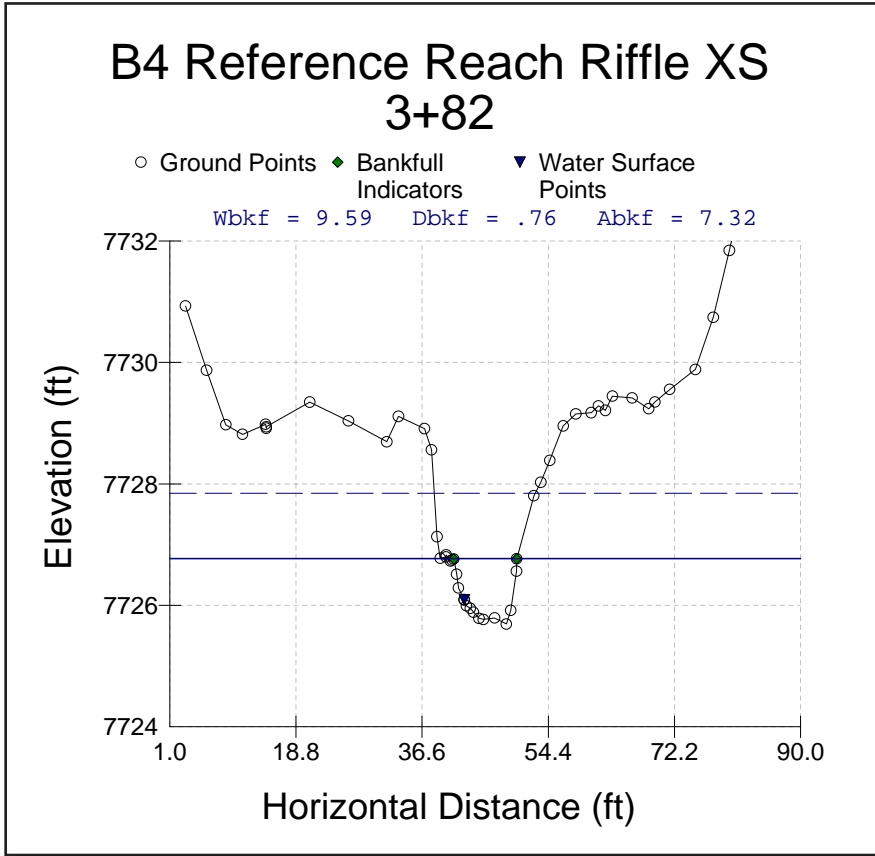
# Survey Summary



Longitudinal Profile (graph generated from RIVERMorph™)

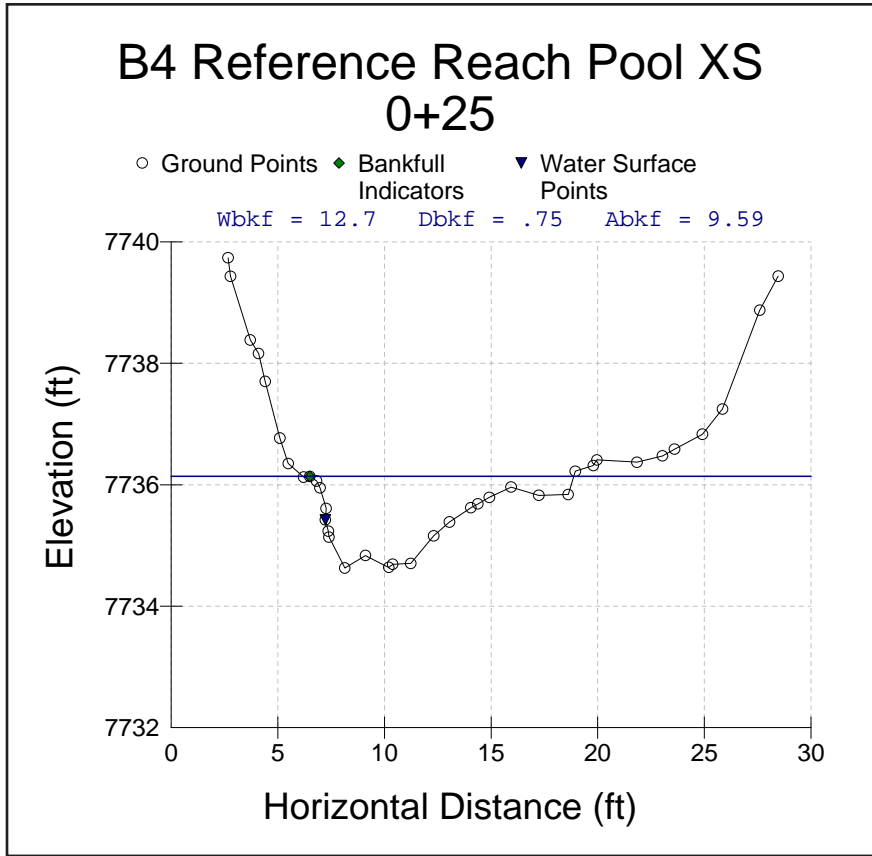


Representative Riffle Cross-section 0+18.5 (graph generated from RIVERMorph™)

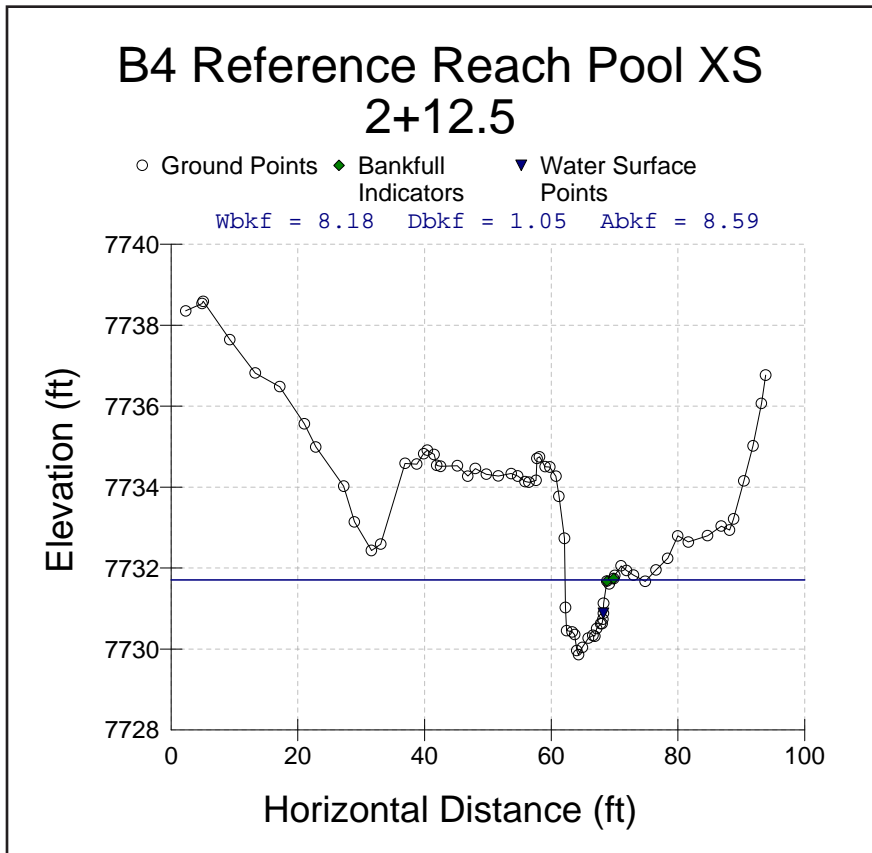


Riffle Cross-section 3+82 (graph generated from RIVERMorph™)

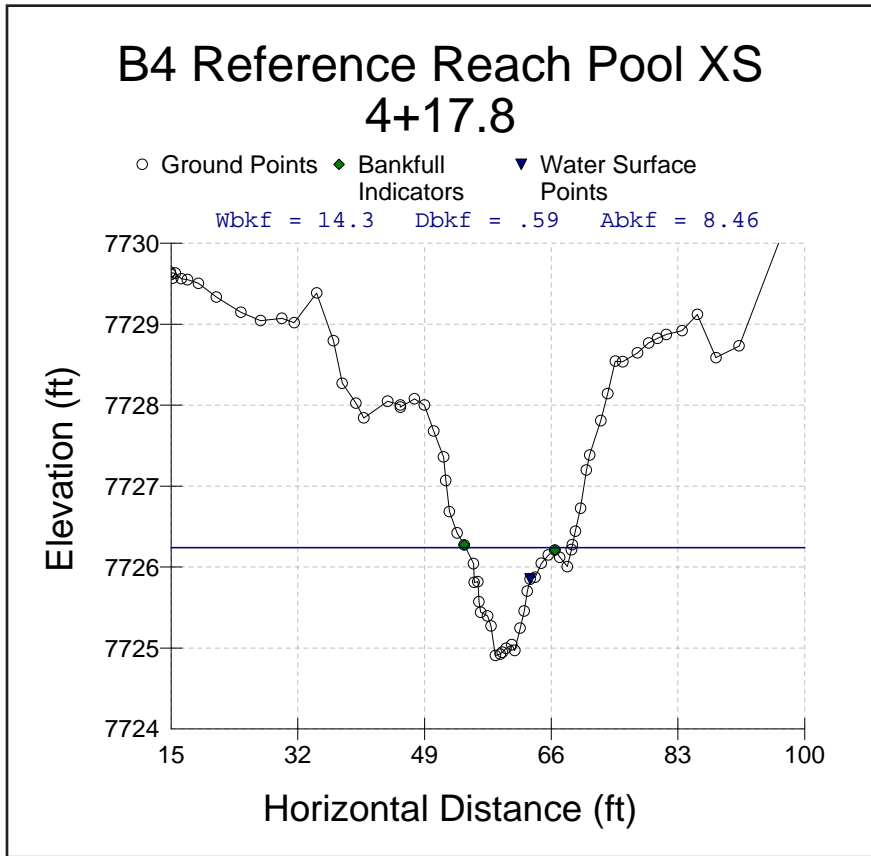




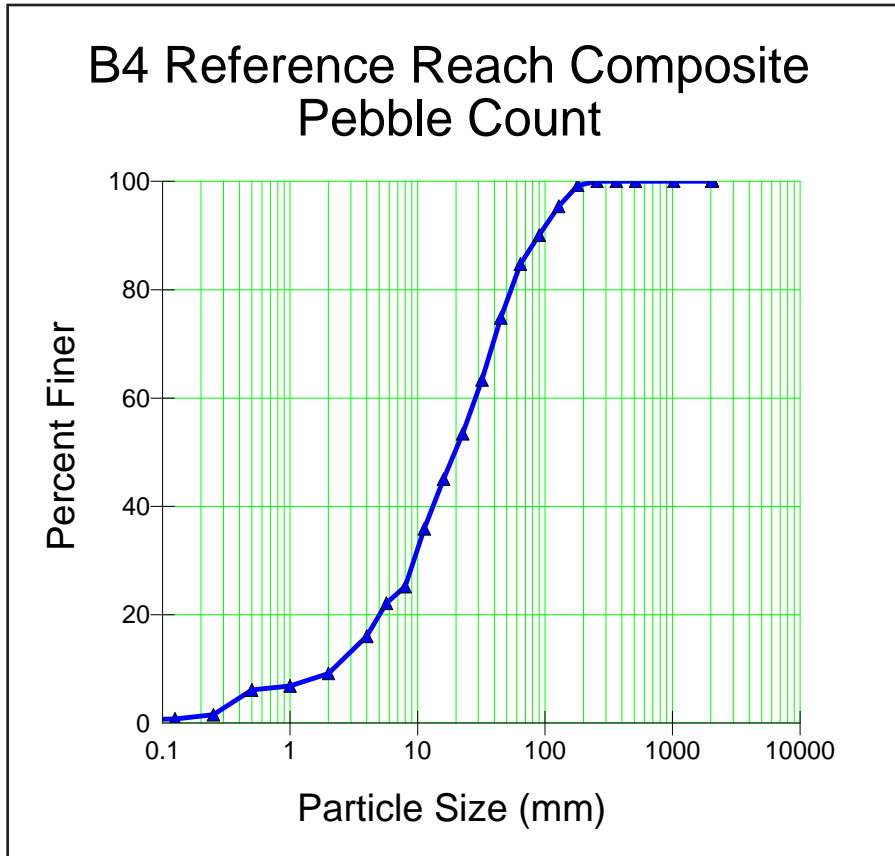
Pool Cross-section 0+25 (graph generated from RIVERMorph™)



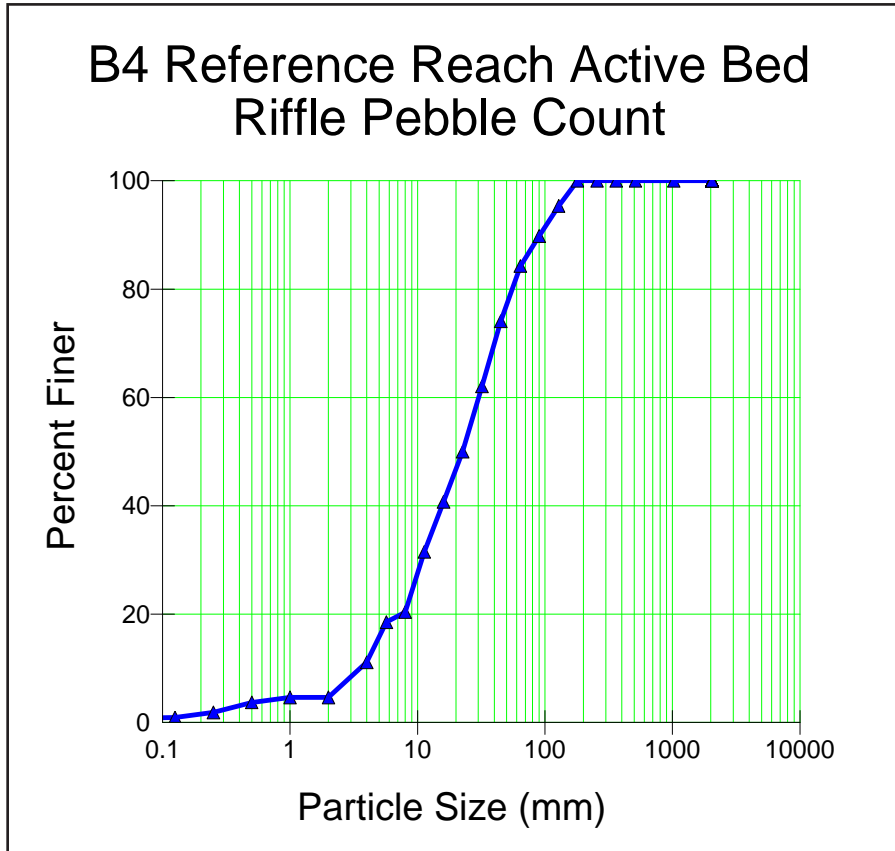
Pool Cross-section 2+12.5 (graph generated from RIVERMorph™)



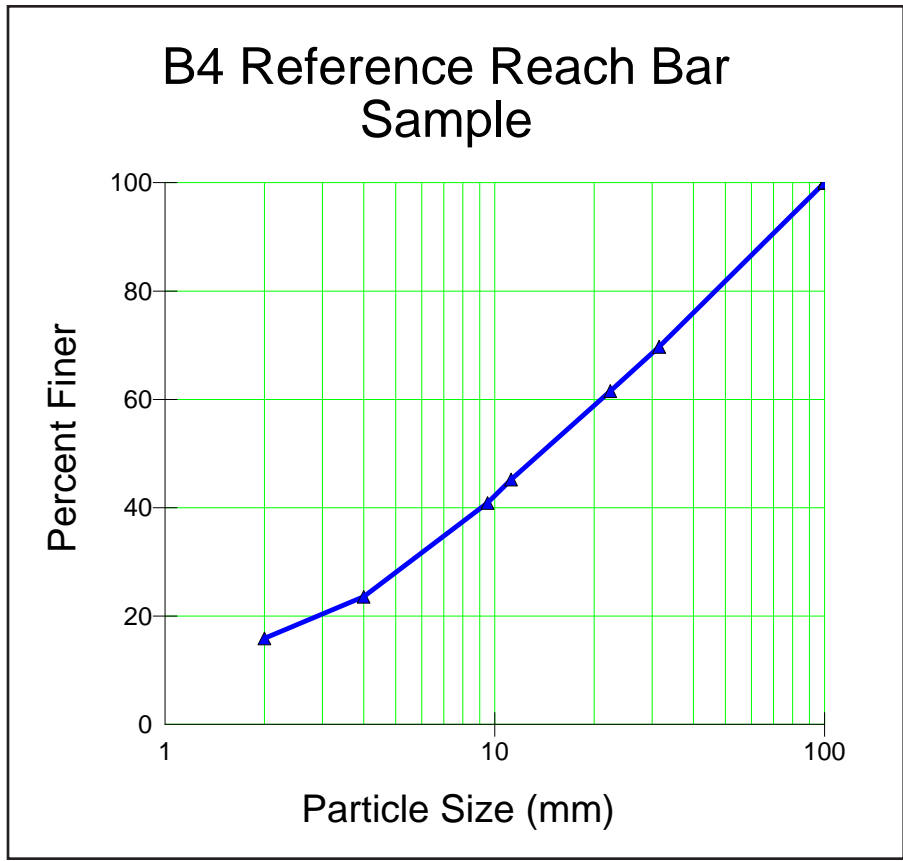
Pool Cross-section 4+17.8 (graph generated from RIVERMorph™)



Composite Pebble Count (graph generated from RIVERMorph™)



Active Bed Riffle Pebble Count (graph generated from RIVERMorph™)



Bar Sample (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates						
Stream:	Trail Creek, B4 Reference Reach			Location:	Riffle 1 XS 0+18.5, Pike N.F., CO	
Date:	8/14/2010	Stream Type:	B4	Valley Type:	VIII	
Observers:	Rosgen & Kasun			HUC:	-- -- -- -- -- -- -- -- -- --	
INPUT VARIABLES			OUTPUT VARIABLES			
Bankfull Riffle Cross-Sectional AREA	6.91	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.74	$d_{bkf}$ (ft)	
Bankfull Riffle WIDTH	9.31	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim (2 * d_{bkf}) + W_{bkf}$	10.32	$W_p$ (ft)	
$D_{84}$ at Riffle	63.52	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.21	$D_{84}$ (ft)	
Bankfull SLOPE	0.0242	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	0.67	R (ft)	
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R(ft) / $D_{84}$ (ft)	3.21	R / $D_{84}$	
Drainage Area	14.3	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.722	$u^*$ (ft/sec)	
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE	
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$			4.12	ft / sec	28.45	cfs
2. Roughness Coefficient: a) Manning's <i>n</i> from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.0374$			4.74	ft / sec	32.78	cfs
2. Roughness Coefficient: b) Manning's <i>n</i> from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.037$			4.79	ft / sec	33.13	cfs
2. Roughness Coefficient: c) Manning's <i>n</i> from Jarrett (USGS): $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ <small>Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for Stream Types A1, A2, A3, B1, B2, B3, C2 &amp; E3</small> $n = 0.101$			1.75	ft / sec	12.12	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Darcy-Weisbach			4.15	ft / sec	28.7	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Hey			4.10	ft / sec	28.3	cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q = \text{ } \text{ year}$ $u = Q / A$				ft / sec		cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$				ft / sec		cfs
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation (R/ $D_{84}$ ) – Estimation Method 1						
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.						
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.						
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.						
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.						

**Worksheet 5-3.** Level II stream classification.

Stream: <b>Trail Creek, B4 Reference Reach, Riffle 1 XS 0+18.5</b>	
Basin:	Drainage Area: <b>9152</b> acres <b>14.3</b> mi <sup>2</sup>
Location: <b>Pike National Forest, Colorado</b>	
Twp.&Rge:	Sec.&Qtr.:
Cross-Section Monuments (Lat./Long.): <b>39.12433 Lat / 105.23528 Long</b> Date: <b>8/14/2010</b>	
Observers: <b>Rosgen &amp; Kasun</b>	Valley Type: <b>VIII</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>9.31</b> ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A_{bkf} / W_{bkf}$ ).	<b>0.74</b> ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>6.91</b> ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>12.57</b> ft/ft
<b>Maximum DEPTH (<math>d_{max}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>1.18</b> ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>18.48</b> ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>1.99</b> ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the median or dominant diameter of channel materials, as sampled proportionately from the channel surface, between the bankfull stage and Thalweg elevations.	<b>19.9</b> mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.0242</b> ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope ( $S_{val} / S$ ).	<b>1.13</b>

<div style="border: 1px solid black; padding: 5px; display: inline-block;">Stream Type</div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: #e0f0ff;"><b>B4</b></div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;">See Classification Key (Figure 2-14)</div>
--	---	---

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, B4 Reference Reach</b>				Location: <b>Pike National Forest, Colorado</b>								
Observers: <b>Rosgen &amp; Kasun</b>				Date: <b>8/14/2010</b>		Valley Type: <b>VIII</b>		Stream Type: <b>B4</b>				
<b>River Reach Dimension Summary Data.....1</b>												
<b>Riffle Dimensions* ** ***</b>	<b>Riffle Dimensions* ** ***</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Width ( $W_{bkt}$ )			<b>11.78</b>	<b>9.31</b>	<b>14.24</b>	ft	Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	<b>7.12</b>	<b>6.91</b>	<b>7.32</b>	
	Mean Riffle Depth ( $d_{bkt}$ )			<b>0.75</b>	<b>0.74</b>	<b>0.76</b>	ft	Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	<b>12.60</b>	<b>12.58</b>	<b>12.62</b>	
	Maximum Riffle Depth ( $d_{max}$ )			<b>1.13</b>	<b>1.08</b>	<b>1.18</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max}/d_{bkt}$ )	<b>1.508</b>	<b>1.421</b>	<b>1.595</b>	
	Width of Flood-Prone Area ( $W_{fpa}$ )			<b>16.4</b>	<b>14.2</b>	<b>18.5</b>	ft	Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )	<b>1.74</b>	<b>1.48</b>	<b>1.99</b>	
	Riffle Inner Berm Width ( $W_{ib}$ )			<b>7.3</b>	<b>5.6</b>	<b>8.8</b>	ft	Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )	<b>0.616</b>	<b>0.476</b>	<b>0.750</b>	
	Riffle Inner Berm Depth ( $d_{ib}$ )			<b>0.32</b>	<b>0.20</b>	<b>0.43</b>	ft	Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )	<b>0.427</b>	<b>0.267</b>	<b>0.573</b>	
	Riffle Inner Berm Area ( $A_{ib}$ )			<b>2.42</b>	<b>1.28</b>	<b>3.79</b>	ft <sup>2</sup>	Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )	<b>0.340</b>	<b>0.180</b>	<b>0.533</b>	
	Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )			<b>23.6</b>	<b>20.5</b>	<b>32.1</b>						
<b>Pool Dimensions* ** ***</b>	<b>Pool Dimensions* ** ***</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Pool Dimensions &amp; Dimensionless Ratios****</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Pool Width ( $W_{bkfp}$ )			<b>14.0</b>	<b>8.2</b>	<b>21.1</b>	ft	Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )	<b>1.190</b>	<b>0.695</b>	<b>1.792</b>	
	Mean Pool Depth ( $d_{bkfp}$ )			<b>0.80</b>	<b>0.59</b>	<b>1.05</b>	ft	Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )	<b>1.067</b>	<b>0.787</b>	<b>1.400</b>	
	Pool Cross-Sectional Area ( $A_{bkfp}$ )			<b>8.9</b>	<b>8.5</b>	<b>9.6</b>	ft	Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )	<b>1.248</b>	<b>1.189</b>	<b>1.348</b>	
	Maximum Pool Depth ( $d_{maxp}$ )			<b>1.56</b>	<b>1.33</b>	<b>1.85</b>	ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	<b>2.080</b>	<b>1.773</b>	<b>2.467</b>	
	Pool Inner Berm Width ( $W_{ibp}$ )			<b>4.8</b>	<b>4.5</b>	<b>5.1</b>	ft	Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )	<b>0.343</b>	<b>0.320</b>	<b>0.361</b>	
	Pool Inner Berm Depth ( $d_{ibp}$ )			<b>0.31</b>	<b>0.22</b>	<b>0.40</b>	ft	Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )	<b>0.388</b>	<b>0.275</b>	<b>0.500</b>	
	Pool Inner Berm Area ( $A_{ibp}$ )			<b>1.5</b>	<b>1.0</b>	<b>2.0</b>	ft <sup>2</sup>	Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )	<b>0.172</b>	<b>0.114</b>	<b>0.226</b>	
	Point Bar Slope ( $S_{pb}$ )			<b>0.290</b>	<b>0.220</b>	<b>0.360</b>	ft/ft	Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )	<b>0.88</b>	<b>0.82</b>	<b>0.93</b>	
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Run Dimensionless Ratios****</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Run Width ( $W_{bktr}$ )						ft	Run Width to Riffle Width ( $W_{bktr} / W_{bkt}$ )				
	Mean Run Depth ( $d_{bktr}$ )						ft	Mean Run Depth to Mean Riffle Depth ( $d_{bktr} / d_{bkt}$ )				
	Run Cross-Sectional Area ( $A_{bktr}$ )						ft	Run Area to Riffle Area ( $A_{bktr} / A_{bkt}$ )				
	Maximum Run Depth ( $d_{maxr}$ )						ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )				
Run Width/Depth Ratio ( $W_{bktr} / d_{bktr}$ )						ft						
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Glide Dimensions &amp; Dimensionless Ratios****</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Glide Width ( $W_{bkfg}$ )						ft	Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )				
	Mean Glide Depth ( $d_{bkfg}$ )						ft	Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )				
	Glide Cross-Sectional Area ( $A_{bkfg}$ )						ft	Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )				
	Maximum Glide Depth ( $d_{maxg}$ )						ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )				
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )						ft/ft	Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )				
	Glide Inner Berm Width ( $W_{ibg}$ )						ft	Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )				
	Glide Inner Berm Depth ( $d_{ibg}$ )						ft	Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )				
Glide Inner Berm Area ( $A_{ibg}$ )						ft <sup>2</sup>	Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )					
<b>Step**</b>	<b>Step Dimensions**</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Step Dimensionless Ratios****</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Step Width ( $W_{bkfs}$ )						ft	Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )				
	Mean Step Depth ( $d_{bkfs}$ )						ft	Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )				
	Step Cross-Sectional Area ( $A_{bkfs}$ )						ft	Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )				
	Maximum Step Depth ( $d_{maxs}$ )						ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )				
Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )												

**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, B4 Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>							
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/20/2010</b>		Valley Type: <b>III</b>		Stream Type: <b>B4</b>			
<b>Hydraulics</b>	<b>River Reach Summary Data.....2</b>								
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )		<b>4.74</b> ft/sec		Estimation Method		<b>Manning's n - RR/FF</b>		
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )		<b>32.78</b> cfs		Drainage Area		<b>14.3</b> mi <sup>2</sup>		
<b>Channel Pattern</b>	<b>Geometry</b>			<b>Dimensionless Geometry Ratios</b>					
	Linear Wavelength ( $\lambda$ )	<b>104.0</b>	<b>87.0</b>	<b>129.0</b> ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )	<b>8.8</b>	<b>7.4</b>	<b>11.0</b>	
	Stream Meander Length ( $L_m$ )	<b>112.0</b>	<b>94.5</b>	<b>135.0</b> ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )	<b>9.5</b>	<b>8.0</b>	<b>11.5</b>	
	Radius of Curvature ( $R_c$ )	<b>64.0</b>	<b>39.5</b>	<b>82.0</b> ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )	<b>5.4</b>	<b>3.4</b>	<b>7.0</b>	
	Belt Width ( $W_{bit}$ )	<b>27.2</b>	<b>14.6</b>	<b>60.0</b> ft	Meander Width Ratio ( $W_{bit} / W_{bkt}$ )	<b>2.3</b>	<b>1.2</b>	<b>5.1</b>	
	Arc Length ( $L_a$ )	<b>39.6</b>	<b>10.0</b>	<b>70.9</b> ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )	<b>3.4</b>	<b>0.8</b>	<b>6.0</b>	
	Riffle Length ( $L_r$ )	<b>14.7</b>	<b>2.7</b>	<b>28.2</b> ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )	<b>1.2</b>	<b>0.2</b>	<b>2.4</b>	
	Individual Pool Length ( $L_p$ )	<b>60.1</b>	<b>23.0</b>	<b>101.0</b> ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )	<b>5.10</b>	<b>1.95</b>	<b>8.58</b>	
Pool to Pool Spacing ( $P_s$ )	<b>28.1</b>	<b>12.2</b>	<b>47.3</b> ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )	<b>2.4</b>	<b>1.0</b>	<b>4.0</b>		
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )	<b>0.0264</b>	ft/ft	Average Water Surface Slope (S)	<b>0.0242</b>	ft/ft	Sinuosity ( $S_{val} / S$ )	<b>1.09</b>	
	Stream Length (SL)	<b>514.1</b>	ft	Valley Length (VL)	<b>581.0</b>	ft	Sinuosity (SL / VL)	<b>1.13</b>	
	Low Bank Height (LBH)	start: <b>1.18</b> ft end: <b>1.08</b> ft		Max Bankfull Depth ( $d_{max}$ )	start: <b>1.18</b> ft end: <b>1.08</b> ft		Bank-Height Ratio (BHR) (LBH / $d_{max}$ )	start: <b>1.0</b> end: <b>1.0</b>	
	<b>Facet Slopes</b>			<b>Dimensionless Facet Slope Ratios</b>					
	Riffle Slope ( $S_{rit}$ )	<b>0.0340</b>	<b>0.0159</b>	<b>0.0585</b> ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rit} / S$ )	<b>1.4037</b>	<b>0.6587</b>	<b>2.4182</b>	
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )	<b>0.0027</b>	<b>0.0001</b>	<b>0.0099</b> ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )	<b>0.1124</b>	<b>0.0041</b>	<b>0.4107</b>	
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )				
	Step Slope ( $S_s$ )	<b>1.0600</b>	<b>0.9300</b>	<b>1.1800</b> ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )	<b>43.80</b>	<b>38.43</b>	<b>48.76</b>	
	<b>Max Depths<sup>a</sup></b>			<b>Dimensionless Depth Ratios</b>					
	Max Riffle Depth ( $d_{maxr}$ )	<b>1.06</b>	<b>0.93</b>	<b>1.18</b> ft	Max Riffle Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )	<b>1.413</b>	<b>1.240</b>	<b>1.573</b>	
	Max Run Depth ( $d_{maxr}$ )			ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )	<b>1.52</b>	<b>1.33</b>	<b>1.85</b> ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	<b>2.027</b>	<b>1.773</b>	<b>2.467</b>	
	Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )				
Max Step Depth ( $d_{maxs}$ )			ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )					
<b>Channel Materials</b>		<b>Reach<sup>b</sup></b>	<b>Riffle<sup>c</sup></b>	<b>Bar</b>	<b>Reach<sup>b</sup></b>	<b>Riffle<sup>c</sup></b>	<b>Bar</b>	<b>Protrusion Height<sup>d</sup></b>	
	% Silt/Clay	<b>0.00</b>	<b>0.00</b>	<b>0.00</b>	$D_{16}$	<b>3.99</b>	<b>5.12</b>	<b>2.03</b>	mm
	% Sand	<b>9.16</b>	<b>4.63</b>	<b>15.87</b>	$D_{35}$	<b>11.03</b>	<b>13.09</b>	<b>7.64</b>	mm
	% Gravel	<b>75.57</b>	<b>79.63</b>	<b>72.43</b>	$D_{50}$	<b>19.90</b>	<b>22.60</b>	<b>14.49</b>	mm
	% Cobble	<b>15.27</b>	<b>15.74</b>	<b>11.70</b>	$D_{84}$	<b>62.60</b>	<b>63.52</b>	<b>63.81</b>	mm
	% Boulder	<b>0.00</b>	<b>0.00</b>	<b>0.00</b>	$D_{95}$	<b>125.01</b>	<b>125.47</b>	<b>88.69</b>	mm
	% Bedrock	<b>0.00</b>	<b>0.00</b>	<b>0.00</b>	$D_{100}$	<b>255.99</b>	<b>180.00</b>	<b>100.00</b>	mm

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.  
<sup>b</sup> Composite sample of riffles and pools within the designated reach.      <sup>c</sup> Active bed of a riffle.      <sup>d</sup> Height of roughness feature above bed.



## Stability Indices

**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation					
Stream: <b>Trail Creek, B4 Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>			
Observers: <b>Rosgen &amp; Kasun</b>		Reference reach <input checked="" type="checkbox"/>	Disturbed (impacted reach) <input type="checkbox"/>	Date: <b>8/13/2010</b>	
Existing species composition: <b>Aspen, Willow, Grasses, Carex Juncus, Mullen, Thistle</b>		Potential species composition: <b>Same but without Thistle and Mullen</b>			
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition
<b>1. Overstory</b>	Canopy layer	<b>30%</b>	<b>&lt; 10%</b>	<b>Willow</b>	<b>95%</b>
				<b>Aspen</b>	<b>5%</b>
				<b>100%</b>	
<b>2. Understory</b>	Shrub layer	<b>70%</b>	<b>70%</b>	<b>Willow</b>	<b>90%</b>
				<b>Raspberry</b>	<b>10%</b>
				<b>100%</b>	
<b>3. Ground level</b>	Herbaceous	<b>95%</b>	<b>95%</b>	<b>Grasses</b>	<b>10%</b>
				<b>Red Top</b>	<b>8%</b>
				<b>Poa</b>	<b>5%</b>
				<b>Carex Juncus</b>	<b>75%</b>
				<b>Mullen</b>	<b>1%</b>
	<b>Thistle</b>	<b>1%</b>			
					<b>100%</b>
Leaf or needle litter				<b>Remarks:</b> Condition, vigor and/or usage of existing reach: <b>Current Riparian Vegetation Condition Good; Recovering Riparian inside of past G/Fb</b>	
Bare ground		<b>5%</b>			
			<b>Column total = 100%</b>		


\*Based on crown closure.

\*\*Based on basal area to surface area.

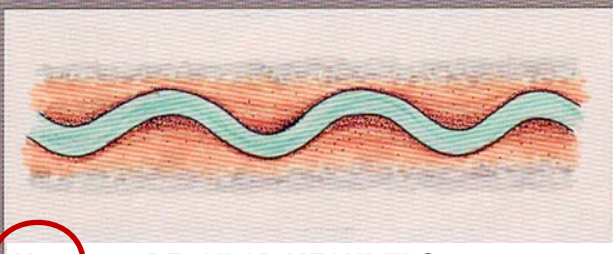


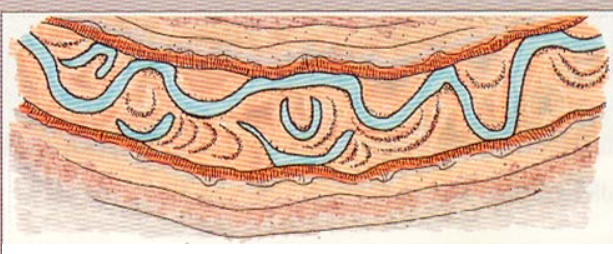


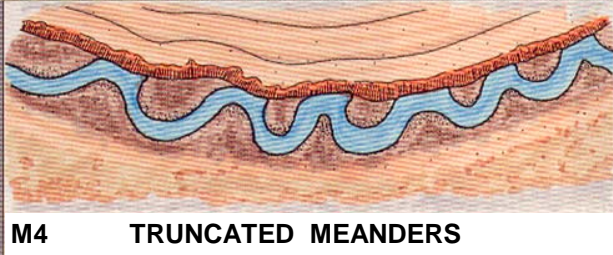
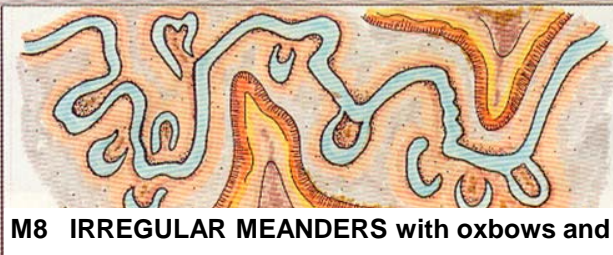
**Worksheet 5-7.** Flow regime.

<b>FLOW REGIME</b>								
Stream: <b>Trail Creek, B4 Reference</b>			Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>Rosgen &amp; Kasun</b>						Date: <b>8/14/2010</b>		
List ALL COMBINATIONS that APPLY..... ➡			P1	P2	P8			
<b>General Category</b>								
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation							
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
<b>P</b>	Perennial stream channels: Surface water persists yearlong.							
<b>Specific Category</b>								
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
<b>4</b>	Streamflow regulated by glacial melt.							
<b>5</b>	Ice flows/ice torrents from ice dam breaches.							
<b>6</b>	Alternating flow/backwater due to tidal influence.							
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.							
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
<b>9</b>	Rain-on-snow generated runoff.							

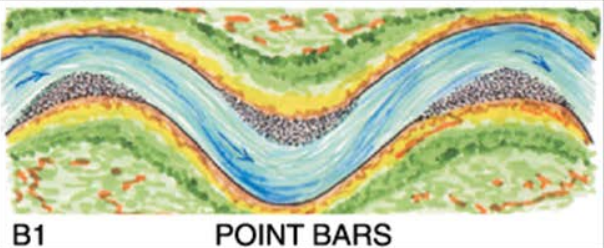
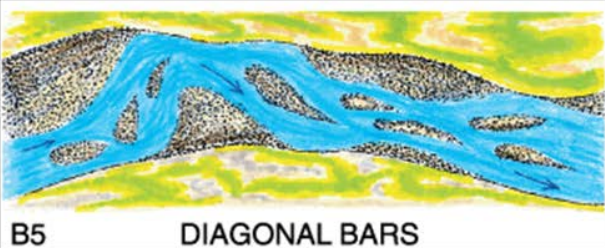
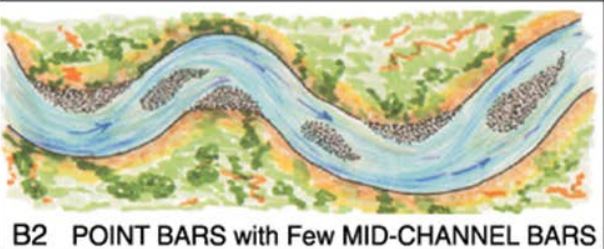
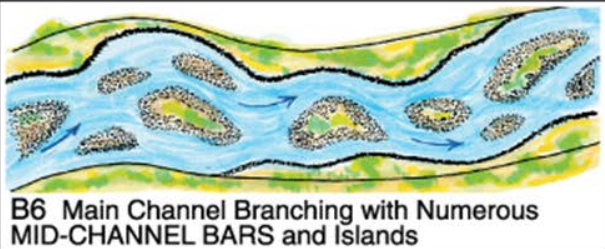
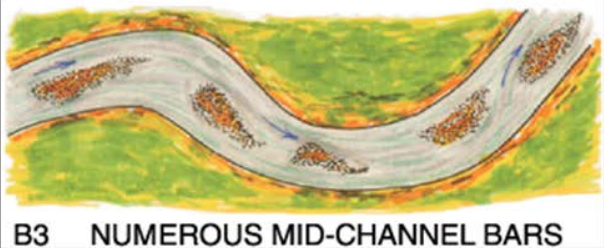
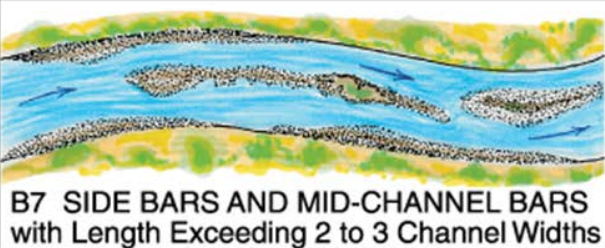

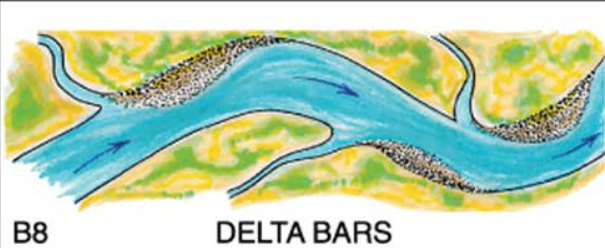
**Worksheet 5-8.** Stream order & stream size.

<b>Stream Size and Order</b>			
Stream:	<b>Trail Creek, B4 Reference Reach</b>		
Location:	<b>Pike National Forest, Colorado</b>		
Observers:	<b>Rosgen &amp; Kasun</b>		
Date:	<b>8/12/2010</b>		
<b>Stream Size Category and Order</b> 			<b>S-3(3)</b>
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0.305	<1	<input type="checkbox"/>
S-2	0.3 – 1.5	1 – 5	<input type="checkbox"/>
<b>S-3</b>	<b>1.5 – 4.6</b>	<b>5 – 15</b>	<input checked="" type="checkbox"/>
S-4	4.6 – 9	15 – 30	<input type="checkbox"/>
S-5	9 – 15	30 – 50	<input type="checkbox"/>
S-6	15 – 22.8	50 – 75	<input type="checkbox"/>
S-7	22.8 – 30.5	75 – 100	<input type="checkbox"/>
S-8	30.5 – 46	100 – 150	<input type="checkbox"/>
S-9	46 – 76	150 – 250	<input type="checkbox"/>
S-10	76 – 107	250 – 350	<input type="checkbox"/>
S-11	107 – 150	350 – 500	<input type="checkbox"/>
S-12	150 – 305	500 – 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
<b>Stream Order</b>			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			

Worksheet 5-9. Meander patterns.

<b>Meander Patterns</b>					
Stream: <b>Trail Creek, B4 Reference Reach</b>			Location: <b>Pike National Forest, CO</b>		
Observers: <b>Rosgen &amp; Kasun</b>			Date: <b>8/14/2010</b>		
List ALL CATEGORIES that APPLY		<b>M1</b>	<b>M3</b>		
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>					
					
<b>M1</b> <b>REGULAR MEANDERS</b>	<b>M5</b> <b>UNCONFINED MEANDER SCROLLS</b>				
					
<b>M2</b> <b>TORTUOUS MEANDERS</b>	<b>M6</b> <b>CONFINED MEANDER SCROLLS</b>				
					
<b>M3</b> <b>IRREGULAR MEANDERS</b>	<b>M7</b> <b>DISTORTED MEANDER LOOPS</b>				
					
<b>M4</b> <b>TRUNCATED MEANDERS</b>	<b>M8</b> <b>IRREGULAR MEANDERS with oxbows and</b>				

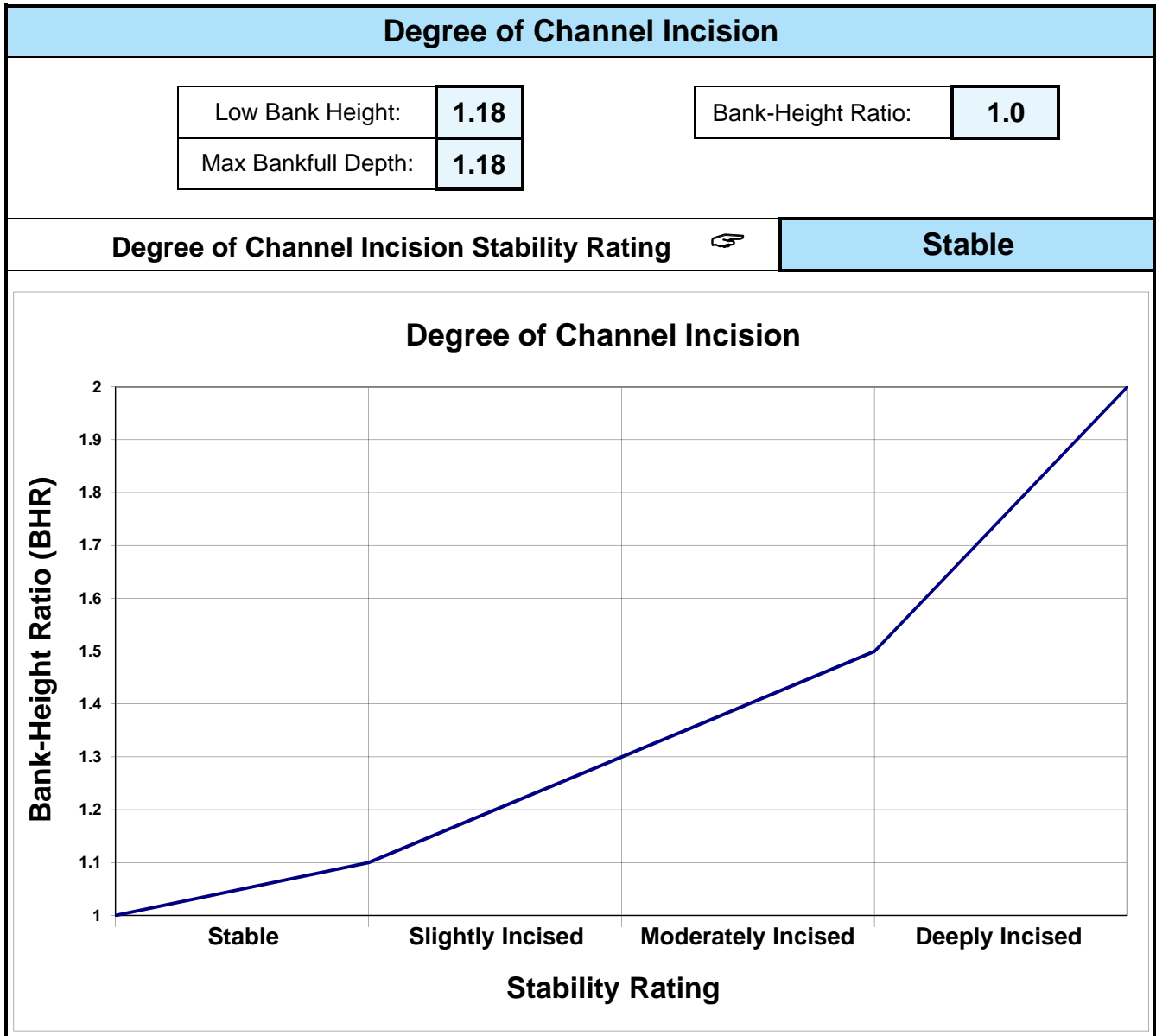
**Worksheet 5-10.** Depositional patterns.

<b>Depositional Patterns</b>					
Stream: <b>Trail Creek, B4 Reference Reach</b>			Location: <b>Pike National Forest, Colorado</b>		
Observers: <b>Rosgen &amp; Kasun</b>			Date: <b>8/14/2010</b>		
List ALL CATEGORIES that APPLY		<b>B4</b>			
<i>Various Depositional Features modified from Galay et al. (1973)</i>					
 <b>B1 POINT BARS</b>		 <b>B5 DIAGONAL BARS</b>			
 <b>B2 POINT BARS with Few MID-CHANNEL BARS</b>		 <b>B6 Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</b>			
 <b>B3 NUMEROUS MID-CHANNEL BARS</b>		 <b>B7 SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</b>			
 <b>B4 SIDE BARS</b>		 <b>B8 DELTA BARS</b>			

**Worksheet 5-11.** Channel blockages.

Channel Blockages		
Stream: <b>Trail Creek, B4 Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>Rosgen &amp; Kasun</b>		Date: <b>8/14/2010</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input checked="" type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input type="checkbox"/>
<b>D4</b> Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

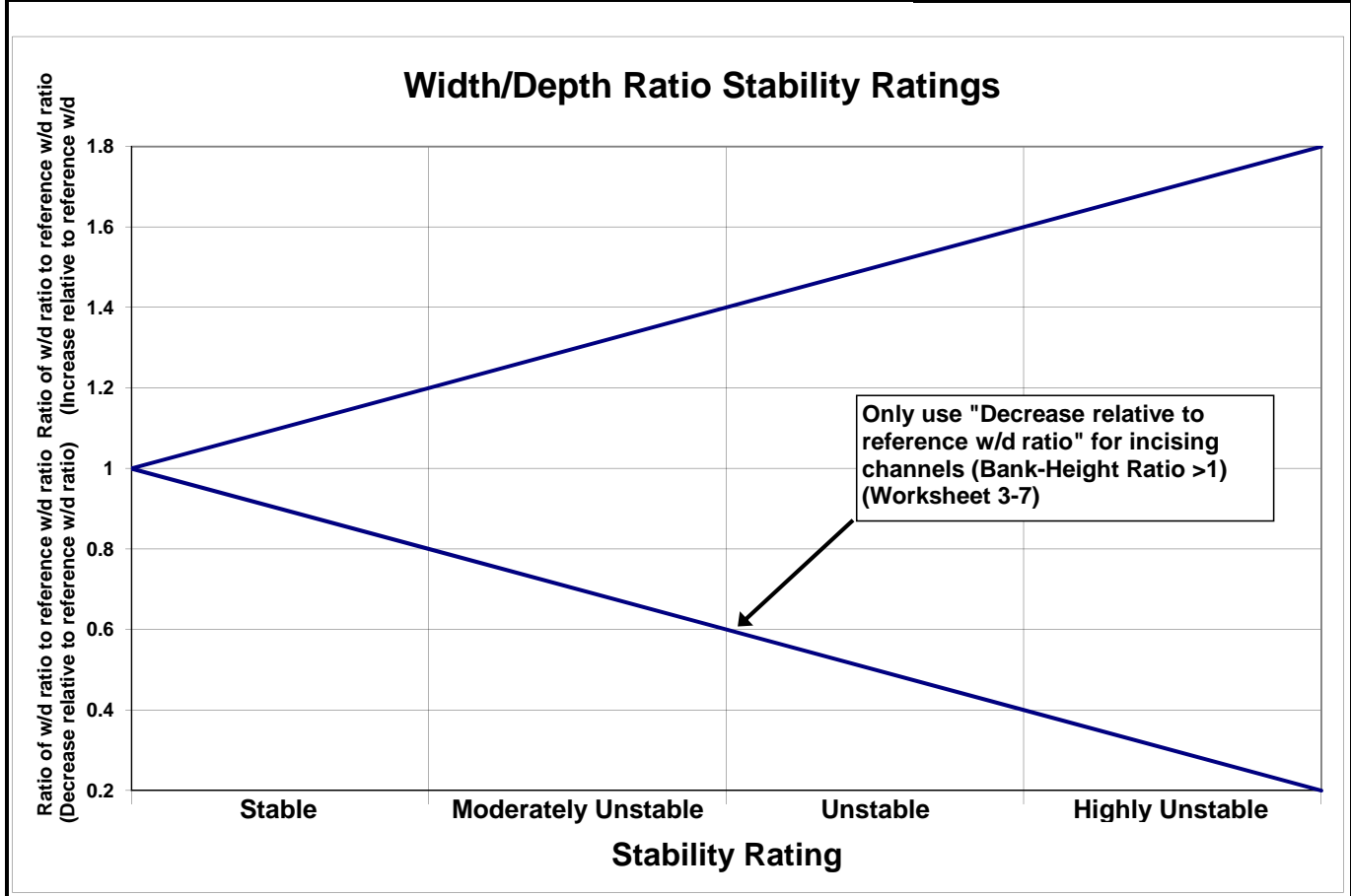
**Worksheet 5-12.** Degree of channel incision.



**Worksheet 5-13.** Width/depth ratio state.

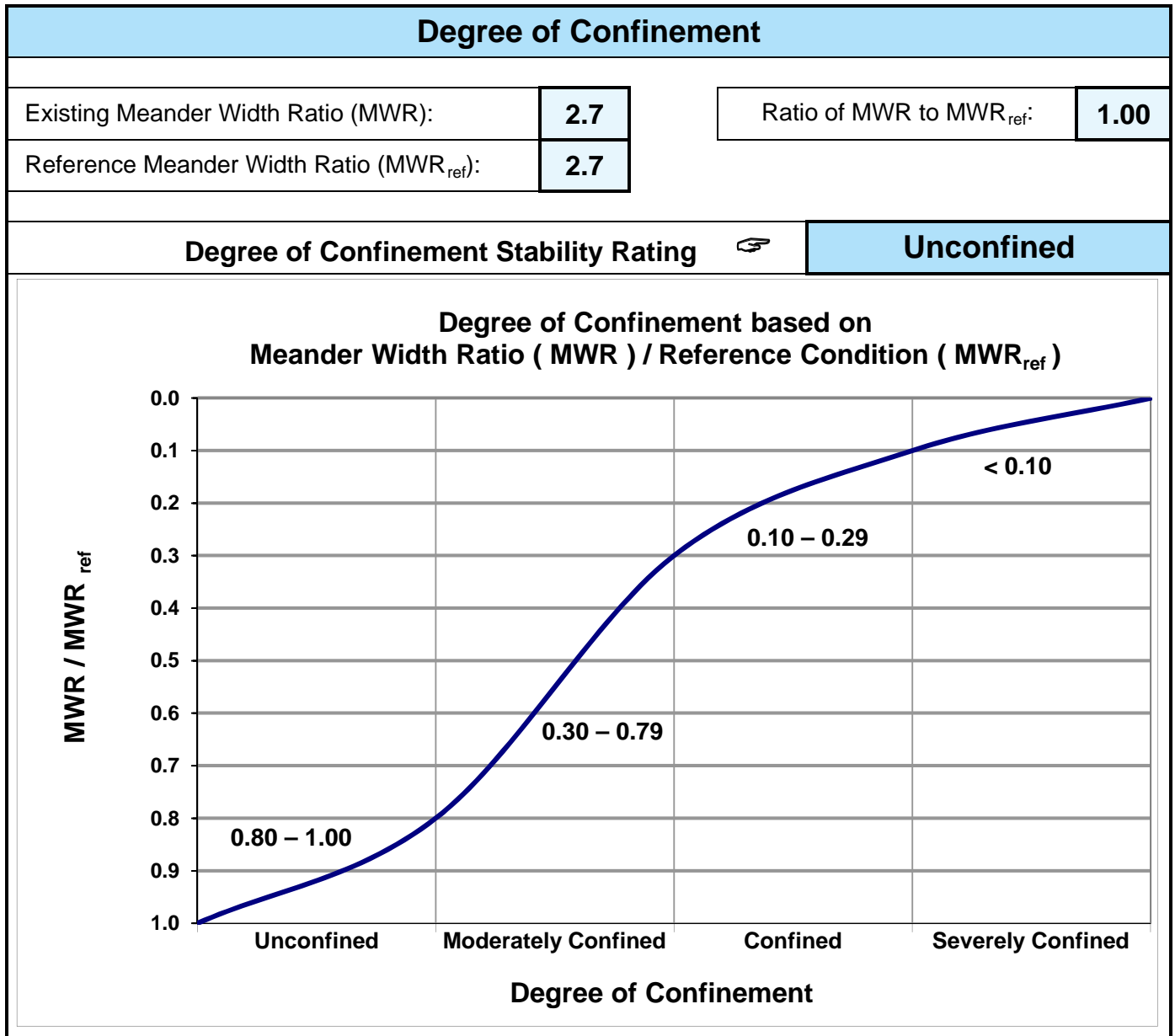
Width/Depth Ratio State			
Existing Width/Depth Ratio:	<b>12.57</b>	Ratio of existing W/d to reference W/d:	<b>1.00</b>
Reference Width/Depth Ratio:	<b>12.57</b>		

<b>Width/Depth Ratio State Stability Rating</b>	<b>Stable</b>
---	---------------





**Worksheet 5-14.** Degree of channel confinement (lateral containment).



Worksheet 5-15. Pfrankuch channel stability rating.

Stream: Trail Creek, B4 Reference Reach		Location: Pike National Forest, CO		Valley Type: VIII		Observers: Rosgen & Kasun		Date: 8/14/2010																
Loca- tion	Key Category	Excellent Description	Rating	Good Description	Rating	Fair Description	Rating	Poor Description	Rating															
Upper banks	1	Landform slope	2	Bank slope gradient <30%.	4	Bank slope gradient 40-60%.	6	Bank slope gradient > 60%.	8															
	2	Mass erosion	4	No evidence of past or future mass erosion.	6	Frequent or large, causing sediment nearly yearlong.	9	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.	12															
	3	Debris jam potential	2	Essentially absent from immediate channel area.	4	Moderate to heavy amounts, mostly larger sizes.	6	Moderate to heavy amounts, predominantly larger sizes.	8															
	4	Vegetative bank protection	3	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	6	70-90% density. Fewer species or less vigor suggest less dense or deep root mass.	9	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.	12															
Lower banks	5	Channel capacity	1	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0.	2	Bankfull stage is contained within banks. Width/depth ratio departure from reference width/depth ratio = 1.0-1.2. Bank-Height Ratio (BHR) = 1.1-1.3.	3	Bankfull stage is not contained. Width/depth ratio departure from reference width/depth ratio = 1.2-1.4. Bank-Height Ratio (BHR) > 1.4.	4															
	6	Bank rock content	2	> 65% with large angular boulders. 12" + common.	4	40-65%. Mostly boulders and small cobbles 6-12".	6	20-40%. Most in the 3-6" diameter class.	8															
	7	Obstructions to flow	2	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	3	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	6	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	8															
	8	Cutting	4	Little or none. Infrequent raw banks <6".	6	Some, intermittently at outcurves and constrictions. Raw banks may be up to 12".	12	Significant. Cuts 12-24" high. Root mat overhangs and sloughing evident.	16															
	9	Deposition	4	Little or no enlargement of channel or point bars.	6	Some new bar increase, mostly from coarse gravel.	12	Moderate deposition of new gravel and coarse sand on old and some new bars.	16															
Bottom	10	Rock angularity	1	Sharp edges and corners. Plane surfaces rough.	2	Rounded corners and edges. Surfaces smooth and flat.	3	Corners and edges well rounded in 2 dimensions.	4															
	11	Brightness	1	Surfaces dull, dark or stained. Generally not bright.	2	Mostly dull, but may have <35% bright surfaces.	3	Mixture dull and bright, i.e., 35-65% mixture range.	4															
	12	Consolidation of particles	2	Assorted sizes tightly packed or overlapping.	4	Moderately packed with some overlapping.	6	Mostly loose assortment with no apparent overlap.	8															
	13	Bottom size distribution	4	No size change evident. Stable material 80-100%.	6	Distribution shift light. Stable material 50-80%.	12	Moderate change in sizes. Stable materials 20-50%.	16															
	14	Scouring and deposition	6	<5% of bottom affected by scour or deposition.	12	5-30% affected. Scour at constrictions and where grades steepen. Some deposition in pools.	18	30-50% affected. Deposits and scour at obstructions, constrictions and bends. Some filling of pools.	24															
	15	Aquatic vegetation	1	Abundant growth moss-like, dark green perennial. In swift water too.	2	Common. Algae forms in low velocity and pool areas. Moss here too.	3	Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick.	4	Perennial types scarce or absent. Yellow-green, short-term bloom may be present.														
		Excellent total = 18		Good total = 31		Fair total = 3		Poor total = 8																
Stream type	A1	A2	A3	A4	A5	A6	B1	B2	B3	B4	B5	B6	C1	C2	C3	C4	C5	C6	D3	D4	D5	D6	Grand total = 60	
Good (Stable)	38-43	38-43	54-90	60-95	60-95	50-80	38-45	38-45	40-60	40-64	48-68	40-60	38-50	38-50	60-85	70-90	70-90	60-85	60-85	85-107	85-107	85-107	85-107	67-98
Fair (Mod. unstable)	44-47	44-47	91-129	96-132	96-142	81-110	46-58	46-58	61-78	65-84	69-88	61-78	51-61	51-61	86-105	91-110	91-110	86-105	86-105	108-132	108-132	108-132	108-132	99-125
Poor (Unstable)	48+	48+	130+	133+	143+	111+	59+	59+	79+	85+	89+	79+	62+	62+	106+	111+	111+	106+	106+	133+	133+	133+	126+	B4
Stream type	DA3	DA4	DA5	DA6	E3	E4	E5	E6	F1	F2	F3	F4	F5	F6	G1	G2	G3	G4	G5	G6	G6	G6	G6	*Potential stream type = B4
Good (Stable)	40-63	40-63	40-63	40-63	40-63	50-75	50-75	40-63	60-85	85-110	85-110	90-115	80-95	80-95	40-60	40-60	85-107	85-107	85-107	90-112	85-107	85-107	85-107	Modified channel stability rating = Good
Fair (Mod. unstable)	64-86	64-86	64-86	64-86	64-86	76-96	76-96	64-86	86-105	86-105	111-125	111-125	116-130	96-110	61-78	61-78	108-120	108-120	108-120	113-125	108-120	108-120	108-120	
Poor (Unstable)	87+	87+	87+	87+	87+	97+	97+	87+	106+	106+	126+	126+	131+	111+	79+	79+	121+	121+	121+	126+	121+	126+	121+	

\*Rating is adjusted to potential stream type, not existing.

## BANCS Model – Streambank Erosion

**Worksheet 5-16a.** The Bank Erosion Hazard Index (BEHI) rating.

Stream: <b>Trail Creek, B4 Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>	
Station: <b>0+00 L</b>		Observers: <b>Rosgen &amp; Kasun</b>	
Date: <b>8/14/2010</b>	Stream Type: <b>B4</b>	Valley Type: <b>VIII</b>	

<b>Study Bank Height / Bankfull Height ( C )</b>					<b>BEHI Score</b> (Fig. 5-15)	
Study Bank Height (ft) =	<b>5.00</b> (A)	Bankfull Height (ft) =	<b>1.00</b> (B)	( A ) / ( B ) =	<b>5.00</b> (C)	<b>10.0</b>
<b>Root Depth / Study Bank Height ( E )</b>						
Root Depth (ft) =	<b>4.50</b> (D)	Study Bank Height (ft) =	<b>5.00</b> (A)	( D ) / ( A ) =	<b>0.90</b> (E)	<b>1.0</b>
<b>Weighted Root Density ( G )</b>						
Root Density as % =	<b>75</b> (F)	( F ) × ( E ) =	<b>67.5</b> (G)		<b>3.0</b>	
<b>Bank Angle ( H )</b>						
Bank Angle as Degrees =	<b>30</b> (H)				<b>3.0</b>	
<b>Surface Protection ( I )</b>						
Surface Protection as % =	<b>95%</b> (I)				<b>1.0</b>	

<b>Bank Material Adjustment:</b>	<b>Bank Material Adjustment</b>
<ul style="list-style-type: none"> <li><b>Bedrock</b> (Overall Very Low BEHI)</li> <li><b>Boulders</b> (Overall Low BEHI)</li> <li><b>Cobble</b> (Subtract 10 points if uniform medium to large cobble)</li> <li><b>Gravel or Composite Matrix</b> (Add 5–10 points depending on percentage of bank material that is composed of sand)</li> <li><b>Sand</b> (Add 10 points)</li> <li><b>Silt/Clay</b> (no adjustment)</li> </ul>	<b>0</b>
	<b>Stratification Adjustment</b> Add 5–10 points, depending on position of unstable layers in relation to bankfull stage
	<b>0</b>

<b>Very Low</b>	<b>Low</b>	<b>Moderate</b>	<b>High</b>	<b>Very High</b>	<b>Extreme</b>	<b>Adjective Rating and Total Score</b>	<b>Low</b>
5 – 9.5	10 – 19.5	20 – 29.5	30 – 39.5	40 – 45	46 – 50		<b>18.0</b>

**Bank Sketch**

**Worksheet 5-16b.** The Bank Erosion Hazard Index (BEHI) rating.

Stream: <b>Trail Creek, B4 Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>	
Station: <b>2+26</b>		Observers: <b>Rosgen &amp; Kasun</b>	
Date: <b>8/14/2010</b>	Stream Type: <b>B4</b>	Valley Type: <b>VIII</b>	

<b>Study Bank Height / Bankfull Height ( C )</b>					<b>BEHI Score</b> (Fig. 5-15)
Study Bank Height (ft) =	<b>1.00</b> (A)	Bankfull Height (ft) =	<b>1.00</b> (B)	( A ) / ( B ) =	<b>1.00</b> (C)
<b>Root Depth / Study Bank Height ( E )</b>					
Root Depth (ft) =	<b>1.00</b> (D)	Study Bank Height (ft) =	<b>1.00</b> (A)	( D ) / ( A ) =	<b>1.00</b> (E)
<b>Weighted Root Density ( G )</b>					
Root Density as % =	<b>85</b> (F)	( F ) × ( E ) =	<b>85</b> (G)	<b>1.0</b>	
<b>Bank Angle ( H )</b>					
Bank Angle as Degrees =	<b>40</b> (H)	<b>3.0</b>			
<b>Surface Protection ( I )</b>					
Surface Protection as % =	<b>85%</b> (I)	<b>1.0</b>			

<p><b>Bank Material Adjustment:</b></p> <ul style="list-style-type: none"> <li><b>Bedrock</b> (Overall Very Low BEHI)</li> <li><b>Boulders</b> (Overall Low BEHI)</li> <li><b>Cobble</b> (Subtract 10 points if uniform medium to large cobble)</li> <li><b>Gravel or Composite Matrix</b> (Add 5–10 points depending on percentage of bank material that is composed of sand)</li> <li><b>Sand</b> (Add 10 points)</li> <li><b>Silt/Clay</b> (no adjustment)</li> </ul>	<p><b>Bank Material Adjustment</b></p> <p style="text-align: center; font-size: 2em; color: blue;">➔</p> <p><b>Stratification Adjustment</b></p> <p>Add 5–10 points, depending on position of unstable layers in relation to bankfull stage</p>
	<b>-10</b>
	<b>0</b>

<b>Very Low</b>	<b>Low</b>	<b>Moderate</b>	<b>High</b>	<b>Very High</b>	<b>Extreme</b>	<b>Adjective Rating and Total Score</b>
5 – 9.5	10 – 19.5	20 – 29.5	30 – 39.5	40 – 45	46 – 50	<b>Very Low</b>
➔						<b>-3.0</b>

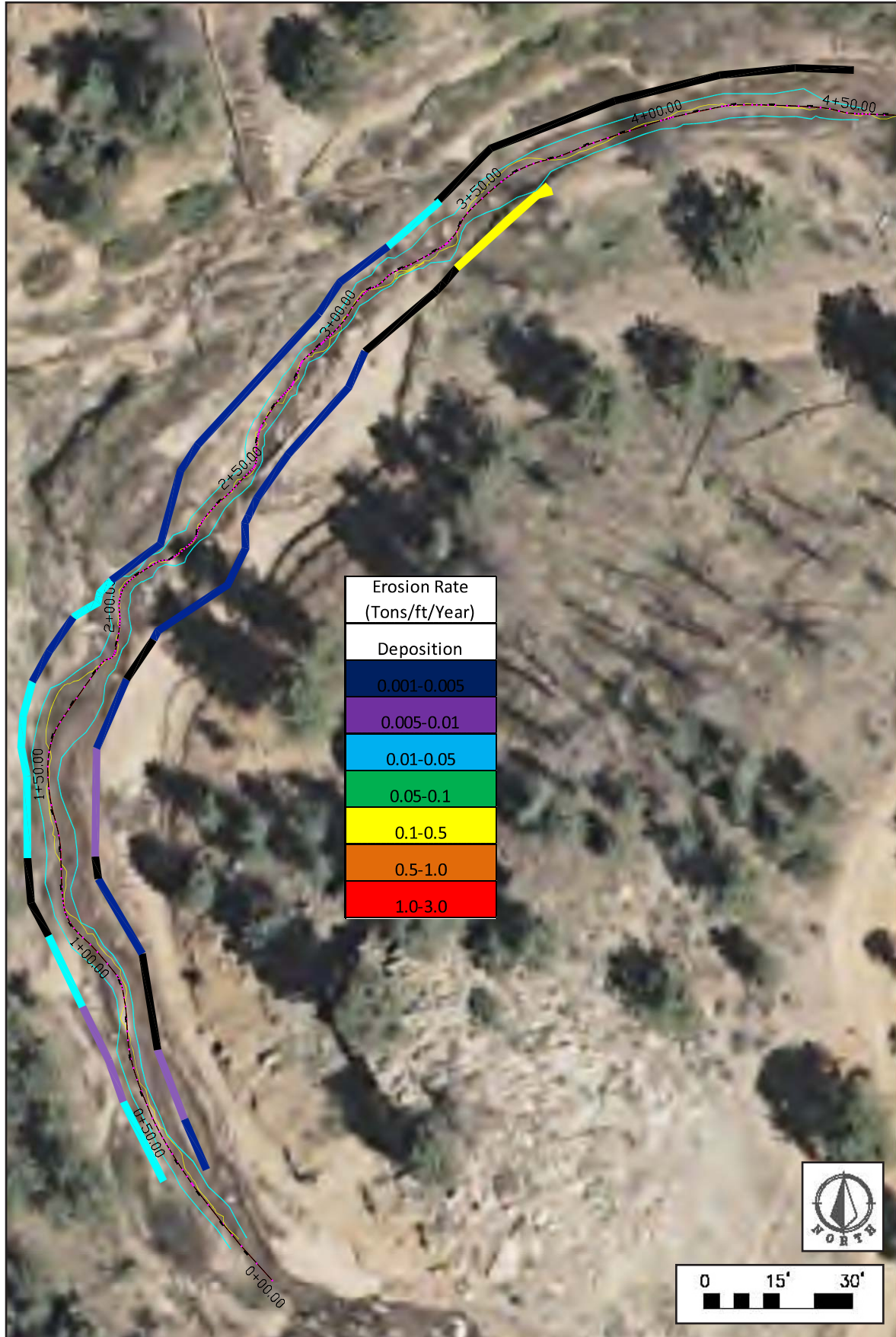
  

<p style="text-align: center;"><b>Bank Sketch</b></p>	
---	--

**Worksheet 5-18.** Annual streambank erosion estimates.

Stream: <b>Trail Creek, B4 Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>					
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>406</b>			Date: <b>8/14/2010</b>		
Observers: <b>Rosgen &amp; Kasun</b>		Valley Type: <b>VIII</b>		Stream Type: <b>B4</b>			
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 5-16) (adjective)	NBS rating (Worksheet 5-17) (adjective)	Bank erosion rate (Figure 5-34 or 5- 35) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [[4]×(5)×(6)] (ft <sup>3</sup> /yr)	Erosion Rate (tons/yr/ft) {[(7)/27] × 1.3 / (5)}
1. <b>0+26L</b>	<b>Low</b>	<b>High</b>	<b>0.15505</b>	<b>26.0</b>	<b>5.0</b>	<b>20.16</b>	<b>0.03733</b>
2. <b>0+20R</b>	<b>Very Low</b>	<b>Low</b>	<b>0.00386</b>	<b>20.0</b>	<b>1.0</b>	<b>0.08</b>	<b>0.00019</b>
3. <b>0+57R</b>	<b>Very Low</b>	<b>High</b>	<b>0.02130</b>	<b>37.0</b>	<b>1.0</b>	<b>0.79</b>	<b>0.00103</b>
4. <b>0+27L</b>	<b>Moderate</b>	<b>Low</b>	<b>0.15287</b>	<b>11.0</b>	<b>1.0</b>	<b>1.68</b>	<b>0.00736</b>
5. <b>0+54L</b>	<b>Very Low</b>	<b>High</b>	<b>0.02130</b>	<b>19.0</b>	<b>1.0</b>	<b>0.40</b>	<b>0.00103</b>
6. <b>0+63R</b>	<b>Low</b>	<b>Moderate</b>	<b>0.07435</b>	<b>20.0</b>	<b>1.0</b>	<b>1.49</b>	<b>0.00358</b>
7. <b>0+92L</b>	<b>Very Low</b>	<b>Low</b>	<b>0.00386</b>	<b>53.0</b>	<b>1.0</b>	<b>0.20</b>	<b>0.00019</b>
8 <b>1+35</b>	<b>Very Low</b>	<b>High</b>	<b>0.02130</b>	<b>17.0</b>	<b>1.0</b>	<b>0.36</b>	<b>0.00103</b>
9 <b>1+38L</b>	<b>Very Low</b>	<b>Very High</b>	<b>0.05002</b>	<b>17.0</b>	<b>1.0</b>	<b>0.85</b>	<b>0.00241</b>
10 <b>1+58R</b>	<b>Very Low</b>	<b>Moderate</b>	<b>0.00907</b>	<b>17.0</b>	<b>1.0</b>	<b>0.15</b>	<b>0.00044</b>
11 <b>1+69L</b>	<b>Very Low</b>	<b>Low</b>	<b>0.00386</b>	<b>6.0</b>	<b>1.0</b>	<b>0.02</b>	<b>0.00019</b>
12 <b>1+75L</b>	<b>Moderate</b>	<b>Low</b>	<b>0.15287</b>	<b>18.0</b>	<b>4.5</b>	<b>12.38</b>	<b>0.03312</b>
13 <b>2+26L</b>	<b>Very Low</b>	<b>Very Low</b>	<b>0.00164</b>	<b>47.0</b>	<b>1.0</b>	<b>0.08</b>	<b>0.00008</b>
14 <b>2+26R</b>	<b>Very Low</b>	<b>Very Low</b>	<b>0.00164</b>	<b>47.0</b>	<b>1.0</b>	<b>0.08</b>	<b>0.00008</b>
15 <b>2+71L</b>	<b>Low</b>	<b>Low</b>	<b>0.03566</b>	<b>29.0</b>	<b>2.0</b>	<b>2.07</b>	<b>0.00343</b>
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					<b>Total Erosion (ft<sup>3</sup>/yr)</b>	<b>40.79</b>	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					<b>Total Erosion (yds<sup>3</sup>/yr)</b>	<b>1.51</b>	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					<b>Total Erosion (tons/yr)</b>	<b>1.96</b>	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					<b>Total Erosion (tons/yr/ft)</b>	<b>0.0048</b>	

Streambank Erosion Map



## FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Equation Type		Equation Source		Equation		Bankfull Discharge (cfs)		Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)				
1. Bedload Sediment		"Good/Fair" Pagosa		$y = -0.0113 + 1.0139x^{2.1929}$		32.78		0.017684404		28.94115478				
2. Suspended Sediment		"Good/Fair" Pagosa		$y = 0.0636 + 0.9326x^{2.4085}$										
From Dimensional Flow-Duration Curve														
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)			
Percentage of Time	Daily Mean Discharge	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Suspended Sediment Discharge	Suspended Sediment Discharge	Dimensionless Bedload Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow [(5)×(6)]			
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>90%</sub> )	(S/S <sub>90%</sub> )	(tons/day)	(b <sub>d</sub> /b <sub>90%</sub> )	(tons/day)	(cfs)			
0%	83.4													
0.10%	71.5	0.05%	0.09%	0.34	77.5	2.363	7.461	45.16	6.670	11.24	26.6			
0.25%	61.9	0.08%	0.15%	0.55	66.7	2.036	5.232	27.28	4.809	8.10	36.5			
0.50%	53.5	0.13%	0.25%	0.91	57.7	1.761	3.706	16.71	3.494	5.89	52.7			
0.75%	45.7	0.13%	0.25%	0.91	49.6	1.513	2.592	10.04	2.502	4.22	45.3			
1%	39.5	0.13%	0.25%	0.91	42.6	1.300	1.817	6.05	1.790	3.02	38.9			
1.5%	33.9	0.25%	0.50%	1.83	36.7	1.120	1.289	3.70	1.289	2.17	67.0			
2%	28.3	0.25%	0.50%	1.83	31.1	0.949	0.886	2.15	0.893	1.50	56.8			
3%	23.8	0.50%	1.00%	3.65	26.1	0.795	0.600	1.22	0.602	1.01	95.1			
4%	20.4	0.50%	1.00%	3.65	22.1	0.674	0.424	0.73	0.415	0.70	80.6			
5%	18.1	0.50%	1.00%	3.65	19.2	0.587	0.322	0.48	0.304	0.51	70.2			
10%	11.4	2.50%	5.00%	18.25	14.8	0.450	0.200	0.23	0.165	0.28	269.3			
20%	6.2	5.00%	10.00%	36.50	8.8	0.269	0.103	0.07	0.045	0.08	321.3			
30%	4.1	5.00%	10.00%	36.50	5.2	0.158	0.075	0.03	0.006	0.01	189.0			
40%	2.9	5.00%	10.00%	36.50	3.5	0.108	0.068	0.02	0.000	0.00	129.1			
50%	2.2	5.00%	10.00%	36.50	2.6	0.079	0.066	0.01	0.000	0.00	94.5			
60%	1.7	5.00%	10.00%	36.50	2.0	0.061	0.065	0.01	0.000	0.00	72.4			
70%	1.4	5.00%	10.00%	36.50	1.6	0.047	0.064	0.01	0.000	0.00	56.7			
80%	1.2	5.00%	10.00%	36.50	1.3	0.039	0.064	0.01	0.000	0.00	47.2			
90%	0.9	5.00%	10.00%	36.50	1.0	0.032	0.064	0.01	0.000	0.00	37.8			
100%	0.2	5.00%	10.00%	36.50	0.5	0.016	0.064	0.00	0.000	0.00	18.9			
<b>Annual Totals:</b>											<b>1,805.9</b> (cfs)	<b>90.2</b> (tons/yr)	<b>43.4</b> (tons/yr)	<b>133.5</b> (tons/yr)
											<b>3,582.0</b> (acre-ft)			

**Worksheet 19b.** Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Equation Type		Equation Source				Equation		Bankfull Discharge (cfs)			Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)								
1. Bedload Sediment		"Good/Fair" Pagosa				$y = -0.0113 + 1.0139x^{2.1929}$		32.78			0.017684404		28.94115478								
2. Suspended Sediment		"Good/Fair" Pagosa				$y = 0.0636 + 0.9326x^{2.4085}$															
From Dimensional Flow-Duration Curve														From Sediment Rating Curves				Calculate		Calculate Sediment Yield	
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)							
Percentage of Time	Daily Mean Discharge	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Suspended Sediment Discharge	Suspended Sediment Discharge	Dimensionless Bedload Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow [(5)×(6)]	Suspended Sediment [(5)×(9)]	Bedload Sediment [(5)×(11)]	Suspended + Bedload Sediment [(13)×(14)]							
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>bed</sub> )	(S/S <sub>bed</sub> )	(tons/day)	(b <sub>y</sub> /b <sub>bed</sub> )	(tons/day)	(cfs)	(tons)	(tons)	(tons)							
0%	113.6																				
0.10%	101.8	0.05%	0.09%	0.34	107.7	3.285	16.420	138.16	13.749	23.16	36.9	47.40	7.95	55.35							
0.25%	92.1	0.08%	0.15%	0.55	97.0	2.958	12.771	96.76	10.923	18.40	53.1	52.97	10.08	63.05							
0.50%	83.7	0.13%	0.25%	0.91	87.9	2.683	10.107	69.45	8.815	14.85	80.2	63.37	13.55	76.92							
0.75%	75.9	0.13%	0.25%	0.91	79.8	2.435	8.017	50.00	7.126	12.01	72.8	45.62	10.95	56.58							
1%	69.7	0.13%	0.25%	0.91	72.8	2.222	6.441	36.66	5.826	9.82	66.5	33.45	8.96	42.41							
1.5%	63.7	0.25%	0.50%	1.83	66.7	2.036	5.230	27.27	4.807	8.10	121.8	49.76	14.78	64.55							
2%	57.7	0.25%	0.50%	1.83	60.7	1.851	4.175	19.80	3.903	6.58	110.8	36.13	12.00	48.13							
3%	53.2	0.50%	1.00%	3.65	55.4	1.691	3.368	14.59	3.197	5.39	202.3	53.25	19.66	72.91							
4%	47.3	0.50%	1.00%	3.65	50.3	1.533	2.675	10.51	2.578	4.34	183.5	38.35	15.85	54.20							
5%	41.9	0.50%	1.00%	3.65	44.6	1.361	2.021	7.04	1.980	3.34	162.8	25.71	12.18	37.89							
10%	26.1	2.50%	5.00%	18.25	34.0	1.036	1.079	2.86	1.085	1.83	619.9	52.29	33.35	85.64							
20%	8.8	5.00%	10.00%	36.50	17.4	0.532	0.267	0.36	0.242	0.41	636.0	13.28	14.90	28.18							
30%	4.3	5.00%	10.00%	36.50	6.5	0.200	0.083	0.04	0.018	0.03	238.8	1.55	1.13	2.67							
40%	2.9	5.00%	10.00%	36.50	3.6	0.111	0.068	0.02	0.000	0.00	132.3	0.71	0.00	0.71							
50%	2.2	5.00%	10.00%	36.50	2.6	0.079	0.066	0.01	0.000	0.00	94.5	0.48	0.00	0.48							
60%	1.7	5.00%	10.00%	36.50	2.0	0.061	0.065	0.01	0.000	0.00	72.4	0.37	0.00	0.37							
70%	1.4	5.00%	10.00%	36.50	1.6	0.047	0.064	0.01	0.000	0.00	56.7	0.28	0.00	0.28							
80%	1.2	5.00%	10.00%	36.50	1.3	0.039	0.064	0.01	0.000	0.00	47.2	0.24	0.00	0.24							
90%	0.9	5.00%	10.00%	36.50	1.0	0.032	0.064	0.01	0.000	0.00	37.8	0.19	0.00	0.19							
100%	0.2	5.00%	10.00%	36.50	0.5	0.016	0.064	0.00	0.000	0.00	18.9	0.09	0.00	0.09							
<b>Annual Totals:</b>											<b>3,045.2</b> (cfs)	<b>515.5</b> (tons/yr)	<b>175.3</b> (tons/yr)	<b>690.8</b> (tons/yr)							
											<b>6,040.1</b> (acre-ft)										



## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>Trail Creek, B4 Reference Reach</b>		Stream Type: <b>B4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>Rosgen &amp; Kasun</b>		Date: <b>8/14/2010</b>			
<b>Enter Required Information for Existing Condition</b>					
22.6	$D_{50}$	Riffle bed material $D_{50}$ (mm)			
14.5	$D_{50}^{\wedge}$	Bar sample $D_{50}$ (mm)			
0.33	$D_{max}$	Largest particle from bar sample (ft)	100	(mm)	304.8 mm/ft
0.0242	S	Existing bankfull water surface slope (ft/ft)			
0.74	d	Existing bankfull mean depth (ft)			
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment			
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>					
1.56	$D_{50}/D_{50}^{\wedge}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 ( D_{50}/D_{50}^{\wedge} )^{-0.872}$		
4.42	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 ( D_{max}/D_{50} )^{-0.887}$		
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED:		
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	d	Required bankfull mean depth (ft)	$d = \frac{\tau^* (\gamma_s - 1) D_{max}}{S}$ (use $D_{max}$ in ft)		
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	S	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^* (\gamma_s - 1) D_{max}}{d}$ (use $D_{max}$ in ft)		
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					
<b>Sediment Competence Using Dimensional Shear Stress</b>					
1.117	Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d) $\gamma = 62.4$ , d = existing depth, S = existing slope				
Shields	CO	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ (Figure 5-49)			
84	180				
Shields	CO	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) (Figure 5-49)			
1.4	0.58				
Shields	CO	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm)		$d = \frac{\tau}{\gamma S}$	
0.93	0.38	$\tau$ = predicted shear stress, $\gamma = 62.4$ , S = existing slope			
Shields	CO	Predicted slope required to initiate movement of measured $D_{max}$ (mm)		$S = \frac{\tau}{\gamma d}$	
0.0303	0.0126	$\tau$ = predicted shear stress, $\gamma = 62.4$ , d = existing depth			
Check: <input checked="" type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					

## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>Trail Creek, B4 Reference</b>	Stream Type: <b>B4</b>
Location: <b>Pike National Forest, CO</b>	Valley Type: <b>VIII</b>
Observers: <b>Rosgen &amp; Kasun</b>	Date: <b>8/14/2010</b>
<b>Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)</b>	<b>Stability Rating (Check Appropriate Rating)</b>
<b>Stream type at potential, (C→E), (F<sub>b</sub>→B), (G→B), (F→B<sub>c</sub>), (F→C), (D→C)</b>	<input checked="" type="checkbox"/> Stable
(E→C), (C→High W/d C)	<input type="checkbox"/> Moderately Unstable
(G→F), (F→D), (C→F)	<input type="checkbox"/> Unstable
(C→D), (B→G), (D→G), (C→G), (E→G)	<input type="checkbox"/> Highly Unstable

Worksheet 5-25. Lateral stability.

Stream: <b>Trail Creek, B4 Reference Reach</b>		Stream Type: <b>B4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>Rosgen &amp; Kasun</b>		Date: <b>8/14/2010</b>			
Lateral stability criteria (choose one stability category for each criterion 1–5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	2
	1.0 (2)	(4)	(6)	(8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	2
	(1)	B4 (2)	(3)	(4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		1
	M1, M3 (1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	2
	(2)	(4)	(6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	1
	1.0 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>8</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input checked="" type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input type="checkbox"/>	<i>Unstable</i> 13 – 21 <input type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	

**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>Trail Creek, B4 Reference Reach</b>		Stream Type: <b>B4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>Rosgen &amp; Kasun</b>		Date: <b>8/14/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
1 <b>Sediment competence</b> (Worksheet 5-22)	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope—slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	2
	(2)	(4)	(6)	(8)	
2 <b>Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	2
	Ref. Reach (2)	(4)	(6)	(8)	
3 <b>W/d Ratio State</b> (Worksheet 5-13)	1.0 – 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	2
	1.0 (2)	(4)	(6)	(8)	
4 <b>Stream Succession States</b> (Worksheet 5-24)	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	2
	at potential (2)	(4)	(6)	(8)	
5 <b>Depositional Patterns</b> (Worksheet 5-10)	B1	B2, B4	B3, B5	B6, B7, B8	2
	(1)	B4 (2)	(3)	(4)	
6 <b>Debris / Blockages</b> (Worksheet 5-11)	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	1
	D2 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>11</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
<b>Vertical Stability for Excess Deposition / Aggradation</b> (use total points and check stability rating)	<i>No Deposition</i> 10 – 14 <input checked="" type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input type="checkbox"/>	<i>Aggradation</i> > 30 <input type="checkbox"/>	

Worksheet 5-27. Vertical stability – degradation.

Stream: <b>Trail Creek, B4 Reference Reach</b>		Stream Type: <b>B4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>Rosgen &amp; Kasun</b>		Date: <b>8/14/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>Sediment Competence</b> (Worksheet 5-22)	Does not indicate excess competence	Trend to move larger sizes than $D_{100}$ of bar or > $D_{84}$ of bed	$D_{100}$ of bed moved	Particles much larger than $D_{100}$ of bed moved	2
	(2)	(4)	(6)	(8)	
<b>Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Does not indicate excess capacity	Slight excess energy: up to 10% increase above reference	Excess energy sufficient to increase load up to 50% of annual load	Excess energy transporting more than 50% of annual load	2
	Ref. Reach (2)	(4)	(6)	(8)	
<b>Degree of Channel Incision (BHR)</b> (Worksheet 5-12)	1.00 – 1.10	1.11 – 1.30	1.31 – 1.50	> 1.50	2
	1.00 (2)	(4)	(6)	(8)	
<b>Stream Succession States</b> (Worksheets 5-12 and 5-24)	Does not indicate incision or degradation	If BHR > 1.1 and stream type has W/d between 5–10	If BHR > 1.1 and stream type has W/d less than 5	(B→G), (C→G), (E→G), (D→G)	2
	(2)	(4)	(6)	(8)	
<b>Confinement (MWR / MWR<sub>ref</sub>)</b> (Worksheet 5-14)	0.80 – 1.00	0.30 – 0.79	0.10 – 0.29	< 0.10	1
	1.00 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>9</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
Vertical Stability for Channel Incision/ Degradation (use total points and check stability rating)	<i>Not Incised</i> 9 – 11 <input checked="" type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input type="checkbox"/>	<i>Degradation</i> > 27 <input type="checkbox"/>	

**Worksheet 5-28.** Channel enlargement.

Stream: <b>Trail Creek, B4 Reference Reach</b>		Stream Type: <b>B4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>Rosgen &amp; Kasun</b>		Date: <b>8/14/2010</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1-4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	2
	at potential (2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	Stable	Moderately Unstable	Unstable	Highly Unstable	2
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	No Deposition	Moderate Deposition	Excess Deposition	Aggradation	2
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	Not Incised	Slightly Incised	Moderately Incised	Degradation	2
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>8</b>
<b>Category Point Range</b>					
Channel Enlargement Prediction (use total points and check stability rating)	<i>No Increase</i> 8 – 10 <input checked="" type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input type="checkbox"/>	<i>Extensive</i> > 24 <input type="checkbox"/>	

Worksheet 5-29. Overall sediment supply.

Stream: <b>Trail Creek, B4 Reference Reach</b>		Stream Type: <b>B4</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>		
Observers: <b>Rosgen &amp; Kasun</b>		Date: <b>8/14/2010</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1–5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	1	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	1	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	1	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	1	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	1	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>5</b>	
<b>Category Point Range</b>				
Overall Sediment Supply Rating (use total points and check stability rating)	<i>Low</i> 5 <input checked="" type="checkbox"/>	<i>Moderate</i> 6 – 10 <input type="checkbox"/>	<i>High</i> 11 – 15 <input type="checkbox"/>	<i>Very High</i> 16 – 20 <input type="checkbox"/>

Worksheet 5-32. Summary of stability condition categories.

Stream: <b>Trail Creek, B4 Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>	
Observers: <b>Rosgen &amp; Kasun</b>		Stream Type: <b>B4</b> Valley Type: <b>VIII</b>	
Channel Dimension (Rifle XS 0+18.5)	Mean Bankfull Depth (ft): <b>0.74</b>	Bankfull Width (ft): <b>9.31</b>	Cross-Sectional Area (ft <sup>2</sup> ): <b>6.91</b>
	Width of Flood-Prone Area (ft): <b>18.48</b>	Entrenchment Ratio: <b>1.99</b>	
Channel Pattern	Mean: $\lambda/W_{bkf}$ : <b>10.4</b>	$L_m/W_{bkf}$ : <b>8.7-12.9</b>	$R_c/W_{bkf}$ : <b>3.9</b>
	Range: <b>8.7-12.9</b>	<b>11.2</b>	<b>9.4-13.5</b>
River Profile & Bed Features	Check: <input type="checkbox"/> Riffle/Pool <input checked="" type="checkbox"/> Step/Pool <input type="checkbox"/> Plane Bed <input type="checkbox"/> Convergence/Divergence <input type="checkbox"/> Dunes/Antidunes/Smooth Bed	Riffle Pool	Pool-to-Pool Ratio
	Max Bankfull Depth (ft): <b>1.06</b>	Depth Ratio (max to mean): <b>1.53</b>	Pool Spacing: <b>2.8</b>
Level III Stream Stability Indices	Riparian Vegetation: <b>Aspen, Willow - High</b>	Potential Composition/Density: <b>Aspen, Willow - High</b>	Remarks: Condition, Vigor & Usage of Existing Reach: <b>Recovering Riparian inside of past G/F<sub>b</sub></b>
	Flow Regime: <b>P1, P2, P8 &amp; Order: P1, P2, P8</b>	Stream Size: <b>S-3(3)</b>	Meander Patterns: <b>M1, M3</b>
	Degree of Incision (Bank-Height Ratio): <b>1.0</b>	Degree of Incision Stability Rating: <b>Stable</b>	Depositional Patterns: <b>B4</b>
	Width/depth Ratio (W/d): <b>12.6</b>	Reference W/d Ratio (W/d <sub>ref</sub> ): <b>12.6</b>	Modified Pfankuch Stability Rating (Numeric & Adjective Rating): <b>60 (Good)</b>
Bank Erosion Summary	Meander Width Ratio (MWR): <b>2.7</b>	Reference MWR <sub>ref</sub> : <b>2.7</b>	W/d Ratio State Stability Rating: <b>Stable</b>
	Length of Reach Studied (ft): <b>406</b>	Annual Streambank Erosion Rate: <b>1.96</b> (tons/yr)	MWR / MWR <sub>ref</sub> Stability Rating: <b>1.0</b>
Sediment Capacity (POWERSED)	<input checked="" type="checkbox"/> Sufficient Capacity <input type="checkbox"/> Insufficient Capacity <input type="checkbox"/> Excess Capacity	Curve Used: <b>Colorado</b>	Remarks:
	Entrainment/Competence	Largest Particle from Bar Sample (mm): <b>100</b>	Required Depth: <b>0.70</b>
Successional Stage Shift	<b>C</b> → <b>G</b> → <b>F</b> → <b>B</b> → <b>B4</b>	Existing Depth: <b>N/A</b>	Existing Slope: <b>.38-</b>
	Lateral Stability	Existing State (Type): <b>Highly Unstable</b>	Required Slope: <b>0.024</b>
Vertical Stability (Aggradation)	<input checked="" type="checkbox"/> Stable <input type="checkbox"/> Mod. Unstable <input type="checkbox"/> Unstable	Existing State (Type): <b>B4</b>	Potential Stream State (Type): <b>B4</b>
	Vertical Stability (Degradation)	<input checked="" type="checkbox"/> No Deposition <input type="checkbox"/> Mod. Deposition <input type="checkbox"/> Ex. Deposition	Remarks/causes: <b>Reference Reach</b>
Channel Enlargement	<input checked="" type="checkbox"/> Not Incised <input type="checkbox"/> Slightly Incised <input type="checkbox"/> Mod. Incised	Remarks/causes: <b>Reference Reach</b>	Remarks/causes: <b>Reference Reach</b>
	Sediment Supply (Channel Source)	<input checked="" type="checkbox"/> No Increase <input type="checkbox"/> Slight Increase <input type="checkbox"/> Mod. Increase <input type="checkbox"/> Extensive	Remarks/causes: <b>Reference Reach</b>
Channel Enlargement	<input checked="" type="checkbox"/> Low <input type="checkbox"/> Moderate <input type="checkbox"/> High <input type="checkbox"/> Very High	Remarks/causes: <b>Reference Reach</b>	Remarks/causes: <b>Reference Reach</b>
	Sediment Supply (Channel Source)	Remarks/causes: <b>Reference Reach</b>	Remarks/causes: <b>Reference Reach</b>



## *Appendix C19*

# **B4/2c Stream Type** *Reference Reach*



# Table of Contents

## *Appendix C19: B4/2c Reference Reach*

<b>Reach Location &amp; Overview.....</b>	<b>C19-2</b>
<b>Survey Summary.....</b>	<b>C19-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C19-6</b>
<b><i>Velocity, Classification &amp; Morphological Relations.....</i></b>	<b>C19-6</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b><i>Stability Indices.....</i></b>	<b>C19-10</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b><i>BANCS Model – Streambank Erosion.....</i></b>	<b>C19-20</b>
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b><i>FLOWSED Model – Total Annual Sediment Yield.....</i></b>	<b>C19-22</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b><i>Sediment Competence/Entrainment.....</i></b>	<b>C19-24</b>
Worksheet 5-22. Sediment competence calculations.	
<b><i>Channel Stability Ratings.....</i></b>	<b>C19-25</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b><i>Summary.....</i></b>	<b>C19-31</b>
Worksheet 5-32. Summary of stability condition categories.	

## B4/2c Reference Reach Location & Overview

The B4/2c reference reach is in a Valley Type VIIIb located on the mainstem on West Monument Creek (see location map **Figure C-1**). This reach is dominated by gravel and influenced by boulders. The channel bed and banks show little sediment yield and good stability from abundant vegetation and boulders. Bed features are generally dominated by rapids and pool. The channel is perennial and streamflow is seasonal by snowmelt and stormflow runoff. Flow is regulated by an upstream dam and is altered due to Waldo Canyon Fire. The reach is a 4<sup>th</sup> order channel. This reach has very low streambank erosion rates ( $0.0050 \text{ tons/yr/ft}$ , see **Worksheet 5-18**).

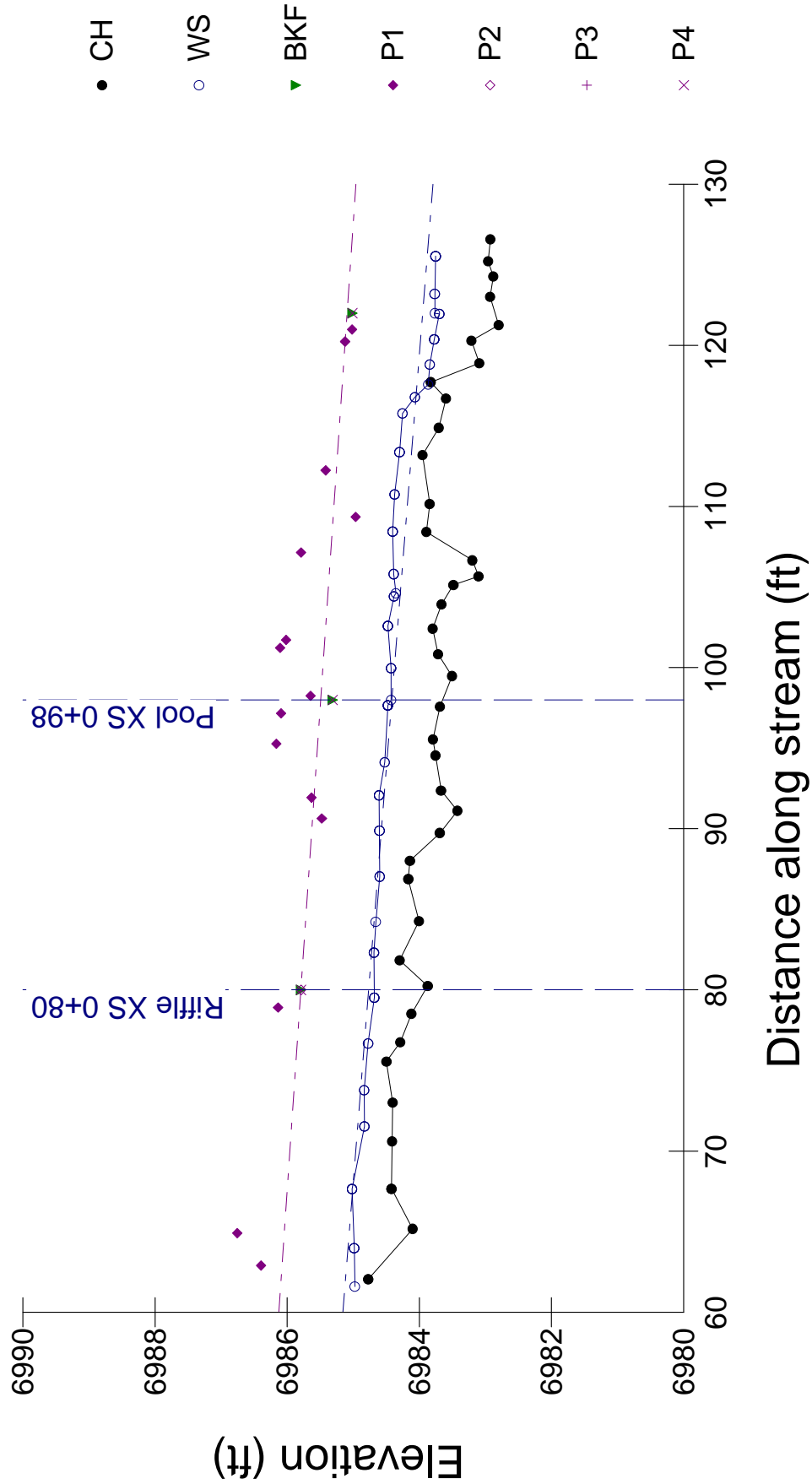
The photograph depicts the stable characteristics of this stream type. There is little to no evidence of active channel-source sediment from this stream type. Such stream types are mapped where they occur by sub-watershed as shown in **Appendix D**.

The details of the dimension, pattern, profile, and materials are summarized. The following summary worksheets provide details of the morphology, hydraulics, stability, and streambank erosion rates for this reference reach. In the situation where impaired B4/2, G4/2, and F4/2 stream types are located, an alternative for mitigation and sediment reduction is to use the data from the stable form to extrapolate for potential implementation of natural channel design.

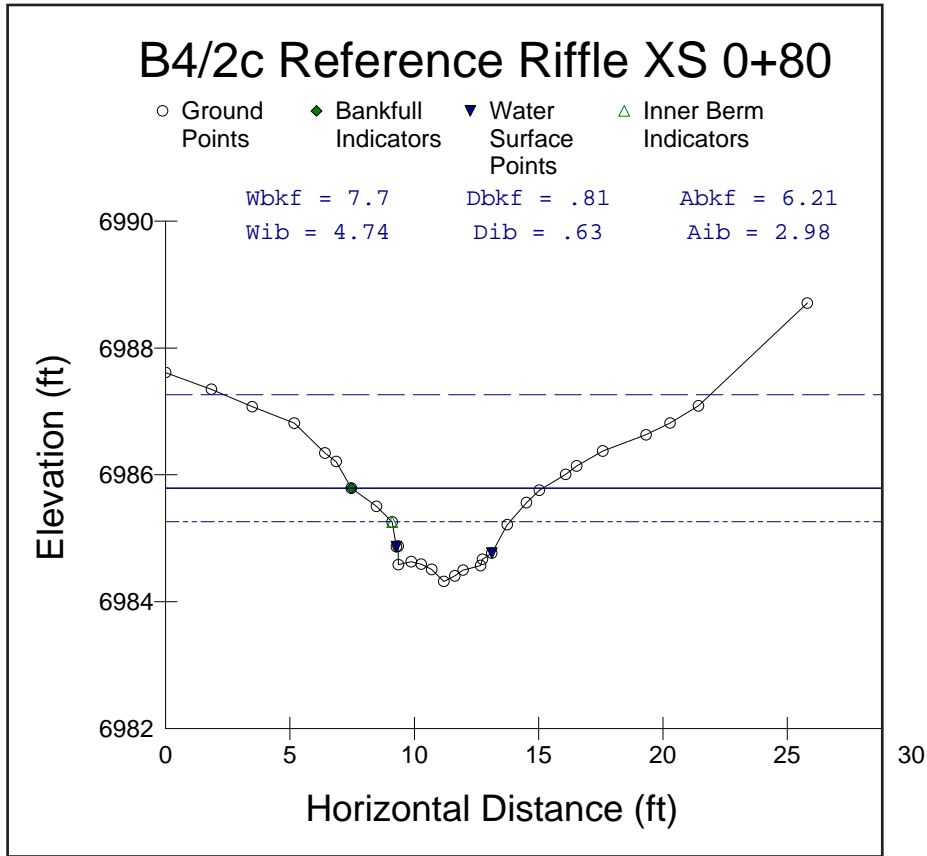


Survey Summary

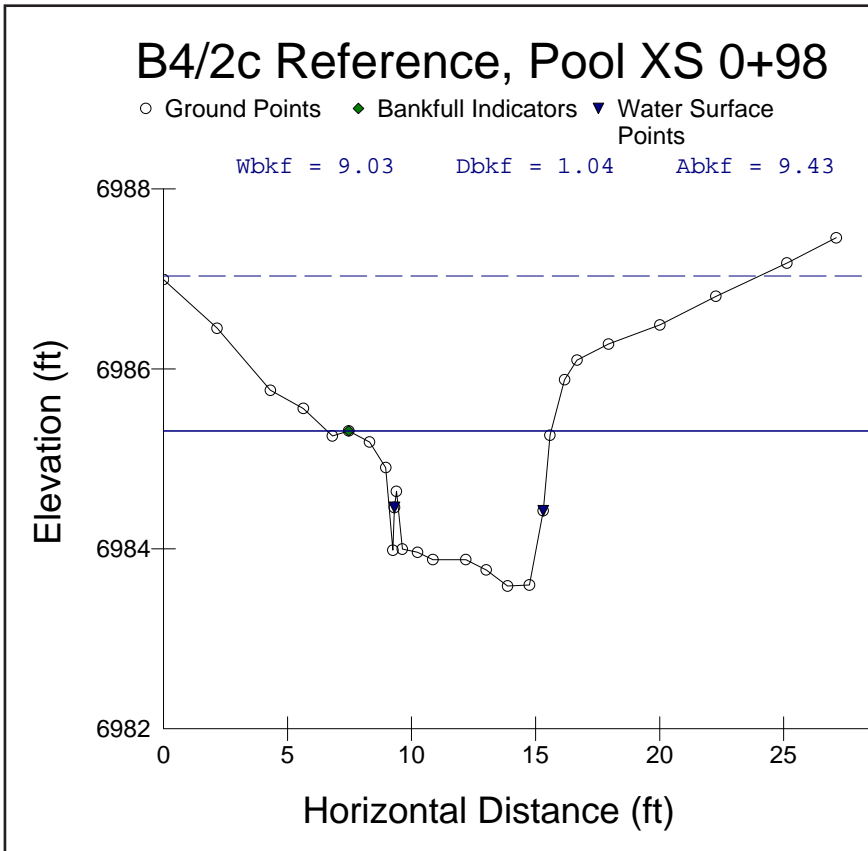
# B4/2c Reference Longitudinal Profile



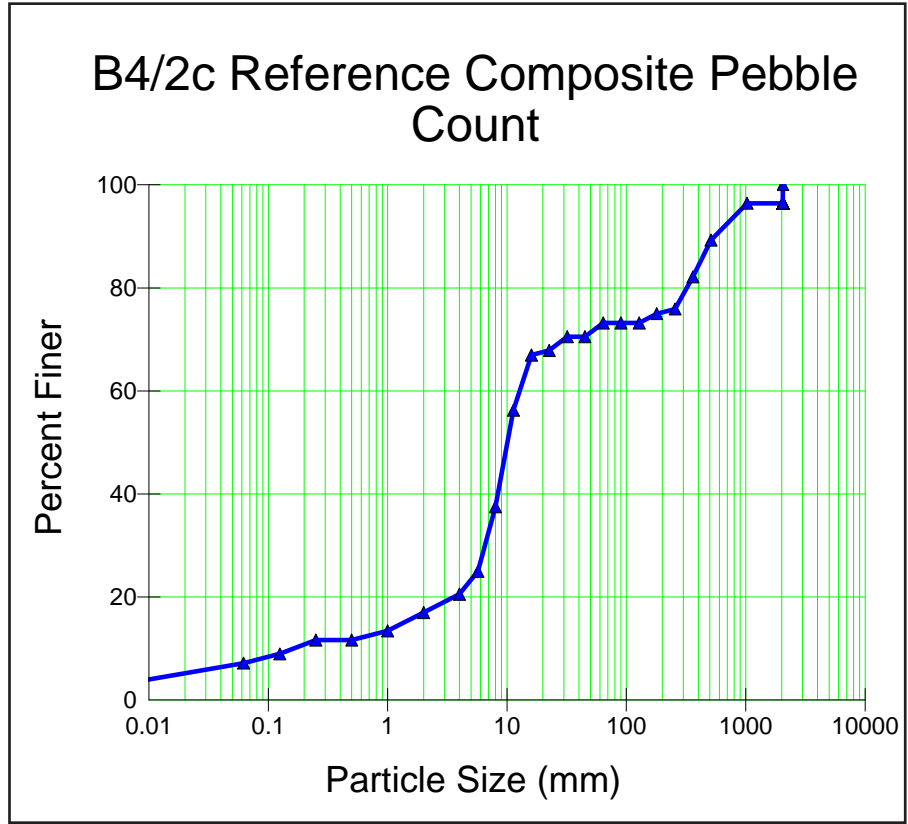
Longitudinal Profile (graph generated from RIVERMorph™)



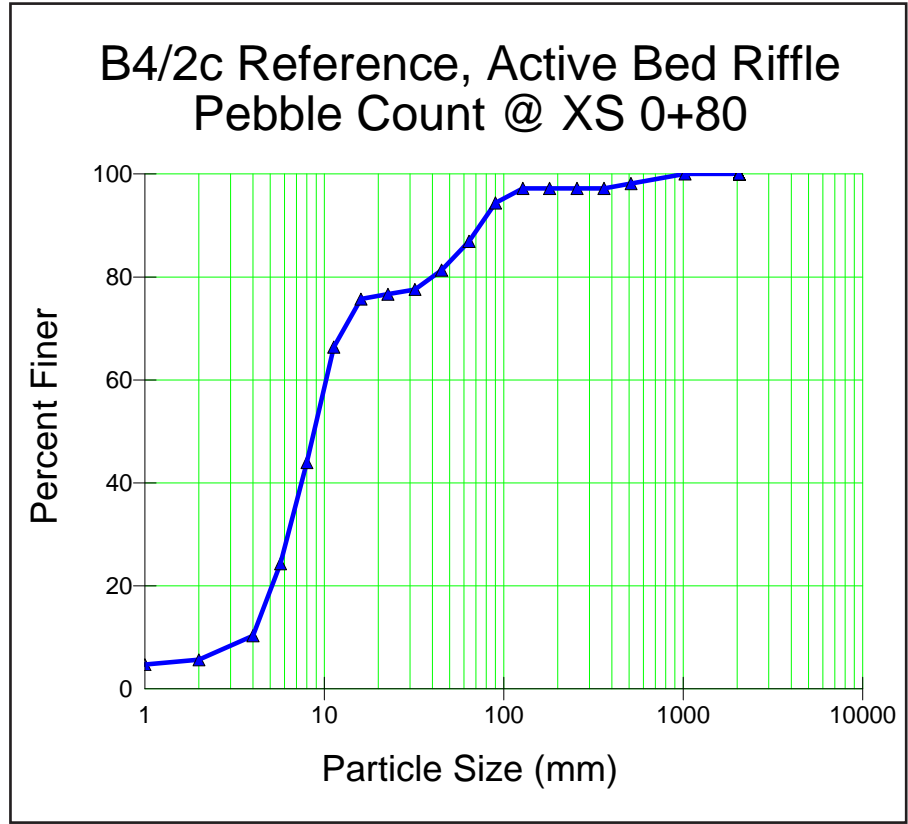
Representative Cross-section 0+80 (graph generated from RIVERMorph™)



Cross-section 0+98 (graph generated from RIVERMorph™)



**Composite Pebble Count** (graph generated from RIVERMorph™)



**Active Bed Pebble Count** (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates					
Stream:	West Monument B4/2c Reference			Location:	XS 0+80, Pike N.F., Colorado
Date:	11/6/2012	Stream Type:	B4/2c	Valley Type:	VIIIb
Observers:	Bones, Kyle, David, Luke, Kim			HUC:	___ ___ ___ ___ ___ ___ ___ ___ ___
INPUT VARIABLES			OUTPUT VARIABLES		
Bankfull Riffle Cross-Sectional AREA	6.21	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.81	$d_{bkf}$ (ft)
Bankfull Riffle WIDTH	7.7	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim (2 * d_{bkf}) + W_{bkf}$	8.72	$W_p$ (ft)
$D_{84}$ at Riffle	54.1	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.18	$D_{84}$ (ft)
Bankfull SLOPE	0.01	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	0.71	R (ft)
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R(ft) / $D_{84}$ (ft)	4.01	R / $D_{84}$
Drainage Area	10.95	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.546	$u^*$ (ft/sec)
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$			3.41	ft / sec	21.18 cfs
2. Roughness Coefficient: a) Manning's n from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.046$			2.94	ft / sec	18.26 cfs
2. Roughness Coefficient: b) Manning's n from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.08$			1.69	ft / sec	10.49 cfs
2. Roughness Coefficient: c) Manning's n from Jarrett (USGS): Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for Stream Types A1, A2, A3, B1, B2, B3, C2 & E3 $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ $n = 0.079$			1.71	ft / sec	10.64 cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Darcy-Weisbach (Leopold, Wolman and Miller)			3.85	ft / sec	23.9 cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)				ft / sec	cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q =$ <input type="text"/> year $u = Q / A$				ft / sec	cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$				ft / sec	cfs
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation (R/ $D_{84}$ ) – Estimation Method 1					
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.					
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.					
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.					
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.					



**Worksheet 5-3.** Level II stream classification.

Stream: <b>West Mounment Creek, B2/4c Reference</b>	
Basin:	Drainage Area: <b>7010</b> acres <b>10.95</b> mi <sup>2</sup>
Location: <b>Pike National Forest, Colorado</b>	
Twp.&Rge: ;	Sec.&Qtr.: ;
Cross-Section Monuments (Lat./Long.): <b>XS 0+80</b>	Date: <b>11/06/12</b>
Observers: <b>Bones, Kyle, David, Luke, Kim</b>	Valley Type: VIIIb

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>7.7</b> ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A_{bkf} / W_{bkf}$ ).	<b>0.81</b> ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>6.21</b> ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>9.51</b> ft/ft
<b>Maximum DEPTH (<math>d_{max}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>1.47</b> ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>19.54</b> ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>2.54</b> ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the median or dominant diameter of channel materials, as sampled proportionately from the channel surface, between the bankfull stage and Thalweg elevations.	<b>10.2</b> mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.013</b> ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope ( $S_{val} / S$ ).	<b>1.06</b>

<b>Stream Type</b>	<b>B2/4c</b>	<b>See Classification Key (Figure 2-14)</b>
--------------------	--------------	---

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>West Monument B4/2c Reference</b>				Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>Bones, Kyle, David, Luke, Kim</b>			Date: <b>11/06/12</b>		Valley Type: <b>VIIIb</b>		Stream Type: <b>B4/2c</b>		
<b>River Reach Dimension Summary Data.....1</b>									
<b>Riffle Dimensions* ** , ***</b>	<b>Riffle Dimensions* ** , ***</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	
	Riffle Width ( $W_{bkt}$ )	8.04	7.70	8.37	ft	Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	5.23	4.25	6.21
	Mean Riffle Depth ( $d_{bkt}$ )	0.66	0.51	0.81	ft	Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	12.96	9.51	16.41
	Maximum Riffle Depth ( $d_{max}$ )	1.12	0.77	1.47	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	1.66	1.51	1.82
	Width of Flood-Prone Area ( $W_{fpa}$ )	16.46	13.37	19.54	ft	Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )	2.07	1.60	2.54
	Riffle Inner Berm Width ( $W_{ib}$ )	5.19	4.74	5.64	ft	Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )	0.65	0.62	0.67
	Riffle Inner Berm Depth ( $d_{ib}$ )	0.48	0.33	0.63	ft	Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )	0.71	0.64	0.78
	Riffle Inner Berm Area ( $A_{ib}$ )	2.41	1.85	2.98	ft <sup>2</sup>	Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )	0.46	0.43	0.48
	Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )	12.39	7.56	17.23					
<b>Pool Dimensions* ** , ***</b>	<b>Pool Dimensions* ** , ***</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Pool Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	
	Pool Width ( $W_{bkfp}$ )	7.010	4.990	9.030	ft	Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )	0.872	0.621	1.123
	Mean Pool Depth ( $d_{bkfp}$ )	1.320	1.040	1.600	ft	Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )	2.000	1.576	2.424
	Pool Cross-Sectional Area ( $A_{bkfp}$ )	8.690	7.990	9.380	ft	Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )	1.662	1.528	1.793
	Maximum Pool Depth ( $d_{maxp}$ )	1.990	1.720	2.260	ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	3.015	2.606	3.424
	Pool Inner Berm Width ( $W_{ibp}$ )	3.2	2.8	3.7	ft	Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )	0.523	0.305	0.740
	Pool Inner Berm Depth ( $d_{ibp}$ )	0.26	0.18	0.34	ft	Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )	0.194	0.176	0.212
	Pool Inner Berm Area ( $A_{ibp}$ )	0.9	0.5	1.3	ft <sup>2</sup>	Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )	0.106	0.054	0.157
	Point Bar Slope ( $S_{pb}$ )				ft/ft	Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )			
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Run Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	
	Run Width ( $W_{bkfr}$ )				ft	Run Width to Riffle Width ( $W_{bkfr} / W_{bkt}$ )			
	Mean Run Depth ( $d_{bkfr}$ )				ft	Mean Run Depth to Mean Riffle Depth ( $d_{bkfr} / d_{bkt}$ )			
	Run Cross-Sectional Area ( $A_{bkfr}$ )				ft	Run Area to Riffle Area ( $A_{bkfr} / A_{bkt}$ )			
	Maximum Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )			
	Run Width/Depth Ratio ( $W_{bkfr} / d_{bkfr}$ )				ft				
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Glide Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	
	Glide Width ( $W_{bkfg}$ )				ft	Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )			
	Mean Glide Depth ( $d_{bkfg}$ )				ft	Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )			
	Glide Cross-Sectional Area ( $A_{bkfg}$ )				ft	Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )			
	Maximum Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )			
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )				ft/ft	Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )			
	Glide Inner Berm Width ( $W_{ibg}$ )				ft	Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )			
	Glide Inner Berm Depth ( $d_{ibg}$ )				ft	Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )			
Glide Inner Berm Area ( $A_{ibg}$ )				ft <sup>2</sup>	Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )				
<b>Step**</b>	<b>Step Dimensions**</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Step Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	
	Step Width ( $W_{bkfs}$ )				ft	Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )			
	Mean Step Depth ( $d_{bkfs}$ )				ft	Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )			
	Step Cross-Sectional Area ( $A_{bkfs}$ )				ft	Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )			
	Maximum Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
	Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )								

**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>West Monument B4/2c Reference</b>		Location: <b>Pike National Forest, Colorado</b>												
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Date: <b>11/6/2012</b>		Valley Type: <b>VIIIb</b>		Stream Type: <b>B4/2c</b>								
<b>Hydraulics</b>	<b>River Reach Summary Data.....2</b>													
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )		<b>1.69</b> ft/sec		Estimation Method		<b>n By Stream Type</b>							
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )		<b>10.49</b> cfs		Drainage Area		<b>10.95</b> mi <sup>2</sup>							
<b>Channel Pattern</b>	<b>Geometry</b>			<b>Dimensionless Geometry Ratios</b>										
	Linear Wavelength ( $\lambda$ )	<b>51.0</b>	<b>43.0</b>	<b>59.0</b> ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )	<b>6.34</b>	<b>5.35</b>	<b>7.34</b>						
	Stream Meander Length ( $L_m$ )	<b>55.0</b>	<b>50.0</b>	<b>60.0</b> ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )	<b>6.84</b>	<b>6.22</b>	<b>7.46</b>						
	Radius of Curvature ( $R_c$ )	<b>22.3</b>	<b>15.0</b>	<b>34.0</b> ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )	<b>2.89</b>	<b>1.95</b>	<b>4.42</b>						
	Belt Width ( $W_{bit}$ )	<b>18.0</b>	<b>15.4</b>	<b>20.4</b> ft	Meander Width Ratio ( $W_{bit} / W_{bkt}$ )	<b>10.45</b>	<b>5.94</b>	<b>18.51</b>						
	Arc Length ( $L_a$ )	<b>12.0</b>	<b>9.4</b>	<b>15.7</b> ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )	<b>1.49</b>	<b>1.17</b>	<b>1.95</b>						
	Riffle Length ( $L_r$ )	<b>13.3</b>	<b>13.3</b>	<b>13.3</b> ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )	<b>1.65</b>	<b>1.65</b>	<b>1.65</b>						
	Individual Pool Length ( $L_p$ )	<b>5.4</b>	<b>5.0</b>	<b>6.1</b> ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )	<b>0.67</b>	<b>0.62</b>	<b>0.76</b>						
Pool to Pool Spacing ( $P_s$ )	<b>20.3</b>	<b>14.5</b>	<b>26.0</b> ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )	<b>2.52</b>	<b>1.80</b>	<b>3.23</b>							
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )		<b>0.0146</b> ft/ft		Average Water Surface Slope ( $S$ )		<b>0.0130</b> ft/ft		Sinuosity ( $S_{val} / S$ )		<b>1.06</b>			
	Stream Length (SL)		<b>154.2</b> ft		Valley Length (VL)		<b>145.4</b> ft		Sinuosity (SL / VL)		<b>1.06</b>			
	Low Bank Height (LBH)		start: <b>1.50</b> ft end: <b>1.50</b> ft		Max Bankfull Depth ( $d_{max}$ )		start: <b>1.50</b> ft end: <b>1.50</b> ft		Bank-Height Ratio (BHR) (LBH / $d_{max}$ )		start: <b>1.0</b> end: <b>1.0</b>			
	<b>Facet Slopes</b>			<b>Dimensionless Facet Slope Ratios</b>										
	Riffle Slope ( $S_{rit}$ )	<b>0.0180</b>	<b>0.0180</b>	<b>0.0180</b> ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rit} / S$ )	<b>1.3846</b>	<b>1.3846</b>	<b>1.3846</b>						
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )									
	Pool Slope ( $S_p$ )	<b>0.0020</b>	<b>0.0000</b>	<b>0.0060</b> ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )	<b>0.1538</b>	<b>0.0000</b>	<b>0.4615</b>						
	Glide Slope ( $S_g$ )	<b>0.0130</b>	<b>0.0130</b>	<b>0.0130</b> ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )	<b>1.0000</b>	<b>1.0000</b>	<b>1.0000</b>						
	Step Slope ( $S_s$ )			ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )									
	<b>Max Depths<sup>a</sup></b>			<b>Dimensionless Depth Ratios</b>										
	Max Riffle Depth ( $d_{max}$ )	<b>1.55</b>	<b>1.55</b>	<b>1.55</b> ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>2.348</b>	<b>2.348</b>	<b>2.348</b>						
	Max Run Depth ( $d_{maxr}$ )			ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )									
	Max Pool Depth ( $d_{maxp}$ )	<b>2.13</b>	<b>1.94</b>	<b>2.25</b> ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	<b>3.227</b>	<b>2.939</b>	<b>3.409</b>						
	Max Glide Depth ( $d_{maxg}$ )	<b>1.41</b>	<b>1.41</b>	<b>1.41</b> ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )	<b>2.136</b>	<b>2.136</b>	<b>2.136</b>						
	Max Step Depth ( $d_{maxs}$ )			ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )									
<b>Channel Materials</b>	<b>Reach<sup>b</sup></b>		<b>Riffle<sup>c</sup></b>		<b>Bar</b>		<b>Reach<sup>b</sup></b>		<b>Riffle<sup>c</sup></b>		<b>Bar</b>		<b>Protrusion Height<sup>d</sup></b>	
	% Silt/Clay	<b>7.14</b>	<b>0.00</b>				$D_{16}$	<b>1.73</b>	<b>4.69</b>					mm
	% Sand	<b>9.82</b>	<b>5.61</b>				$D_{35}$	<b>7.54</b>	<b>6.95</b>					mm
	% Gravel	<b>56.25</b>	<b>81.31</b>				$D_{50}$	<b>10.20</b>	<b>8.89</b>					mm
	% Cobble	<b>2.68</b>	<b>10.28</b>				$D_{84}$	<b>401.02</b>	<b>54.11</b>					mm
	% Boulder	<b>20.54</b>	<b>2.80</b>				$D_{95}$	<b>921.46</b>	<b>98.25</b>					mm
	% Bedrock	<b>3.57</b>	<b>0.00</b>				$D_{100}$	<b>Bedrock</b>	<b>1023.97</b>					mm

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.  
<sup>b</sup> Composite sample of riffles and pools within the designated reach.      <sup>c</sup> Active bed of a riffle.      <sup>d</sup> Height of roughness feature above bed.

## Stability Indices


**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation						
Stream: <b>West Monument B4/2c Reference</b>		Location: <b>Pike National Forest, Colorado</b>				
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Reference reach <input checked="" type="checkbox"/>	Disturbed (impacted reach) <input type="checkbox"/>	Date: <b>11/6/2012</b>		
Existing species composition: <b>Spruce, Aspen, Willows, Choke Cherry, Grass and Moss</b>		Potential species composition: <b>Spruce, Aspen, Willows, Choke Cherry, Grass and Moss</b>				
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition	
<b>1. Overstory</b>	Canopy layer	<b>85%</b>	<b>15%</b>	blue spruce	<b>50%</b>	
				aspen	<b>40%</b>	
				douglas fir	<b>10%</b>	
					<b>0%</b>	
					<b>0%</b>	
				<b>100%</b>		
<b>2. Understory</b>	Shrub layer	<b>10%</b>	<b>10%</b>	willow	<b>60%</b>	
				redtwig dogwood	<b>5%</b>	
				rose	<b>5%</b>	
				chokecherry	<b>30%</b>	
					<b>0%</b>	
				<b>100%</b>		
<b>3. Ground level</b>	Herbaceous	<b>5%</b>	<b>5%</b>	grasses	<b>70%</b>	
				moss	<b>30%</b>	
					<b>0%</b>	
	Leaf or needle litter	<b>65%</b>	<b>65%</b>			<b>0%</b>
						<b>0%</b>
Bare ground	<b>5%</b>	<b>5%</b>			<b>100%</b>	
*Based on crown closure. **Based on basal area to surface area.			<b>Column Total = 100%</b>		<b>Remarks:</b> Condition, vigor and/or usage of existing reach: <b>Riparian zone is vigorous and healthy</b>	

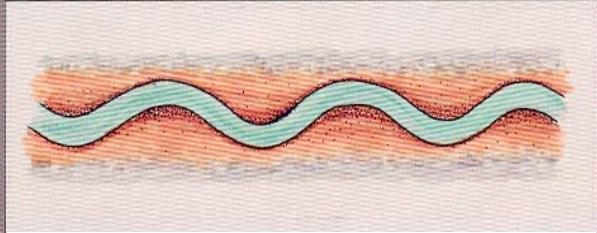

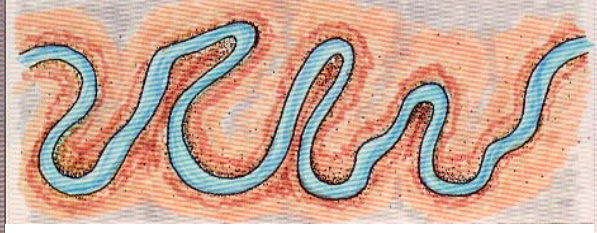
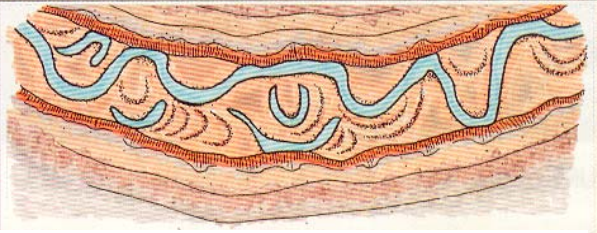


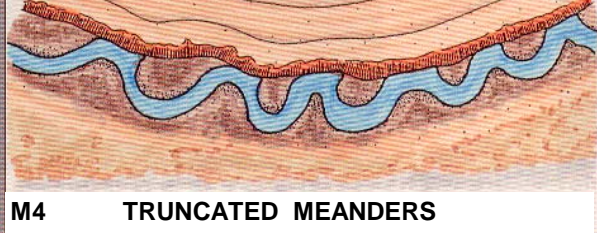

Worksheet 5-7. Flow regime.

FLOW REGIME								
Stream: <b>West Monument B4/2c Referenc</b> Location: <b>Pike National Forest, Colorado</b>								
Observers: <b>Bones, Kyle, David, Luke, Kim</b>						Date: <b>11/6/2012</b>		
<b>List ALL COMBINATIONS that APPLY.....</b>	<b>P1</b>	<b>P2</b>	<b>P7</b>	<b>P8</b>				
General Category								
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation							
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
<b>P</b>	Perennial stream channels: Surface water persists yearlong.							
Specific Category								
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
<b>4</b>	Streamflow regulated by glacial melt.							
<b>5</b>	Ice flows/ice torrents from ice dam breaches.							
<b>6</b>	Alternating flow/backwater due to tidal influence.							
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.							
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
<b>9</b>	Rain-on-snow generated runoff.							

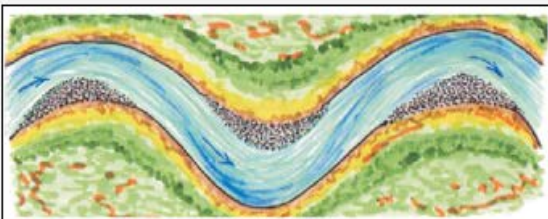
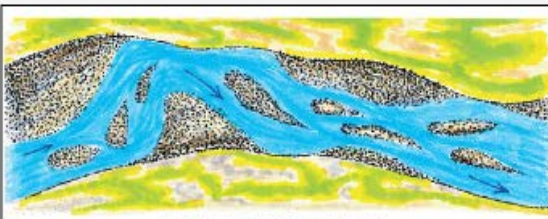
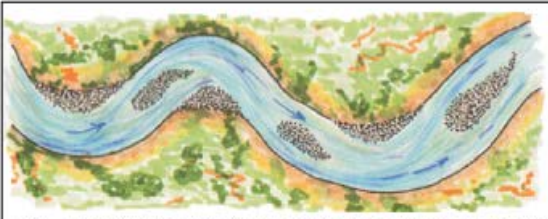
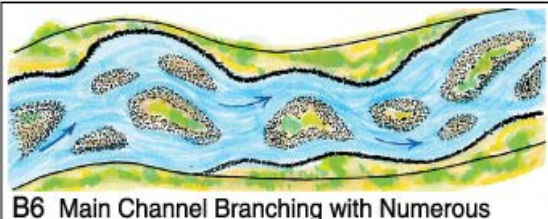

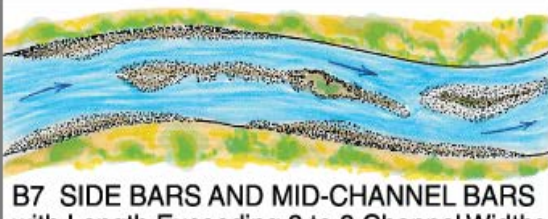

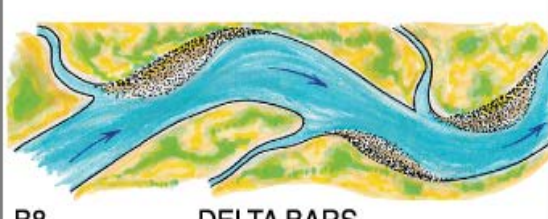
**Worksheet 5-8.** Stream order & stream size.

Stream Size and Order			
Stream:	West Monument B4/2c Reference		
Location:	Pike National Forest, Colorado		
Observers:	Bones, Kyle, David, Luke, Kim		
Date:	11/6/2012		
Stream Size Category and Order 			S-3(4)
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0.305	<1	<input type="checkbox"/>
S-2	0.3 – 1.5	1 – 5	<input type="checkbox"/>
<b>S-3</b>	<b>1.5 – 4.6</b>	<b>5 – 15</b>	<input checked="" type="checkbox"/>
S-4	4.6 – 9	15 – 30	<input type="checkbox"/>
S-5	9 – 15	30 – 50	<input type="checkbox"/>
S-6	15 – 22.8	50 – 75	<input type="checkbox"/>
S-7	22.8 – 30.5	75 – 100	<input type="checkbox"/>
S-8	30.5 – 46	100 – 150	<input type="checkbox"/>
S-9	46 – 76	150 – 250	<input type="checkbox"/>
S-10	76 – 107	250 – 350	<input type="checkbox"/>
S-11	107 – 150	350 – 500	<input type="checkbox"/>
S-12	150 – 305	500 – 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
Stream Order			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			

Worksheet 5-9. Meander patterns.

Meander Patterns					
Stream:	West Monument B4/2c Reference	Location:	Pike National Forest, CO		
Observers:	Bones, Kyle, David, Luke, Kim	Date:	11/6/2012		
List ALL CATEGORIES that APPLY	<b>M3</b>				
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>					
 <b>M1</b> <b>REGULAR MEANDERS</b>	 <b>M5</b> <b>UNCONFINED MEANDER SCROLLS</b>				
 <b>M2</b> <b>TORTUOUS MEANDERS</b>	 <b>M6</b> <b>CONFINED MEANDER SCROLLS</b>				
 <b>M3</b> <b>IRREGULAR MEANDERS</b>	 <b>M7</b> <b>DISTORTED MEANDER LOOPS</b>				
 <b>M4</b> <b>TRUNCATED MEANDERS</b>	 <b>M8</b> <b>IRREGULAR MEANDERS with oxbows and oxbow cutoffs</b>				

**Worksheet 5-10.** Depositional patterns.

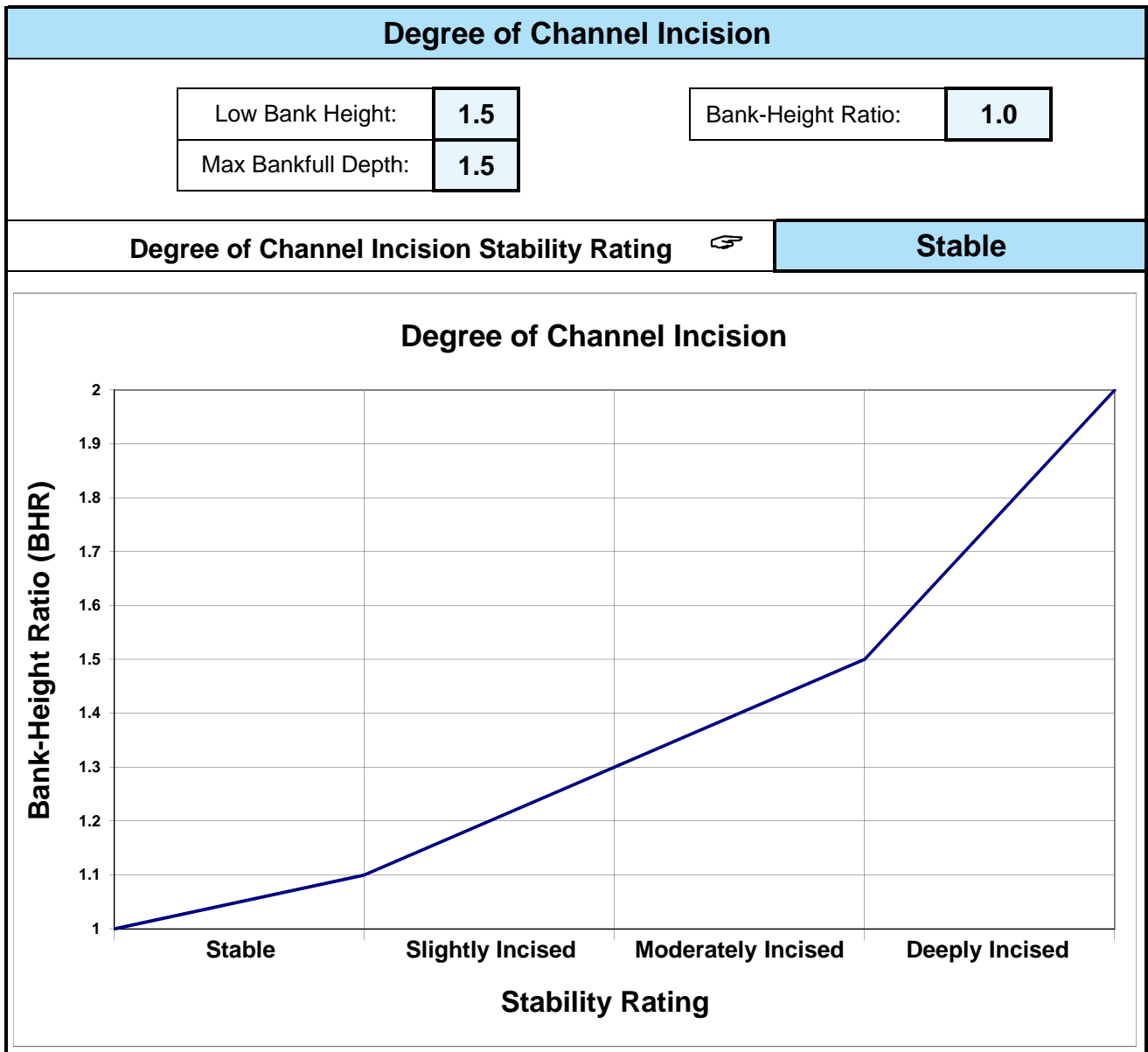
<b>Depositional Patterns</b>					
Stream:	West Monument B4/2c Reference	Location:	Pike National Forest, Colorado		
Observers:	Bones, Kyle, David, Luke, Kim	Date:	11/6/2012		
List ALL CATEGORIES that APPLY	NA				
<i>Various Depositional Features modified from Galay et al. (1973)</i>					
 <b>B1 POINT BARS</b>	 <b>B5 DIAGONAL BARS</b>				
 <b>B2 POINT BARS with Few MID-CHANNEL BARS</b>	 <b>B6 Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</b>				
 <b>B3 NUMEROUS MID-CHANNEL BARS</b>	 <b>B7 SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</b>				
 <b>B4 SIDE BARS</b>	 <b>B8 DELTA BARS</b>				



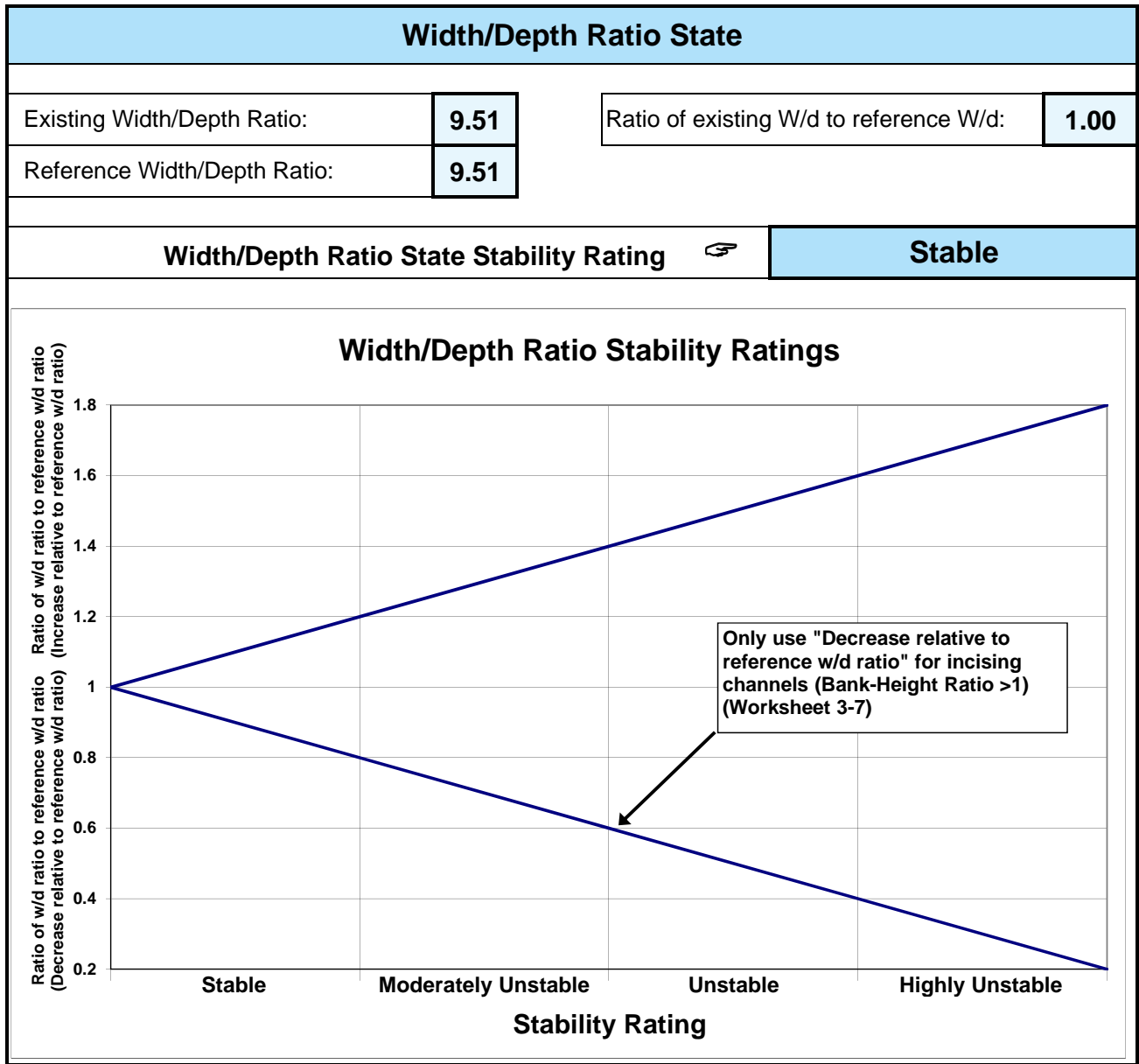
## Worksheet 5-11. Channel blockages.

Channel Blockages		
Stream: <b>West Monument B4/2c Reference</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Date: <b>11/6/2012</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input checked="" type="checkbox"/>
<b>D4</b> Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

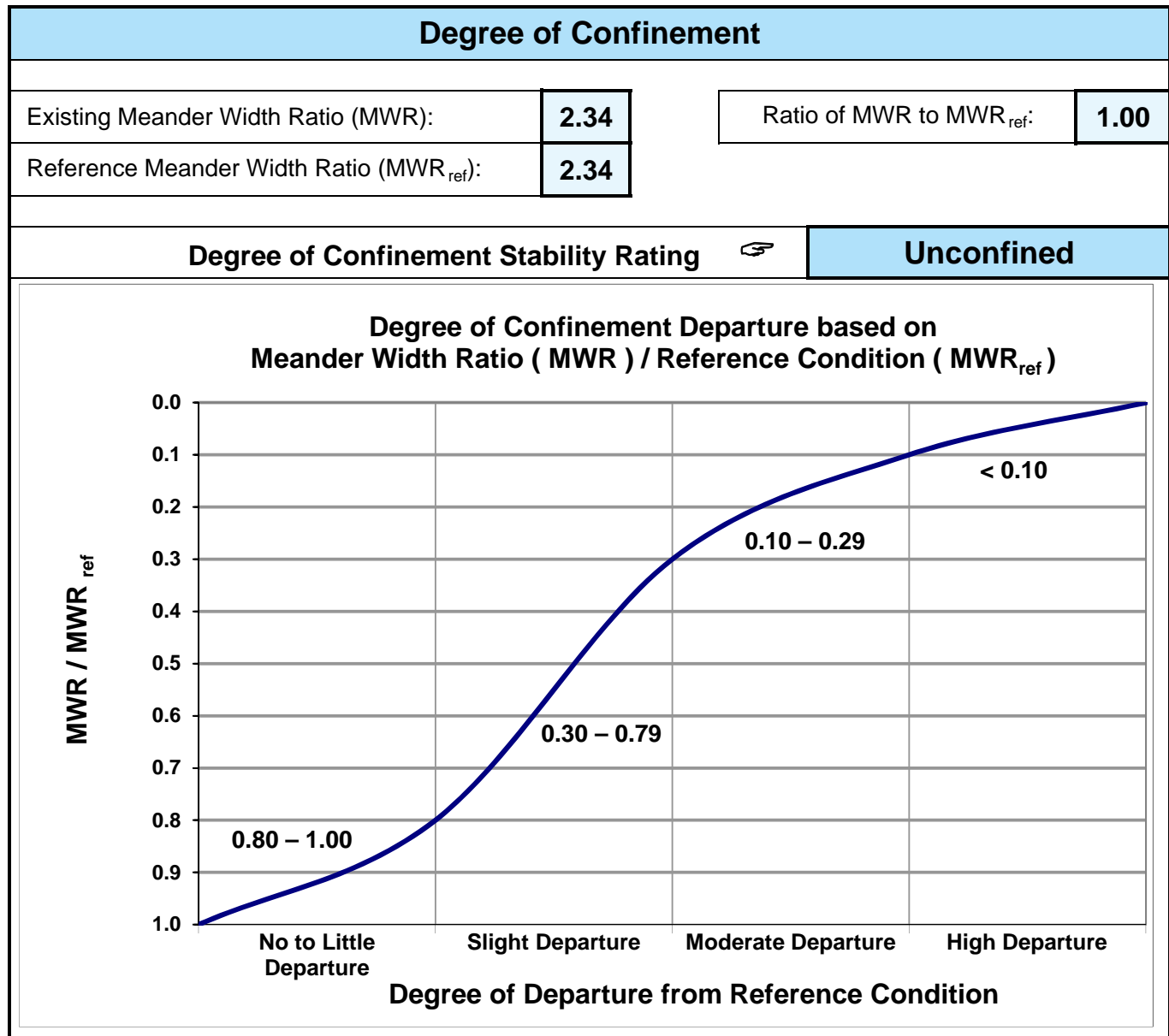
**Worksheet 5-12.** Degree of channel incision.



**Worksheet 5-13.** Width/depth ratio state.



**Worksheet 5-14.** Degree of channel confinement (lateral containment).



**Worksheet 5-15. Pfankuch channel stability rating.**

Stream: West Monument B4/2c Reference		Location: Pike National Forest, CO		Valley Type: Vllib		Observers: Bones, Kyle, David, Luke, Kim		Date: 11/6/2012																
Local- tion	Key	Category	Excellent	Good	Fair	Poor	Rating	Description	Rating															
Upper banks	1	Landform slope	Bank slope gradient <30%.	Bank slope gradient 30–40%.	Bank slope gradient 40–60%.	Bank slope gradient > 60%.	2		6															
	2	Mass erosion	No evidence of past or future mass erosion.	Infrequent. Mostly healed over. Low future potential.	Frequent or large, causing sediment nearly yearlong.	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.	3		9															
	3	Debris jam potential	Essentially absent from immediate channel area.	Present, but mostly small twigs and limbs.	Moderate to heavy amounts, mostly larger sizes.	Moderate to heavy amounts, predominantly larger sizes.	2		6															
	4	Vegetative bank protection	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	70–90% density. Fewer species or less vigor suggest less dense or deep root mass.	50–70% density. Lower vigor and fewer species from a shallow, discontinuous root mass.	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.	3		9															
Lower banks	5	Channel capacity	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0-1.1.	Bankfull stage is contained within banks. Width/depth ratio departure from reference width/depth ratio = 1.0–1.2. Bank-Height Ratio (BHR) = 1.0-1.1.	Bankfull stage is not contained. Width/depth ratio departure from reference width/depth ratio = 1.2–1.4. Bank-Height Ratio (BHR) = 1.1-1.3.	Bankfull stage is not contained; over-bank flows are common with flows less than bankfull. W/c/d/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.	1		3															
	6	Bank rock content	> 65% with large angular boulders. 12"+ common.	40–65%. Mostly boulders and small cobbles 6–12".	20–40%. Most in the 3–6" diameter class.	<20%, rock fragments of gravel sizes, 1–3" or less.	2		6															
	7	Obstructions to flow	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	Frequent obstructions and deflectors cause bank erosion yearlong. Sediment traps full, channel migration occurring.	2		4															
	8	Cutting	Little or none. Infrequent raw banks <6".	Some, intermittently at outcrops and constrictions. Raw banks may be up to 12".	Significant. Cuts 12–24" high. Root mat overhangs and sloughing evident.	Almost continuous cuts, some over 24" high. Failure of overhangs frequent.	4		12															
	9	Deposition	Little or no enlargement of channel or point bars.	Some new bar increase, mostly from coarse gravel.	Moderate deposition of new gravel and coarse sand on old and some new bars.	Extensive deposit of predominantly fine particles. Accelerated bar development.	4		8															
Bottom	10	Rock angularity	Sharp edges and corners. Plane surfaces rough.	Rounded corners and edges. Surfaces smooth and flat.	Corners and edges well rounded in 2 dimensions.	Well rounded in all dimensions, surfaces smooth.	1		2															
	11	Brightness	Surfaces dull, dark or stained. Generally not bright.	Mostly dull, but may have <35% bright surfaces.	Mixture dull and bright, i.e., 35–65% mixture range.	Predominantly bright, > 65%, exposed or scoured surfaces.	1		3															
	12	Consolidation of particles	Assorted sizes tightly packed or overlapping.	Moderately packed with some overlapping.	Mostly loose assortment with no apparent overlap.	No packing evident. Loose assortment, easily moved.	2		6															
	13	Bottom size distribution	No size change evident. Stable material 80–100%.	Distribution shift light. Stable material 50–80%.	Moderate change in sizes. Stable materials 20–50%.	Marked distribution change. Stable materials 0–20%.	4		12															
	14	Scouring and deposition	<5% of bottom affected by scour or deposition.	5–30% affected. Scour at constrictions and where grades steepen. Some deposition in pools.	30–50% affected. Deposits and scour at obstructions, constrictions and bends. Some filling of pools.	More than 50% of the bottom in a state of flux or change nearly yearlong.	6		20															
	15	Aquatic vegetation	Abundant growth moss-like, dark green perennial. In swift water too.	Common. Algae forms in low velocity and pool areas. Moss here too.	Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick.	Perennial types scarce or absent. Yellow-green, short-term bloom may be present.	1		3															
			<b>Excellent total = 25</b>	<b>Good total = 29</b>	<b>Fair total = 6</b>	<b>Poor total = 0</b>																		
<b>Stream type</b>	<b>A1</b>	<b>A2</b>	<b>A3</b>	<b>A4</b>	<b>A5</b>	<b>A6</b>	<b>B1</b>	<b>B2</b>	<b>B3</b>	<b>B4</b>	<b>B5</b>	<b>B6</b>	<b>C1</b>	<b>C2</b>	<b>C3</b>	<b>C4</b>	<b>C5</b>	<b>C6</b>	<b>D3</b>	<b>D4</b>	<b>D5</b>	<b>D6</b>	<b>Grand total = 54</b>	
Good (Stable)	38-43	38-43	54-90	60-95	60-95	50-80	38-45	38-45	40-60	40-64	48-68	40-60	38-50	38-50	60-85	70-90	70-90	60-85	85-107	85-107	85-107	85-107	87-98	54
Fair (Mod. unstable)	44-47	44-47	91-129	96-132	96-142	81-110	46-58	46-58	61-78	65-84	69-88	61-78	51-61	51-61	86-105	91-110	91-110	86-105	108-132	108-132	108-132	108-132	99-125	B2/4c
Poor (Unstable)	48+	48+	130+	133+	143+	111+	59+	59+	79+	85+	89+	79+	62+	62+	106+	111+	111+	106+	133+	133+	133+	126+	*Potential stream type = B2/4c	
<b>Stream type</b>	<b>DA3</b>	<b>DA4</b>	<b>DA5</b>	<b>DA6</b>	<b>DA7</b>	<b>DA8</b>	<b>E1</b>	<b>E2</b>	<b>E3</b>	<b>E4</b>	<b>E5</b>	<b>E6</b>	<b>F1</b>	<b>F2</b>	<b>F3</b>	<b>F4</b>	<b>F5</b>	<b>F6</b>	<b>G1</b>	<b>G2</b>	<b>G3</b>	<b>G4</b>	<b>G5</b>	<b>Modified channel stability rating =</b>
Good (Stable)	40-63	40-63	40-63	40-63	50-75	50-75	40-63	40-63	60-85	60-85	85-110	85-110	90-115	80-95	80-95	40-60	40-60	85-107	85-107	90-112	90-112	85-107	85-107	B2/4c
Fair (Mod. unstable)	64-86	64-86	64-86	64-86	76-96	76-96	64-86	64-86	86-105	86-105	111-125	111-125	116-130	96-110	96-110	61-78	61-78	108-120	108-120	113-125	113-125	108-120	108-120	B2/4c
Poor (Unstable)	87+	87+	87+	87+	97+	97+	87+	87+	106+	106+	126+	126+	131+	111+	111+	79+	79+	121+	121+	126+	126+	121+	121+	Good

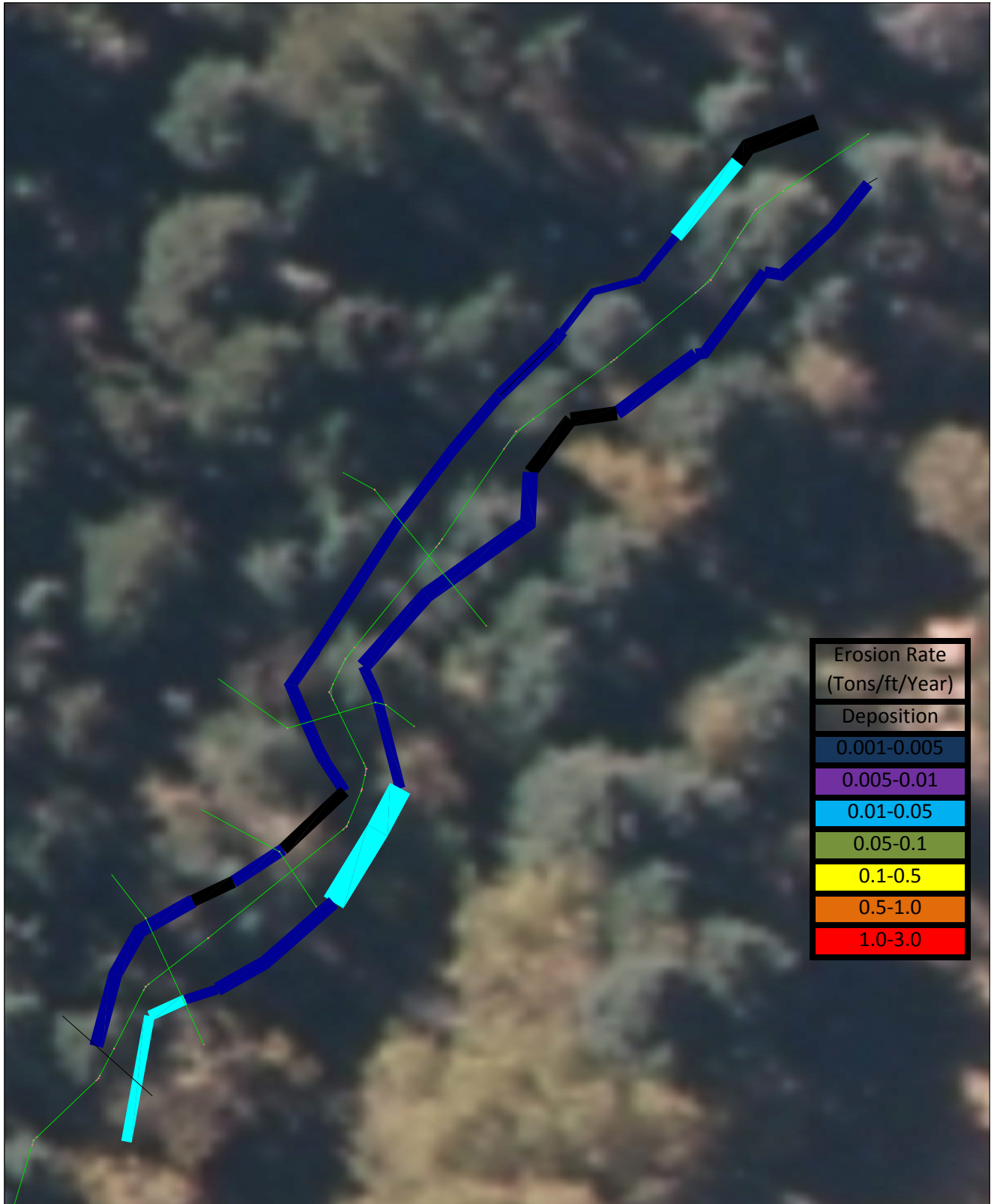
\*Rating is adjusted to potential stream type, not existing.

## BANCS Model – Streambank Erosion

**Worksheet 5-18.** Annual streambank erosion estimates.

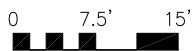
Stream: <b>West Monument B4/2c Reference</b>				Location: <b>B4/2c Reference</b>			
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>115</b>			Date: <b>11/6/2012</b>		
Observers: <b>David Luke Bones Kyle Kim</b>		Valley Type: <b>VIIIb</b>		Stream Type: <b>B4/2c</b>			
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 3-11) (adjective)	NBS rating (Worksheet 3-12) (adjective)	Bank erosion rate (Figure 3-9 or 3-10) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [[4]x(5)x(6)] (ft <sup>3</sup> /yr)	Erosion Rate (tons/yr/ft) {[(7)/27] × 1.3 / (5)}
1. RB 10 to 22	Moderate	Low	0.153	12.0	1.7	3.12	0.01250
2. LB 0 to 17	Very Low	Low	0.004	17.0	1.5	0.10	0.00030
3. LB 17 to 32	Low	Very Low	0.018	15.0	1.4	0.37	0.00120
4. RB 22 to 32	Very Low	Low	0.004	10.0	1.0	0.04	0.00020
5. LB 32 to 42	Low	Low	0.042	10.0	1.7	0.71	0.00340
6. RB 32 to 42	Low	Low	0.042	10.0	0.9	0.38	0.00180
7. RB 42 to 51	Low	Low	0.042	9.0	1.5	0.56	0.00300
8. RB 51 to 58	Low	Low	0.042	7.0	1.4	0.41	0.00280
9. LB 56 to 89	Very Low	Low	0.004	33.0	1.9	0.24	0.00040
10. RB 58 to 89	Low	Moderate	0.073	31.0	1.4	3.15	0.00490
11. LB 89 to 97	Very Low	Low	0.004	12.0	1.3	0.06	0.00020
12. RB 89 to 99	Low	Low	0.042	14.0	1.5	0.88	0.00300
13. LB 97 to 101	Moderate	Low	0.153	4.0	2.8	1.71	0.02060
14. RB 99 to 104	Low	Very Low	0.018	5.0	1.4	0.12	0.00110
15. LB 101 to 115	Very Low	Moderate	0.009	14.0	1.7	0.22	0.00070
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					Total Erosion (ft <sup>3</sup> /yr)	12.06	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					Total Erosion (yds <sup>3</sup> /yr)	0.45	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					Total Erosion (tons/yr)	0.58	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					Unit Erosion Rate (tons/yr/ft)	0.0050	

Streambank Erosion Map



Erosion Rate (Tons/ft/Year)
Deposition
0.001-0.005
0.005-0.01
0.01-0.05
0.05-0.1
0.1-0.5
0.5-1.0
1.0-3.0

Waldo Canyon Fire WARSSS  
Typical Reach



Wildland Hydrology  
11210 North County Road 19  
Fort Collins, CO  
80524  
Tel: 970-568-0002  
Fax: 970.568.0014

# FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Equation type	Intercept	Coefficient	Exponent	Form (e.g., linear, non-linear, etc.)	Equation name	Bankfull discharge (cfs)	Bankfull bedload (kg/s)	Bankfull suspended (mg/l)						
									Pagoosa Springs Reference Curve	Pagoosa Springs Reference Curve				
1. Bedload (dimensionless)	-0.0113	1.0139	2.1929	Non-Linear		8.30	0.0163	11.50						
2. Suspended sediment (dimensionless)	0.0636	0.9326	2.4085	Non-Linear										
3. User-defined relations (bedload)														
4. User-defined relations (suspended sediment)														
Notes: Pre-Fire Flow Duration Curve, Good/Fair Sediment Curves, Good/Fair Regional Sediment Curves														
From dimensioned flow-duration curve			From sediment rating curves			Calculate								
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Flow exceedence	Daily mean discharge	Mid-ordinate	Time increment (percent)	Time increment (days)	Mid-ordinate streamflow	Dimensionless streamflow	Dimensionless suspended sediment discharge	Suspended sediment discharge	Dimensionless bedload discharge	Bedload	Time adjusted streamflow	Suspended sediment	Bedload sediment	Suspended + bedload
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>med</sub> )	(S/S <sub>med</sub> )	(tons/day)	(b <sub>v</sub> /b <sub>med</sub> )	(tons/day)	(cfs)	(tons)	(tons)	(tons)
100.000	0.1													
90.000	0.3	95.00	10.00	36.50	0.2	0.02	0.8	0.0	0.0000	0.00	1.70	0.00	0.00	0.00
80.000	0.4	85.00	10.00	36.50	0.3	0.04	0.8	0.0	0.0000	0.00	3.30	0.00	0.00	0.00
70.000	0.4	75.00	10.00	36.50	0.4	0.05	0.8	0.0	0.0000	0.00	4.10	0.00	0.00	0.00
60.000	0.6	65.00	10.00	36.50	0.5	0.06	0.8	0.0	0.0000	0.00	4.90	0.00	0.00	0.00
50.000	0.7	55.00	10.00	36.50	0.6	0.08	0.8	0.0	0.0000	0.00	6.30	0.00	0.00	0.00
40.000	0.9	45.00	10.00	36.50	0.8	0.10	0.8	0.0	0.0000	0.00	8.20	0.00	0.00	0.00
30.000	1.3	35.00	10.00	36.50	1.1	0.14	0.8	0.0	0.0001	0.00	11.30	0.00	0.00	0.00
20.000	2.0	25.00	10.00	36.50	1.7	0.20	0.9	0.0	0.0004	0.00	16.50	0.00	0.00	0.00
10.000	3.6	15.00	10.00	36.50	2.8	0.34	1.2	0.0	0.0017	0.09	27.90	0.36	3.28	3.64
5.000	5.8	7.50	5.00	18.25	4.7	0.57	2.3	0.0	0.0060	0.26	23.50	0.55	4.75	5.30
4.000	6.5	4.50	1.00	3.65	6.1	0.74	3.7	0.1	0.0109	0.48	6.13	0.22	1.75	1.97
3.000	7.6	3.50	1.00	3.65	7.0	0.85	4.8	0.1	0.0148	0.65	7.03	0.33	2.37	2.70
2.000	9.0	2.50	1.00	3.65	8.3	1.00	6.8	0.2	0.0214	0.91	8.29	0.55	3.32	3.87
1.500	10.3	1.75	0.50	1.83	9.7	1.17	9.6	0.3	0.0302	1.30	4.83	0.46	2.37	2.83
1.000	12.6	1.25	0.50	1.83	11.5	1.38	14.0	0.4	0.0439	1.90	5.73	0.78	3.47	4.25
0.900	13.4	0.95	0.10	0.37	13.0	1.57	17.4	0.7	0.0540	2.51	1.30	0.24	0.92	1.16
0.800	14.2	0.85	0.10	0.37	13.8	1.66	17.4	0.8	0.0540	2.85	1.38	0.29	1.04	1.33
0.700	14.9	0.75	0.10	0.37	14.6	1.76	17.4	1.0	0.0540	3.20	1.46	0.35	1.17	1.52
0.600	15.9	0.65	0.10	0.37	15.4	1.86	17.4	1.2	0.0540	3.63	1.54	0.42	1.32	1.74
0.500	17.0	0.55	0.10	0.37	16.5	1.99	17.4	1.5	0.0540	4.23	1.65	0.53	1.54	2.07
0.250	19.7	0.38	0.25	0.91	18.4	2.22	17.4	2.1	0.0540	5.36	4.59	1.91	4.89	6.80
0.100	22.8	0.18	0.15	0.55	21.3	2.56	17.4	3.4	0.0540	7.39	3.19	1.86	4.05	5.91
0.050	24.4	0.08	0.05	0.18	23.6	2.84	17.4	4.9	0.0540	9.29	1.18	0.89	1.70	2.59
0.010	26.5	0.03	0.04	0.15	25.5	3.07	17.4	6.3	0.0540	10.97	1.02	0.92	1.60	2.52
0.005	26.5	0.01	0.01	0.02	26.5	3.20	17.4	7.2	0.0540	12.01	0.13	0.11	0.22	0.35
0.001	26.5	0.00	0.00	0.01	26.5	3.20	17.4	7.2	0.0540	12.01	0.11	0.11	0.18	0.29
Annual totals:											10.9 (tons/yr)	39.9 (tons/yr)	50.8 (tons/yr)	



**Worksheet 19b.** Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Equation type	Intercept	Coefficient	Exponent	Form (e.g., linear, non-linear, etc.)	Equation name		Bankfull discharge (cfs)	Bankfull bedload (kg/s)	Bankfull suspended (mg/l)					
					Pagosa Springs Reference Curve	Pagosa Springs Reference Curve								
1. Bedload (dimensionless)	-0.0113	1.0139	2.1929	Non-Linear			8.30	0.0163	11.50					
2. Suspended sediment (dimensionless)	0.0636	0.9326	2.4085	Non-Linear										
3. User-defined relations (bedload)														
4. User-defined relations (suspended sediment)														
Notes: Post-Fire Flow Duration Curve, Good/Fair Sediment Curves, Good/Fair Regional Sediment Curves														
(1)	From dimensioned flow-duration curve				From sediment rating curves				Calculate		Calculate sediment yield			
	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Flow exceedence	Daily mean discharge	Mid-ordinate	Time increment (percent)	Time increment (days)	Mid-ordinate streamflow	Dimensionless streamflow	Dimensionless suspended sediment discharge	Suspended sediment discharge	Dimensionless bedload discharge	Bedload	Time adjusted streamflow	Suspended sediment [(5)×(9)]	Bedload sediment [(5)×(11)]	Suspended bedload [(13)×(14)]
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>med</sub> )	(S/S <sub>med</sub> )	(tons/day)	(b <sub>p</sub> /b <sub>med</sub> )	(tons/day)	(cfs)	(tons)	(tons)	(tons)
100.000	0.1													
90.000	0.3	95.00	10.00	36.50	0.2	0.02	0.8	0.0	0.0000	0.00	1.60	0.00	0.00	0.00
80.000	0.4	85.00	10.00	36.50	0.3	0.04	0.8	0.0	0.0000	0.00	3.30	0.00	0.00	0.00
70.000	0.4	75.00	10.00	36.50	0.4	0.05	0.8	0.0	0.0000	0.00	4.10	0.00	0.00	0.00
60.000	0.6	65.00	10.00	36.50	0.5	0.06	0.8	0.0	0.0000	0.00	4.90	0.00	0.00	0.00
50.000	0.7	55.00	10.00	36.50	0.6	0.08	0.8	0.0	0.0000	0.00	6.30	0.00	0.00	0.00
40.000	0.9	45.00	10.00	36.50	0.8	0.10	0.8	0.0	0.0000	0.00	8.20	0.00	0.00	0.00
30.000	1.5	35.00	10.00	36.50	1.2	0.14	0.8	0.0	0.0001	0.00	11.90	0.00	0.00	0.00
20.000	2.9	25.00	10.00	36.50	2.2	0.26	1.0	0.0	0.0008	0.04	21.80	0.36	1.46	1.82
10.000	6.0	15.00	10.00	36.50	4.4	0.53	2.1	0.0	0.0052	0.22	44.30	0.73	8.03	8.76
5.000	8.9	7.50	5.00	18.25	7.4	0.89	5.4	0.1	0.0166	0.73	37.05	2.01	13.32	15.33
4.000	9.7	4.50	1.00	3.65	9.3	1.12	8.7	0.2	0.0275	1.17	9.28	0.80	4.27	5.07
3.000	11.0	3.50	1.00	3.65	10.3	1.25	11.1	0.3	0.0350	1.51	10.34	1.13	5.51	6.64
2.000	12.4	2.50	1.00	3.65	11.7	1.41	14.7	0.5	0.0460	1.99	11.71	1.68	7.26	8.94
1.500	13.8	1.75	0.50	1.83	13.1	1.58	17.4	0.7	0.0540	2.55	6.57	1.24	4.65	5.89
1.000	16.1	1.25	0.50	1.83	15.0	1.80	17.4	1.0	0.0540	3.41	7.47	1.90	6.22	8.12
0.900	16.9	0.95	0.10	0.37	16.5	1.99	17.4	1.5	0.0540	4.23	1.65	0.53	1.54	2.07
0.800	17.7	0.85	0.10	0.37	17.3	2.09	17.4	1.7	0.0540	4.71	1.73	0.62	1.72	2.34
0.700	18.5	0.75	0.10	0.37	18.1	2.18	17.4	2.0	0.0540	5.14	1.81	0.72	1.88	2.60
0.600	19.4	0.65	0.10	0.37	19.0	2.28	17.4	2.3	0.0540	5.75	1.90	0.84	2.10	2.94
0.500	20.5	0.55	0.10	0.37	20.0	2.41	17.4	2.8	0.0540	6.44	2.00	1.01	2.35	3.36
0.250	23.2	0.38	0.25	0.91	21.9	2.64	17.4	3.8	0.0540	7.86	5.47	3.43	7.17	10.60
0.100	26.3	0.18	0.15	0.55	24.8	2.99	17.4	5.7	0.0540	10.32	3.72	3.13	5.65	8.78
0.050	27.9	0.08	0.05	0.18	27.1	3.27	17.4	7.8	0.0540	12.57	1.35	1.41	2.29	3.70
0.010	30.0	0.03	0.04	0.15	29.0	3.49	17.4	9.7	0.0540	14.56	1.16	1.42	2.13	3.55
0.005	30.0	0.01	0.01	0.02	30.0	3.62	17.4	11.0	0.0540	15.81	0.15	0.20	0.29	0.49
0.001	30.0	0.00	0.00	0.01	30.0	3.62	17.4	11.0	0.0540	15.81	0.12	0.16	0.23	0.39
Annual totals:											23.3 (tons/yr)	78.1 (tons/yr)	101.4 (tons/yr)	

## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>West Monument B4/2c Reference</b>		Stream Type: <b>B4/2c</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIIb</b>			
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Date: <b>11/6/2012</b>			
<b>Enter Required Information for Existing Condition</b>					
8.9	$D_{50}$	Riffle bed material $D_{50}$ (mm)			
0.0	$\hat{D}_{50}$	Bar sample $D_{50}$ (mm)			
0.322	$D_{max}$	Largest particle from <b>Bed Material</b> (ft)	98	(mm)	304.8 mm/ft
0.13000	S	Existing bankfull water surface slope (ft/ft)			
0.81	d	Existing bankfull mean depth (ft)			
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment			
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>					
0.00	$D_{50}/\hat{D}_{50}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 ( D_{50}/\hat{D}_{50} )^{-0.872}$		
12.37	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 ( D_{max}/D_{50} )^{-0.887}$		
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED:	2	
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	d	Required bankfull mean depth (ft)	$d = \frac{\tau^* (\gamma_s - 1) D_{max}}{S}$ (use $D_{max}$ in ft)		
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	S	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^* (\gamma_s - 1) D_{max}}{d}$ (use $D_{max}$ in ft)		
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					
<b>Sediment Competence Using Dimensional Shear Stress</b>					
0.657	Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d) $\gamma = 62.4$ , d = existing depth, S = existing slope				
Shields 50.33	CO 111.6	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ (Figure 5-49)			
Shields 1.391	CO 0.644	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) (Figure 5-49)			
Shields 1.72	CO 0.79	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm)		$d = \frac{\tau}{\gamma S}$	
		$\tau$ = predicted shear stress, $\gamma = 62.4$ , S = existing slope			
Shields 0.0275	CO 0.0127	Predicted slope required to initiate movement of measured $D_{max}$ (mm)		$S = \frac{\tau}{\gamma d}$	
		$\tau$ = predicted shear stress, $\gamma = 62.4$ , d = existing depth			
Check: <input checked="" type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					

## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>West Monument B4/2c Referenc</b> Stream Type: <b>B4/2c</b>	
Location: <b>Pike National Forest, CO</b> Valley Type: <b>VIIIb</b>	
Observers: <b>Bones, Kyle, David, Luke, Kim</b> Date: <b>11/06/2012</b>	
Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)	Stability Rating (Check Appropriate Rating)
Stream Type at potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	<input checked="" type="checkbox"/> Stable
(E→C), (C→High W/d C)	<input type="checkbox"/> Moderately Unstable
(G→F), (F→D), (C→F)	<input type="checkbox"/> Unstable
(C→D), (B→G), (D→G), (C→G), (E→G)	<input type="checkbox"/> Highly Unstable

**Worksheet 5-25.** Lateral stability.

Stream: <b>West Monument B4/2c Reference</b>		Stream Type: <b>B4/2c</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIIb</b>			
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Date: <b>11/06/2012</b>			
Lateral stability criteria (choose one stability category for each criterion 1-5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	2
	(2)	(4)	(6)	(8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	1
	(1)	(2)	(3)	(4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		1
	(1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	2
	(2)	(4)	(6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	1
	(1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>7</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input checked="" type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input type="checkbox"/>	<i>Unstable</i> 13 – 21 <input type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	

**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>West Monument B4/2c Reference</b>		Stream Type: <b>B4/2c</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIIb</b>			
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Date: <b>11/06/2012</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
<b>1 Sediment competence (Worksheet 5-22)</b>	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope—slightly incompetent	Cannot move $D_{35}$ of bed material and/or $D_{100}$ of bar material	Cannot move $D_{16}$ of bed material and/or $D_{100}$ of bar or sub-pavement size	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>2 Sediment Capacity (POWERSED) (Worksheet 5-20)</b>	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	<b>2</b>
	(2)	(4)	(6)	(7)	
<b>3 W/d Ratio State (Worksheet 5-13)</b>	1.0 – 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>4 Stream Succession States (Worksheet 5-24)</b>	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>5 Depositional Patterns (Worksheet 5-10)</b>	B1	B2, B4	B3, B5	B6, B7, B8	<b>1</b>
	(1)	(2)	(3)	(4)	
<b>6 Debris / Blockages (Worksheet 5-11)</b>	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	<b>1</b>
	(1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>10</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
<b>Vertical Stability for Excess Deposition / Aggradation (use total points and check stability rating)</b>	<i>No Deposition</i> 10 – 14 <input checked="" type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input type="checkbox"/>	<i>Aggradation</i> > 30 <input type="checkbox"/>	

**Worksheet 5-27.** Vertical stability – degradation.

Stream: <b>West Monument B4/2c Reference</b>		Stream Type: <b>B4/2c</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIIb</b>			
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Date: <b>11/06/2012</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>Sediment Competence</b> (Worksheet 5-22)	Does not indicate excess competence <b>(2)</b>	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed <b>(4)</b>	$D_{100}$ of bed moved <b>(6)</b>	Particles much larger than $D_{100}$ of bed moved <b>(8)</b>	<b>2</b>
<b>Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Does not indicate excess capacity <b>(2)</b>	Slight excess energy: up to 10% increase above reference <b>(4)</b>	Excess energy sufficient to increase load up to 50% of annual load <b>(6)</b>	Excess energy transporting more than 50% of annual load <b>(8)</b>	<b>2</b>
<b>Degree of Channel Incision (BHR)</b> (Worksheet 5-12)	1.00 – 1.10 <b>(2)</b>	1.11 – 1.30 <b>(4)</b>	1.31 – 1.50 <b>(6)</b>	> 1.50 <b>(8)</b>	<b>2</b>
<b>Stream Succession States</b> (Worksheets 5-12 and 5-24)	Does not indicate incision or degradation <b>(2)</b>	If BHR > 1.1 and stream type has W/d between 5–10 <b>(4)</b>	If BHR > 1.1 and stream type has W/d less than 5 <b>(6)</b>	(B→G), (C→G), (E→G), (D→G) <b>(8)</b>	<b>2</b>
<b>Confinement (MWR / MWR<sub>ref</sub>)</b> (Worksheet 5-14)	0.80 – 1.00 <b>(1)</b>	0.30 – 0.79 <b>(2)</b>	0.10 – 0.29 <b>(3)</b>	< 0.10 <b>(4)</b>	<b>1</b>
<b>Total Points</b>					<b>9</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation (use total points and check stability rating)</b>	<i>Not Incised</i> 9 – 11 <input checked="" type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input type="checkbox"/>	<i>Degradation</i> > 27 <input type="checkbox"/>	

Worksheet 5-28. Channel enlargement.

Stream: <b>West Monument B4/2c Reference</b>		Stream Type: <b>B4/2c</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIIb</b>			
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Date: <b>11/06/2012</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1–4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	2
	(2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	2
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	2
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	2
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>8</b>
<b>Category Point Range</b>					
Channel Enlargement Prediction (use total points and check stability rating)	<i>No Increase</i> 8 – 10 <input checked="" type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input type="checkbox"/>	<i>Extensive</i> > 24 <input type="checkbox"/>	

**Worksheet 5-29.** Overall sediment supply.

Stream: <b>West Monument B4/2c Reference</b>		Stream Type: <b>B4/2c</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIIIb</b>		
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Date: <b>11/06/2012</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1–5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	1	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	1	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	1	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	1	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	1	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>5</b>	
<b>Category Point Range</b>				
Overall Sediment Supply Rating (use total points and check stability rating)	<b>Low</b> 5 <input checked="" type="checkbox"/>	<b>Moderate</b> 6 – 10 <input type="checkbox"/>	<b>High</b> 11 – 15 <input type="checkbox"/>	<b>Very High</b> 16 – 20 <input type="checkbox"/>



Worksheet 5-32. Summary of stability condition categories.

Stream: <b>West Monument B4/2c Reference</b>		Location: <b>Pike National Forest, Colorado</b>	
Observers: <b>Bones, Kyle, David, Luke, Kim</b>	Date: <b>11/6/2012</b>	Stream Type: <b>B4/2c</b>	Valley Type: <b>VIIIb</b>
<b>Channel Dimension</b>	Mean Bankfull Depth (ft): <b>0.81</b>	Bankfull Width (ft): <b>7.7</b>	Cross-Sectional Area (ft <sup>2</sup> ): <b>6.21</b>
<b>Channel Pattern</b>	Width of Flood-Prone Area (ft): <b>9.51</b>	Entrenchment Ratio: <b>2.54</b>	
<b>River Profile &amp; Bed Features</b>	Mean: $\lambda/W_{bkl}$ : <b>6.62</b>	$L_{rfl}/W_{bkl}$ : <b>7.14</b>	$R_c/W_{bkl}$ : <b>1.53</b>
	Range: $\lambda/W_{bkl}$ : <b>5.58-7.66</b>	$L_{rfl}/W_{bkl}$ : <b>6.49-7.79</b>	MWR: <b>2.34</b>
	Check: <input checked="" type="checkbox"/> Riffle/Pool	<input type="checkbox"/> Step/Pool	<input type="checkbox"/> Plane Bed
	<input type="checkbox"/> Riffle	<input type="checkbox"/> Pool	<input type="checkbox"/> Convergence/Divergence
	Max Bankfull Depth (ft): <b>1.47</b>	Depth Ratio (max to mean): <b>1.81</b>	<input type="checkbox"/> Dunes/Antidunes/Smooth Bed
			<input type="checkbox"/> Pool
			<input type="checkbox"/> Riffle
			<input type="checkbox"/> Pool
			<input type="checkbox"/> Pool-to-Pool Ratio
			<input type="checkbox"/> Slope
			<input type="checkbox"/> Valley: <b>0.0146</b>
			<input type="checkbox"/> Water Surface: <b>0.013</b>
<b>Level III Stream Stability Indices</b>	Riparian Vegetation: <b>Spruce, Aspen, Willows, Chok At Potnetial</b>	Potential Composition/Density:	Remarks: Condition, Vigor & Usage of Existing Reach:
	Flow Regime: <b>P1, 2, &amp; Order: 7, 8</b>	Meander Patterns: <b>M3</b>	<b>Riparian zone is vigorous and healthy</b>
	Degree of Incision (Bank-Height Ratio): <b>1.0</b>	Degree of Incision Stability Rating: <b>Stable</b>	Modified Pfankuch Stability Rating (Numeric & Adjective Rating): <b>54 (Good)</b>
	Width/depth Ratio (W/d): <b>9.51</b>	Reference W/d Ratio (W/d <sub>ref</sub> ): <b>9.51</b>	W/d Ratio State Stability Rating: <b>Stable</b>
	Meander Width Ratio (MWR): <b>2.34</b>	Reference MWR <sub>ref</sub> : <b>2.34</b>	MWR / MWR <sub>ref</sub> Stability Rating: <b>Stable</b>
<b>Bank Erosion Summary</b>	Length of Reach Studied (ft): <b>115</b>	Annual Streambank Erosion Rate: (tons/yr) <b>0.005</b>	Curve Used: <b>Colorado</b>
<b>Sediment Capacity (POWERSED)</b>	<input checked="" type="checkbox"/> Sufficient Capacity	<input type="checkbox"/> Insufficient Capacity	Remarks:
<b>Entrainment/Competence</b>	Largest Particle from Bar Sample (mm): <b>98</b>	$\tau =$ <b>1.183</b>	$\tau^* =$ <b>N/A</b>
<b>Successional Stage Shift</b>	$\rightarrow$	$\rightarrow$	$\rightarrow$
<b>Lateral Stability</b>	<input checked="" type="checkbox"/> Stable	<input type="checkbox"/> Mod. Unstable	<input type="checkbox"/> Highly Unstable
<b>Vertical Stability (Aggradation)</b>	<input checked="" type="checkbox"/> No Deposition	<input type="checkbox"/> Mod. Deposition	<input type="checkbox"/> Ex. Deposition
<b>Vertical Stability (Degradation)</b>	<input checked="" type="checkbox"/> Not Incised	<input type="checkbox"/> Slightly Incised	<input type="checkbox"/> Mod. Incised
<b>Channel Enlargement</b>	<input checked="" type="checkbox"/> No Increase	<input type="checkbox"/> Slight Increase	<input type="checkbox"/> Mod. Increase
<b>Sediment Supply (Channel Source)</b>	<input checked="" type="checkbox"/> Low	<input type="checkbox"/> Moderate	<input type="checkbox"/> High
		<input type="checkbox"/> Very High	Remarks/causes: <b>Little Channel Source Sediment</b>
			Remarks/causes: <b>Stable for Lateral Stability</b>
			Remarks/causes: <b>No Deposition</b>
			Remarks/causes: <b>Channel not incised</b>
			Remarks/causes: <b>No increase in channel enlargement</b>
			Remarks/causes: <b>Used Yellowstone curve for very low BEHI</b>
			Remarks/causes: <b>Required Slope: 0.0127</b>
			Remarks/causes: <b>Existing Slope: 0.79</b>
			Remarks/causes: <b>Potential Stream State (Type): B2/4c</b>
			Remarks/causes: <b>Stable for Lateral Stability</b>



## *Appendix C20*

# **C4 Stream Type**

## *Reference Reach*



# Table of Contents

## *Appendix C20: C4 Reference Reach*

<b>Reach Location &amp; Overview.....</b>	<b>C20-2</b>
<b>Survey Summary.....</b>	<b>C20-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C20-9</b>
<b><i>Velocity, Classification &amp; Morphological Relations.....</i></b>	<b>C20-9</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b><i>Stability Indices.....</i></b>	<b>C20-13</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b><i>BANCS Model – Streambank Erosion.....</i></b>	<b>C20-23</b>
Worksheet 5-16. Bank Erosion Hazard Index (BEHI) rating.	
Worksheet 5-17. Near-Bank Stress (NBS) rating.	
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b><i>FLOWSED Model – Total Annual Sediment Yield.....</i></b>	<b>C20-27</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b><i>Sediment Competence/Entrainment.....</i></b>	<b>C20-29</b>
Worksheet 5-22. Sediment competence calculations.	
<b><i>Channel Stability Ratings.....</i></b>	<b>C20-30</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b><i>Summary.....</i></b>	<b>C20-36</b>
Worksheet 5-32. Summary of stability condition categories.	

## C4 Reference Reach Location & Overview

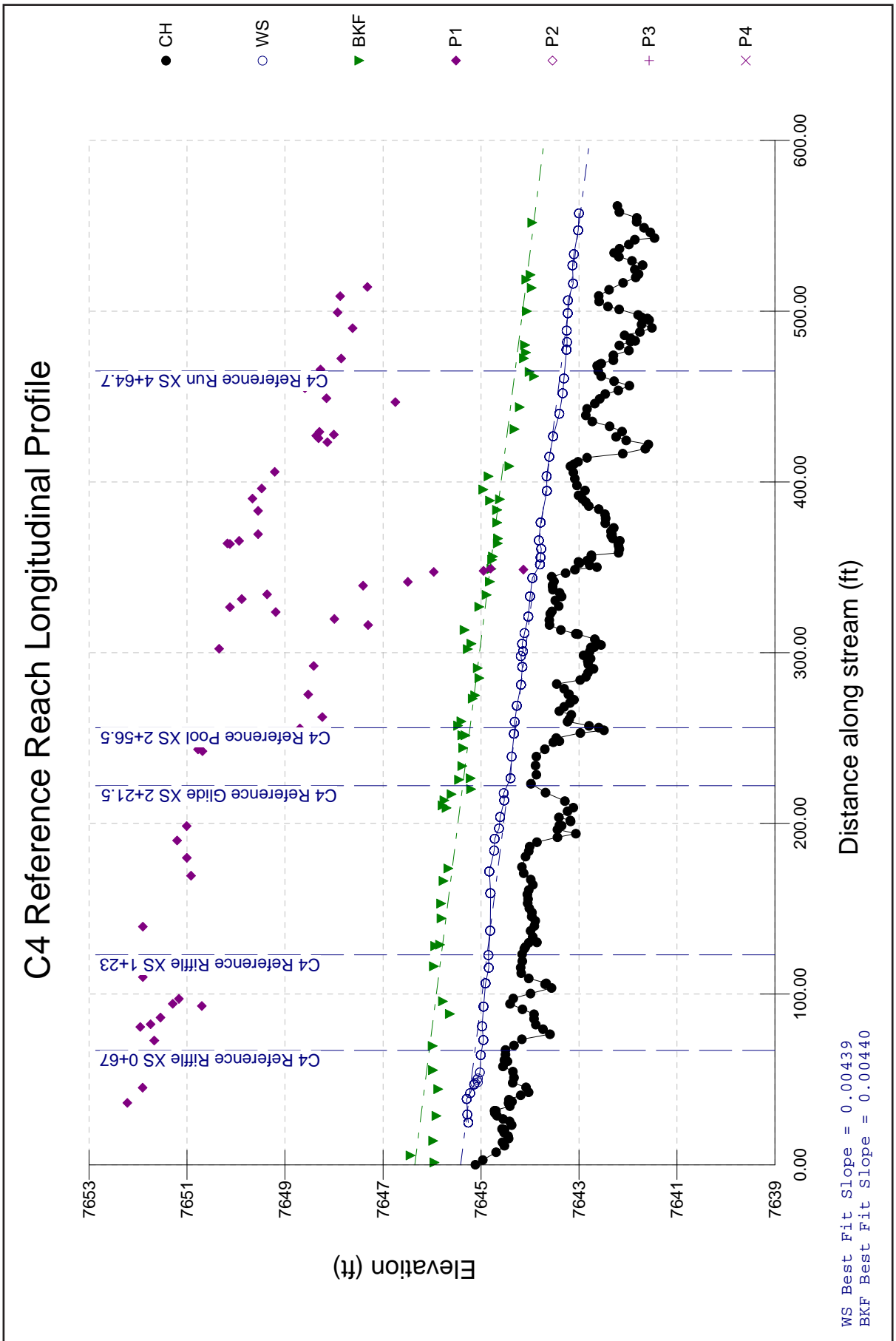
The C4 reference reach is in a terraced, alluvial Valley Type VIII and is typical of a gravel-bed stream channel. The channel bed and banks are potentially erodible, but due to the good vegetation condition, this reference reach shows little sediment yield from this reach. Bed features are dominated by riffles and pools with runs and glide features. This perennial channel is located on Trout Creek across from the Manitou Experimental Forest Headquarters. The stream is a meandering, low gradient channel with a well-developed floodplain. The morphological data from this reach will be used to develop dimension, pattern, and profile data for impaired streams that potentially should be C4 stream types in a Valley Type VIII. There is moderate sediment storage in point and central bars, typical of this stream type. The natural or geologic rate of streambank erosion is higher than the B4 reference reach; however, the excellent riparian vegetation of willow and Carex/Juncus understory has helped maintain an erosion rate of *0.0063 tons/yr/ft* (**Worksheet 5-18**). Streambank erosion rates for impaired conditions of this stream type can be associated with rates that are three orders of magnitude larger than exhibited in this reference reach.

Typical of C4 stream types are large entrenchment ratios (not entrenched), low to moderate width/depth ratios, and a relatively sinuous pattern with a sinuosity greater than 1.3. The channel is not laterally contained or confined with meander width ratios greater than 5.0. There is not an acceleration of sediment supply from this reach during high runoff events due to the good riparian vegetation coverage.

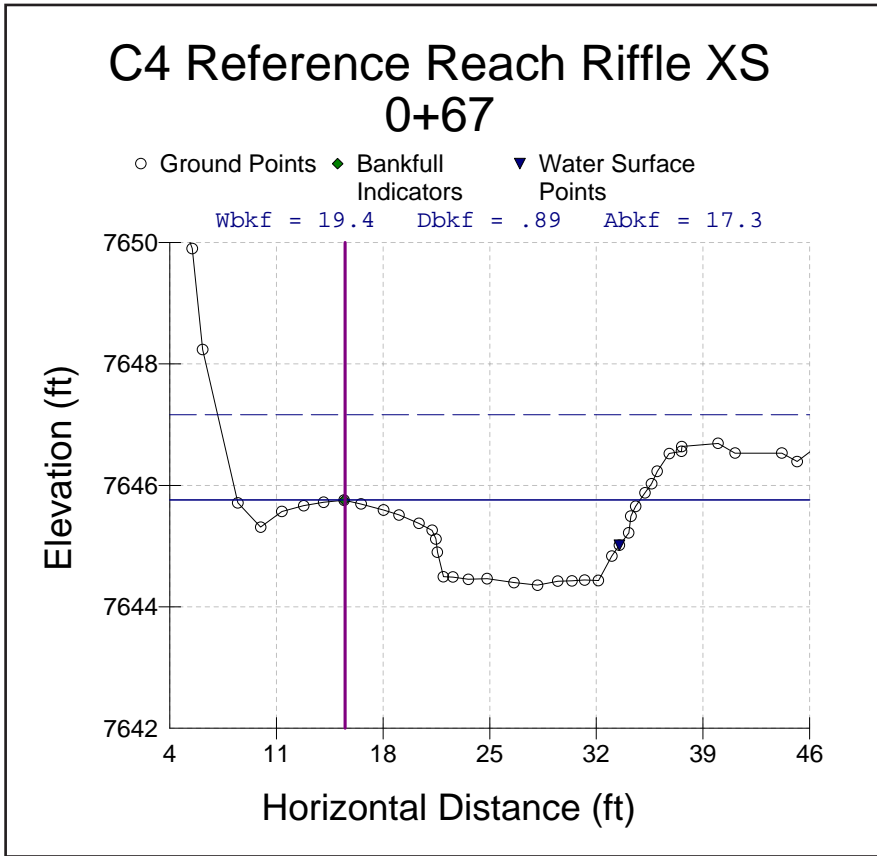
The photograph depicts the good riparian community and the stable characteristics of the C4 stream type. There is little to no evidence of active channel-source sediment. The details of the dimension, pattern, profile and materials are summarized. The POWERSED model was not run on this reference reach as the bed is obviously stable. The following summary worksheets provide the detail of the morphology, hydraulics, streambank erosion rates, and stability. In the situation where impaired G4c, F4c, and some D4 stream types are located, an alternative for mitigation and sediment reduction from increased flow in these stream types is to use the data from the stable form of the C4 reference reach to extrapolate for potential implementation of natural channel design.



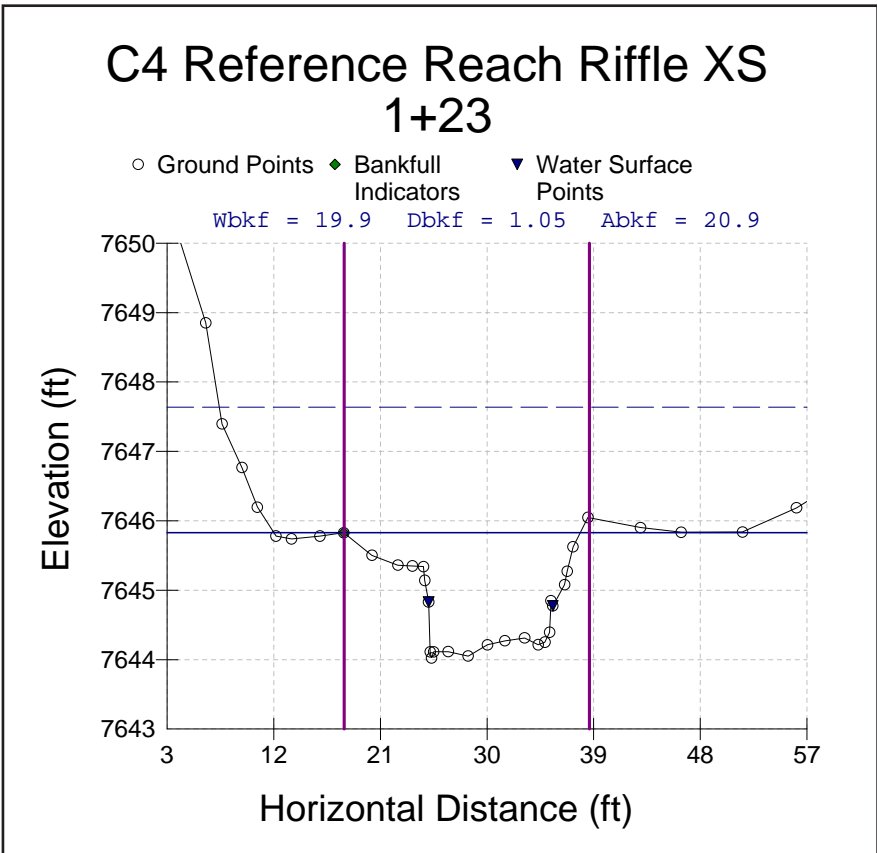
# Survey Summary



Longitudinal Profile (graph generated from RIVERMorph™)

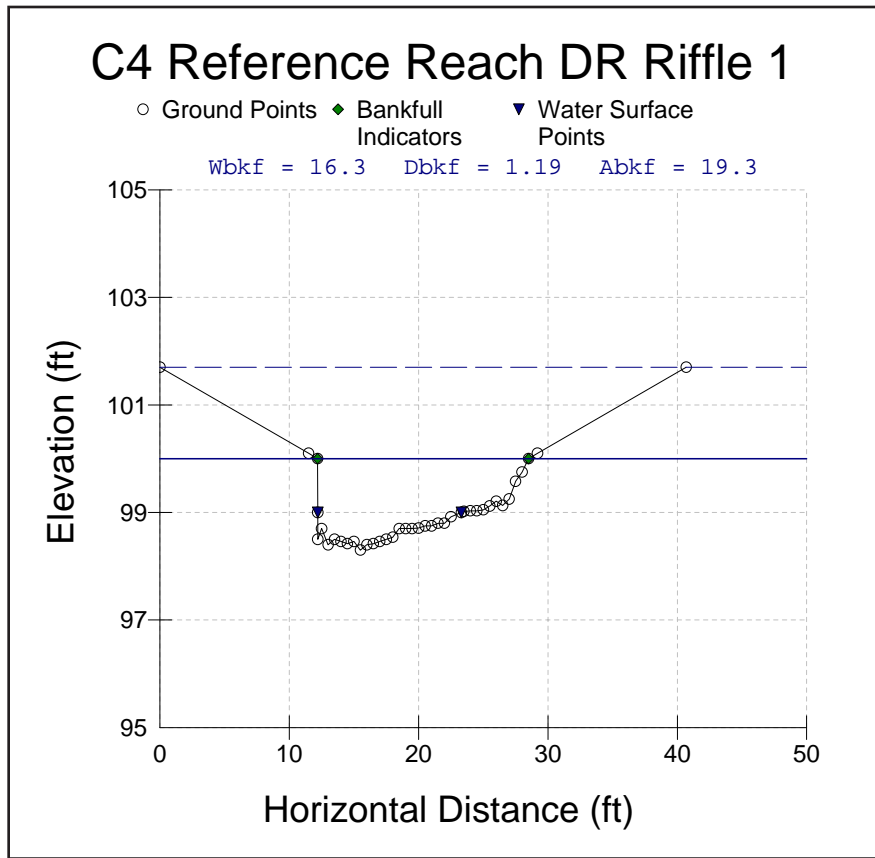


Riffle Cross-section 0+67 (graph generated from RIVERMorph™)

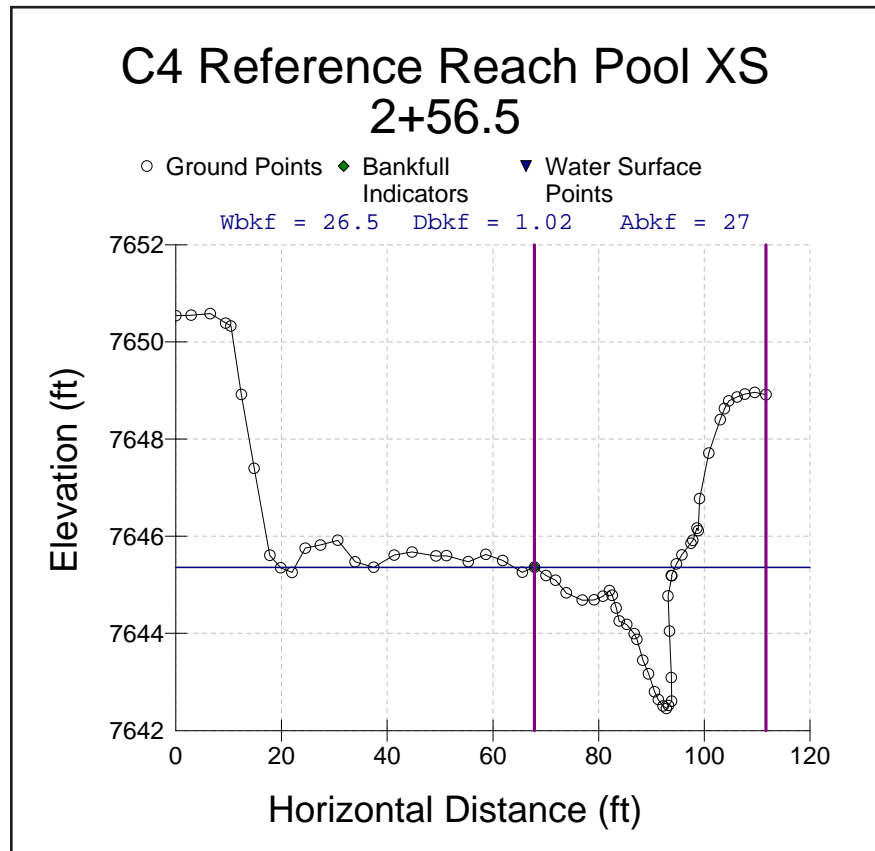


Riffle Cross-section 1+23 (graph generated from RIVERMorph™)

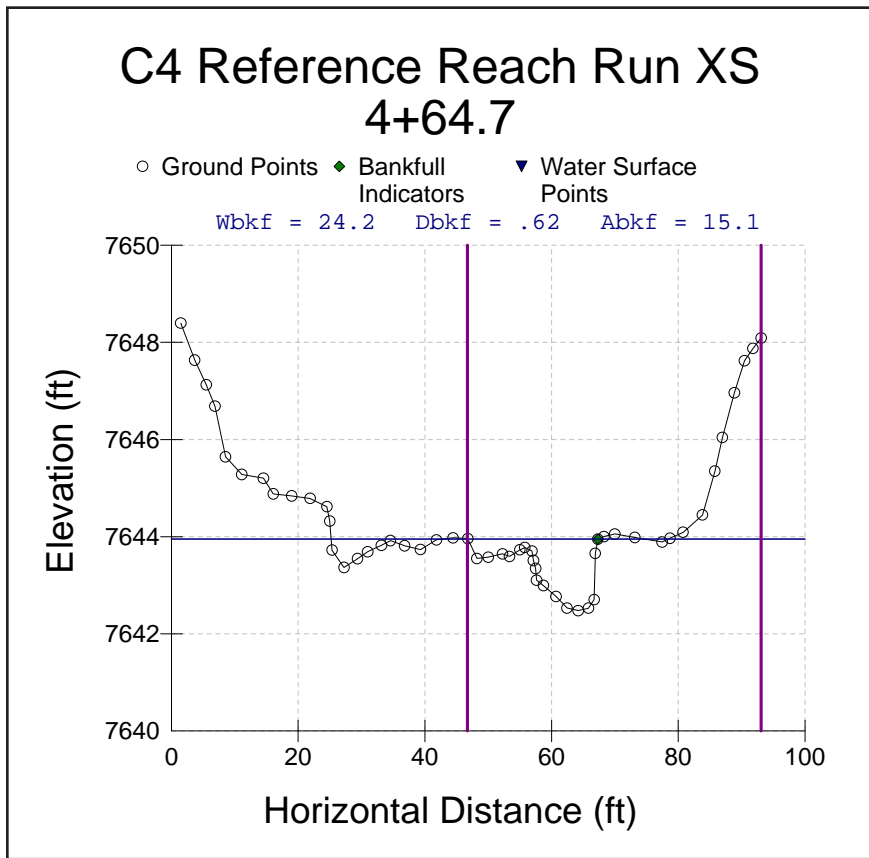




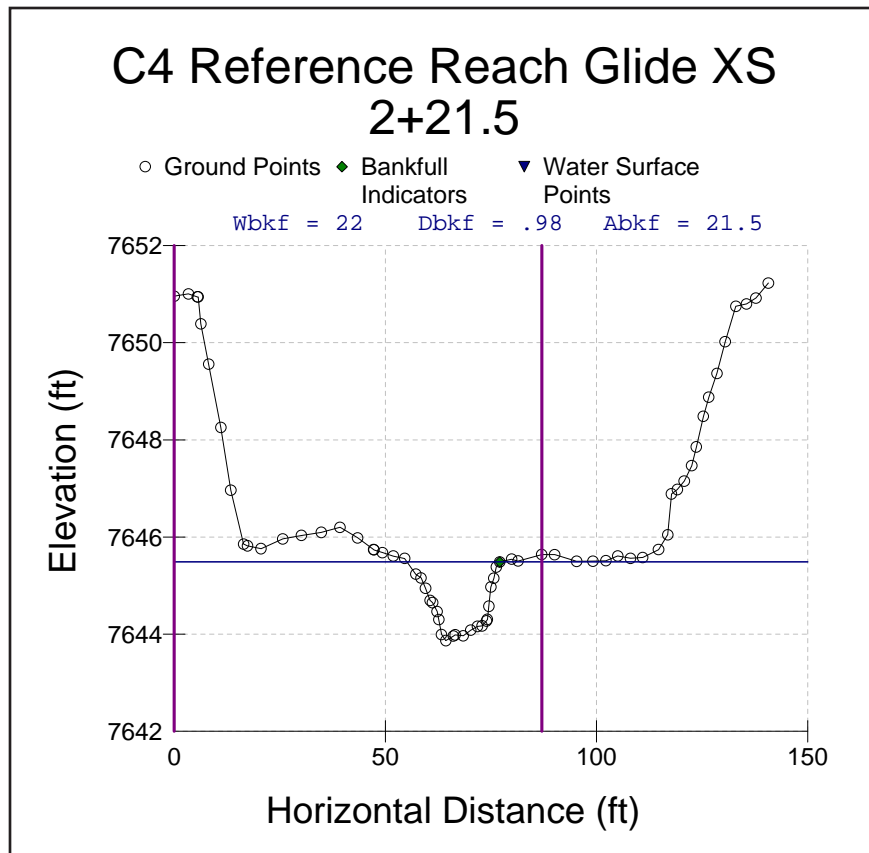
Riffle Cross-section DR\_Riffle 1 (graph generated from RIVERMorph™)



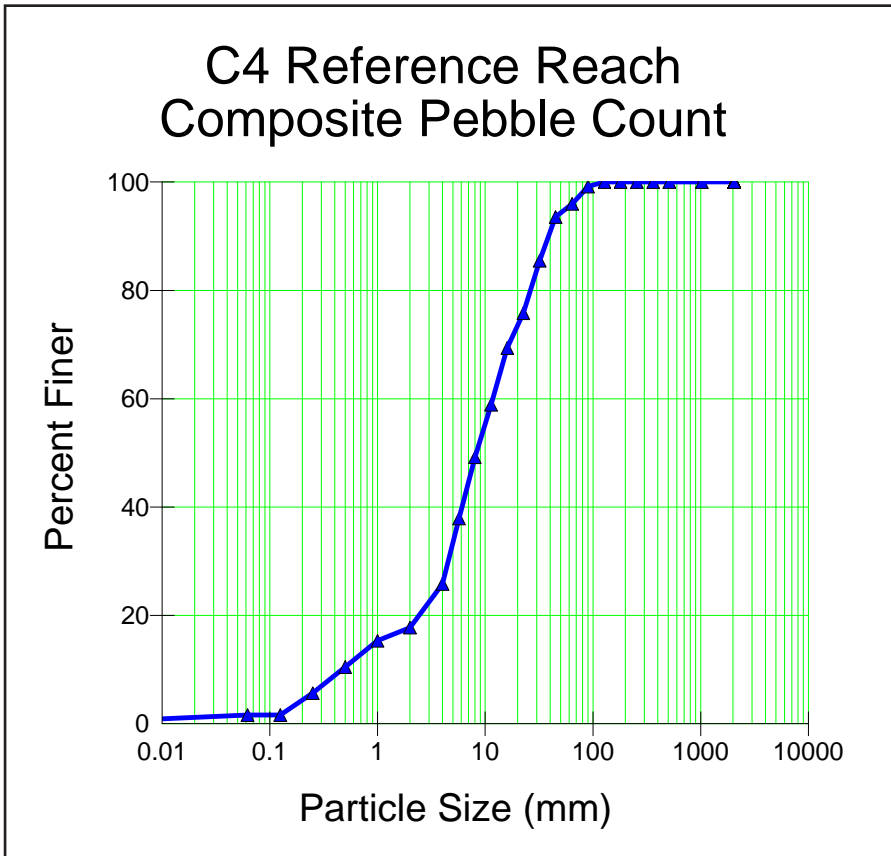
Pool Cross-section 2+56.5 (graph generated from RIVERMorph™)



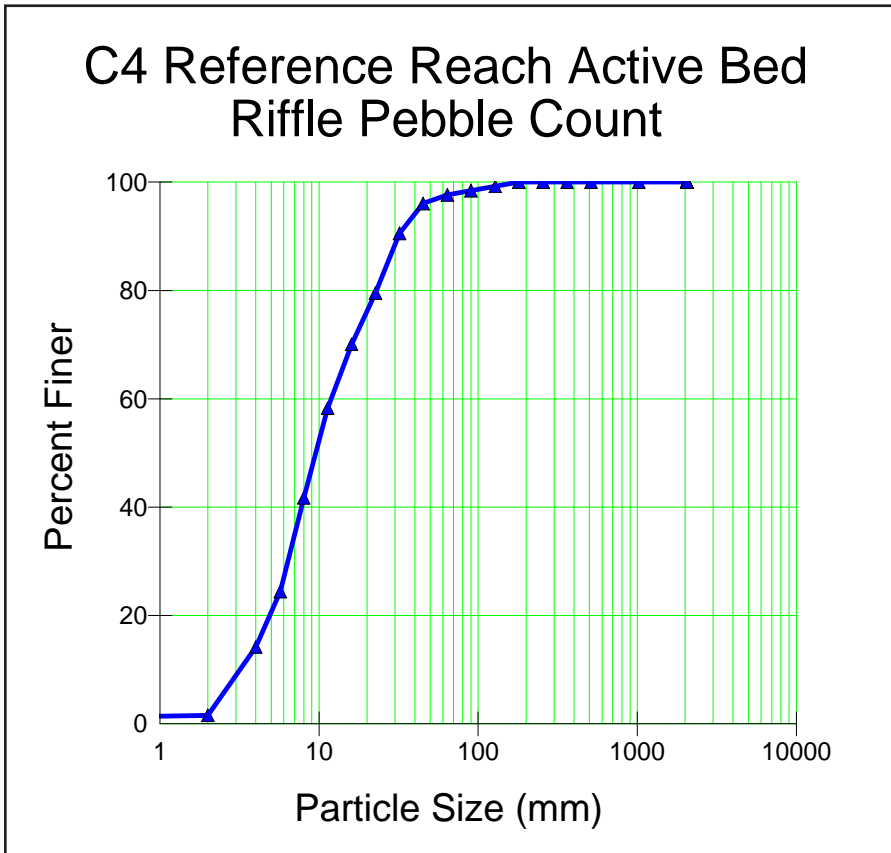
Run Cross-section 4+64.7 (graph generated from RIVERMorph™)



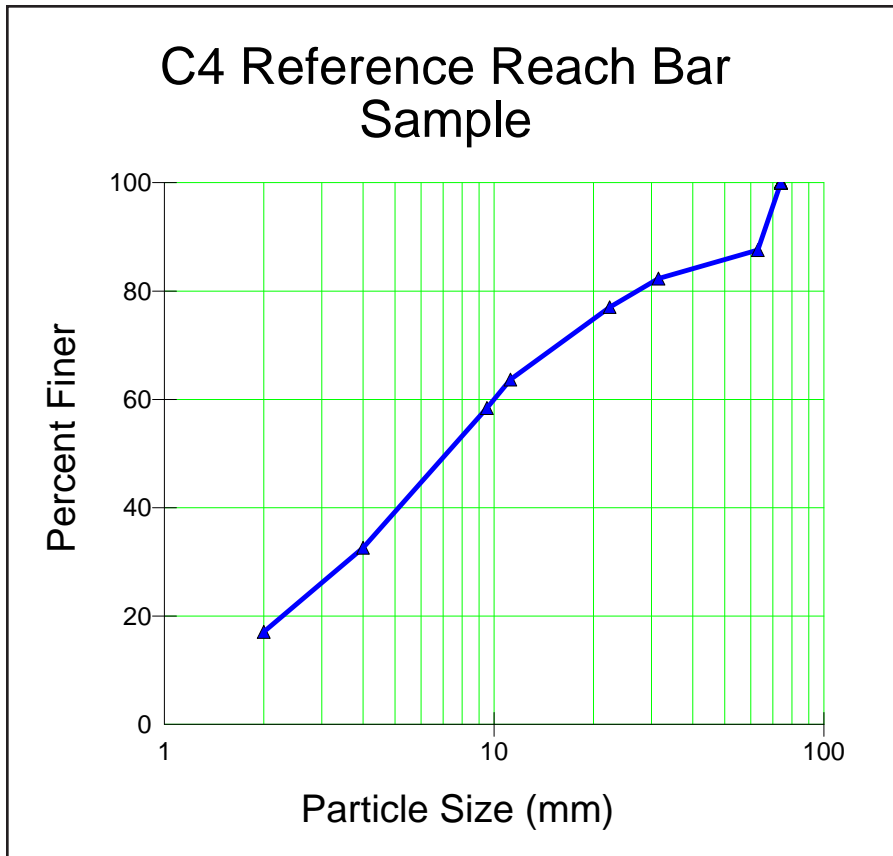
Glide Cross-section 2+21.5 (graph generated from RIVERMorph™)



**Composite Pebble Count** (graph generated from RIVERMorph™)



**Active Bed Riffle Pebble Count** (graph generated from RIVERMorph™)



**Bar Sample** (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates					
Stream:	Trout Creek, C4 Reference Reach			Location:	Riffle XS 0+67, Pike N.F., Colorado
Date:	8/13/2010	Stream Type:	C4	Valley Type:	VIII
Observers:	D. Rosgen et al.			HUC:	__ __ __ __ __ __ __ __ __ __
INPUT VARIABLES			OUTPUT VARIABLES		
Bankfull Riffle Cross-Sectional AREA	17.3	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.89	$d_{bkf}$ (ft)
Bankfull Riffle WIDTH	19.4	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim (2 * d_{bkf}) + W_{bkf}$	21.15	$W_p$ (ft)
$D_{84}$ at Riffle	26.4	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.09	$D_{84}$ (ft)
Bankfull SLOPE	0.0044	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	0.82	R (ft)
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R(ft) / $D_{84}$ (ft)	9.45	R / $D_{84}$
Drainage Area	71.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.341	$u^*$ (ft/sec)
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$			2.96	ft / sec	51.27 cfs
2. Roughness Coefficient: a) Manning's n from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ n = 0.034			2.54	ft / sec	44.07 cfs
2. Roughness Coefficient: b) Manning's n from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ n = 0.031			2.79	ft / sec	48.32 cfs
2. Roughness Coefficient: c) Manning's n from Jarrett (USGS): $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for n = 0.051			1.69	ft / sec	29.25 cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Limerinos n			3.12	ft / sec	54.0 cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Darcy-Weisbach			2.98	ft / sec	51.6 cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge Q = _____ year $u = Q / A$				ft / sec	cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$				ft / sec	cfs
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation (R/ $D_{84}$ ) – Estimation Method 1					
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.					
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.					
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.					
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.					

**Worksheet 5-3.** Level II stream classification.

Stream: <b>Trout Creek, C4 Reference Reach</b>	
Basin: <b>Trout Creek</b>	Drainage Area: <b>45440</b> acres <b>71</b> mi <sup>2</sup>
Location: <b>Pike National Forest, Colorado</b>	
Twp.&Rge:	Sec.&Qtr.:
Cross-Section Monuments (Lat./Long.): <b>Riffle XS 0+67</b>	Date: <b>8/13/2010</b>
Observers: <b>D. Rosgen et al.</b>	Valley Type: <b>VIII</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>19.37</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A_{bkf} / W_{bkf}$ ).	<b>0.89</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>17.32</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>21.76</b>	ft/ft
<b>Maximum DEPTH (<math>d_{max}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>1.40</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>41.92</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>2.16</b>	ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the median or dominant diameter of channel materials, as sampled proportionately from the channel surface, between the bankfull stage and Thalweg elevations.	<b>8.28</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.0044</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length ( $SL / VL$ ); or estimated from a ratio of valley slope divided by channel slope ( $S_{val} / S$ ).	<b>1.38</b>	

<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>Stream Type</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>C4</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>See Classification Key (Figure 2-14)</b> </div>
---	--	--

Worksheet 5-4a. Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trout Creek, C4 Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>						
Observers: <b>D. Rosgen et al.</b>		Date: <b>8/13/2010</b>		Valley Type: <b>VIII</b>		Stream Type: <b>C4</b>		
<b>River Reach Dimension Summary Data.....1</b>								
<b>Riffle Dimensions* ** * **</b>	<b>Riffle Dimensions* ** * **</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Width ( $W_{bkt}$ )	18.5	16.3	19.9	ft Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	19.2	17.3	20.9
	Mean Riffle Depth ( $d_{bkt}$ )	1.04	0.89	1.19	ft Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	18.1	13.7	21.8
	Maximum Riffle Depth ( $d_{max}$ )	1.64	1.40	1.81	ft Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	1.575	1.429	1.724
	Width of Flood-Prone Area ( $W_{fpa}$ )	58.8	41.9	69.4	ft Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )	3.21	2.16	3.99
	Riffle Inner Berm Width ( $W_{ib}$ )	11.4	10.4	12.9	ft Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )	0.619	0.522	0.668
	Riffle Inner Berm Depth ( $d_{ib}$ )	0.57	0.38	0.73	ft Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )	0.567	0.319	0.820
	Riffle Inner Berm Area ( $A_{ib}$ )	6.5	4.1	9.4	ft <sup>2</sup> Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )	0.349	0.214	0.542
	Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )	21.3	17.6	28.7				
<b>Pool Dimensions* ** * **</b>	<b>Pool Dimensions* ** * **</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Pool Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Pool Width ( $W_{bkfp}$ )	26.5			ft Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )	1.430		
	Mean Pool Depth ( $d_{bkfp}$ )	1.02			ft Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )	0.978		
	Pool Cross-Sectional Area ( $A_{bkfp}$ )	27.05			ft Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )	1.409		
	Maximum Pool Depth ( $d_{maxp}$ )	2.9			ft Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	2.8		
	Pool Inner Berm Width ( $W_{ibp}$ )	9.4			ft Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )	0.354		
	Pool Inner Berm Depth ( $d_{ibp}$ )	0.92			ft Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )	0.902		
	Pool Inner Berm Area ( $A_{ibp}$ )	8.6			ft <sup>2</sup> Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )	0.319		
	Point Bar Slope ( $S_{pb}$ )	0.260			ft/ft Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )	10.18		
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Run Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Run Width ( $W_{bkfr}$ )	24.2			ft Run Width to Riffle Width ( $W_{bkfr} / W_{bkt}$ )	1.307		
	Mean Run Depth ( $d_{bkfr}$ )	0.62			ft Mean Run Depth to Mean Riffle Depth ( $d_{bkfr} / d_{bkt}$ )	0.594		
	Run Cross-Sectional Area ( $A_{bkfr}$ )	15.07			ft Run Area to Riffle Area ( $A_{bkfr} / A_{bkt}$ )	0.785		
	Maximum Run Depth ( $d_{maxr}$ )	1.5			ft Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )	1.409		
	Run Width/Depth Ratio ( $W_{bkfr} / d_{bkfr}$ )	39.1						
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Glide Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Glide Width ( $W_{bkfg}$ )	22.0			ft Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )	1.189		
	Mean Glide Depth ( $d_{bkfg}$ )	0.98			ft Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )	0.939		
	Glide Cross-Sectional Area ( $A_{bkfg}$ )	21.54			ft Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )	1.122		
	Maximum Glide Depth ( $d_{maxg}$ )	1.62			ft Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )	1.553		
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )	22.5			ft/ft Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )	26.77		
	Glide Inner Berm Width ( $W_{ibg}$ )	12.9			ft Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )	0.583		
	Glide Inner Berm Depth ( $d_{ibg}$ )	0.48			ft Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )	0.490		
Glide Inner Berm Area ( $A_{ibg}$ )	6.18			ft <sup>2</sup> Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )	0.287			
<b>Step**</b>	<b>Step Dimensions**</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Step Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Step Width ( $W_{bkfs}$ )				ft Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )			
	Mean Step Depth ( $d_{bkfs}$ )				ft Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )			
	Step Cross-Sectional Area ( $A_{bkfs}$ )				ft Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )			
	Maximum Step Depth ( $d_{maxs}$ )				ft Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )								

**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trout Creek, C4 Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>												
Observers: <b>D. Rosgen et al.</b>		Date: <b>8/13/2010</b>		Valley Type: <b>VIII</b>		Stream Type: <b>C4</b>								
<b>Hydraulics</b>	<b>River Reach Summary Data.....2</b>													
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $U_{bkt}$ )		<b>2.98</b>		ft/sec		Estimation Method	<b>Darcy-Weisbach</b>						
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )		<b>51.6</b>		cfs		Drainage Area	<b>71.0</b> mi <sup>2</sup>						
<b>Channel Pattern</b>	<b>Geometry</b>			<b>Dimensionless Geometry Ratios</b>										
	Linear Wavelength ( $\lambda$ )	<b>84.5</b>	<b>62.0</b>	<b>114.5</b>	ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )	<b>4.56</b>	<b>3.35</b>	<b>6.18</b>					
	Stream Meander Length ( $L_m$ )	<b>104.6</b>	<b>72.6</b>	<b>161.0</b>	ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )	<b>5.64</b>	<b>3.92</b>	<b>8.69</b>					
	Radius of Curvature ( $R_c$ )	<b>42.8</b>	<b>31.1</b>	<b>65.0</b>	ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )	<b>2.31</b>	<b>1.68</b>	<b>3.51</b>					
	Belt Width ( $W_{bt}$ )	<b>66.1</b>	<b>42.8</b>	<b>82.8</b>	ft	Meander Width Ratio ( $W_{bt} / W_{bkt}$ )	<b>3.57</b>	<b>2.31</b>	<b>4.47</b>					
	Arc Length ( $L_a$ )	<b>37.7</b>	<b>20.1</b>	<b>46.0</b>	ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )	<b>2.03</b>	<b>1.08</b>	<b>2.48</b>					
	Riffle Length ( $L_r$ )	<b>23.1</b>	<b>8.5</b>	<b>82.4</b>	ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )	<b>1.25</b>	<b>0.46</b>	<b>4.45</b>					
	Individual Pool Length ( $L_p$ )	<b>17.6</b>	<b>8.5</b>	<b>27.5</b>	ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )	<b>0.95</b>	<b>0.46</b>	<b>1.48</b>					
Pool to Pool Spacing ( $P_s$ )	<b>55.5</b>	<b>22.0</b>	<b>107.5</b>	ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )	<b>3.00</b>	<b>1.19</b>	<b>5.80</b>						
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )		<b>0.0061</b>	ft/ft	Average Water Surface Slope ( $S$ )		<b>0.0044</b>	ft/ft	Sinuosity ( $S_{val} / S$ )		<b>1.38</b>			
	Stream Length (SL)		<b>567.7</b>	ft	Valley Length (VL)		<b>783.4</b>	ft	Sinuosity (SL / VL)		<b>1.38</b>			
	Low Bank Height (LBH)	start: <b>1.40</b> ft	end: <b>1.80</b> ft	Max Bankfull Depth ( $d_{max}$ )	start: <b>1.40</b> ft	end: <b>1.80</b> ft	Bank-Height Ratio (BHR) (LBH / $d_{max}$ )		start: <b>1.0</b>	end: <b>1.0</b>				
	<b>Facet Slopes</b>			<b>Dimensionless Facet Slope Ratios</b>										
	Riffle Slope ( $S_{rif}$ )	<b>0.0045</b>	<b>0.0029</b>	<b>0.0054</b>	ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0205</b>	<b>0.6477</b>	<b>1.2341</b>					
	Run Slope ( $S_{run}$ )	<b>0.0113</b>	<b>0.0066</b>	<b>0.0140</b>	ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )	<b>2.5614</b>	<b>1.5000</b>	<b>3.1705</b>					
	Pool Slope ( $S_p$ )	<b>0.0023</b>	<b>0.0008</b>	<b>0.0038</b>	ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )	<b>0.5250</b>	<b>0.1841</b>	<b>0.8636</b>					
	Glide Slope ( $S_g$ )	<b>0.0034</b>	<b>0.0026</b>	<b>0.0039</b>	ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )	<b>0.7750</b>	<b>0.5909</b>	<b>0.8864</b>					
	Step Slope ( $S_s$ )				ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )								
	<b>Max Depths<sup>a</sup></b>			<b>Dimensionless Depth Ratios</b>										
	Max Riffle Depth ( $d_{max}$ )	<b>1.60</b>	<b>1.40</b>	<b>1.75</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>1.534</b>	<b>1.342</b>	<b>1.677</b>					
	Max Run Depth ( $d_{maxr}$ )	<b>1.74</b>	<b>1.57</b>	<b>1.95</b>	ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )	<b>1.668</b>	<b>1.505</b>	<b>1.869</b>					
	Max Pool Depth ( $d_{maxp}$ )	<b>2.46</b>	<b>2.12</b>	<b>2.95</b>	ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	<b>2.358</b>	<b>2.038</b>	<b>2.837</b>					
	Max Glide Depth ( $d_{maxg}$ )	<b>1.55</b>	<b>1.33</b>	<b>1.78</b>	ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )	<b>1.486</b>	<b>1.275</b>	<b>1.706</b>					
Max Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )									
<b>Channel Materials</b>	<b>Reach<sup>b</sup></b>		<b>Riffle<sup>c</sup></b>		<b>Bar</b>		<b>Reach<sup>b</sup></b>		<b>Riffle<sup>c</sup></b>		<b>Bar</b>		<b>Protrusion Height<sup>d</sup></b>	
	% Silt/Clay	<b>2</b>	<b>0</b>	<b>0</b>	$D_{16}$	<b>1.3</b>	<b>4.3</b>	<b>0.0</b>						mm
	% Sand	<b>16</b>	<b>2</b>	<b>17</b>	$D_{35}$	<b>5.3</b>	<b>7.1</b>	<b>4.5</b>						mm
	% Gravel	<b>78</b>	<b>96</b>	<b>72</b>	$D_{50}$	<b>8.3</b>	<b>9.7</b>	<b>7.7</b>						mm
	% Cobble	<b>4</b>	<b>2</b>	<b>11</b>	$D_{84}$	<b>30.6</b>	<b>26.4</b>	<b>41.7</b>						mm
	% Boulder	<b>0</b>	<b>0</b>	<b>0</b>	$D_{95}$	<b>56.4</b>	<b>42.5</b>	<b>69.6</b>						mm
	% Bedrock	<b>0</b>	<b>0</b>	<b>0</b>	$D_{100}$	<b>128.0</b>	<b>180.0</b>	<b>74.0</b>						mm

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.  
<sup>b</sup> Composite sample of riffles and pools within the designated reach.  
<sup>c</sup> Active bed of a riffle.  
<sup>d</sup> Height of roughness feature above bed.



## Stability Indices


**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation					
Stream: <b>Trout Creek, C4 Reference Reach</b>			Location: <b>Pike National Forest, Colorado, above Manitou Expt. Forest</b>		
Observers: <b>D. Rosgen et al.</b>		Reference reach <input checked="" type="checkbox"/>	Disturbed (impacted reach) <input type="checkbox"/>	Date: <b>8/13/2010</b>	
Existing species composition: <b>Willow, Redtop, Carex/Juncus</b>			Potential species composition: <b>Same as Existing but without Invasives</b>		
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition
<b>1. Overstory</b>	Canopy layer	5-10%	10%	<b>Willow</b>	<b>100%</b>
					<b>100%</b>
<b>2. Understory</b>	Shrub layer		30%	<b>Willow</b>	<b>100%</b>
					<b>100%</b>
<b>3. Ground level</b>	Herbaceous		58%	<b>Carex/juncus</b>	<b>75%</b>
				<b>Hairgrass</b>	<b>5%</b>
				<b>Poa</b>	<b>5%</b>
				<b>Thistle</b>	<b>10%</b>
				<b>Smart weed</b>	<b>1%</b>
					<b>100%</b>
	Leaf or needle litter			<b>Remarks:</b> Condition, vigor and/or usage of existing reach: <b>Recovering C4 inside of an F4 stream type, naturally confined between terraces. One-half mile below reservoir, and although stream has a sediment trap, there is an ample sediment supply.</b>	
	Bare ground		2%		
*Based on crown closure.			<b>Column total = 100%</b>		
**Based on basal area to surface area.					

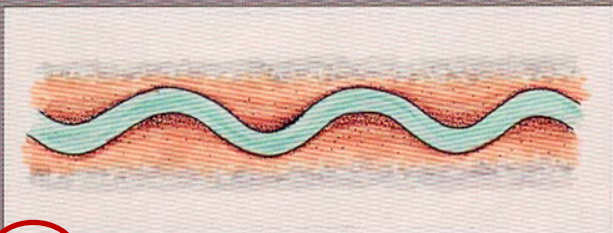



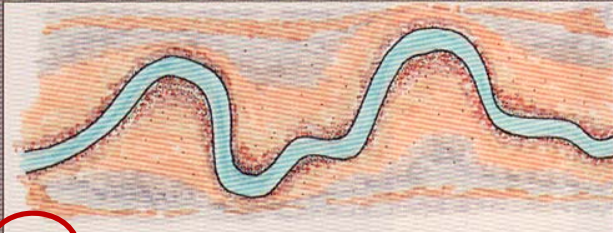
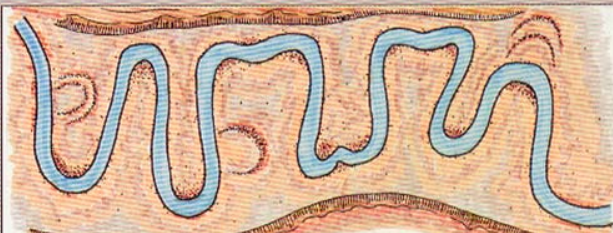
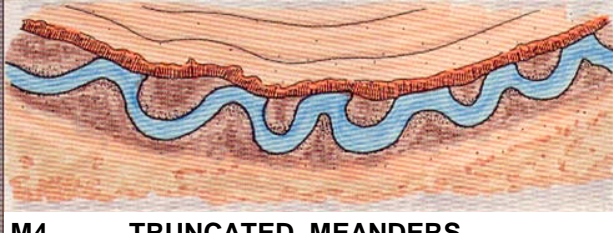

**Worksheet 5-7. Flow regime.**

<b>FLOW REGIME</b>								
Stream: <b>Trout Creek, C4 Reference</b>			Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>D. Rosgen et al.</b>						Date: <b>8/13/2010</b>		
List ALL COMBINATIONS that APPLY.....			<b>P1</b>	<b>P2</b>	<b>P8</b>			
<b>General Category</b>								
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation							
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
<b>P</b>	Perennial stream channels: Surface water persists yearlong.							
<b>Specific Category</b>								
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
<b>4</b>	Streamflow regulated by glacial melt.							
<b>5</b>	Ice flows/ice torrents from ice dam breaches.							
<b>6</b>	Alternating flow/backwater due to tidal influence.							
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.							
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
<b>9</b>	Rain-on-snow generated runoff.							

**Worksheet 5-8.** Stream order & stream size.

Stream Size and Order			
Stream:	Trout Creek, C4 Reference Reach		
Location:	Pike National Forest, Colorado		
Observers:	D. Rosgen <i>et al.</i>		
Date:	8/13/2010		
Stream Size Category and Order 			S-4(4)
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0.305	<1	<input type="checkbox"/>
S-2	0.3 – 1.5	1 – 5	<input type="checkbox"/>
S-3	1.5 – 4.6	5 – 15	<input type="checkbox"/>
<b>S-4</b>	<b>4.6 – 9</b>	<b>15 – 30</b>	<input checked="" type="checkbox"/>
S-5	9 – 15	30 – 50	<input type="checkbox"/>
S-6	15 – 22.8	50 – 75	<input type="checkbox"/>
S-7	22.8 – 30.5	75 – 100	<input type="checkbox"/>
S-8	30.5 – 46	100 – 150	<input type="checkbox"/>
S-9	46 – 76	150 – 250	<input type="checkbox"/>
S-10	76 – 107	250 – 350	<input type="checkbox"/>
S-11	107 – 150	350 – 500	<input type="checkbox"/>
S-12	150 – 305	500 – 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
Stream Order			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			

**Worksheet 5-9.** Meander patterns.

<b>Meander Patterns</b>				
Stream: <b>Trout Creek, C4 Reference Reach</b>	Location: <b>Pike National Forest, CO</b>			
Observers: <b>D. Rosgen et al.</b>	Date: <b>8/13/2010</b>			
<b>List ALL CATEGORIES that APPLY</b>	<b>M1</b>	<b>M3</b>		
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>				
 <div style="display: flex; justify-content: space-between; align-items: center; padding: 5px;"> <span style="border: 1px solid red; border-radius: 50%; padding: 2px 5px;"><b>M1</b></span> <span><b>REGULAR MEANDERS</b></span> </div>	 <div style="display: flex; justify-content: space-between; align-items: center; padding: 5px;"> <span><b>M5</b></span> <span><b>UNCONFINED MEANDER SCROLLS</b></span> </div>			
 <div style="display: flex; justify-content: space-between; align-items: center; padding: 5px;"> <span><b>M2</b></span> <span><b>TORTUOUS MEANDERS</b></span> </div>	 <div style="display: flex; justify-content: space-between; align-items: center; padding: 5px;"> <span><b>M6</b></span> <span><b>CONFINED MEANDER SCROLLS</b></span> </div>			
 <div style="display: flex; justify-content: space-between; align-items: center; padding: 5px;"> <span style="border: 1px solid red; border-radius: 50%; padding: 2px 5px;"><b>M3</b></span> <span><b>IRREGULAR MEANDERS</b></span> </div>	 <div style="display: flex; justify-content: space-between; align-items: center; padding: 5px;"> <span><b>M7</b></span> <span><b>DISTORTED MEANDER LOOPS</b></span> </div>			
 <div style="display: flex; justify-content: space-between; align-items: center; padding: 5px;"> <span><b>M4</b></span> <span><b>TRUNCATED MEANDERS</b></span> </div>	 <div style="display: flex; justify-content: space-between; align-items: center; padding: 5px;"> <span><b>M8</b></span> <span><b>IRREGULAR MEANDERS with oxbows and</b></span> </div>			

**Worksheet 5-10.** Depositional patterns.

**Depositional Patterns**

Stream: **Trout Creek, C4 Reference Reach**

Location: **Pike National Forest, Colorado**

Observers: **D. Rosgen et al.**

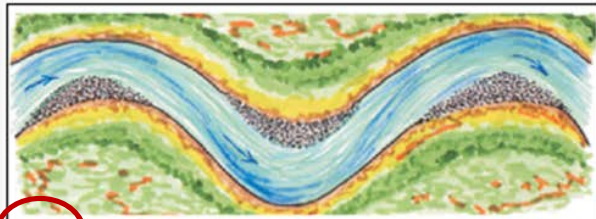
Date: **8/13/2010**

List ALL CATEGORIES that APPLY

**B1**

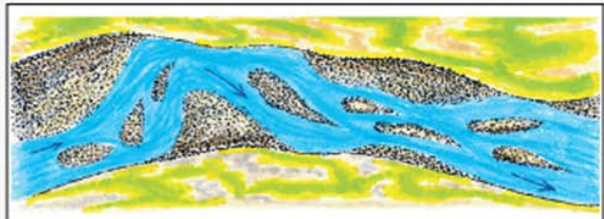
**B2**

*Various Depositional Features modified from Galay et al. (1973)*



**B1**

**POINT BARS**



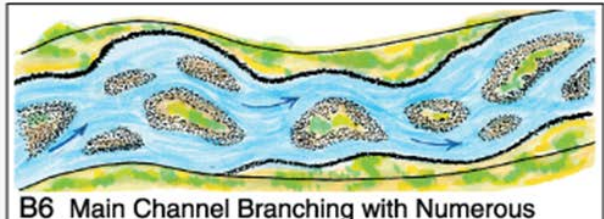
**B5**

**DIAGONAL BARS**

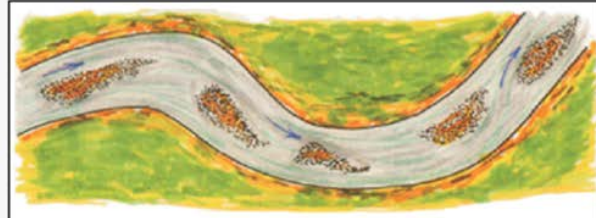


**B2**

**POINT BARS with Few MID-CHANNEL BARS**

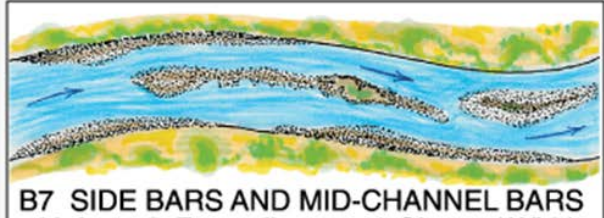


**B6 Main Channel Branching with Numerous MID-CHANNEL BARS and Islands**



**B3**

**NUMEROUS MID-CHANNEL BARS**

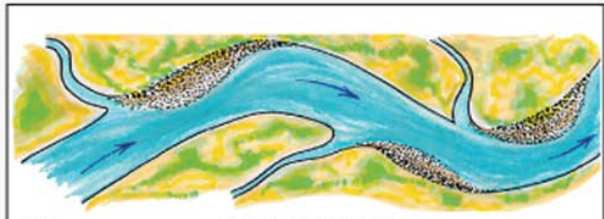


**B7 SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths**



**B4**

**SIDE BARS**



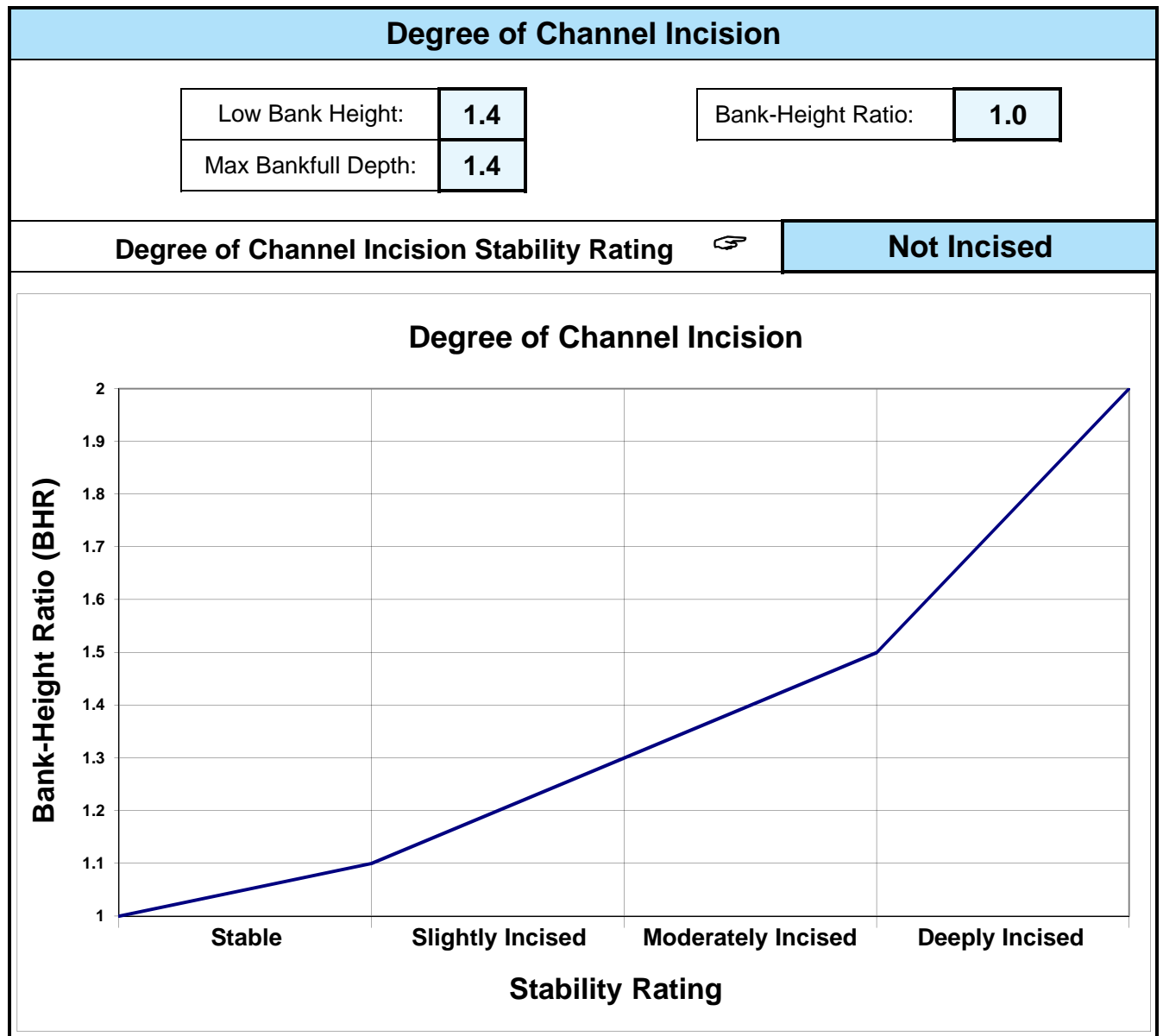
**B8**

**DELTA BARS**

**Worksheet 5-11.** Channel blockages.

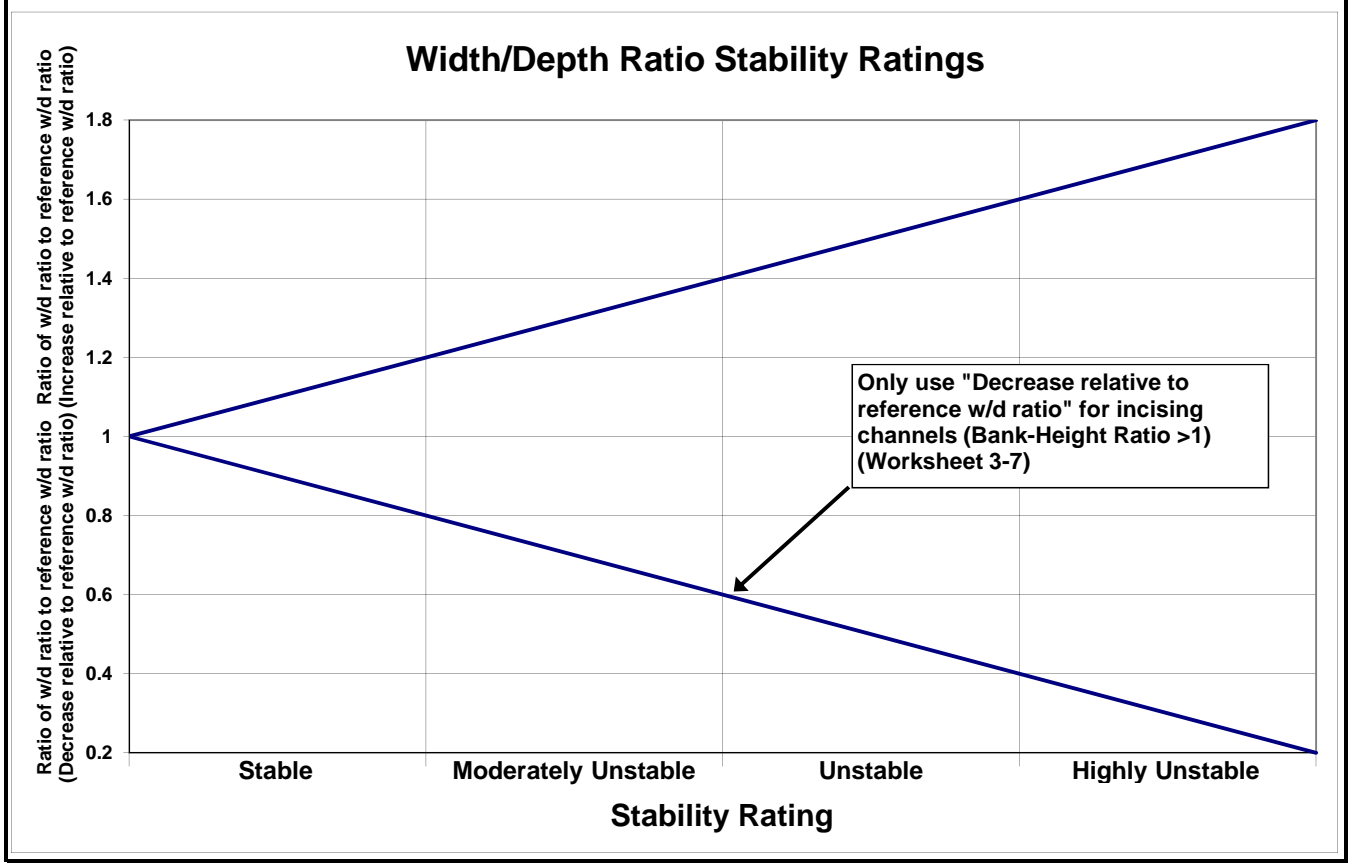
Channel Blockages		
Stream: <b>Trout Creek, C4 Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>D. Rosgen et al.</b>		Date: <b>8/13/2010</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input checked="" type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input type="checkbox"/>
<b>D4</b> Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

**Worksheet 5-12.** Degree of channel incision.



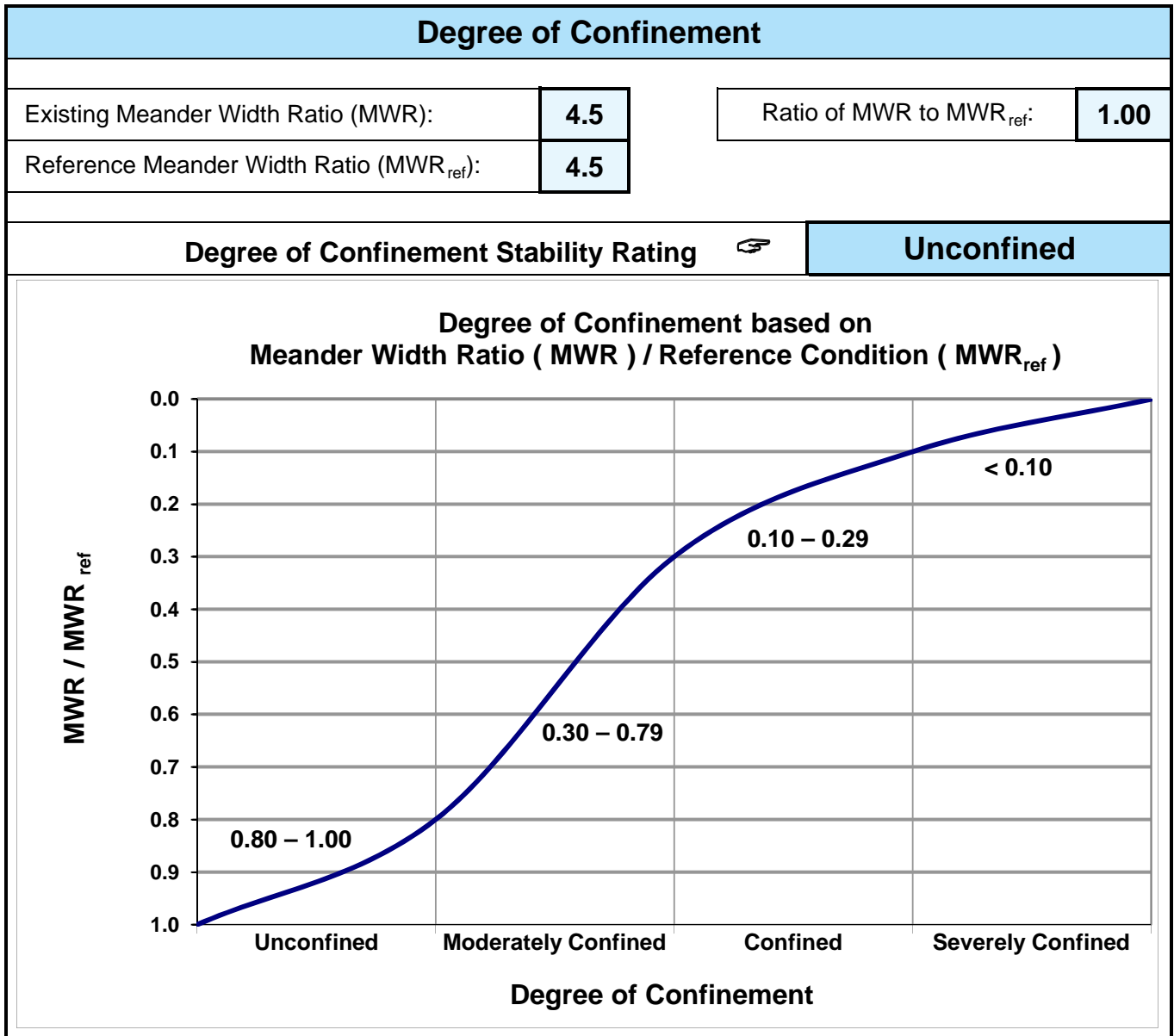
**Worksheet 5-13.** Width/depth ratio state.

Width/Depth Ratio State			
Existing Width/Depth Ratio:	<b>13.7</b>	Ratio of existing W/d to reference W/d:	<b>1.00</b>
Reference Width/Depth Ratio:	<b>13.7</b>		
<b>Width/Depth Ratio State Stability Rating</b>			<b>Stable</b>





**Worksheet 5-14.** Degree of channel confinement (lateral containment).



Worksheet 5-15. Pfankuch channel stability rating.

Stream: Trout Creek, C4 Reference Reach		Location: Pike National Forest, CO		Valley Type: VIII		Observers: D. Rosgen et al.		Date: 8/13/2010																																							
Local- tion	Key	Category	Excellent	Good	Fair	Poor	Description	Rating	Rating																																						
Upper banks	1	Landform slope	Bank slope gradient <30%.	Bank slope gradient 30-40%.	Bank slope gradient 40-60%.	Bank slope gradient > 60%.	Bank slope gradient > 60%.	6	8																																						
	2	Mass erosion	No evidence of past or future mass erosion.	Infrequent. Mostly healed over. Low future potential.	Frequent or large, causing sediment nearly yearlong.	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.		9	12																																						
	3	Debris jam potential	Essentially absent from immediate channel area.	Present, but mostly small twigs and limbs.	Moderate to heavy amounts, mostly larger sizes.	Moderate to heavy amounts, predominantly larger sizes.		6	8																																						
	4	Vegetative bank protection	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	70-90% density. Fewer species or less vigor suggest less dense or deep root mass.	50-70% density. Lower vigor and fewer species from a shallow, discontinuous root mass.	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.		9	12																																						
Lower banks	5	Channel capacity	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference with/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0.	Bankfull stage is contained within banks. Width/depth ratio departure from reference with/depth ratio = 1.0-1.2. Bank-Height Ratio (BHR) = 1.0-1.1.	Bankfull stage is not contained. Width/depth ratio departure from reference with/depth ratio = 1.2-1.4. Bank-Height Ratio (BHR) > 1.3.	Bankfull stage is not contained; over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference with/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.		3	4																																						
	6	Bank rock content	> 65% with large angular boulders. 12'+ common.	40-65%. Mostly boulders and small cobbles 6-12".	20-40%. Most in the 3-6" diameter class.	<20% rock fragments of gravel sizes, 1-3" or less.		6	8																																						
	7	Obstructions to flow	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	Frequent obstructions and deflectors cause bank erosion yearlong. Sediment traps full, channel migration occurring.		6	8																																						
	8	Cutting	Little or none. Infrequent raw banks <6".	Some, intermittently at outcrops and constrictions. Raw banks may be up to 12".	Significant. Cuts 12-24" high. Root overhangs and sloughing evident.	Almost continuous cuts, some over 24" high. Failure of overhangs frequent.		12	16																																						
	9	Deposition	Little or no enlargement of channel or point bars.	Some new bar increase, mostly from coarse gravel.	Moderate deposition of new gravel and coarse sand on old and some new bars.	Extensive deposit of predominantly fine particles. Accelerated bar development.		12	16																																						
Bottom	10	Rock angularity	Sharp edges and corners. Plane surfaces rough.	Rounded corners and edges. Surfaces smooth and flat.	Conners and edges well rounded in 2 dimensions.	Well rounded in all dimensions, surfaces smooth.		2	4																																						
	11	Brightness	Surfaces dull, dark or stained. Generally not bright.	Mostly dull, but may have <35% bright surfaces.	Mixture dull and bright, i.e., 35-65% mixture range.	Predominantly bright, > 65%, exposed or scoured surfaces.		2	4																																						
	12	Consolidation of particles	Assorted sizes tightly packed or overlapping.	Moderately packed with some overlapping.	Mostly loose assortment with no apparent overlap.	No packing evident. Loose assortment, easily moved.		4	8																																						
	13	Bottom size distribution	No size change evident. Stable material 80-100%.	Distribution shift light. Stable material 50-80%.	Moderate change in sizes. Stable materials 20-50%.	Marked distribution change. Stable materials 0-20%.		12	16																																						
	14	Scouring and deposition	<5% of bottom affected by scour or deposition.	5-30% affected. Scour at constrictions and where grades steepen. Some deposition in pools.	30-50% affected. Deposits and scour at obstructions, constrictions and bends. Some filling of pools.	More than 50% of the bottom in a state of flux or change nearly yearlong.		20	24																																						
	15	Aquatic vegetation	Abundant growth moss-like, dark green perennial. In swift water too.	Common. Algae forms in low velocity and pool areas. Moss here too.	Present but spotty, mostly in backwaters. Seasonal algae growth makes rocks slick.	Perennial types scarce or absent. Yellow-green, short-term bloom may be present.		3	4																																						
			<b>Excellent total = 21</b>	<b>Good total = 6</b>	<b>Fair total = 26</b>	<b>Poor total = 20</b>																																									
<b>Stream type</b>	<b>A1</b>	<b>A2</b>	<b>A3</b>	<b>A4</b>	<b>A5</b>	<b>A6</b>	<b>B1</b>	<b>B2</b>	<b>B3</b>	<b>B4</b>	<b>B5</b>	<b>B6</b>	<b>C1</b>	<b>C2</b>	<b>C3</b>	<b>C4</b>	<b>C5</b>	<b>C6</b>	<b>D3</b>	<b>D4</b>	<b>D5</b>	<b>D6</b>	<b>Grand total = 73</b>																								
Good (Stable)	38-43	38-43	54-90	60-95	60-95	50-80	38-45	38-45	40-60	40-64	48-68	40-60	38-50	38-50	60-85	70-90	70-90	60-85	85-107	85-107	85-107	85-107	67-98																								
Fair (Mod. unstable)	44-47	44-47	91-129	96-132	96-142	81-110	46-58	46-58	61-78	65-84	69-88	61-78	51-61	51-61	86-105	91-110	91-110	86-105	108-132	108-132	108-132	108-132	99-125																								
Poor (Unstable)	48+	48+	130+	133+	143+	111+	59+	59+	79+	85+	89+	79+	62+	62+	106+	111+	111+	106+	133+	133+	133+	133+	126+																								
<b>Stream type</b>	<b>DA3</b>	<b>DA4</b>	<b>DA5</b>	<b>DA6</b>	<b>E3</b>	<b>E4</b>	<b>E5</b>	<b>E6</b>	<b>F1</b>	<b>F2</b>	<b>F3</b>	<b>F4</b>	<b>F5</b>	<b>F6</b>	<b>G1</b>	<b>G2</b>	<b>G3</b>	<b>G4</b>	<b>G5</b>	<b>G6</b>	<b>G6</b>	<b>G6</b>	<b>G6</b>	<b>C4</b>																							
Good (Stable)	40-63	40-63	40-63	40-63	40-63	50-75	50-75	40-63	60-85	60-85	85-110	85-110	90-115	90-95	40-60	40-60	40-60	85-107	85-107	90-112	90-112	90-112	85-107																								
Fair (Mod. unstable)	64-86	64-86	64-86	64-86	64-86	76-96	76-96	64-86	86-105	86-105	111-125	111-125	116-130	96-110	61-78	61-78	108-120	108-120	113-125	113-125	108-120	108-120	108-120																								
Poor (Unstable)	87+	87+	87+	87+	87+	97+	97+	87+	106+	106+	126+	126+	131+	111+	79+	79+	121+	121+	126+	126+	126+	126+	121+																								
			<b>Excellent total = 21</b>	<b>Good total = 6</b>	<b>Fair total = 26</b>	<b>Poor total = 20</b>																																									
																							<b>Modified channel stability rating =</b>	<b>Good</b>																							

\*Rating is adjusted to potential stream type, not existing.

## BANCS Model – Streambank Erosion

**Worksheet 5-16.** The Bank Erosion Hazard Index (BEHI) rating.

Stream: <b>Trout Creek, C4 Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>	
Station: <b>above Manitou Expt. Station</b>		Observers: <b>D. Rosgen et al.</b>	
Date: <b>8/13/2010</b>	Stream Type: <b>C4</b>	Valley Type: <b>VIII</b>	

<b>Study Bank Height / Bankfull Height ( C )</b>					<b>BEHI Score</b> (Fig. 5-15)	
Study Bank Height (ft) =	1.40 (A)	Bankfull Height (ft) =	1.20 (B)	( A ) / ( B ) =	1.17 (C)	<b>1.0</b>
<b>Root Depth / Study Bank Height ( E )</b>						
Root Depth (ft) =	1.30 (D)	Study Bank Height (ft) =	1.40 (A)	( D ) / ( A ) =	0.93 (E)	<b>2.0</b>
<b>Weighted Root Density ( G )</b>						
Root Density as % =	70 (F)	( F ) × ( E ) =	98 (G)		<b>1.0</b>	
<b>Bank Angle ( H )</b>						
Bank Angle as Degrees =	70 (H)				<b>5.0</b>	
<b>Surface Protection ( I )</b>						
Surface Protection as % =	90% (I)				<b>1.0</b>	

<b>Bank Material Adjustment:</b>	<b>Bank Material Adjustment</b>
<ul style="list-style-type: none"> <li><b>Bedrock</b> (Overall Very Low BEHI)</li> <li><b>Boulders</b> (Overall Low BEHI)</li> <li><b>Cobble</b> (Subtract 10 points if uniform medium to large cobble)</li> <li><b>Gravel or Composite Matrix</b> (Add 5–10 points depending on percentage of bank material that is composed of sand)</li> <li><b>Sand</b> (Add 10 points)</li> <li><b>Silt/Clay</b> (no adjustment)</li> </ul>	<b>5</b>
	<b>Stratification Adjustment</b>
	Add 5–10 points, depending on position of unstable layers in relation to bankfull stage
	<b>0</b>

Very Low	Low	Moderate	High	Very High	Extreme	<b>Adjective Rating and Total Score</b>	<b>Low</b>
5 – 9.5	10 – 19.5	20 – 29.5	30 – 39.5	40 – 45	46 – 50	<b>15.0</b>	<b>15.0</b>

**Bank Sketch**

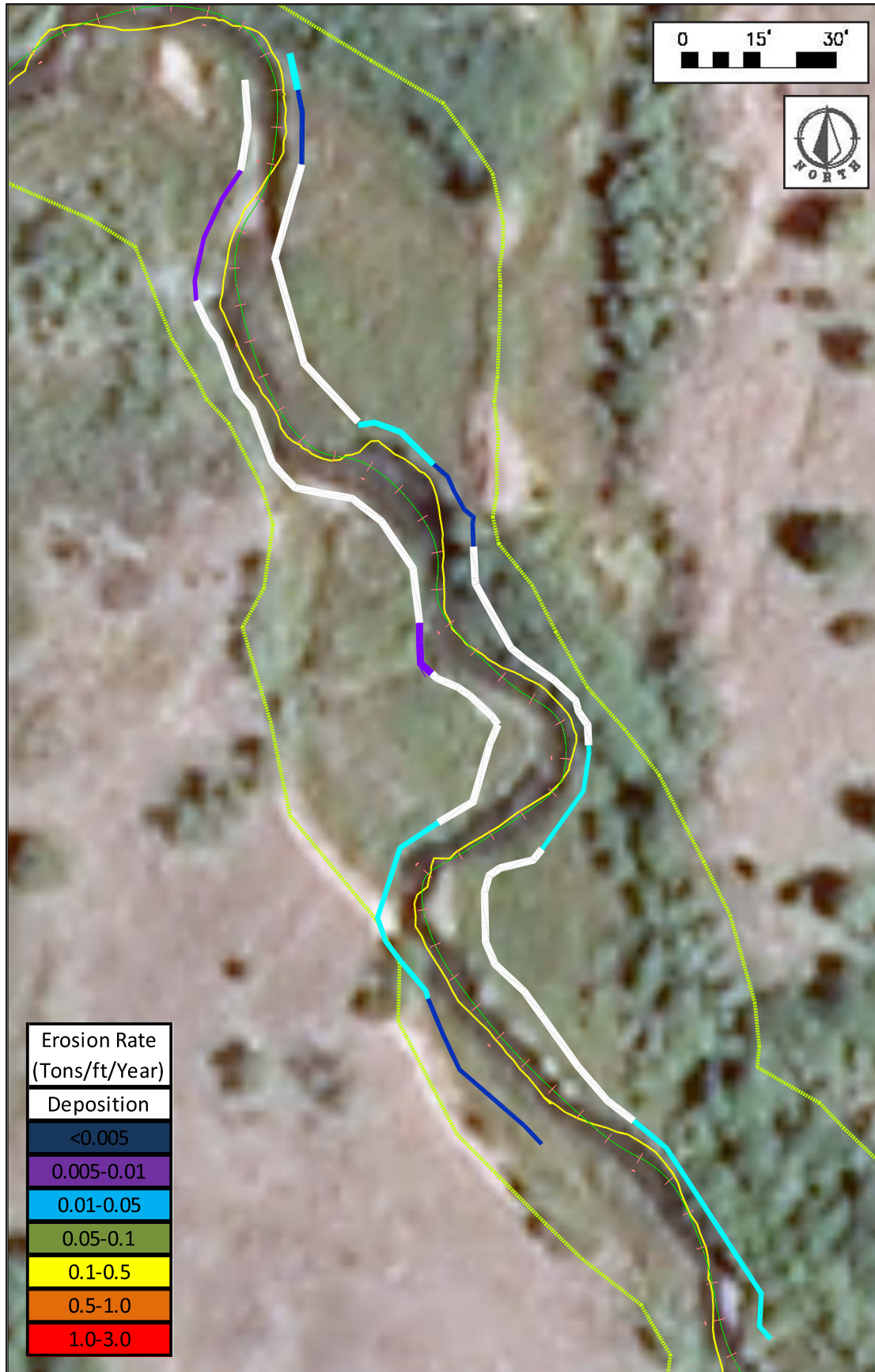
**Worksheet 5-17. Near-Bank Stress (NBS) rating.**

<b>Estimating Near-Bank Stress ( NBS )</b>									
Stream: <b>Trout Creek, C4 Reference Reach</b>					Location: <b>Trout Creek, C4 Reference Reach</b>				
Station: <b>0+20R</b>			Stream Type: <b>C4</b>			Valley Type: <b>VIII</b>			
Observers: <b>D. Rosgen et al.</b>							Date: <b>8/13/2010</b>		
<b>Methods for Estimating Near-Bank Stress (NBS)</b>									
(1)	Channel pattern, transverse bar or split channel/central bar creating NBS				Level I	Reconnaissance			
(2)	Ratio of radius of curvature to bankfull width ( $R_c / W_{bkf}$ )				Level II	General prediction			
(3)	Ratio of pool slope to average water surface slope ( $S_p / S$ )				Level II	General prediction			
(4)	Ratio of pool slope to riffle slope ( $S_p / S_{rif}$ )				Level II	General prediction			
(5)	Ratio of near-bank maximum depth to bankfull mean depth ( $d_{nb} / d_{bkf}$ )				Level III	Detailed prediction			
(6)	Ratio of near-bank shear stress to bankfull shear stress ( $\tau_{nb} / \tau_{bkf}$ )				Level III	Detailed prediction			
(7)	Velocity profiles / Isovels / Velocity gradient				Level IV	Validation			
<b>Level I</b>	<b>(1)</b>	Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High							
		Extensive deposition (continuous, cross-channel).....NBS = Extreme							
		Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme							
<b>Level II</b>	<b>(2)</b>	Radius of Curvature $R_c$ (ft)	Bankfull Width $W_{bkf}$ (ft)	Ratio $R_c / W_{bkf}$	Near-Bank Stress (NBS)	<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>Dominant Near-Bank Stress</b>  <b>Low</b> </div>			
	<b>(3)</b>	Pool Slope $S_p$	Average Slope $S$	Ratio $S_p / S$	Near-Bank Stress (NBS)				
<b>(4)</b>	Pool Slope $S_p$	Riffle Slope $S_{rif}$	Ratio $S_p / S_{rif}$	Near-Bank Stress (NBS)					
<b>Level III</b>	<b>(5)</b>	Near-Bank Max Depth $d_{nb}$ (ft)	Mean Depth $d_{bkf}$ (ft)	Ratio $d_{nb} / d_{bkf}$	Near-Bank Stress (NBS)				
		<b>2.2</b>	<b>1.4</b>	<b>1.5</b>	<b>Low</b>				
<b>(6)</b>	Near-Bank Max Depth $d_{nb}$ (ft)	Near-Bank Slope $S_{nb}$	Near-Bank Shear Stress $\tau_{nb}$ ( lb/ft <sup>2</sup> )	Mean Depth $d_{bkf}$ (ft)	Average Slope $S$	Bankfull Shear Stress $\tau_{bkf}$ ( lb/ft <sup>2</sup> )	Ratio $\tau_{nb} / \tau_{bkf}$	Near-Bank Stress (NBS)	
<b>Level IV</b>	<b>(7)</b>	Velocity Gradient ( ft / sec / ft )		Near-Bank Stress (NBS)					
<b>Converting Values to a Near-Bank Stress (NBS) Rating</b>									
Near-Bank Stress (NBS) ratings	Method number								
	(1)	(2)	(3)	(4)	(5)	(6)	(7)		
<b>Very Low</b>	N/A	> 3.00	< 0.20	< 0.40	< 1.00	< 0.80	< 0.50		
<b>Low</b>	N/A	2.21 – 3.00	0.20 – 0.40	0.41 – 0.60	1.00 – 1.50	0.80 – 1.05	0.50 – 1.00		
<b>Moderate</b>	N/A	2.01 – 2.20	0.41 – 0.60	0.61 – 0.80	1.51 – 1.80	1.06 – 1.14	1.01 – 1.60		
<b>High</b>	See	1.81 – 2.00	0.61 – 0.80	0.81 – 1.00	1.81 – 2.50	1.15 – 1.19	1.61 – 2.00		
<b>Very High</b>	(1)	1.50 – 1.80	0.81 – 1.00	1.01 – 1.20	2.51 – 3.00	1.20 – 1.60	2.01 – 2.40		
<b>Extreme</b>	Above	< 1.50	> 1.00	> 1.20	> 3.00	> 1.60	> 2.40		
<b>Overall Near-Bank Stress (NBS) rating</b>						<b>Low</b>			

**Worksheet 5-18.** Annual streambank erosion estimates.

Stream: <b>Trout Creek, C4 Reference Reach</b>		Location: <b>Trout Creek, C4 Reference Reach</b>					
Graph Used: <b>Colorado</b>		Total Bank Length (ft): <b>463</b>			Date: <b>8/13/2010</b>		
Observers: <b>D. Rosgen et al.</b>		Valley Type: <b>VIII</b>			Stream Type: <b>C4</b>		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 5-16) (adjective)	NBS rating (Worksheet 5-17) (adjective)	Bank erosion rate (Figure 5-34 or 5-35) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal $[(4) \times (5) \times (6)]$ (ft <sup>3</sup> /yr)	Erosion Rate (tons/yr/ft) $\{[(7)/27] \times 1.3 / (5)\}$
1.	Low	Very High	0.32332	40.0	1.4	18.11	0.02179
2.	Low	High	0.15505	20.0	1.4	4.34	0.01045
3.	Low	Moderate	0.07435	50.0	1.2	4.46	0.00430
4.	Low	High	0.15505	20.0	1.4	4.34	0.01045
5.	Low	High	0.15505	27.0	1.2	5.02	0.00896
6.	Low	Moderate	0.07435	10.0	1.9	1.41	0.00680
7.	Low	Moderate	0.07435	40.0	1.2	3.57	0.00430
8	Low	High	0.15505	16.0	1.5	3.72	0.01120
9	Low	High	0.15505	40.0	1.2	7.44	0.00896
10	Low	Moderate	0.07435	40.0	1.3	3.87	0.00465
11	Low	High	0.15505	16.0	1.9	4.71	0.01418
12							
13							
14							
15							
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					Total Erosion (ft <sup>3</sup> /yr)	<b>61.00</b>	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					Total Erosion (yds <sup>3</sup> /yr)	<b>2.26</b>	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					Total Erosion (tons/yr)	<b>2.94</b>	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					Total Erosion (tons/yr/ft)	<b>0.0063</b>	

Streambank Erosion Map



# FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Equation Type		Equation Source				Equation				Bankfull Discharge (cfs)			Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)			
1. Bedload Sediment		"Good/Fair" Pagosa				$y = -0.0113 + 1.0139x^{2.1929}$				51.6			0.028095864		114.7625704			
2. Suspended Sediment		"Good/Fair" Pagosa				$y = 0.0636 + 0.9326x^{2.4085}$												
From Dimensional Flow-Duration Curve												From Sediment Rating Curves			Calculate		Calculate Sediment Yield	
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)				
Percentage of Time	Daily Mean Discharge (cfs)	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Sediment Discharge	Suspended Sediment Discharge	Dimensionless Bedload Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow [(5)×(6)]	Suspended Sediment [(5)×(9)]	Bedload Sediment [(5)×(11)]	Suspended Sediment + Bedload Sediment [(13)×(14)]				
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>bkf</sub> )	(S/S <sub>bkf</sub> )	(tons/day)	(b <sub>s</sub> /b <sub>bkf</sub> )	(tons/day)	(cfs)	(tons)	(tons)	(tons)				
0%	131.2																	
0.10%	112.6	0.05%	0.09%	0.34	121.9	2.363	7.461	281.87	6.670	17.85	41.8	96.71	6.13	102.83				
0.25%	97.5	0.08%	0.15%	0.55	105.1	2.036	5.232	170.30	4.809	12.87	57.5	93.24	7.05	100.28				
0.50%	84.2	0.13%	0.25%	0.91	90.8	1.761	3.706	104.32	3.494	9.35	82.9	95.19	8.53	103.73				
0.75%	71.9	0.13%	0.25%	0.91	78.1	1.513	2.592	62.69	2.502	6.70	71.2	57.21	6.11	63.32				
1%	62.2	0.13%	0.25%	0.91	67.1	1.300	1.817	37.76	1.790	4.79	61.2	34.45	4.37	38.83				
1.5%	53.4	0.25%	0.50%	1.83	57.8	1.120	1.289	23.09	1.289	3.45	105.5	42.14	6.30	48.43				
2%	44.6	0.25%	0.50%	1.83	49.0	0.949	0.886	13.44	0.893	2.39	89.4	24.53	4.36	28.89				
3%	37.5	0.50%	1.00%	3.65	41.0	0.795	0.600	7.63	0.602	1.61	149.7	27.85	5.88	33.73				
4%	32.1	0.50%	1.00%	3.65	34.8	0.674	0.424	4.57	0.415	1.11	126.9	16.68	4.06	20.74				
5%	28.5	0.50%	1.00%	3.65	30.3	0.587	0.322	3.02	0.304	0.81	110.6	11.04	2.97	14.01				
10%	17.9	2.50%	5.00%	18.25	23.2	0.450	0.200	1.44	0.165	0.44	423.9	26.27	8.05	34.32				
20%	9.8	5.00%	10.00%	36.50	13.9	0.269	0.103	0.44	0.045	0.12	505.7	16.12	4.44	20.56				
30%	6.5	5.00%	10.00%	36.50	8.2	0.158	0.075	0.19	0.006	0.02	297.5	6.87	0.63	7.50				
40%	4.6	5.00%	10.00%	36.50	5.6	0.108	0.068	0.12	0.000	0.00	203.3	4.28	0.00	4.28				
50%	3.5	5.00%	10.00%	36.50	4.1	0.079	0.066	0.08	0.000	0.00	148.7	3.03	0.00	3.03				
60%	2.7	5.00%	10.00%	36.50	3.1	0.061	0.065	0.06	0.000	0.00	114.0	2.29	0.00	2.29				
70%	2.2	5.00%	10.00%	36.50	2.4	0.047	0.064	0.05	0.000	0.00	89.2	1.78	0.00	1.78				
80%	1.9	5.00%	10.00%	36.50	2.0	0.039	0.064	0.04	0.000	0.00	74.4	1.47	0.00	1.47				
90%	1.4	5.00%	10.00%	36.50	1.6	0.032	0.064	0.03	0.000	0.00	59.5	1.18	0.00	1.18				
100%	0.3	5.00%	10.00%	36.50	0.8	0.016	0.064	0.02	0.000	0.00	29.7	0.59	0.00	0.59				
<b>Annual Totals:</b>										2,842.7 (cfs)	562.9 (tons/yr)	68.9 (tons/yr)	631.8 (tons/yr)					
										5,638.6 (acre-ft)								

**Worksheet 19b.** Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Equation Type		Equation Source		Equation		Bankfull Discharge (cfs)		Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)			
1. Bedload Sediment		"Good/Fair" Pagosa		$Y = -0.0113 + 1.0139X^{2.1929}$		51.6		0.028095864		114.7625704			
2. Suspended Sediment		"Good/Fair" Pagosa		$Y = 0.06336 + 0.9326X^{2.4085}$									
From Dimensional Flow-Duration Curve													
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)		
Percentage of Time	Daily Mean Discharge (cfs)	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Suspended Sediment Discharge	Suspended Sediment Discharge	Dimensionless Bedload Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow [(5)×(6)]		
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>bed</sub> )	(S/S <sub>bed</sub> )	(tons/day)	(b <sub>g</sub> /b <sub>bed</sub> )	(tons/day)	(cfs)		
(15)	(14)	(13)	(12)	(11)	(10)	(9)	(8)	(7)	(6)	(5)	(4)		
Suspended Sediment + Bedload Sediment [(13)+(14)]	Bedload Sediment [(5)×(11)]	Suspended Sediment [(5)×(9)]	Time Adjusted Streamflow [(5)×(6)]	Bedload Sediment Discharge	Dimensionless Bedload Discharge	Suspended Sediment Discharge	Dimensionless Suspended Sediment Discharge	Mid-Ordinate Streamflow	Time Increment (percent)	Daily Mean Discharge (cfs)	Percentage of Time		
0%													
0.10%	131.2												
0.25%	112.6	0.05%	0.09%	0.34	121.9	2.363	7.461	281.87	6.670	17.85	41.8		
0.50%	97.5	0.08%	0.15%	0.55	105.1	2.036	5.232	170.30	4.809	12.87	57.5		
0.75%	84.2	0.13%	0.25%	0.91	90.8	1.761	3.706	104.32	3.494	9.35	82.9		
1%	71.9	0.13%	0.25%	0.91	78.1	1.513	2.592	62.69	2.502	6.70	71.2		
1.5%	62.2	0.13%	0.25%	0.91	67.1	1.300	1.817	37.76	1.790	4.79	61.2		
2%	53.4	0.25%	0.50%	1.83	57.8	1.120	1.289	23.09	1.289	3.45	105.5		
3%	44.6	0.25%	0.50%	1.83	49.0	0.949	0.886	13.44	0.893	2.39	89.4		
4%	37.5	0.50%	1.00%	3.65	41.0	0.795	0.600	7.63	0.602	1.61	149.7		
5%	32.1	0.50%	1.00%	3.65	34.8	0.674	0.424	4.57	0.415	1.11	126.9		
10%	28.5	0.50%	1.00%	3.65	30.3	0.587	0.322	3.02	0.304	0.81	110.6		
20%	17.9	2.50%	5.00%	18.25	23.2	0.450	0.200	1.44	0.165	0.44	423.9		
30%	9.8	5.00%	10.00%	36.50	13.9	0.269	0.103	0.44	0.045	0.12	505.7		
40%	6.5	5.00%	10.00%	36.50	8.2	0.158	0.075	0.19	0.006	0.02	297.5		
50%	4.6	5.00%	10.00%	36.50	5.6	0.108	0.068	0.12	0.000	0.00	203.3		
60%	3.5	5.00%	10.00%	36.50	4.1	0.079	0.066	0.08	0.000	0.00	148.7		
70%	2.7	5.00%	10.00%	36.50	3.1	0.061	0.065	0.06	0.000	0.00	114.0		
80%	2.2	5.00%	10.00%	36.50	2.4	0.047	0.064	0.05	0.000	0.00	89.2		
90%	1.9	5.00%	10.00%	36.50	2.0	0.039	0.064	0.04	0.000	0.00	74.4		
100%	1.4	5.00%	10.00%	36.50	1.6	0.032	0.064	0.03	0.000	0.00	59.5		
	0.3	5.00%	10.00%	36.50	0.8	0.016	0.064	0.02	0.000	0.00	29.7		
<b>Annual Totals:</b>											<b>2,842.7</b> (cfs)	<b>562.9</b> (tons/yr)	<b>631.8</b> (tons/yr)
											<b>5,638.6</b> (acre-ft)	<b>68.9</b> (tons/yr)	



## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>Trout Creek, C4 Reference Reach</b>		Stream Type: <b>C4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>D. Rosgen et al., XS DR_Riffle 1</b>		Date: <b>8/13/2010</b>			
<b>Enter Required Information for Existing Condition</b>					
9.7	$D_{50}$	Riffle bed material $D_{50}$ (mm)			
7.7	$D_{50}^{\wedge}$	Bar sample $D_{50}$ (mm)			
0.24	$D_{max}$	Largest particle from bar sample (ft)	74	(mm)	304.8 mm/ft
0.0044	S	Existing bankfull water surface slope (ft/ft)			
1.19	d	Existing bankfull mean depth (ft)			
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment			
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>					
1.25	$D_{50}/D_{50}^{\wedge}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 ( D_{50}/D_{50}^{\wedge} )^{-0.872}$		
7.62	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 ( D_{max}/D_{50} )^{-0.887}$		
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED:		
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	d	Required bankfull mean depth (ft)	$d = \frac{\tau^* (\gamma_s - 1) D_{max}}{S}$ (use $D_{max}$ in ft)		
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	S	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^* (\gamma_s - 1) D_{max}}{d}$ (use $D_{max}$ in ft)		
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					
<b>Sediment Competence Using Dimensional Shear Stress</b>					
0.327	Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d) $\gamma = 62.4$ , d = existing depth, S = existing slope				
Shields 24	CO 70	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ (Figure 5-49)			
Shields 1	CO 0.35	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) (Figure 5-49)			
Shields 3.64	CO 1.27	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm)		$d = \frac{\tau}{\gamma S}$	
Shields 0.0135	CO 0.0047	Predicted slope required to initiate movement of measured $D_{max}$ (mm)		$S = \frac{\tau}{\gamma d}$	
Check: <input checked="" type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					

## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>Trout Creek, C4 Reference</b>	Stream Type: <b>C4</b>
Location: <b>Pike National Forest, CO</b>	Valley Type: <b>VIII</b>
Observers: <b>D. Rosgen et al.</b>	Date: <b>8/13/2010</b>
<b>Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)</b>	<b>Stability Rating (Check Appropriate Rating)</b>
<b>Stream Type at potential, (C→E), (F<sub>b</sub>→B), (G→B), (F→B<sub>c</sub>), (F→C), (D→C)</b>	<input checked="" type="checkbox"/> Stable
(E→C), (C→High W/d C)	<input type="checkbox"/> Moderately Unstable
(G→F), (F→D), (C→F)	<input type="checkbox"/> Unstable
(C→D), (B→G), (D→G), (C→G), (E→G)	<input type="checkbox"/> Highly Unstable

Worksheet 5-25. Lateral stability.

Stream: <b>Trout Creek, C4 Reference Reach</b>		Stream Type: <b>C4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>D. Rosgen et al.</b>		Date: <b>8/13/2010</b>			
Lateral stability criteria (choose one stability category for each criterion 1–5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	2
	1.0 (2)	(4)	(6)	(8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	1
	B1, B2 (1)	(2)	(3)	(4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		1
	M1, M3 (1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	2
	L/M (2)	(4)	(6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	1
	1.0 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>7</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input checked="" type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input type="checkbox"/>	<i>Unstable</i> 13 – 21 <input type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	

**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>Trout Creek, C4 Reference Reach</b>		Stream Type: <b>C4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>D. Rosgen et al.</b>		Date: <b>8/13/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	No Deposition	Moderate Deposition	Excess Deposition	Aggradation	
1 <b>Sediment competence (Worksheet 5-22)</b>	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope-slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	2
	(2)	(4)	(6)	(8)	
2 <b>Sediment Capacity (POWERSED) (Worksheet 5-20)</b>	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	2
	Ref. Reach (2)	(4)	(6)	(8)	
3 <b>W/d Ratio State (Worksheet 5-13)</b>	1.0 – 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	1
	1.0 (1)	(4)	(6)	(8)	
4 <b>Stream Succession States (Worksheet 5-24)</b>	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	2
	at potential (2)	(4)	(6)	(8)	
5 <b>Depositional Patterns (Worksheet 5-10)</b>	B1	B2, B4	B3, B5	B6, B7, B8	2
	(1)	B1, B2 (2)	(3)	(4)	
6 <b>Debris / Blockages (Worksheet 5-11)</b>	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	1
	D1 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>10</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
Vertical Stability for Excess Deposition / Aggradation (use total points and check stability rating)	No Deposition 10 – 14 <input checked="" type="checkbox"/>	Moderate Deposition 15 – 20 <input type="checkbox"/>	Excess Deposition 21 – 30 <input type="checkbox"/>	Aggradation > 30 <input type="checkbox"/>	

Worksheet 5-27. Vertical stability – degradation.

Stream: <b>Trout Creek, C4 Reference Reach</b>		Stream Type: <b>C4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>D. Rosgen et al.</b>		Date: <b>8/13/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>1 Sediment Competence (Worksheet 5-22)</b>	Does not indicate excess competence	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed	$D_{100}$ of bed moved	Particles much larger than $D_{100}$ of bed moved	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>2 Sediment Capacity (POWERSED) (Worksheet 5-20)</b>	Does not indicate excess capacity	Slight excess energy: up to 10% increase above reference	Excess energy sufficient to increase load up to 50% of annual load	Excess energy transporting more than 50% of annual load	<b>2</b>
	Ref. Reach (2)	(4)	(6)	(8)	
<b>3 Degree of Channel Incision (BHR) (Worksheet 5-12)</b>	1.00 – 1.10	1.11 – 1.30	1.31 – 1.50	> 1.50	<b>2</b>
	1.00 (2)	(4)	(6)	(8)	
<b>4 Stream Succession States (Worksheets 5-12 and 5-24)</b>	Does not indicate incision or degradation	If BHR > 1.1 and stream type has W/d between 5–10	If BHR > 1.1 and stream type has W/d less than 5	(B→G), (C→G), (E→G), (D→G)	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>5 Confinement (MWR / MWR<sub>ref</sub>) (Worksheet 5-14)</b>	0.80 – 1.00	0.30 – 0.79	0.10 – 0.29	< 0.10	<b>1</b>
	1.00 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>9</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation (use total points and check stability rating)</b>	<i>Not Incised</i> 9 – 11 <input checked="" type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input type="checkbox"/>	<i>Degradation</i> > 27 <input type="checkbox"/>	

Worksheet 5-28. Channel enlargement.

Stream: <b>Trout Creek, C4 Reference Reach</b>		Stream Type: <b>C4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>			
Observers: <b>D. Rosgen et al.</b>		Date: <b>8/13/2010</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1-4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	2
	at potential (2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	2
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	2
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	2
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>8</b>
<b>Category Point Range</b>					
<b>Channel Enlargement Prediction (use total points and check stability rating)</b>	<i>No Increase</i> 8 – 10 <input checked="" type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input type="checkbox"/>	<i>Extensive</i> > 24 <input type="checkbox"/>	

Worksheet 5-29. Overall sediment supply.

Stream: <b>Trout Creek, C4 Reference Reach</b>		Stream Type: <b>C4</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>VIII</b>		
Observers: <b>D. Rosgen et al.</b>		Date: <b>8/13/2010</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1–5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	1	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	1	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	1	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	1	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	1	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>5</b>	
<b>Category Point Range</b>				
Overall Sediment Supply Rating (use total points and check stability rating)	<b>Low</b> 5 <input checked="" type="checkbox"/>	<b>Moderate</b> 6 – 10 <input type="checkbox"/>	<b>High</b> 11 – 15 <input type="checkbox"/>	<b>Very High</b> 16 – 20 <input type="checkbox"/>

Worksheet 5-32. Summary of stability condition categories.

Stream:	Trout Creek, C4 Reference Reach										Location: Pike National Forest, Colorado																						
Observers:	D. Rosgen et al.										Date: 8/14/2010		Stream Type: C4		Valley Type: VIII																		
Channel Dimension (Rifle XS 0+67)	Mean Bankfull Depth (ft):	0.89	Bankfull Width (ft):	19.37	Cross-Sectional Area (ft <sup>2</sup> ):	17.32	Width of Flood-Prone Area (ft):	41.92	Entrenchment Ratio:	2.16	Channel Pattern	Mean Range:	4.67	λ/W <sub>bkf</sub> :	3.43-6.33	L <sub>m</sub> /W <sub>bkf</sub> :	5.79	R <sub>c</sub> /W <sub>bkf</sub> :	1.72	MWR:	3.66	Sinuosity:	1.38										
River Profile & Bed Features	Check:	<input checked="" type="checkbox"/> Riffle/Pool	<input type="checkbox"/> Step/Pool	<input type="checkbox"/> Plane Bed	<input type="checkbox"/> Convergence/Divergence	<input type="checkbox"/> Dunes/Antidunes/Smooth Bed	Max Bankfull Depth (ft):	1.6	Depth Ratio (max to mean):	1.53	Pool Spacing:	3	Pool-to-Pool Ratio	3	Valley:	0.0061	Water Surface:	0.0044	Riparian	Current Composition/Density:	Potential Composition/Density:	Remarks:	Condition, Vigor & Usage of Existing Reach:										
Level III Stream Stability Indices	Vegetation	Willow, Redtop, Carex/ Juncus	Same but without invasives	Recovering C4 inside of an F4 Stream Type	Flow Regime:	P1, P2, P8 & Order:	S-4(4)	Meander Patterns:	M1, M3	Debris/Channel Blockages:	B1, B2	Degree of Incision (Bank-Height Ratio):	1.0	Degree of Incision Stability Rating:	No Incision	Modified Pfankuch Stability Rating (Numeric & Adjective Rating):	73 (Good)	Width/depth Ratio (W/d):	13.7	Reference W/d Ratio (W/d <sub>ref</sub> ):	13.7	W/d Ratio State Stability Rating:	1.0	Stable									
Bank Erosion Summary	Meander Width Ratio (MWR):	4.5	Reference MWR <sub>ref</sub> :	4.5	Degree of confinement (MWR / MWR <sub>ref</sub> ):	1.0	Length of Reach Studied (ft):	463	Annual Streambank Erosion Rate: (tons/yr)	2.94	Curve Used:	Colorado	Remarks:	Unconfined	MWR / MWR <sub>ref</sub> Stability Rating:	1.0	Stable	MWR / MWR <sub>ref</sub> Stability Rating:	1.0	Unconfined	MWR / MWR <sub>ref</sub> Stability Rating:	1.0	Stable										
Sediment Capacity (POWERSED)	Sufficient Capacity	<input type="checkbox"/>	Insufficient Capacity	<input type="checkbox"/>	Excess Capacity	<input type="checkbox"/>	Remarks:	Reference Reach	Largest Particle from Bar Sample (mm):	74	τ =	0.327	τ* =	N/A	Existing Depth:	1.19	Required Depth:	1.27	Existing Slope:	1.27	Required Slope:	0.0044	Potential Stream State (Type):	C4									
Entrainment/Competence	C →	D →	G →	F →	C →	Remarks/causes:	Reference Reach	Successional Stage Shift	C →	D →	G →	F →	C →	Remarks/causes:	Reference Reach	Lateral Stability	Stable	Mod. Unstable	<input type="checkbox"/>	Unstable	Highly Unstable	Remarks/causes:	Reference Reach										
Vertical Stability (Aggradation)	Vertical Stability (Aggradation)	<input checked="" type="checkbox"/>	No Deposition	<input type="checkbox"/>	Mod. Deposition	<input type="checkbox"/>	Ex. Deposition	<input type="checkbox"/>	Aggradation	Remarks/causes:	Reference Reach	Vertical Stability (Degradation)	<input checked="" type="checkbox"/>	Not Incised	<input type="checkbox"/>	Slightly Incised	<input type="checkbox"/>	Mod. Incised	<input type="checkbox"/>	Degradation	Remarks/causes:	Reference Reach	Channel Enlargement	<input checked="" type="checkbox"/>	No Increase	<input type="checkbox"/>	Slight Increase	<input type="checkbox"/>	Mod. Increase	<input type="checkbox"/>	Extensive	Remarks/causes:	Reference Reach
Sediment Supply (Channel Source)	Sediment Supply (Channel Source)	<input checked="" type="checkbox"/>	Low	<input type="checkbox"/>	Moderate	<input type="checkbox"/>	High	<input type="checkbox"/>	Very High	Remarks/causes:	Reference Reach	Channel Enlargement	<input checked="" type="checkbox"/>	Low	<input type="checkbox"/>	Moderate	<input type="checkbox"/>	High	<input type="checkbox"/>	Very High	Remarks/causes:	Reference Reach	Channel Enlargement	<input checked="" type="checkbox"/>	Low	<input type="checkbox"/>	Moderate	<input type="checkbox"/>	High	<input type="checkbox"/>	Very High	Remarks/causes:	Reference Reach



## *Appendix C21*

# **D4a Stream Type**

## *Reference Reach*



# Table of Contents

## *Appendix C21: D4a Reference Reach*

<b>Reach Location &amp; Overview.....</b>	<b>C21-2</b>
<b>Survey Summary.....</b>	<b>C21-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C21-8</b>
<b><i>Velocity, Classification &amp; Morphological Relations.....</i></b>	<b>C21-8</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b><i>Stability Indices.....</i></b>	<b>C21-12</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b><i>FLOWSED Model – Total Annual Sediment Yield.....</i></b>	<b>C21-22</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b><i>Sediment Competence/Entrainment.....</i></b>	<b>C21-24</b>
Worksheet 5-22. Sediment competence calculations.	
<b><i>Channel Stability Ratings.....</i></b>	<b>C21-25</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b><i>Summary.....</i></b>	<b>C21-31</b>
Worksheet 5-32. Summary of stability condition categories.	

## D4a Reference Reach Location & Overview

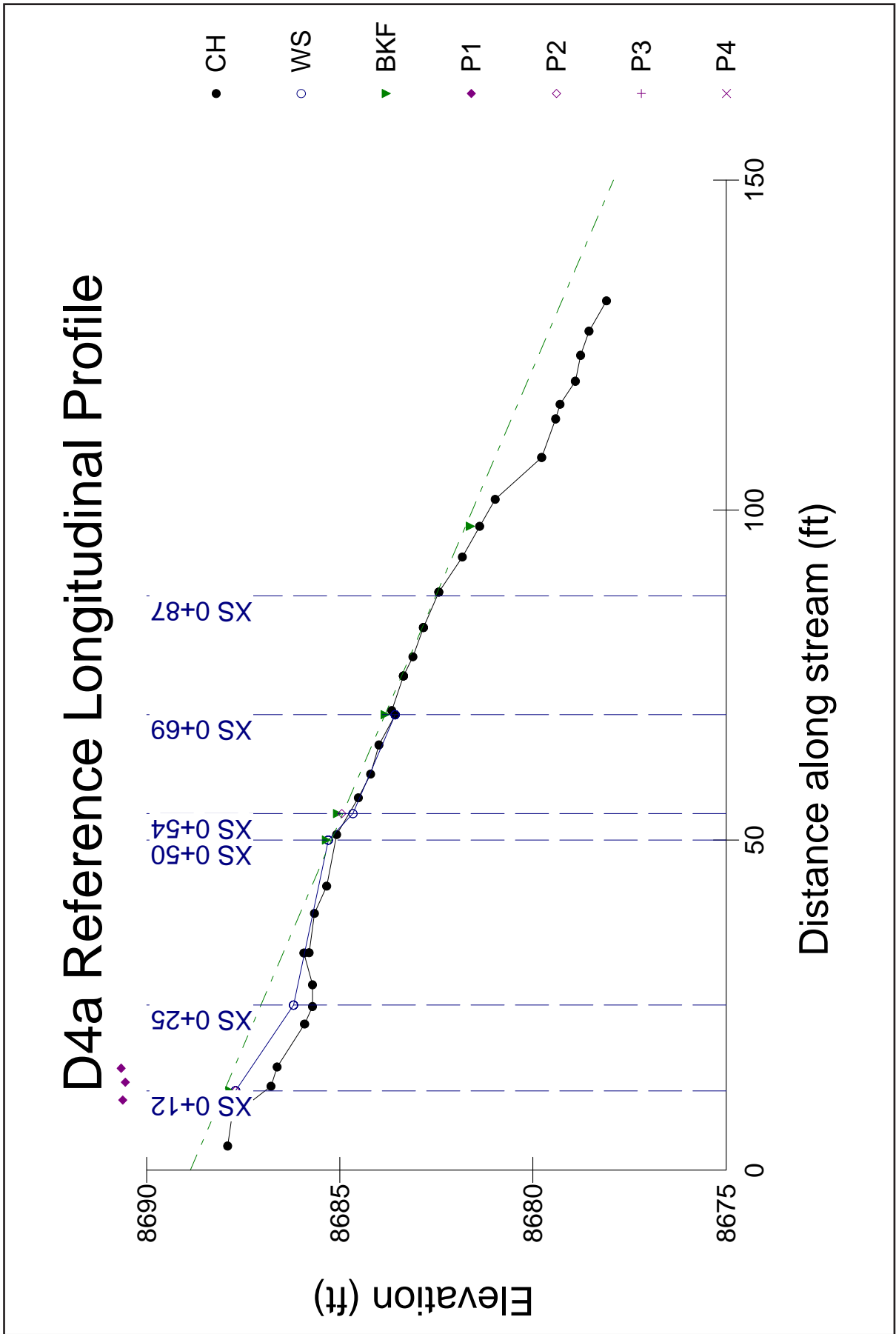
The D4a reference reach is in a Valley Type IIIa located in Northfield Gulch. This 3<sup>rd</sup> order channel is braided with large amounts of sediment depositing from upstream. The channel bed and banks show sediment deposition from upstream with riparian vegetation encouraging further deposition. Bed features are a result of a convergence/divergence process of local bed scour and sediment deposition. The channel is ephemeral and streamflow is seasonal by snowmelt and stormflow runoff. Flow is altered due to Waldo Canyon Fire.

Typical of D stream types, the channel is unconfined and has a high width/depth ratio. Excess deposition in this reach is expected especially with additional sediment being deposited due to the fire. The location of this reach is shown in **Figure C-1**, and the photograph depicts the typical characteristics of this stream type. Stream types are mapped where they occur by sub-watershed as shown in **Appendix D**.

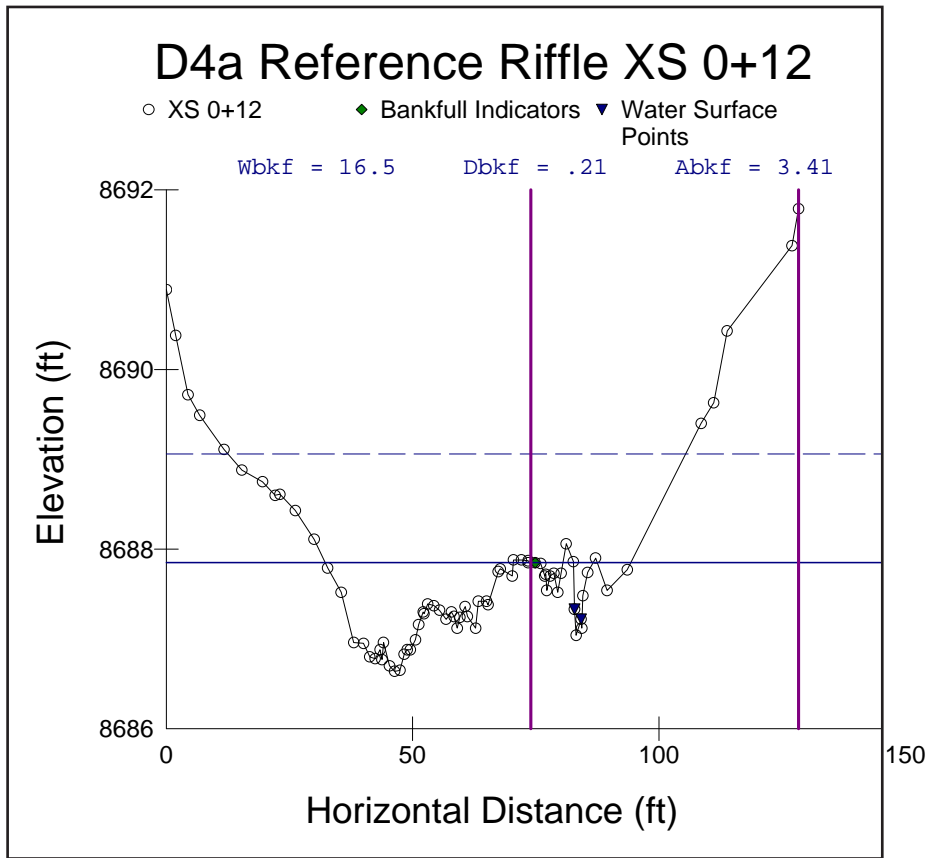
The details of the dimension, pattern, profile and materials are summarized. The following summary worksheets provide details of the morphology, hydraulics, stability, and streambank erosion rates for this reference reach. In the situation where impaired A4 and F4b stream types are located on active alluvial fans, an alternative for mitigation and sediment reduction is to use the data from the stable form to extrapolate for potential implementation of natural channel design.



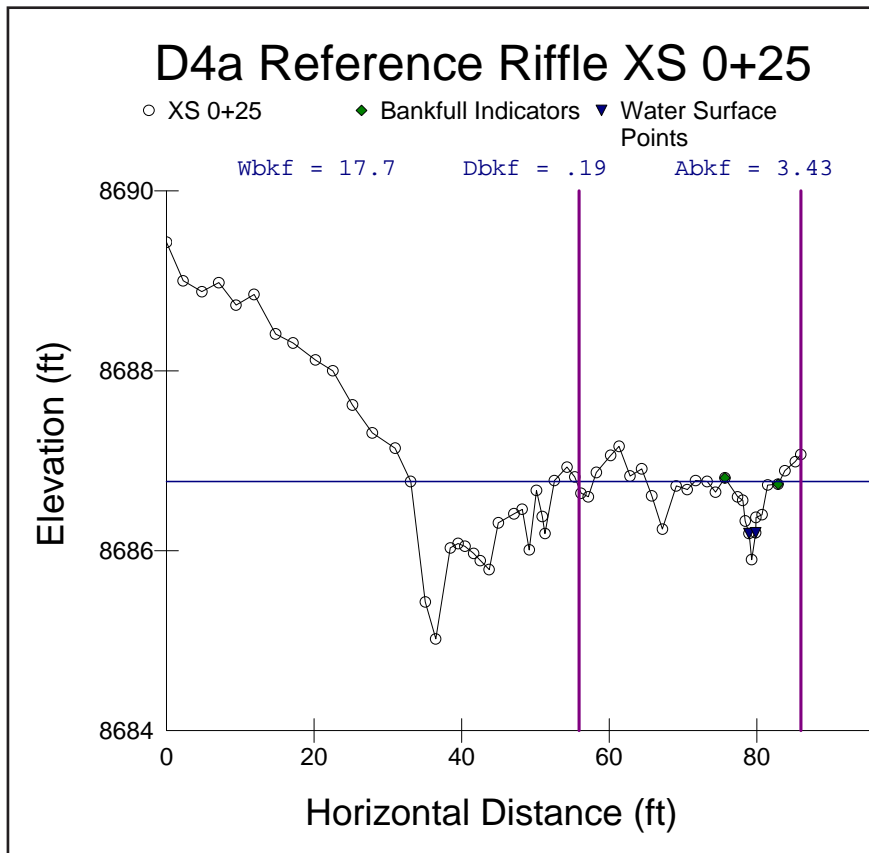
Survey Summary



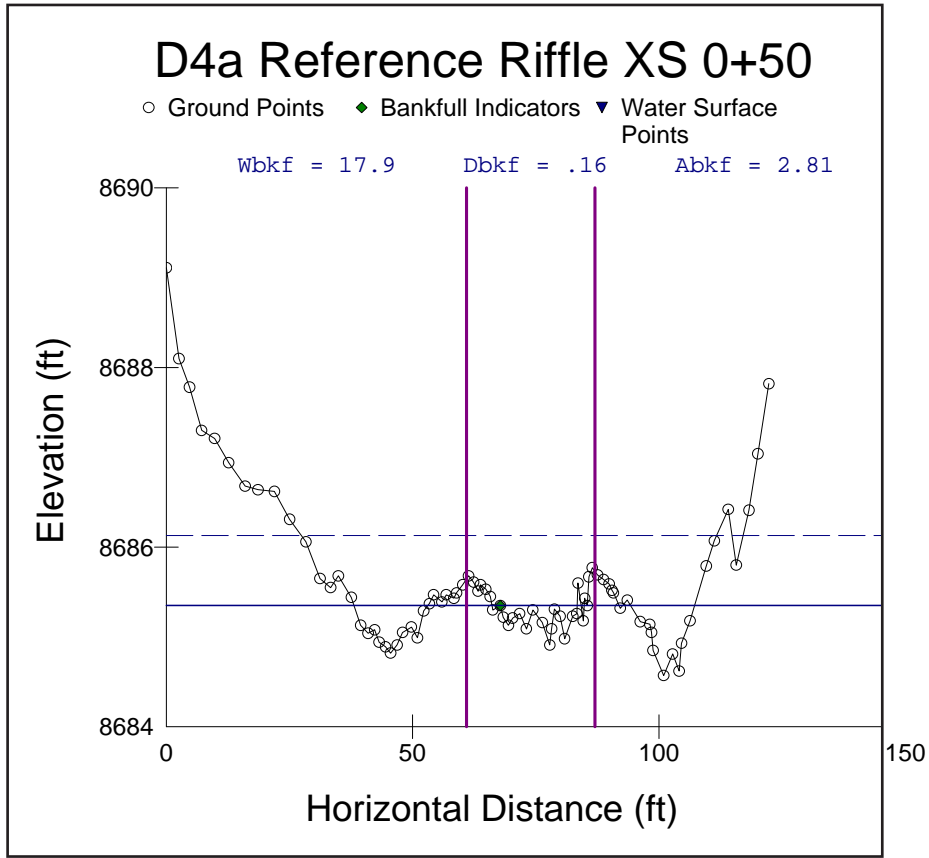
Longitudinal Profile (graph generated from RIVERMorph™)



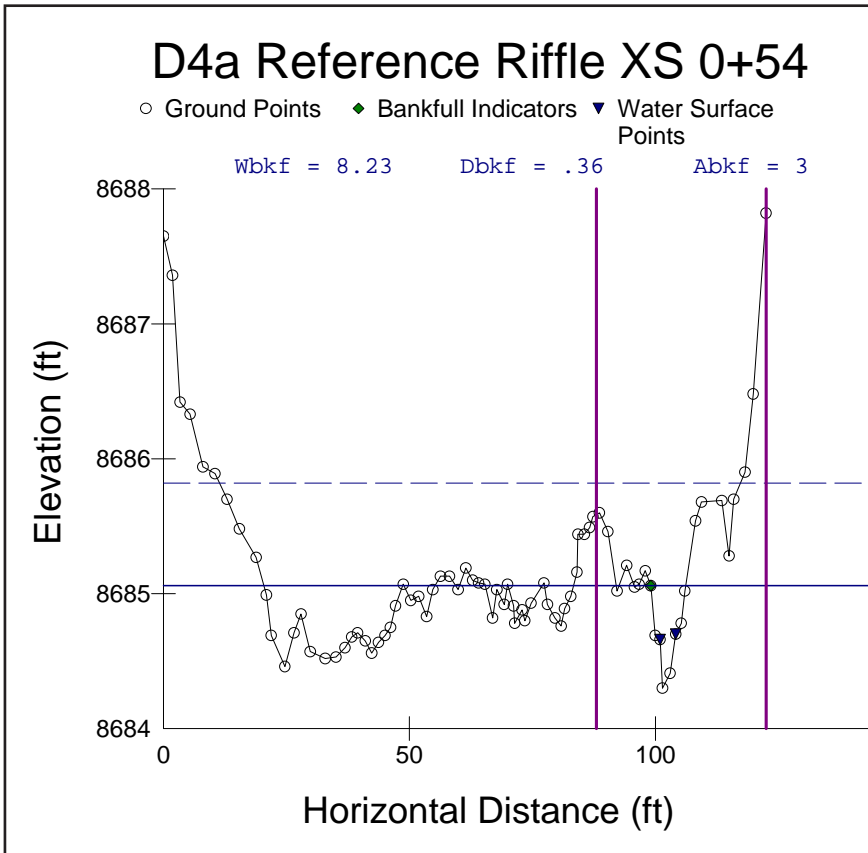
**Representative Cross-section 0+12** (graph generated from RIVERMorph™)



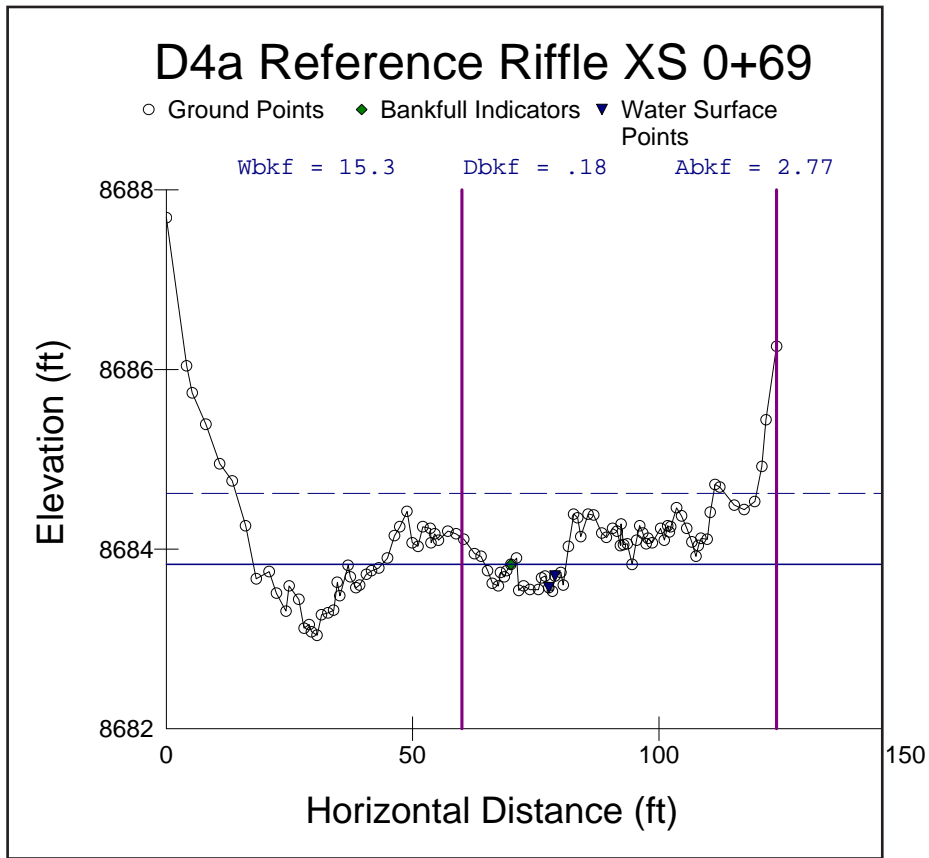
**Cross-section 0+25** (graph generated from RIVERMorph™)



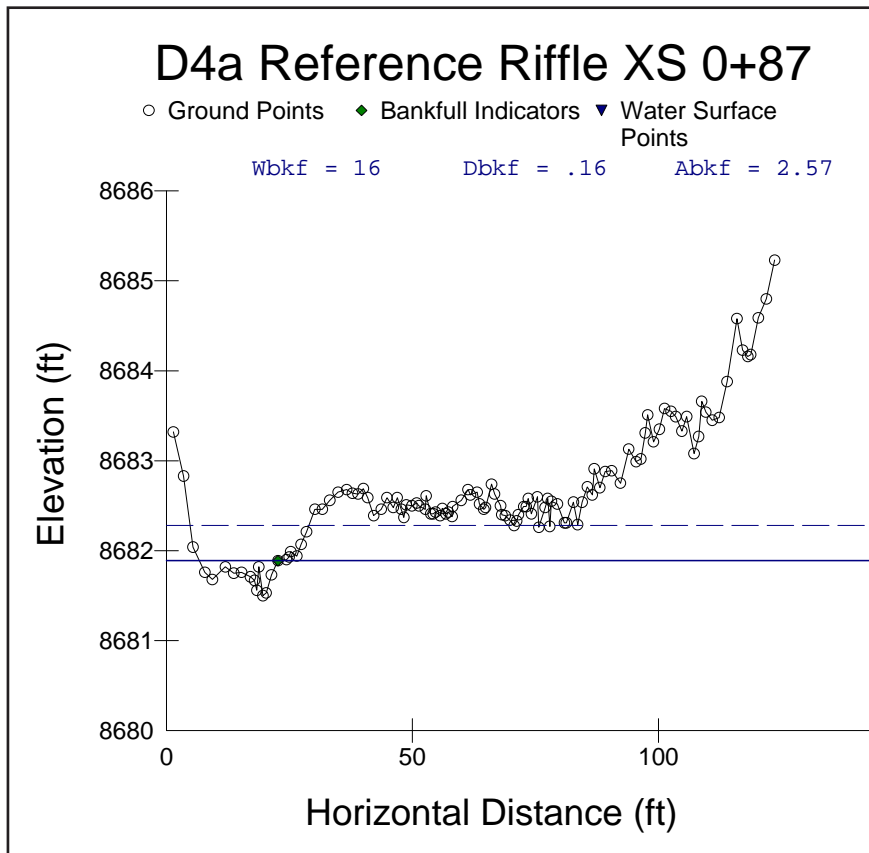
Cross-section 0+50 (graph generated from RIVERMorph™)



Cross-section 0+54 (graph generated from RIVERMorph™)

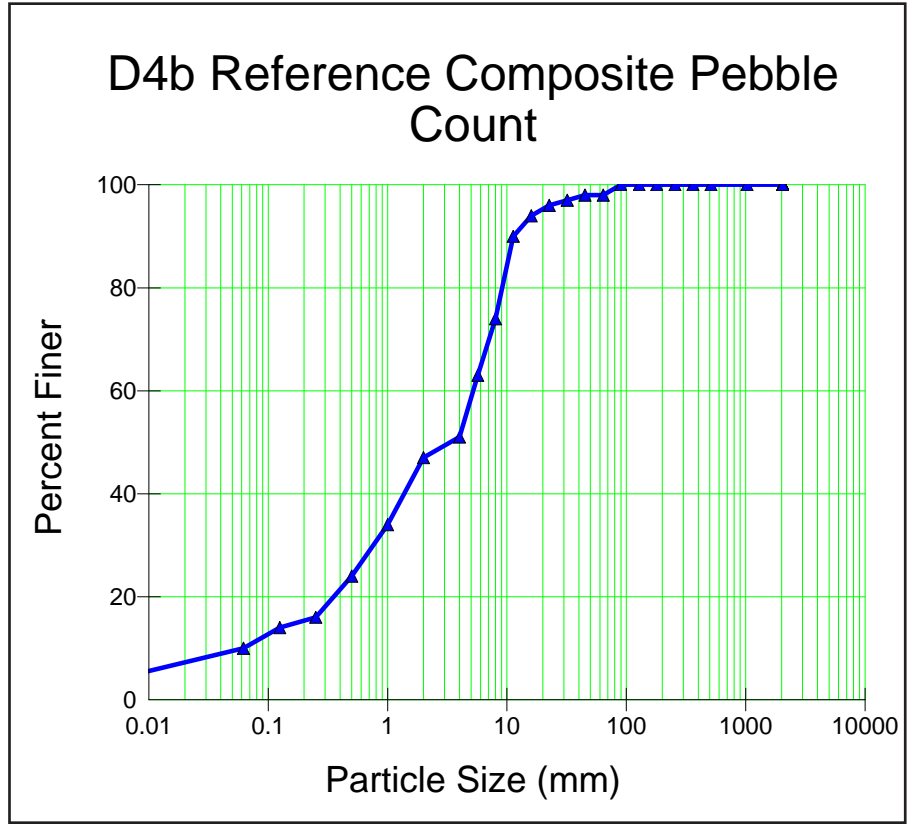


Cross-section 0+69 (graph generated from RIVERMorph™)

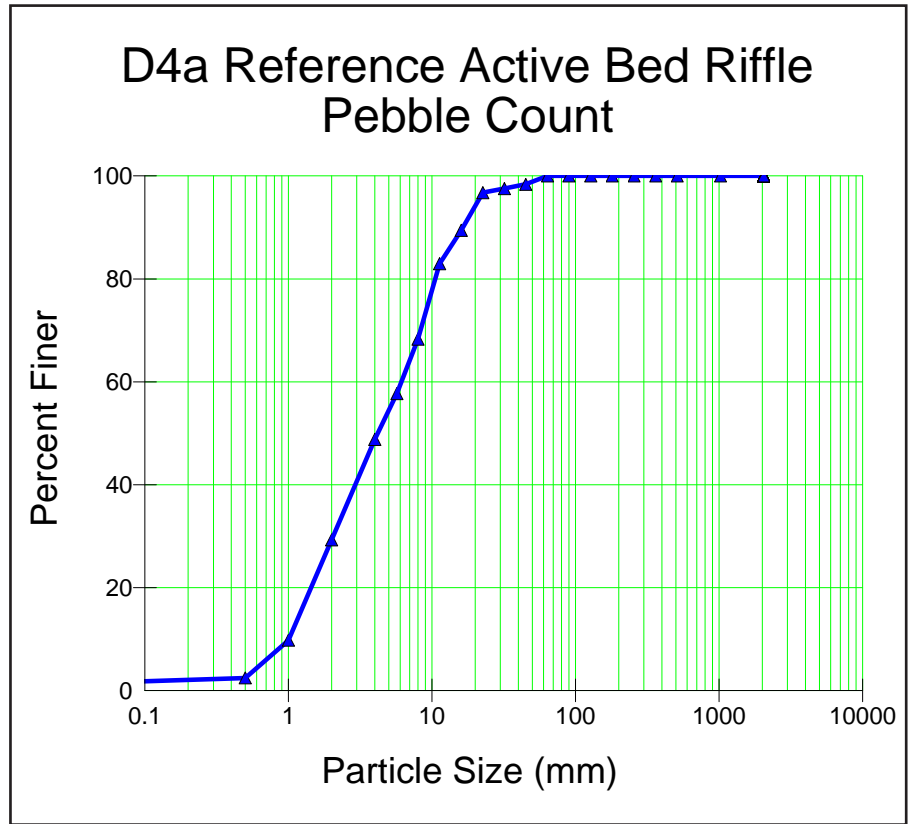


Cross-section 0+87 (graph generated from RIVERMorph™)





Composite Pebble Count (graph generated from RIVERMorph™)



Active Bed Pebble Count (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates						
Stream:	Northfield Gulch D4a Reference			Location:	Pike National Forest, Colorado	
Date:	11/8/2012	Stream Type:	D4a	Valley Type:	IIla	
Observers:	Bones, Kyle, David, Luke, Kim			HUC:	___ ___ ___ ___ ___ ___ ___ ___ ___	
INPUT VARIABLES			OUTPUT VARIABLES			
Bankfull Riffle Cross-Sectional AREA	2.81	$A_{b\text{bkf}}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.16	$d_{b\text{bkf}}$ (ft)	
Bankfull Riffle WIDTH	17.9	$W_{b\text{bkf}}$ (ft)	Wetted PERIMETER $\sim (2 * d_{b\text{bkf}}) + W_{b\text{bkf}}$	18.24	$W_p$ (ft)	
$D_{84}$ at Riffle	12.1	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.04	$D_{84}$ (ft)	
Bankfull SLOPE	0.07	$S_{b\text{bkf}}$ (ft / ft)	Hydraulic RADIUS $A_{b\text{bkf}} / W_p$	0.15	R (ft)	
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R(ft) / $D_{84}$ (ft)	3.89	R / $D_{84}$	
Drainage Area	0.42	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.601	$u^*$ (ft/sec)	
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE	
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$			3.70	ft / sec	10.40	cfs
2. Roughness Coefficient: a) Manning's n from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n =$ <b>0.064</b>			1.80	ft / sec	5.06	cfs
2. Roughness Coefficient: b) Manning's n from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n =$ <b>0.064</b>			1.80	ft / sec	5.06	cfs
2. Roughness Coefficient: c) Manning's n from Jarrett (USGS): Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for Stream Types A1, A2, A3, B1, B2, B3, C2 & E3 $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ $n =$ <b>0.194</b>			0.59	ft / sec	1.67	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Darcy-Weisbach (Leopold, Wolman and Miller)			3.86	ft / sec	10.8	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)				ft / sec		cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q =$ <input type="text"/> year $u = Q / A$				ft / sec		cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$				ft / sec		cfs
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation (R/ $D_{84}$ ) – Estimation Method 1						
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.						
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.						
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.						
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.						

**Worksheet 5-3.** Level II stream classification.

<b>Stream: Northfield Gulch, D4a Reference</b>	
<b>Basin:</b>	<b>Drainage Area: 272 acres      0.42 mi<sup>2</sup></b>
<b>Location: Pike National Forest, Colorado</b>	
<b>Twp.&amp;Rge:</b>	<b>Sec.&amp;Qtr.:</b>
<b>Cross-Section Monuments (Lat./Long.): XS 0+12</b>	<b>Date: 11/08/2012</b>
<b>Observers: Bones, Kyle, David, Luke, Kim</b>	<b>Valley Type: IIIa</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>17.92</b> ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A_{bkf} / W_{bkf}$ ).	<b>0.16</b> ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>2.81</b> ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>112</b> ft/ft
<b>Maximum DEPTH (<math>d_{max}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>0.78</b> ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>86.58</b> ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>4.83</b> ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the median or dominant diameter of channel materials, as sampled proportionately from the channel surface, between the bankfull stage and Thalweg elevations.	<b>3.5</b> mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.07277</b> ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope ( $S_{val} / S$ ).	<b>1</b>

<b>Stream Type</b>	<div style="border: 1px solid black; padding: 5px; display: inline-block;"><b>D4a</b></div>	<b>See Classification Key (Figure 2-14)</b>
--------------------	---	---

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Northfield Gulch D4a Reference</b>				Location: <b>Pike National Forest, Colorado</b>							
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Date: <b>11/08/12</b>		Valley Type: <b>IIIa</b>		Stream Type: <b>D4a</b>					
<b>River Reach Dimension Summary Data.....1</b>											
<b>Riffle Dimensions*</b> , **, ***	<b>Riffle Dimensions*</b> , **, ***			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Width ( $W_{bkt}$ )	<b>17.5</b>	<b>16.5</b>	<b>18.0</b>	ft	Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	<b>3.2</b>	<b>2.8</b>	<b>3.4</b>		
	Mean Riffle Depth ( $d_{bkt}$ )	<b>0.19</b>	<b>0.16</b>	<b>0.21</b>	ft	Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	<b>95.1</b>	<b>78.5</b>	<b>112.0</b>		
	Maximum Riffle Depth ( $d_{max}$ )	<b>1.25</b>	<b>0.78</b>	<b>1.75</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>6.579</b>	<b>4.105</b>	<b>9.211</b>		
	Width of Flood-Prone Area ( $W_{fpa}$ )	<b>83.8</b>	<b>71.9</b>	<b>92.9</b>	ft	Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )					
	Riffle Inner Berm Width ( $W_{ib}$ )				ft	Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )					
	Riffle Inner Berm Depth ( $d_{ib}$ )				ft	Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )					
	Riffle Inner Berm Area ( $A_{ib}$ )				ft <sup>2</sup>	Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )					
	Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )										
<b>Pool Dimensions*</b> , **, ***	<b>Pool Dimensions*</b> , **, ***			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Pool Dimensions &amp; Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Pool Width ( $W_{bkfp}$ )				ft	Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )					
	Mean Pool Depth ( $d_{bkfp}$ )				ft	Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )					
	Pool Cross-Sectional Area ( $A_{bkfp}$ )				ft	Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )					
	Maximum Pool Depth ( $d_{maxp}$ )				ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )					
	Pool Inner Berm Width ( $W_{ibp}$ )				ft	Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )					
	Pool Inner Berm Depth ( $d_{ibp}$ )				ft	Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )					
	Pool Inner Berm Area ( $A_{ibp}$ )				ft <sup>2</sup>	Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )					
	Point Bar Slope ( $S_{pb}$ )				ft/ft	Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )					
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Run Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Run Width ( $W_{bkfr}$ )				ft	Run Width to Riffle Width ( $W_{bkfr} / W_{bkt}$ )					
	Mean Run Depth ( $d_{bkfr}$ )				ft	Mean Run Depth to Mean Riffle Depth ( $d_{bkfr} / d_{bkt}$ )					
	Run Cross-Sectional Area ( $A_{bkfr}$ )				ft	Run Area to Riffle Area ( $A_{bkfr} / A_{bkt}$ )					
	Maximum Run Depth ( $d_{maxr}$ )				ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )					
	Run Width/Depth Ratio ( $W_{bkfr} / d_{bkfr}$ )				ft						
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Glide Dimensions &amp; Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Glide Width ( $W_{bkfg}$ )				ft	Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )					
	Mean Glide Depth ( $d_{bkfg}$ )				ft	Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )					
	Glide Cross-Sectional Area ( $A_{bkfg}$ )				ft	Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )					
	Maximum Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )					
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )				ft/ft	Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )					
	Glide Inner Berm Width ( $W_{ibg}$ )				ft	Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )					
	Glide Inner Berm Depth ( $d_{ibg}$ )				ft	Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )					
Glide Inner Berm Area ( $A_{ibg}$ )				ft <sup>2</sup>	Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )						
<b>Step**</b>	<b>Step Dimensions**</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Step Dimensionless Ratios****</b>		<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Step Width ( $W_{bkfs}$ )				ft	Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )					
	Mean Step Depth ( $d_{bkfs}$ )				ft	Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )					
	Step Cross-Sectional Area ( $A_{bkfs}$ )				ft	Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )					
	Maximum Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )					
	Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )										

**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Northfield Gulch, D4a Reference</b>		Location: <b>Pike National Forest, Colorado</b>										
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Date: <b>11/8/2012</b>		Valley Type: <b>IIIa</b>		Stream Type: <b>D4a</b>						
<b>River Reach Summary Data.....2</b>												
<b>Hydraulics</b>	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )		<b>1.80</b> ft/sec		Estimation Method		<b>Roughness Coefficient</b>					
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )		<b>5.05</b> cfs		Drainage Area		<b>0.42</b> mi <sup>2</sup>					
<b>Channel Pattern</b>	<b>Geometry</b>			<b>Dimensionless Geometry Ratios</b>								
	Linear Wavelength ( $\lambda$ )			ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )							
	Stream Meander Length ( $L_m$ )			ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )							
	Radius of Curvature ( $R_c$ )			ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )							
	Belt Width ( $W_{bit}$ )	<b>60.0</b>		ft	Meander Width Ratio ( $W_{bit} / W_{bkt}$ )	<b>3.43</b>						
	Arc Length ( $L_a$ )			ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )							
	Riffle Length ( $L_r$ )			ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )							
	Individual Pool Length ( $L_p$ )			ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )							
Pool to Pool Spacing ( $P_s$ )			ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )								
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )		<b>0.0728</b> ft/ft		Average Water Surface Slope (S)		<b>0.0728</b> ft/ft		Sinuosity ( $S_{val} / S$ )		<b>1.00</b>	
	Stream Length (SL)		<b>128.0</b> ft		Valley Length (VL)		<b>128.0</b> ft		Sinuosity (SL / VL)		<b>1.00</b>	
	Low Bank Height (LBH)	start: <b>1.00</b> ft	end: <b>0.25</b> ft	Max Bankfull Depth ( $d_{max}$ )	start: <b>1.00</b> ft	end: <b>0.25</b> ft	Bank-Height Ratio (BHR) (LBH / $d_{max}$ )		start: <b>1.0</b>	end: <b>1.0</b>		
	<b>Facet Slopes</b>			<b>Dimensionless Facet Slope Ratios</b>								
	Riffle Slope ( $S_{rit}$ )			ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rit} / S$ )							
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )							
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )							
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )							
	Step Slope ( $S_s$ )			ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )							
	<b>Max Depths<sup>a</sup></b>			<b>Dimensionless Depth Ratios</b>								
	Max Riffle Depth ( $d_{max}$ )	<b>0.62</b>	<b>0.20</b>	<b>1.37</b> ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>3.263</b>	<b>1.053</b>	<b>7.211</b>				
	Max Run Depth ( $d_{maxr}$ )			ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )							
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )							
	Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )							
	Max Step Depth ( $d_{maxs}$ )			ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )							
<b>Channel Materials</b>			<b>Reach<sup>b</sup></b>		<b>Riffle<sup>c</sup></b>		<b>Bar</b>				<b>Protrusion Height<sup>d</sup></b>	
	% Silt/Clay		<b>10.00</b>	<b>0.00</b>	$D_{16}$	<b>0.25</b>	<b>1.32</b>					mm
	% Sand		<b>37.00</b>	<b>29.27</b>	$D_{35}$	<b>1.08</b>	<b>2.59</b>					mm
	% Gravel		<b>51.00</b>	<b>70.73</b>	$D_{50}$	<b>3.50</b>	<b>4.23</b>					mm
	% Cobble		<b>2.00</b>	<b>0.00</b>	$D_{84}$	<b>10.06</b>	<b>12.07</b>					mm
	% Boulder		<b>0.00</b>	<b>0.00</b>	$D_{95}$	<b>19.30</b>	<b>21.02</b>					mm
	% Bedrock		<b>0.00</b>	<b>0.00</b>	$D_{100}$	<b>90.00</b>	<b>64.00</b>					mm

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.  
<sup>b</sup> Composite sample of riffles and pools within the designated reach.      <sup>c</sup> Active bed of a riffle.      <sup>d</sup> Height of roughness feature above bed.

## Stability Indices


**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation					
Stream: <b>Northfield Gulch D4a Reference</b>		Location: <b>Pike National Forest, Colorado</b>			
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Reference reach <input checked="" type="checkbox"/>	Disturbed (impacted reach) <input type="checkbox"/>	Date: <b>11/08/2012</b>	
Existing species composition: <b>Mixed conifer, aspen, willow</b>		Potential species composition: <b>At potential</b>			
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition
<b>1. Overstory</b>	Canopy layer	<b>75%</b>	<b>20%</b>	<b>Aspen</b>	<b>60%</b>
				<b>Ponderosa</b>	<b>15%</b>
				<b>Limber Pine</b>	<b>5%</b>
				<b>Spruce</b>	<b>20%</b>
					<b>0%</b>
				<b>0%</b>	<b>100%</b>
<b>2. Understory</b>	Shrub layer		<b>25%</b>	<b>Willow</b>	<b>80%</b>
				<b>Potentilla</b>	<b>20%</b>
					<b>0%</b>
					<b>0%</b>
					<b>0%</b>
				<b>0%</b>	<b>100%</b>
<b>3. Ground level</b>	Herbaceous		<b>30%</b>	<b>Grass</b>	<b>80%</b>
				<b>Forbs</b>	<b>20%</b>
				<b>Leaf and needle litter</b>	<b>0%</b>
					<b>0%</b>
		<b>0%</b>			
Leaf or needle litter	5%	<b>Remarks:</b> Condition, vigor and/or usage of existing reach: <b>Vigorous</b>			<b>100%</b>
Bare ground	20%				
					<b>100%</b>
*Based on crown closure. **Based on basal area to surface area.		<b>Column Total = 100%</b>			

Worksheet 5-7. Flow regime.

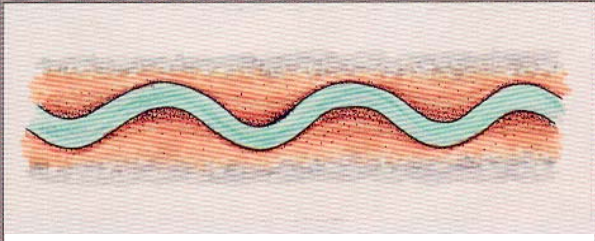
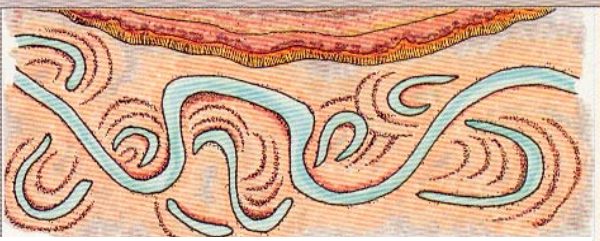

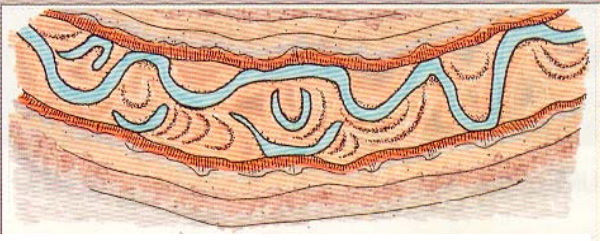


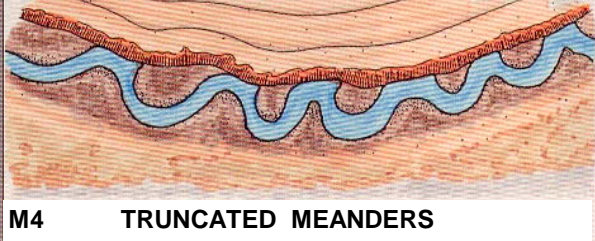
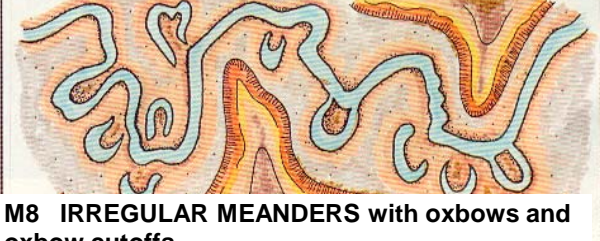
<b>FLOW REGIME</b>								
Stream: <b>Northfield Gulch A4a+ Poor</b>			Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>Bones, Kyle, David, Luke, Kim</b>						Date: <b>11/8/2012</b>		
List ALL COMBINATIONS that APPLY.....☞			E1	E2	E7	E8		
<b>General Category</b>								
E	Ephemeral stream channels: Flows only in response to precipitation							
S	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
I	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
P	Perennial stream channels: Surface water persists yearlong.							
<b>Specific Category</b>								
1	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
2	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
3	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
4	Streamflow regulated by glacial melt.							
5	Ice flows/ice torrents from ice dam breaches.							
6	Alternating flow/backwater due to tidal influence.							
7	Regulated streamflow due to diversions, dam release, dewatering, etc.							
8	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
9	Rain-on-snow generated runoff.							

**Worksheet 5-8.** Stream order & stream size.

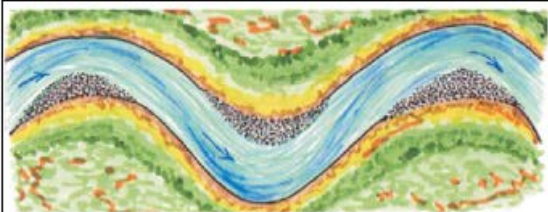

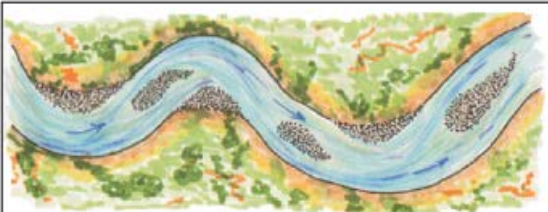
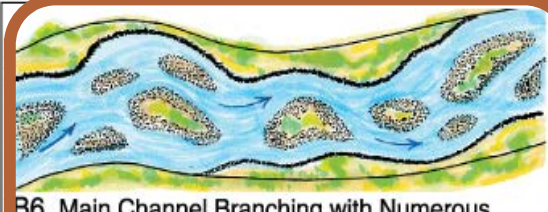
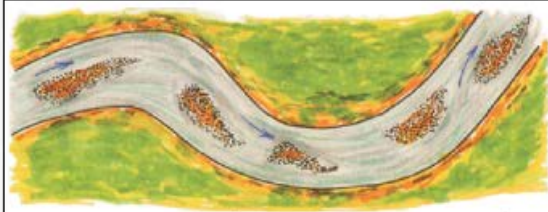
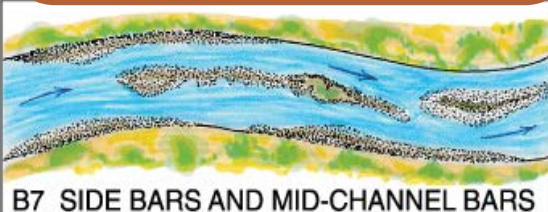


Stream Size and Order			
Stream:	Northfield Gulch D4a Reference		
Location:	Pike National Forest, Colorado		
Observers:	Bones, Kyle, David, Luke, Kim		
Date:	11/8/2012		
Stream Size Category and Order 			S-4(3)
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0.305	<1	<input type="checkbox"/>
S-2	0.3 – 1.5	1 – 5	<input type="checkbox"/>
S-3	1.5 – 4.6	5 – 15	<input type="checkbox"/>
S-4	4.6 – 9	15 – 30	<input checked="" type="checkbox"/>
S-5	9 – 15	30 – 50	<input type="checkbox"/>
S-6	15 – 22.8	50 – 75	<input type="checkbox"/>
S-7	22.8 – 30.5	75 – 100	<input type="checkbox"/>
S-8	30.5 – 46	100 – 150	<input type="checkbox"/>
S-9	46 – 76	150 – 250	<input type="checkbox"/>
S-10	76 – 107	250 – 350	<input type="checkbox"/>
S-11	107 – 150	350 – 500	<input type="checkbox"/>
S-12	150 – 305	500 – 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
Stream Order			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			



Worksheet 5-9. Meander patterns.

<b>Meander Patterns</b>					
Stream:	<b>Northfield Gulch, D4a Reference</b>	Location:	<b>Pike National Forest, CO</b>		
Observers:	<b>Bones, Kyle, David, Luke, Kim</b>	Date:	<b>11/8/2012</b>		
List ALL CATEGORIES that APPLY	<b>N/A</b>				
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>					
 <b>M1</b> <b>REGULAR MEANDERS</b>	 <b>M5</b> <b>UNCONFINED MEANDER SCROLLS</b>				
 <b>M2</b> <b>TORTUOUS MEANDERS</b>	 <b>M6</b> <b>CONFINED MEANDER SCROLLS</b>				
 <b>M3</b> <b>IRREGULAR MEANDERS</b>	 <b>M7</b> <b>DISTORTED MEANDER LOOPS</b>				
 <b>M4</b> <b>TRUNCATED MEANDERS</b>	 <b>M8</b> <b>IRREGULAR MEANDERS with oxbows and oxbow cutoffs</b>				

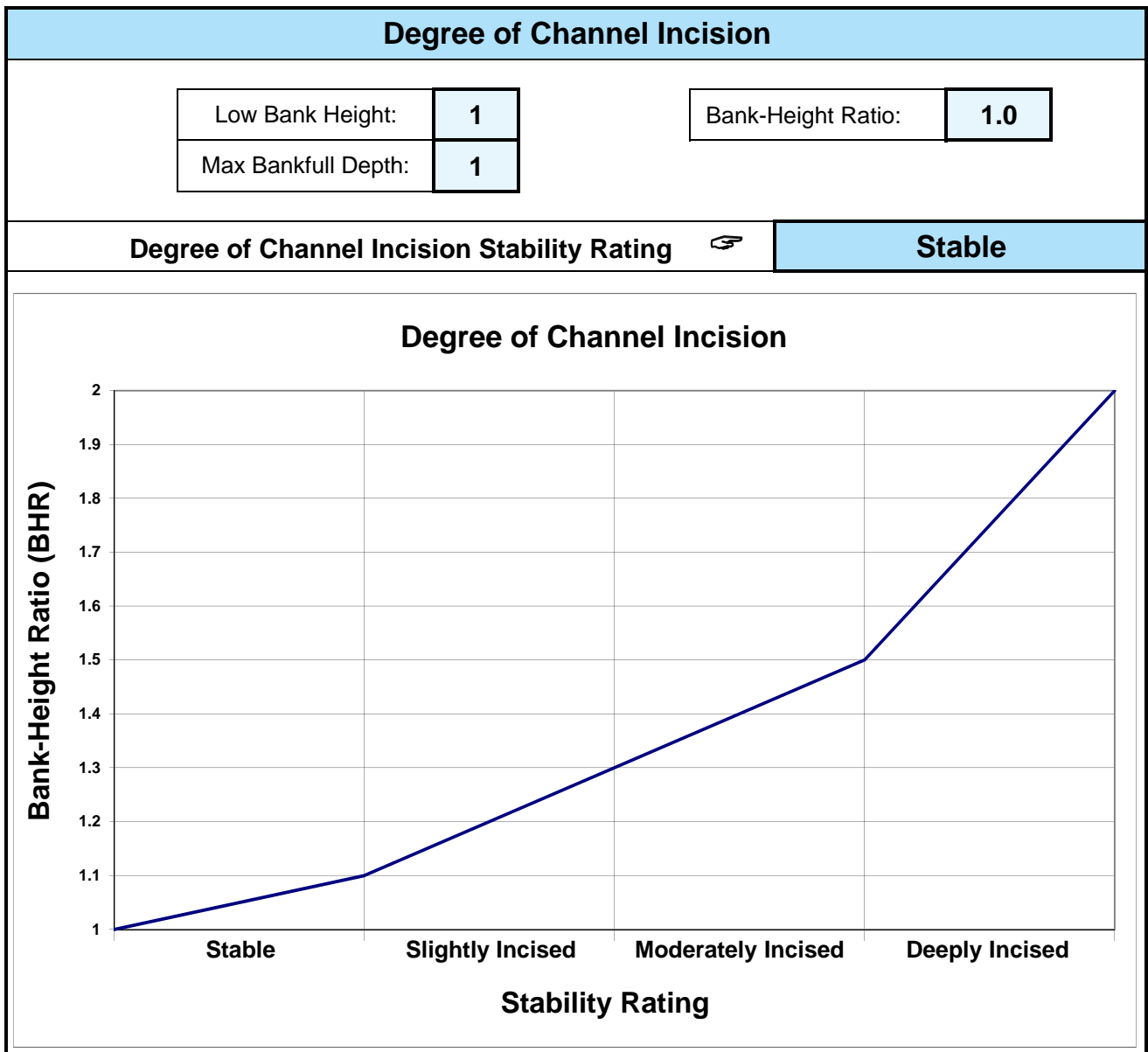
**Worksheet 5-10.** Depositional patterns.

<b>Depositional Patterns</b>					
Stream:	Northfield D4a Reference	Location:	Pike National Forest, Colorado		
Observers:	Bones, Kyle, David, Luke, Kim	Date:	11/8/2012		
List ALL CATEGORIES that APPLY	<b>B6</b>				
<i>Various Depositional Features modified from Galay et al. (1973)</i>					
 <b>B1 POINT BARS</b>	 <b>B5 DIAGONAL BARS</b>				
 <b>B2 POINT BARS with Few MID-CHANNEL BARS</b>	 <b>B6 Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</b>				
 <b>B3 NUMEROUS MID-CHANNEL BARS</b>	 <b>B7 SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</b>				
 <b>B4 SIDE BARS</b>	 <b>B8 DELTA BARS</b>				

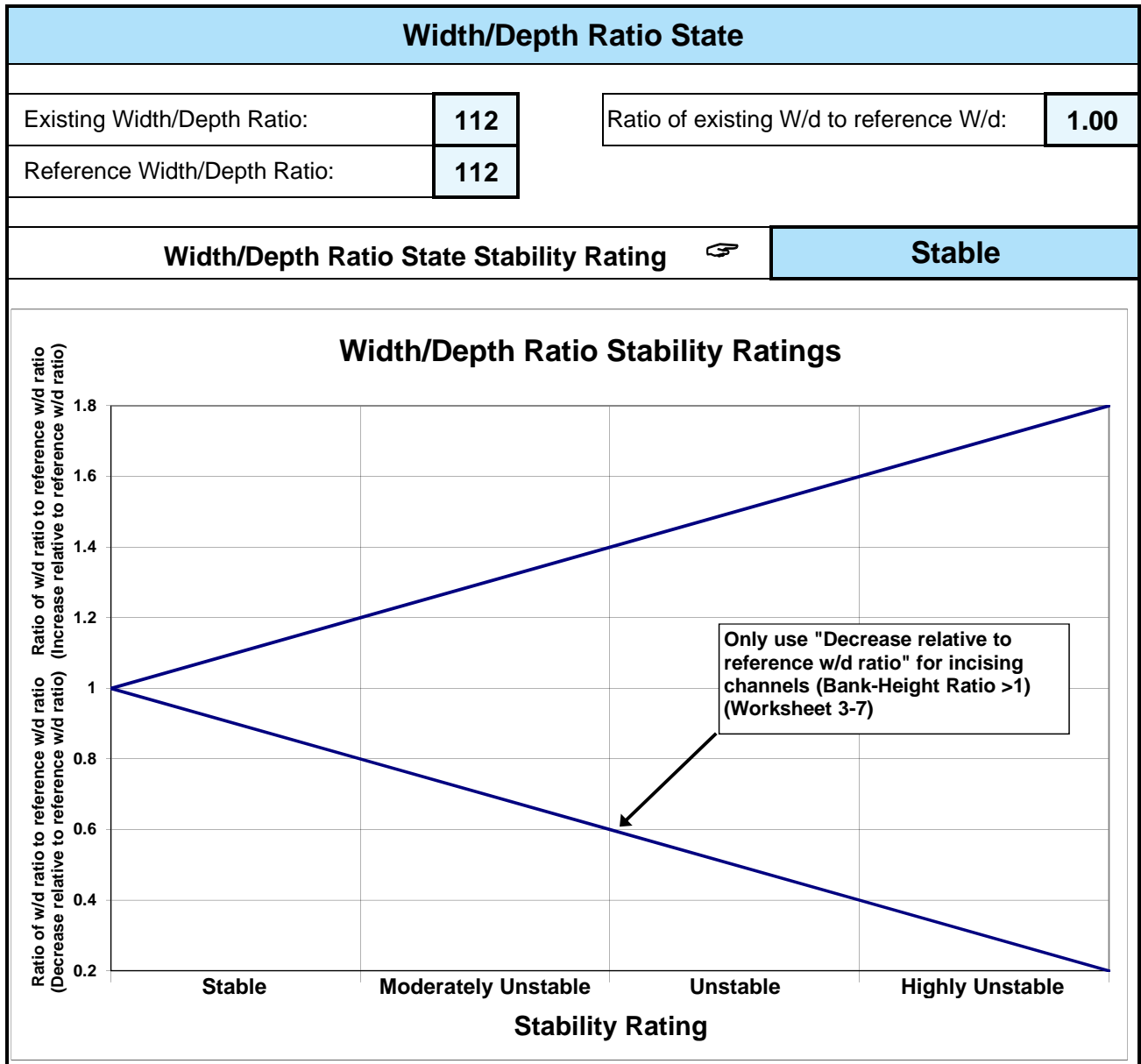
## Worksheet 5-11. Channel blockages.

Channel Blockages		
Stream: <b>Northfield Gulch D4a Reference</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Date: <b>11/8/2012</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input checked="" type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input type="checkbox"/>
<b>D4</b> Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

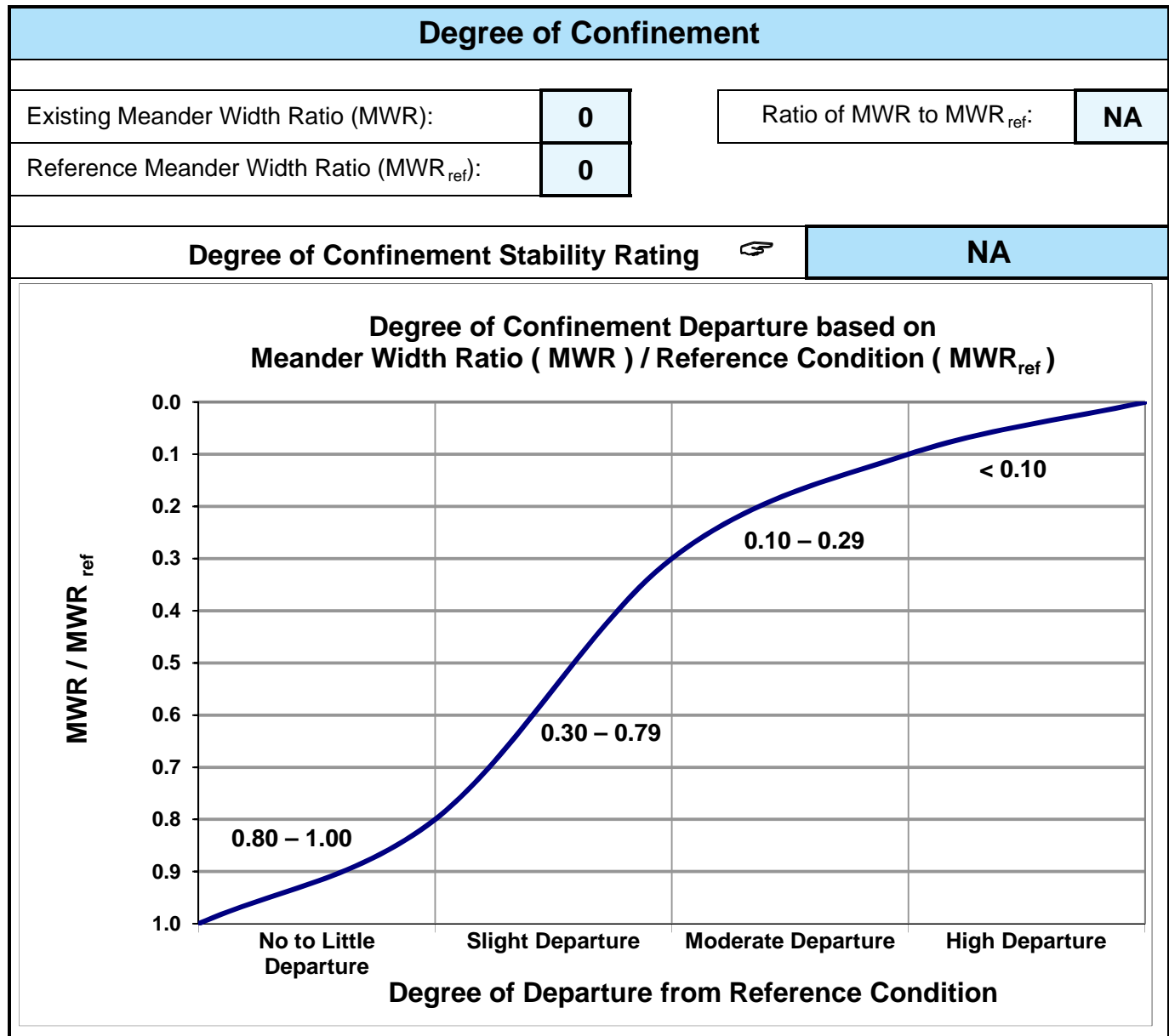
**Worksheet 5-12.** Degree of channel incision.



**Worksheet 5-13.** Width/depth ratio state.



**Worksheet 5-14.** Degree of channel confinement (lateral containment).



Worksheet 5-15. Pfankuch channel stability rating.

Stream: Northfield Gulch D4a Reference		Location: Pike National Forest, CO			Valley Type: Illia			Observers: Bones, Kyle, David, Luke, Kim			Date: 11/8/2012												
Loca- tion	Key	Category	Excellent		Good		Fair		Poor		Rating	Rating											
			Description	Rating	Description	Rating	Description	Rating	Description	Rating													
Upper banks	1	Landform slope	Bank slope gradient <30%.	2	Bank slope gradient 30–40%.	4	Bank slope gradient 40–60%.	6	Bank slope gradient > 60%.	8													
	2	Mass erosion	No evidence of past or future mass erosion.	3	Infrequent. Mostly healed over. Low future potential.	6	Frequent or large, causing sediment nearly yearlong.	9	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.	12													
	3	Debris jam	Essentially absent from immediate channel area.	2	Present, but mostly small twigs and limbs.	4	Moderate to heavy amounts, mostly larger sizes.	6	Moderate to heavy amounts, predominantly larger sizes.	8													
	4	Vegetative bank protection	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	3	70–90% density. Fewer species or less vigor suggest less dense or deep root mass.	6	50–70% density. Lower vigor and fewer species from a shallow, discontinuous root mass.	9	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.	12													
Lower banks	5	Channel capacity	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0.	1	Bankfull stage is contained within banks. Width/depth ratio departure from reference width/depth ratio = 1.0–1.2. Bank-Height Ratio (BHR) = 1.0–1.1.	2	Bankfull stage is not contained. Width/depth ratio departure from reference width/depth ratio = 1.2–1.4. Bank-Height Ratio (BHR) > 1.3.	3	Bankfull stage is not contained; over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.	4													
	6	Bank rock content	> 65% with large angular boulders. 12+ common.	2	40–65%. Mostly boulders and small cobbles 6–12".	4	20–40%. Most in the 3–6" diameter class.	6	<20% rock fragments of gravel sizes, 1–3" or less.	8													
	7	Obstructions to flow	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	2	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	4	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	6	Frequent obstructions and deflectors cause bank erosion yearlong. Sediment traps full, channel migration occurring.	8													
	8	Cutting	Little or none. Infrequent raw banks	4	Some, intermittently at outcaves and constrictions. Raw banks may be up to 12".	9	Significant. Cuts 12–24" high. Root mat overhangs and sloughing evident.	12	Almost continuous cuts, some over 24" high. Failure of overhangs frequent.	16													
	9	Deposition	Little or no enlargement of channel or point bars.	4	Some new bar increase, mostly from coarse gravel.	8	Moderate deposition of new gravel and coarse sand on old and some new bars.	10	Extensive deposit of predominantly fine particles. Accelerated bar development.	16													
Bottom	10	Rock angularity	Sharp edges and corners. Plane surfaces rough.	2	Rounded corners and edges. Surfaces smooth and flat.	2	Corners and edges well rounded in 2 dimensions.	3	Well rounded in all dimensions, surfaces smooth.	4													
	11	Brightness	Surfaces dull, dark or stained. Generally not bright.	1	Mostly dull, but may have <35% bright surfaces.	2	Mixture dull and bright, i.e., 35–65% mixture range.	3	Predominantly bright, > 65% exposed or scored surfaces.	4													
	12	Consolidation of particles	Assorted sizes tightly packed or overlapping.	2	Moderately packed with some overlapping.	4	Mostly loose assortment with no apparent overlap.	5	No packing evident. Loose assortment, easily moved.	8													
	13	Bottom size distribution	No size change evident. Stable material 80–100%.	4	Distribution shift light. Stable material 50–80%.	8	Moderate change in sizes. Stable materials 20–50%.	12	Marked distribution change. Stable materials 0–20%.	16													
	14	Scouring and deposition	<5% of bottom affected by scour or deposition.	6	5–30% affected. Scour at constrictions and where grades steepen. Some deposition in pools.	12	30–50% affected. Deposits and scour at obstructions, constrictions and bends. Some filling of pools.	20	More than 50% of the bottom in a state of flux or change nearly yearlong.	24													
	15	Aquatic vegetation	Abundant growth moss-like, dark green perennials. In swift water too.	1	Common. Algae forms in low velocity and pool areas. Moss here too.	2	Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick.	3	Perennial types scarce or absent. Yellow-green, short-term bloom may be present.	4													
				<b>Excellent total = 21</b>	<b>Good total = 4</b>	<b>Fair total = 15</b>	<b>Poor total = 40</b>																
Stream type	A1	A2	A3	A4	A5	A6	B1	B2	B3	B4	B5	B6	C1	C2	C3	C4	C5	C6	D3	D4	D5	D6	Grand total =
Good (Stable)	38-43	38-43	54-90	60-95	60-95	50-80	38-45	38-45	40-60	40-64	48-68	40-60	38-50	38-50	60-85	70-90	70-90	60-85	85-107	85-107	85-107	67-98	80
Fair (Mod. unstable)	44-47	44-47	91-129	96-132	96-142	81-110	46-58	46-58	61-78	65-84	69-88	61-78	51-61	51-61	86-105	91-110	91-110	86-105	108-132	108-132	108-132	99-125	D4a
Poor (Unstable)	48+	48+	130+	133+	143+	111+	59+	59+	79+	85+	89+	79+	62+	62+	106+	111+	111+	106+	133+	133+	133+	126+	D4a
Stream type	DA3	DA4	DA5	DA6	E3	E4	E5	E6	F1	F2	F3	F4	F5	F6	G1	G2	G3	G4	G5	G6	G7	G8	*Potential stream type =
Good (Stable)	40-63	40-63	40-63	40-63	40-63	50-75	50-75	40-63	60-85	60-85	85-110	85-110	90-115	90-95	80-95	40-60	40-60	85-107	85-107	90-112	85-107	85-107	D4a
Fair (Mod. unstable)	64-86	64-86	64-86	64-86	64-86	76-96	76-96	64-86	86-105	86-105	111-125	111-125	116-130	96-110	61-78	61-78	108-120	108-120	113-125	108-120	108-120	108-120	Modified channel stability rating =
Poor (Unstable)	87+	87+	87+	87+	87+	97+	97+	87+	106+	106+	126+	126+	131+	111+	79+	79+	121+	121+	126+	126+	121+	121+	Good

\*Rating is adjusted to potential stream type, not existing.

# FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Equation type	Intercept	Coefficient	Exponent	Form (e.g., linear, non-linear, etc.)	Equation name	Bankfull discharge (cfs)	Bankfull bedload (kg/s)	Bankfull suspended (mg/l)						
1. Bedload (dimensionless)	-0.0113	1.0139	2.1929	Non-L-linear	Pagosa Springs Reference Curve	3.99	0.0064	1.39						
2. Suspended sediment (dimensionless)	0.0636	0.9326	2.4085	Non-L-linear	Pagosa Springs Reference Curve									
Notes: Pre-Fire Flow Duration Curve, Good/Fair Sediment Curves, Good/Fair Regional Sediment Curves														
From dimensioned flow-duration curve			From sediment rating curves			Calculate								
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Flow exceedence	Daily mean discharge	Mid-ordinate	Time increment (percent)	Time increment (days)	Mid-ordinate streamflow	Dimensionless streamflow	Dimensionless suspended sediment discharge	Suspended sediment discharge	Dimensionless bedload discharge	Bedload	Time adjusted streamflow	Suspended sediment	Bedload sediment	Suspended + bedload
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q <sub>10</sub> /Q <sub>100</sub> )	(S/S <sub>100</sub> )	(tons/day)	(b <sub>y</sub> /b <sub>100</sub> )	(tons/day)	(cfs)	(tons)	[(5)*9]	[(1*3)+(14)]
100.000	0.0													
90.000	0.1	95.00	10.00	36.50	0.1	0.02	1.5	0.0	0.0000	0.00	0.80	0.00	0.00	0.00
80.000	0.2	85.00	10.00	36.50	0.2	0.04	1.5	0.0	0.0000	0.00	1.50	0.00	0.00	0.00
70.000	0.2	75.00	10.00	36.50	0.2	0.05	1.5	0.0	0.0000	0.00	2.00	0.00	0.00	0.00
60.000	0.3	65.00	10.00	36.50	0.2	0.06	1.5	0.0	0.0000	0.00	2.30	0.00	0.00	0.00
50.000	0.3	55.00	10.00	36.50	0.3	0.08	1.5	0.0	0.0000	0.00	3.00	0.00	0.00	0.00
40.000	0.5	45.00	10.00	36.50	0.4	0.10	1.5	0.0	0.0000	0.00	4.00	0.00	0.00	0.00
30.000	0.6	35.00	10.00	36.50	0.5	0.14	1.5	0.0	0.0000	0.00	5.40	0.00	0.00	0.00
20.000	1.0	25.00	10.00	36.50	0.8	0.20	1.5	0.0	0.0000	0.00	7.90	0.00	0.00	0.00
10.000	1.7	15.00	10.00	36.50	1.3	0.34	1.7	0.0	0.0004	0.04	13.40	0.00	1.46	1.46
5.000	2.8	7.50	5.00	18.25	2.3	0.56	2.3	0.0	0.0015	0.09	11.25	0.00	1.64	1.64
4.000	3.1	4.50	1.00	3.65	3.0	0.74	3.0	0.0	0.0029	0.17	2.95	0.00	0.62	0.62
3.000	3.7	3.50	1.00	3.65	3.4	0.85	3.6	0.0	0.0041	0.26	3.38	0.04	0.95	0.99
2.000	4.3	2.50	1.00	3.65	4.0	1.00	4.6	0.0	0.0060	0.35	3.99	0.04	1.28	1.32
1.500	5.0	1.75	0.50	1.83	4.7	1.17	6.0	0.0	0.0085	0.52	2.33	0.02	0.95	0.97
1.000	6.1	1.25	0.50	1.83	5.5	1.38	8.3	0.0	0.0125	0.73	2.75	0.05	1.33	1.38
0.900	6.5	0.95	0.10	0.37	6.3	1.57	10.7	0.0	0.0166	0.99	0.63	0.01	0.36	0.37
0.800	6.8	0.85	0.10	0.37	6.6	1.66	12.1	0.1	0.0190	1.12	0.66	0.02	0.41	0.43
0.700	7.2	0.75	0.10	0.37	7.0	1.76	13.6	0.1	0.0214	1.25	0.70	0.02	0.46	0.48
0.600	7.7	0.65	0.10	0.37	7.4	1.86	15.5	0.1	0.0245	1.43	0.74	0.03	0.52	0.55
0.500	8.2	0.55	0.10	0.37	7.9	1.99	17.7	0.1	0.0281	1.64	0.79	0.03	0.60	0.63
0.250	9.5	0.38	0.25	0.91	8.8	2.22	22.6	0.1	0.0358	2.07	2.21	0.11	1.89	2.00
0.100	11.0	0.18	0.15	0.55	10.2	2.56	31.6	0.2	0.0495	2.89	1.53	0.11	1.58	1.69
0.050	11.7	0.08	0.05	0.18	11.4	2.84	34.6	0.3	0.0540	3.63	0.57	0.05	0.66	0.71
0.010	12.8	0.03	0.04	0.15	12.3	3.07	34.6	0.4	0.0540	4.28	0.49	0.05	0.62	0.67
0.005	12.8	0.01	0.01	0.02	12.8	3.20	34.6	0.4	0.0540	4.71	0.06	0.01	0.09	0.10
0.001	12.8	0.00	0.00	0.01	12.8	3.20	34.6	0.4	0.0540	4.71	0.05	0.01	0.07	0.08
Annual totals:											0.6 (tons/yr)	15.5 (tons/yr)	16.1 (tons/yr)	



**Worksheet 19b.** Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Equation type	Intercept	Coefficient	Exponent	Form (e.g., linear, non-linear, etc.)	Equation name		Bankfull discharge (cfs)	Bankfull bedload (kg/s)	Bankfull suspended (mg/l)					
					Pagosa Springs Reference Curve	Pagosa Springs Reference Curve								
1. Bedload (dimensionless)	-0.0113	1.0139	2.1929	Non-Linear			3.99	0.0064	1.39					
2. Suspended sediment (dimensionless)	0.0636	0.9326	2.4085	Non-Linear										
3. User-defined relations (bedload)														
4. User-defined relations (suspended sediment)														
Notes: Post-Fire Flow Duration Curve, Good/Fair Sediment Curves, Good/Fair Regional Sediment Curves														
Flow exceedence (%)	From dimensioned flow-duration curve				From sediment rating curves				Calculate		Calculate sediment yield			
	(2) Daily mean discharge (cfs)	(3) Mid-ordinate (%)	(4) Time increment (percent)	(5) Time increment (days)	(6) Mid-ordinate streamflow (cfs)	(7) Dimension-less streamflow (Q/Q <sub>med</sub> )	(8) Dimension-less suspended sediment discharge (S/S <sub>med</sub> )	(9) Suspended sediment discharge (tons/day)	(10) Dimension-less bedload discharge (b <sub>p</sub> /b <sub>med</sub> )	(11) Bedload (tons/day)	(12) Time adjusted streamflow [(5)×(9)] (cfs)	(13) Suspended sediment [(5)×(9)] (tons)	(14) Bedload sediment [(13)×(14)] (tons)	(15) Suspended + bedload [(13)+(14)] (tons)
100.000	0.0													
90.000	0.1	95.00	10.00	36.50	0.1	0.02	1.5	0.0	0.0000	0.00	0.80	0.00	0.00	0.00
80.000	0.2	85.00	10.00	36.50	0.2	0.04	1.5	0.0	0.0000	0.00	1.50	0.00	0.00	0.00
70.000	0.2	75.00	10.00	36.50	0.2	0.05	1.5	0.0	0.0000	0.00	2.00	0.00	0.00	0.00
60.000	0.3	65.00	10.00	36.50	0.2	0.06	1.5	0.0	0.0000	0.00	2.30	0.00	0.00	0.00
50.000	0.3	55.00	10.00	36.50	0.3	0.08	1.5	0.0	0.0000	0.00	3.00	0.00	0.00	0.00
40.000	0.5	45.00	10.00	36.50	0.4	0.10	1.5	0.0	0.0000	0.00	4.00	0.00	0.00	0.00
30.000	0.7	35.00	10.00	36.50	0.6	0.14	1.5	0.0	0.0000	0.00	5.70	0.00	0.00	0.00
20.000	1.4	25.00	10.00	36.50	1.1	0.27	1.6	0.0	0.0001	0.00	10.60	0.00	0.00	0.00
10.000	2.9	15.00	10.00	36.50	2.2	0.55	2.2	0.0	0.0014	0.09	21.80	0.00	3.28	3.28
5.000	4.4	7.50	5.00	18.25	3.7	0.91	4.0	0.0	0.0049	0.30	18.25	0.18	5.47	5.65
4.000	4.8	4.50	1.00	3.65	4.6	1.14	5.8	0.0	0.0081	0.48	4.56	0.04	1.75	1.79
3.000	5.4	3.50	1.00	3.65	5.1	1.27	7.1	0.0	0.0104	0.60	5.07	0.07	2.19	2.26
2.000	6.1	2.50	1.00	3.65	5.7	1.44	9.0	0.0	0.0138	0.82	5.74	0.11	2.99	3.10
1.500	6.8	1.75	0.50	1.83	6.4	1.61	11.3	0.0	0.0177	1.04	3.21	0.07	1.90	1.97
1.000	7.8	1.25	0.50	1.83	7.3	1.83	14.9	0.1	0.0235	1.38	3.65	0.11	2.52	2.63
0.900	8.2	0.95	0.10	0.37	8.0	2.02	18.3	0.1	0.0291	1.68	0.80	0.03	0.61	0.64
0.800	8.6	0.85	0.10	0.37	8.4	2.11	20.4	0.1	0.0324	1.90	0.84	0.04	0.69	0.73
0.700	9.0	0.75	0.10	0.37	8.8	2.20	22.4	0.1	0.0354	2.07	0.88	0.04	0.76	0.80
0.600	9.5	0.65	0.10	0.37	9.2	2.31	25.0	0.1	0.0395	2.29	0.92	0.05	0.84	0.89
0.500	10.0	0.55	0.10	0.37	9.7	2.44	28.1	0.2	0.0442	2.59	0.97	0.06	0.95	1.01
0.250	11.3	0.38	0.25	0.91	10.6	2.66	34.5	0.2	0.0539	3.15	2.66	0.21	2.87	3.08
0.100	12.8	0.18	0.15	0.55	12.0	3.01	34.6	0.3	0.0540	4.10	1.80	0.19	2.24	2.43
0.050	13.5	0.08	0.05	0.18	13.1	3.29	34.6	0.5	0.0540	5.01	0.66	0.08	0.91	0.99
0.010	14.6	0.03	0.04	0.15	14.0	3.52	34.6	0.6	0.0540	5.79	0.56	0.08	0.85	0.93
0.005	14.6	0.01	0.01	0.02	14.6	3.65	34.6	0.7	0.0540	6.26	0.07	0.01	0.11	0.12
0.001	14.6	0.00	0.00	0.01	14.6	3.65	34.6	0.7	0.0540	6.26	0.06	0.01	0.09	0.10
Annual totals:										1.4 (tons/yr)	31.0 (tons/yr)	32.4 (tons/yr)		

## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>Northfield Gulch D4a Reference</b>		Stream Type: <b>D4a</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>IIIa</b>			
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Date: <b>11/08/2012</b>			
<b>Enter Required Information for Existing Condition</b>					
4.2	$D_{50}$	Riffle bed material $D_{50}$ (mm)			
0.0	$\hat{D}_{50}$	Bar sample $D_{50}$ (mm)			
0.210	$D_{max}$	Largest particle from <b>Bed Material</b> (ft)	64	(mm)	304.8 mm/ft
0.07277	S	Existing bankfull water surface slope (ft/ft)			
0.16	d	Existing bankfull mean depth (ft)			
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment			
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>					
N/A	$D_{50}/\hat{D}_{50}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 ( D_{50}/\hat{D}_{50} )^{-0.872}$		
N/A	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 ( D_{max}/D_{50} )^{-0.887}$		
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED:	2	
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	d	Required bankfull mean depth (ft)	$d = \frac{\tau^* (\gamma_s - 1) D_{max}}{S}$ (use $D_{max}$ in ft)		
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	S	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^* (\gamma_s - 1) D_{max}}{d}$ (use $D_{max}$ in ft)		
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					
<b>Sediment Competence Using Dimensional Shear Stress</b>					
0.727	Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d) $\gamma = 62.4$ , d = existing depth, S = existing slope				
Shields 55.89	CO 120.2	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ (Figure 5-49)			
Shields 0.827	CO 0.308	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) (Figure 5-49)			
Shields 0.18	CO 0.07	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm) $\tau =$ predicted shear stress, $\gamma = 62.4$ , S = existing slope		$d = \frac{\tau}{\gamma S}$	
Shields 0.0829	CO 0.0309	Predicted slope required to initiate movement of measured $D_{max}$ (mm) $\tau =$ predicted shear stress, $\gamma = 62.4$ , d = existing depth		$S = \frac{\tau}{\gamma d}$	
Check: <input type="checkbox"/> Stable <input checked="" type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					

## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>Northfield Gulch D4a Reference</b>		Stream Type: <b>D4a</b>
Location: <b>Pike National Forest, CO</b>		Valley Type: <b>IIIa</b>
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Date: <b>11/08/2012</b>
Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)	Stability Rating (Check Appropriate Rating)	
Stream Type at potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	<input checked="" type="checkbox"/> Stable	
(E→C), (C→High W/d C)	<input type="checkbox"/> Moderately Unstable	
(G→F), (F→D), (C→F)	<input type="checkbox"/> Unstable	
(C→D), (B→G), (D→G), (C→G), (E→G)	<input type="checkbox"/> Highly Unstable	

**Worksheet 5-25.** Lateral stability.

Stream: <b>Northfield Gulch D4a Reference</b>		Stream Type: <b>D4a</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>IIIa</b>			
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Date: <b>11/08/2012</b>			
Lateral stability criteria (choose one stability category for each criterion 1-5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	2
	(2)	(4)	(6)	(8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	4
	(1)	(2)	(3)	(4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		N/A
	(1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	N/A
	(2)	(4)	(6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	1
	(1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>7</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input checked="" type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input type="checkbox"/>	<i>Unstable</i> 13 – 21 <input type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	

**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>Northfield Gulch D4a Reference</b>		Stream Type: <b>D4a</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>IIIa</b>			
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Date: <b>11/08/2012</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
<b>1 Sediment competence (Worksheet 5-22)</b>	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope-slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	<b>8</b>
	(2)	(4)	(6)	(8)	
<b>2 Sediment Capacity (POWERSED) (Worksheet 5-20)</b>	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	<b>8</b>
	(2)	(4)	(6)	(8)	
<b>3 W/d Ratio State (Worksheet 5-13)</b>	1.0 – 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>4 Stream Succession States (Worksheet 5-24)</b>	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	<b>2</b>
	(2)	(4)	(6)	(8)	
<b>5 Depositional Patterns (Worksheet 5-10)</b>	B1	B2, B4	B3, B5	B6, B7, B8	<b>4</b>
	(1)	(2)	(3)	(4)	
<b>6 Debris / Blockages (Worksheet 5-11)</b>	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	<b>1</b>
	(1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>25</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
<b>Vertical Stability for Excess Deposition / Aggradation (use total points and check stability rating)</b>	<i>No Deposition</i> 10 – 14 <input type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input checked="" type="checkbox"/>	<i>Aggradation</i> > 30 <input type="checkbox"/>	

**Worksheet 5-27.** Vertical stability – degradation.

Stream: <b>Northfield Gulch D4a Reference</b>		Stream Type: <b>D4a</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>Illa</b>			
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Date: <b>11/08/2012</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>Sediment Competence</b> (Worksheet 5-22)	Does not indicate excess competence <b>(2)</b>	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed <b>(4)</b>	$D_{100}$ of bed moved <b>(6)</b>	Particles much larger than $D_{100}$ of bed moved <b>(8)</b>	<b>2</b>
<b>Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Does not indicate excess capacity <b>(2)</b>	Slight excess energy: up to 10% increase above reference <b>(4)</b>	Excess energy sufficient to increase load up to 50% of annual load <b>(6)</b>	Excess energy transporting more than 50% of annual load <b>(8)</b>	<b>2</b>
<b>Degree of Channel Incision (BHR)</b> (Worksheet 5-12)	1.00 – 1.10 <b>(2)</b>	1.11 – 1.30 <b>(4)</b>	1.31 – 1.50 <b>(6)</b>	> 1.50 <b>(8)</b>	<b>2</b>
<b>Stream Succession States</b> (Worksheets 5-12 and 5-24)	Does not indicate incision or degradation <b>(2)</b>	If BHR > 1.1 and stream type has W/d between 5–10 <b>(4)</b>	If BHR > 1.1 and stream type has W/d less than 5 <b>(6)</b>	(B→G), (C→G), (E→G), (D→G) <b>(8)</b>	<b>2</b>
<b>Confinement (MWR / MWR<sub>ref</sub>)</b> (Worksheet 5-14)	0.80 – 1.00 <b>(1)</b>	0.30 – 0.79 <b>(2)</b>	0.10 – 0.29 <b>(3)</b>	< 0.10 <b>(4)</b>	<b>1</b>
<b>Total Points</b>					<b>9</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation</b> (use total points and check stability rating)	<i>Not Incised</i> 9 – 11 <input checked="" type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input type="checkbox"/>	<i>Degradation</i> > 27 <input type="checkbox"/>	

**Worksheet 5-28.** Channel enlargement.

Stream: <b>Northfield Gulch D4a Reference</b>		Stream Type: <b>D4a</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>Illa</b>			
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Date: <b>11/08/2012</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1-4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	2
	(2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	2
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	6
	(2)	(4)	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	2
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>12</b>
<b>Category Point Range</b>					
<b>Channel Enlargement Prediction (use total points and check stability rating)</b>	<i>No Increase</i> 8 – 10 <input type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input checked="" type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input type="checkbox"/>	<i>Extensive</i> > 24 <input type="checkbox"/>	

Worksheet 5-29. Overall sediment supply.

Stream: <b>Northfield Gulch D4a Reference</b>		Stream Type: <b>D4a</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>IIIa</b>		
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Date: <b>11/08/2012</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1–5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	1	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	3	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	1	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	2	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	1	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>8</b>	
<b>Category Point Range</b>				
Overall Sediment Supply Rating (use total points and check stability rating)	<b>Low</b> 5 <input type="checkbox"/>	<b>Moderate</b> 6 – 10 <input checked="" type="checkbox"/>	<b>High</b> 11 – 15 <input type="checkbox"/>	<b>Very High</b> 16 – 20 <input type="checkbox"/>



Worksheet 5-32. Summary of stability condition categories.

Stream: <b>Northfield Gulch D4a Reference</b>		Location: <b>Pike National Forest, Colorado</b>	
Observers: <b>Bones, Kyle, David, Luke, Kim</b>		Date: <b>11/8/2012</b>	Stream Type: <b>D4a</b> Valley Type: <b>Illa</b>
<b>Channel Dimension</b>	Mean Bankfull Depth (ft): <b>0.16</b>	Bankfull Width (ft): <b>17.92</b>	Cross-Sectional Area (ft <sup>2</sup> ): <b>2.81</b> Width of Flood-Prone Area (ft): <b>8.16</b> Entrenchment Ratio: <b>1.1</b>
<b>Channel Pattern</b>	Mean Range: $\lambda/W_{bkr}$ : <b>N/A</b>	$L_{rr}/W_{bkr}$ : <b>N/A</b>	$R_c/W_{bkr}$ : <b>N/A</b> MWR: <b>3.35</b> Sinuosity: <b>1</b>
<b>River Profile &amp; Bed Features</b>	Check: <input type="checkbox"/> Riffle/Pool <input type="checkbox"/> Step/Pool <input checked="" type="checkbox"/> Plane Bed <input type="checkbox"/> Convergence/Divergence <input type="checkbox"/> Dunes/Antidunes/Smooth Bed		
	Max Bankfull Depth (ft): <b>0.78</b>	Riffle Pool	Pool Spacing: <b>4.88</b>
Riparian Vegetation: <b>Mixed conifer, aspen, willow</b> At potential <b>Vigorous</b>			
Flow Regime: <b>E(1, 2, Stream Size S-4(3) &amp; Order: 7, 8)</b> Meander Patterns: <b>N/A</b> Depositional Patterns: <b>B6</b> Debris/Channel Blockages: <b>D2</b>			
<b>Level III Stream Stability Indices</b>	Degree of Incision (Bank-Height Ratio): <b>1.0</b>	Degree of Incision Stability Rating: <b>Stable</b>	Modified Pfankuch Stability Rating (Numeric & Adjective Rating): <b>80 (Good)</b>
<b>Bank Erosion Summary</b>	Width/depth Ratio (W/d): <b>112</b>	Reference W/d Ratio (W/d <sub>ref</sub> ): <b>100</b>	W/d Ratio State Stability Rating: <b>Stable</b>
	Meander Width Ratio (MWR): <b>0</b>	Reference MWR <sub>ref</sub> : <b>0</b>	MWR / MWR <sub>ref</sub> Stability Rating: <b>Stable</b>
Length of Reach Studied (ft):		Annual Streambank Erosion Rate: (tons/yr)	Curve Used: <b>NA for this depositional reach</b>
<input type="checkbox"/> Sufficient Capacity <input checked="" type="checkbox"/> Insufficient Capacity <input type="checkbox"/> Excess Capacity Remarks:			
<b>Entrainment/Competence</b>	Largest Particle from Bar Sample (mm): <b>64</b>	$\tau = 0.308$	$\tau^* = N/A$
<b>Successional Stage Shift</b>	→	→	→
<b>Lateral Stability</b>	<input checked="" type="checkbox"/> Stable	<input checked="" type="checkbox"/> Mod. Unstable	<input type="checkbox"/> Unstable <input type="checkbox"/> Highly Unstable
<b>Vertical Stability (Aggradation)</b>	<input type="checkbox"/> No Deposition	<input type="checkbox"/> Mod. Deposition	<input checked="" type="checkbox"/> Ex. Deposition <input type="checkbox"/> Aggradation
<b>Vertical Stability (Degradation)</b>	<input checked="" type="checkbox"/> Not Incised	<input type="checkbox"/> Slightly Incised	<input type="checkbox"/> Mod. Incised <input type="checkbox"/> Degradation
<b>Channel Enlargement</b>	<input type="checkbox"/> No Increase	<input checked="" type="checkbox"/> Slight Increase	<input type="checkbox"/> Mod. Increase <input type="checkbox"/> Extensive
<b>Sediment Supply (Channel Source)</b>	<input checked="" type="checkbox"/> Low	<input type="checkbox"/> Moderate	<input type="checkbox"/> High <input type="checkbox"/> Very High
Remarks/causes: <b>Recent influx of sediment from post fire flooding</b>			



## *Appendix C22*

# **E4 Stream Type**

## *Reference Reach*



# Table of Contents

## *Appendix C22: E4 Reference Reach*

<b>Reach Location &amp; Overview.....</b>	<b>C22-2</b>
<b>Survey Summary.....</b>	<b>C22-3</b>
Longitudinal Profile	
Cross-Sections	
Pebble Counts	
<b>WARSSS Worksheets.....</b>	<b>C22-10</b>
<b><i>Velocity, Classification &amp; Morphological Relations.....</i></b>	<b>C22-10</b>
Worksheet 5-2. Computations of velocity and bankfull discharge.	
Worksheet 5-3. Level II stream classification.	
Worksheet 5-4. Morphological relations (modified from Rosgen, 2006/2009).	
<b><i>Stability Indices.....</i></b>	<b>C22-14</b>
Worksheet 5-6. Riparian vegetation.	
Worksheet 5-7. Flow regime.	
Worksheet 5-8. Stream order and stream size.	
Worksheet 5-9. Meander patterns.	
Worksheet 5-10. Depositional patterns.	
Worksheet 5-11. Channel blockages.	
Worksheet 5-12. Degree of channel incision.	
Worksheet 5-13. Width/depth ratio state.	
Worksheet 5-14. Degree of channel confinement (lateral containment).	
Worksheet 5-15. Pfankuch channel stability rating.	
<b><i>BANCS Model – Streambank Erosion.....</i></b>	<b>C22-24</b>
Worksheet 5-18. Annual streambank erosion estimates.	
Streambank Erosion Map	
<b><i>FLOWSED Model – Total Annual Sediment Yield.....</i></b>	<b>C22-26</b>
Worksheet 5-19a. Total annual sediment yield, pre-fire condition.	
Worksheet 5-19b. Total annual sediment yield, post-fire condition.	
<b><i>Sediment Competence/Entrainment.....</i></b>	<b>C22-28</b>
Worksheet 5-22. Sediment competence calculations.	
<b><i>Channel Stability Ratings.....</i></b>	<b>C22-29</b>
Worksheet 5-24. Successional stage shifts.	
Worksheet 5-25. Lateral stability.	
Worksheet 5-26. Vertical stability – aggradation.	
Worksheet 5-27. Vertical stability – degradation.	
Worksheet 5-28. Channel enlargement.	
Worksheet 5-29. Overall sediment supply.	
<b><i>Summary.....</i></b>	<b>C22-35</b>
Worksheet 5-32. Summary of stability condition categories.	

## E4 Reference Reach Location & Overview

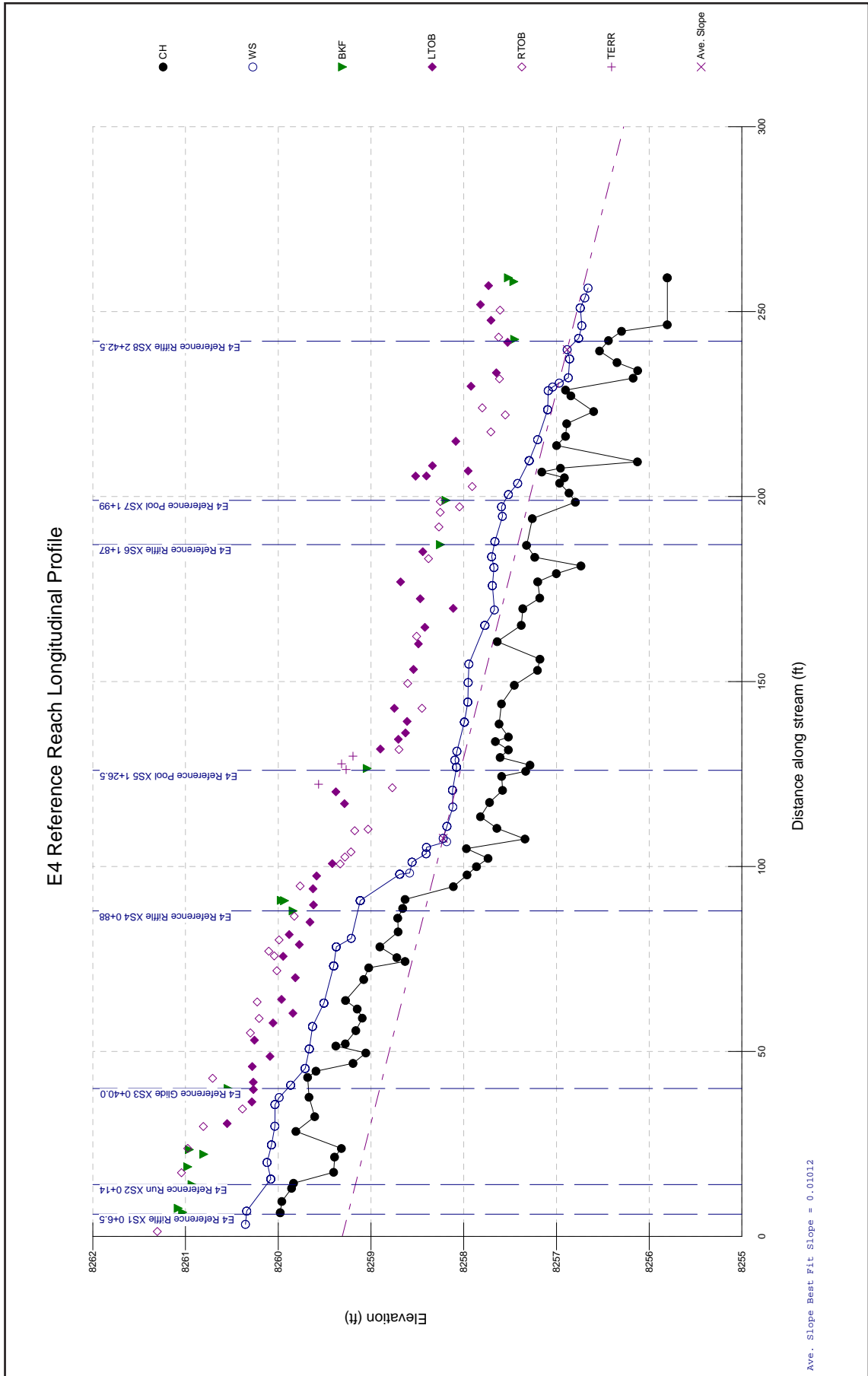
The E4 reference reach exists in a lacustrine Valley Type X and is typical of a very low width/depth ratio channel on gentle slopes with a gravel-bed. The channel bed and banks are potentially erodible, but due to the good vegetation condition, this E4 reference reach shows little sediment yield from this reach. Bed features are generally dominated by riffles and pools with runs and glide features. The channel is located on Upper Trail Creek as shown in **Figure C-2**. The stream is a perennial, meandering stream, unconfined, not entrenched with a well-developed floodplain. The morphological data from this reach will be used to develop dimension, pattern, and profile data for impaired streams that potentially should be E4 stream types. There is little sediment storage in this stream type due to the lack of point bars and other depositional features. The natural or geologic rate of streambank erosion is generally low due to the excellent riparian vegetation of willow and *Carex/Juncus*. An erosion rate of  $0.0017 \text{ tons/yr/ft}$  (**Worksheet 5-18**) is typical for this stream type in a similar condition; streambank erosion rates for impaired conditions of this stream type can be associated with rates three orders of magnitude larger. This stream is sensitive to disturbance but fast to recover following impacts.

Typical of E4 stream types are large entrenchment ratios (not entrenched) that are not laterally contained or confined. There is not an acceleration of sediment supply from this reach during high runoff events due to the good riparian vegetation coverage. This stream type is critically linked to streambank vegetation to maintain its low width/depth ratio.

The photograph shows the good riparian community and the stable characteristics of this E4 stream type. There is little to no evidence of active channel-source sediment. The details of the dimension, pattern, profile, and materials are summarized. The POWERSED model was not run on this reference reach as the bed is obviously stable. The following summary worksheets provide the detail of the morphology, hydraulics, streambank erosion rates and stability. In the situation where impaired G4c, F4c, and some C4 stream types are located, an alternative for mitigation and sediment reduction from increased flow in these stream types is to use the data from the stable form of the E4 to extrapolate for potential implementation of natural channel design.

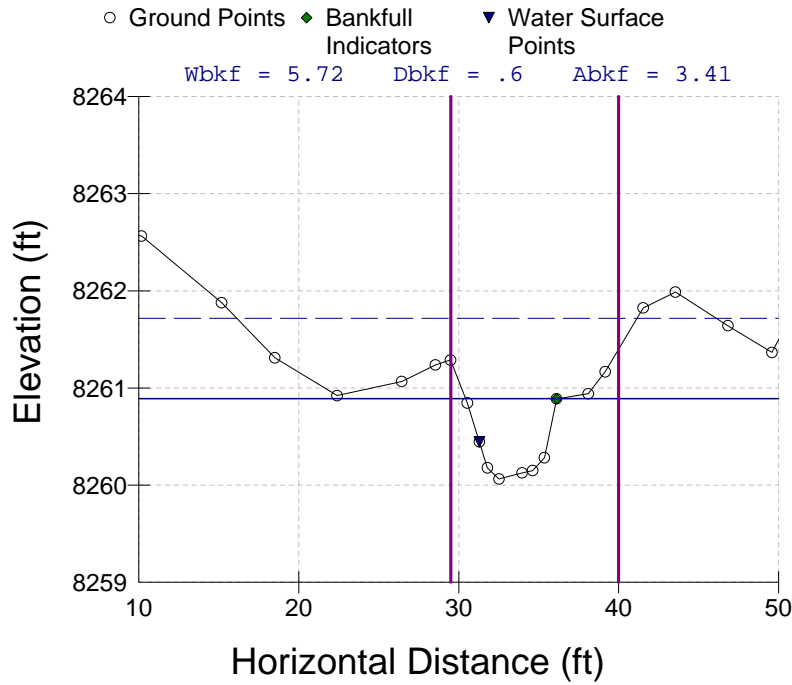


# Survey Summary



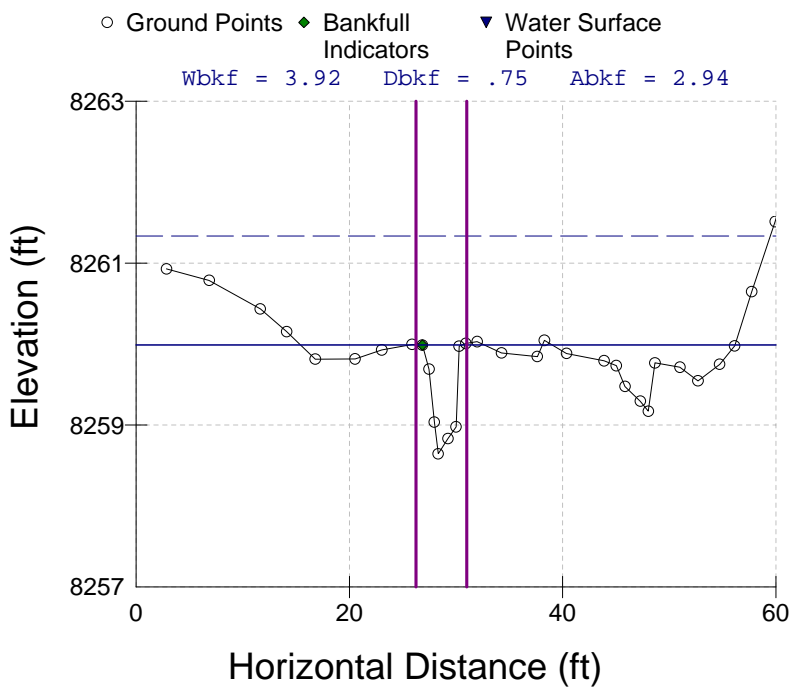
Longitudinal Profile (graph generated from RIVERMorph™)

### E4 Reference Reach Riffle XS 0+6.5



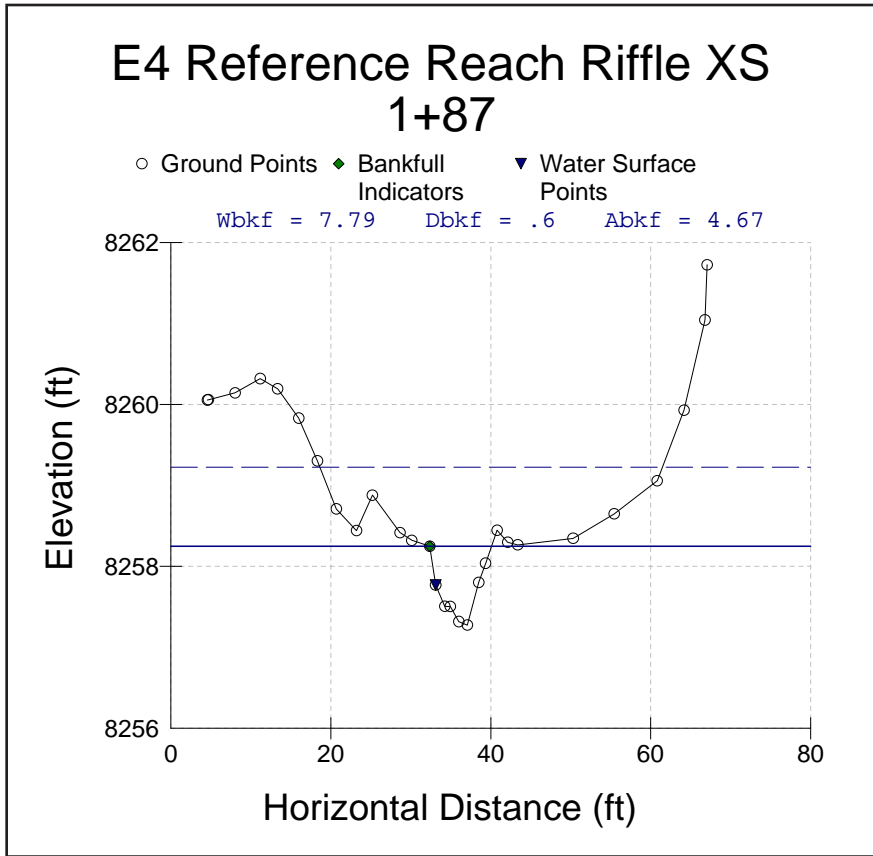
Riffle Cross-section 0+6.5 (graph generated from RIVERMorph™)

### E4 Reference Reach Riffle XS 0+88

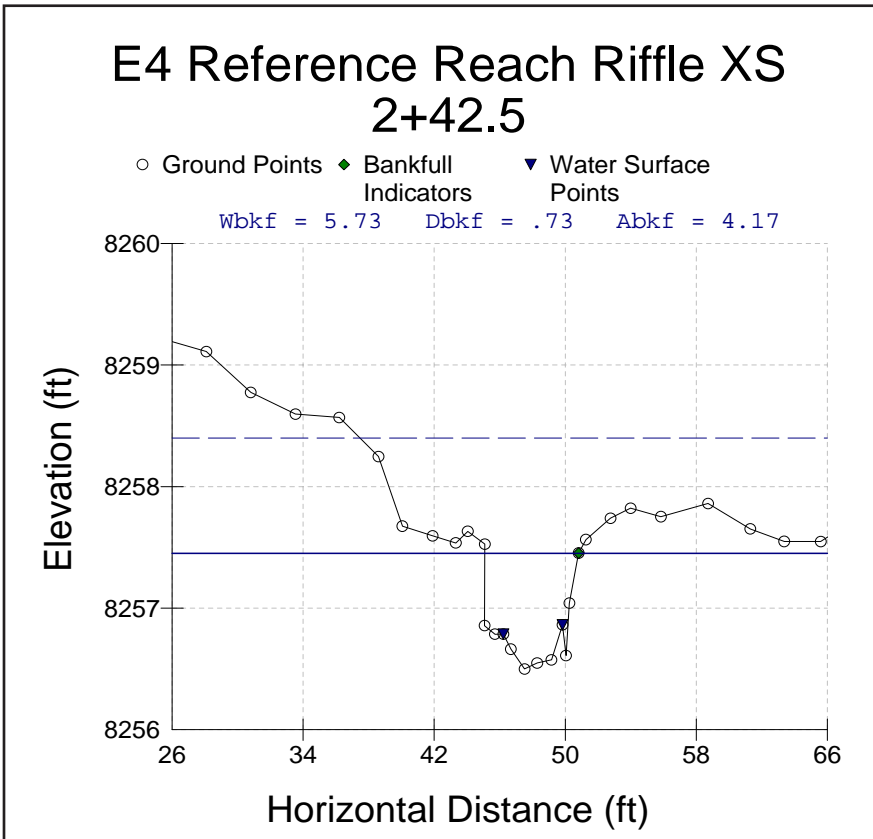


Riffle Cross-section 0+88 (graph generated from RIVERMorph™)

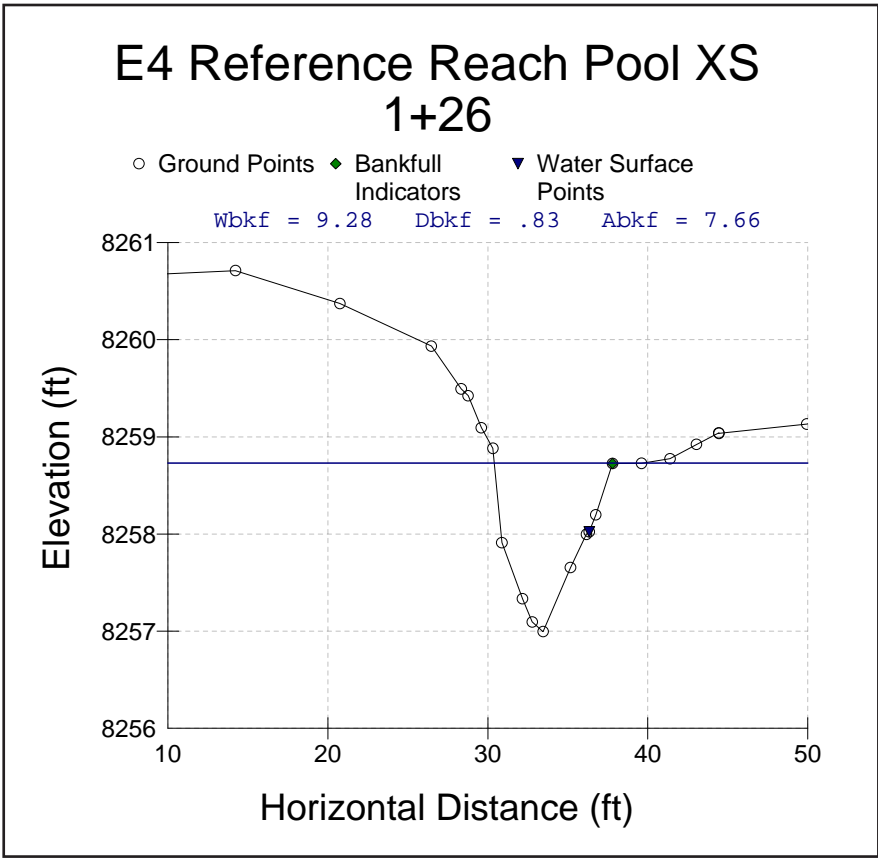




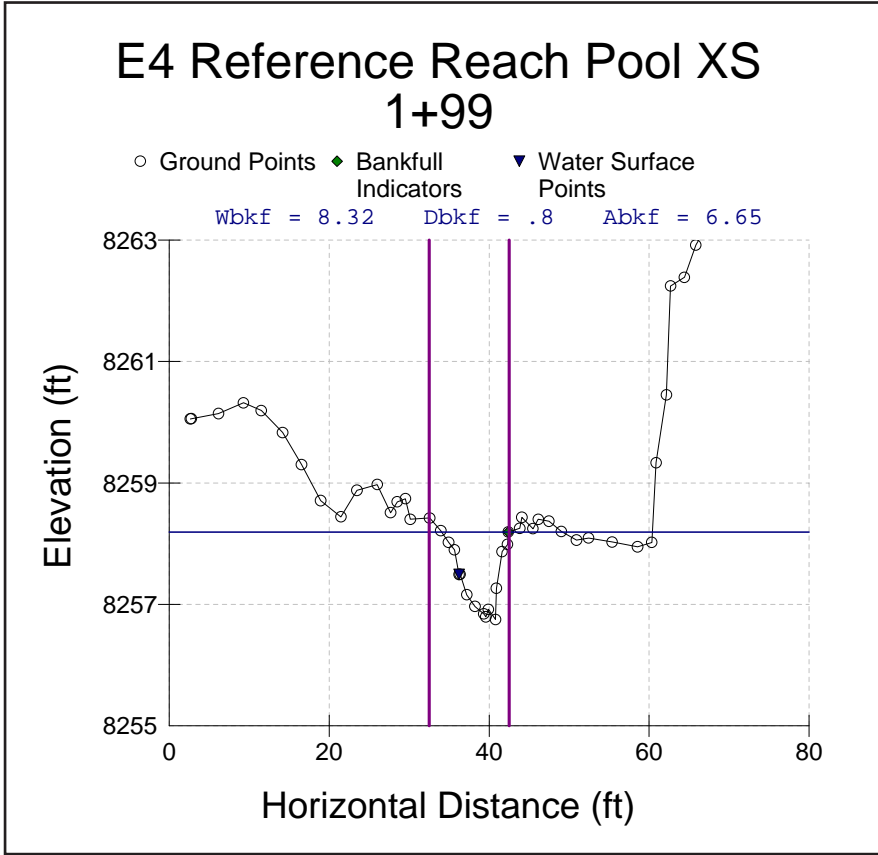
Riffle Cross-section 1+87 (graph generated from RIVERMorph™)



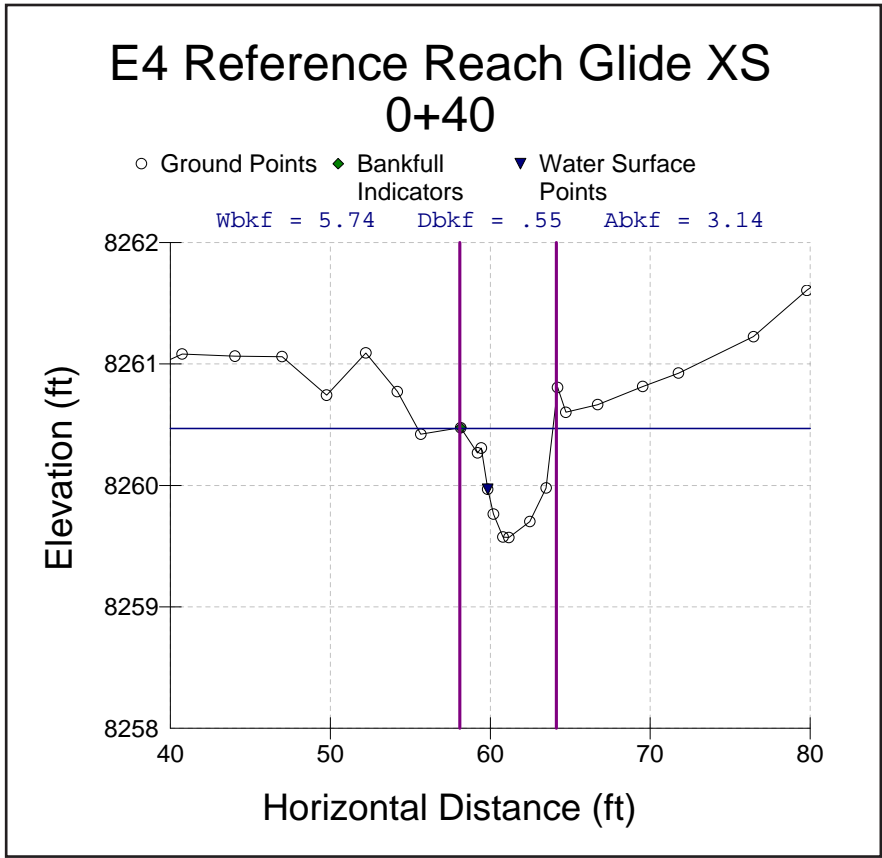
Representative Riffle Cross-section 2+42.5 (graph generated from RIVERMorph™)



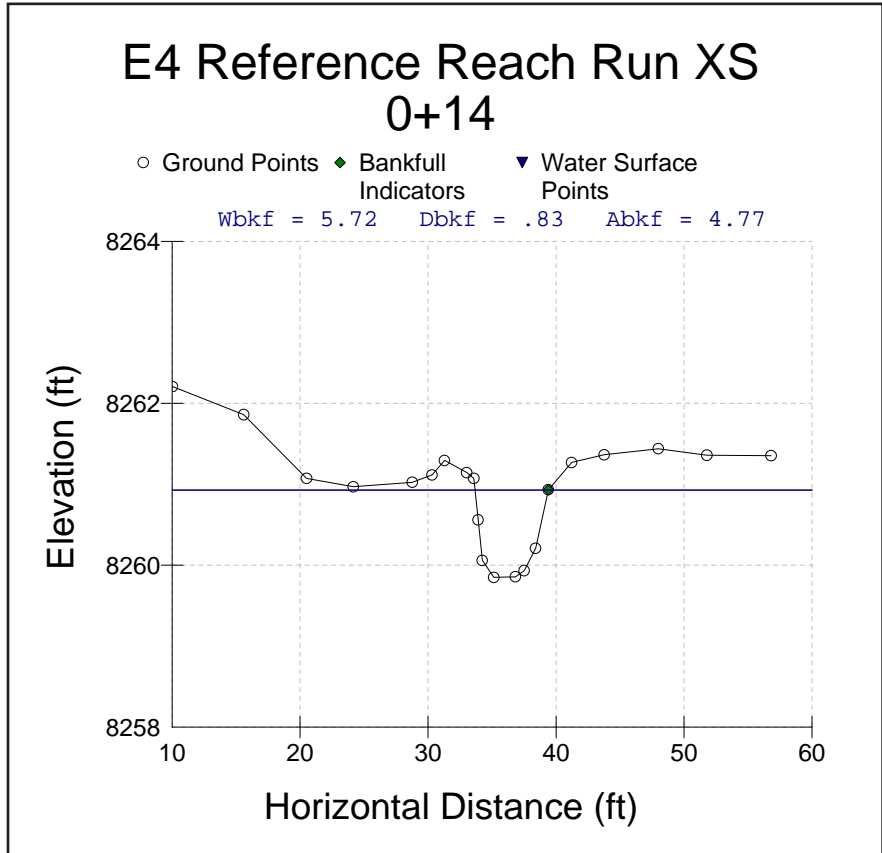
Pool Cross-section 1+26 (graph generated from RIVERMorph™)



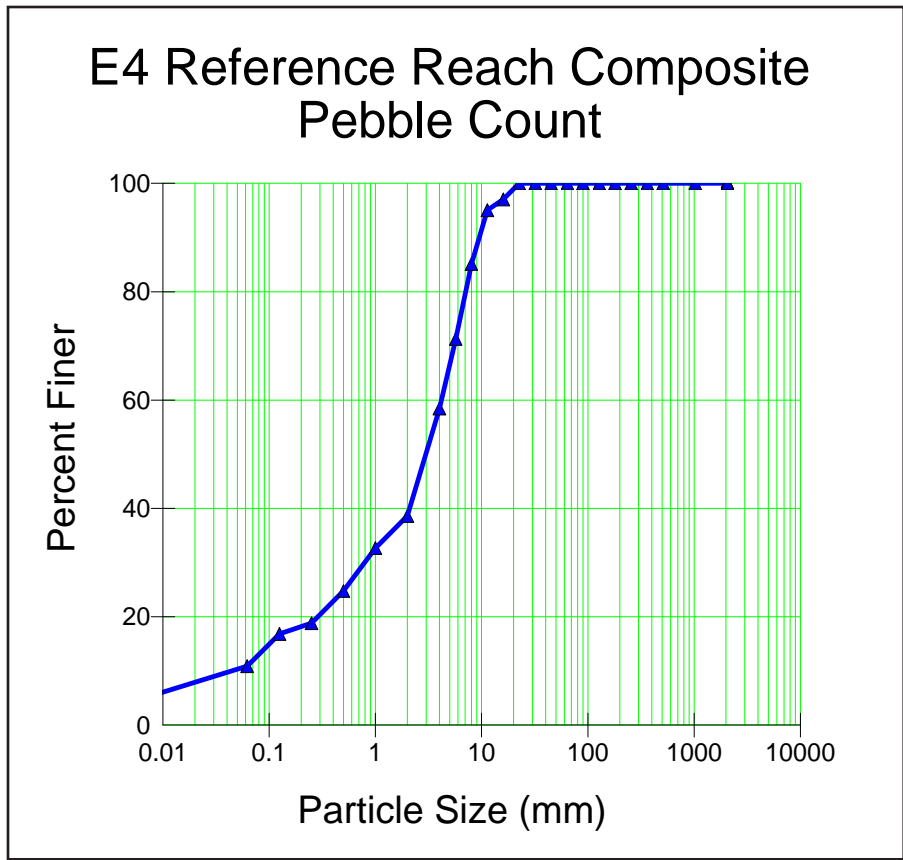
Pool Cross-section 1+99 (graph generated from RIVERMorph™)



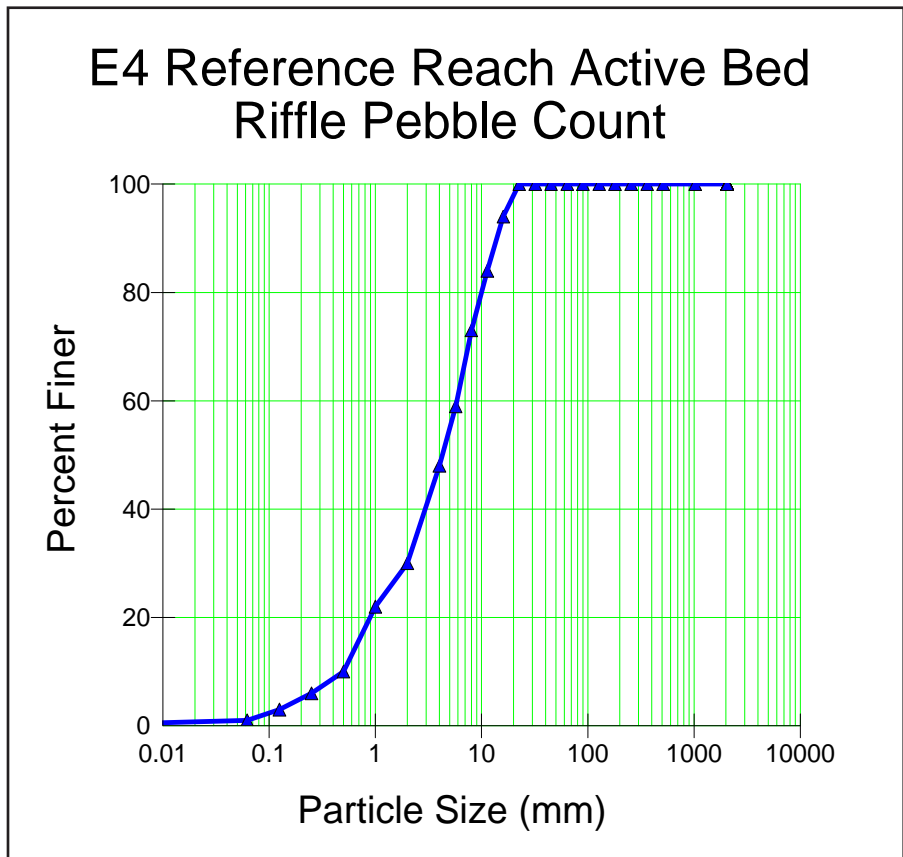
Glide Cross-section 0+40 (graph generated from RIVERMorph™)



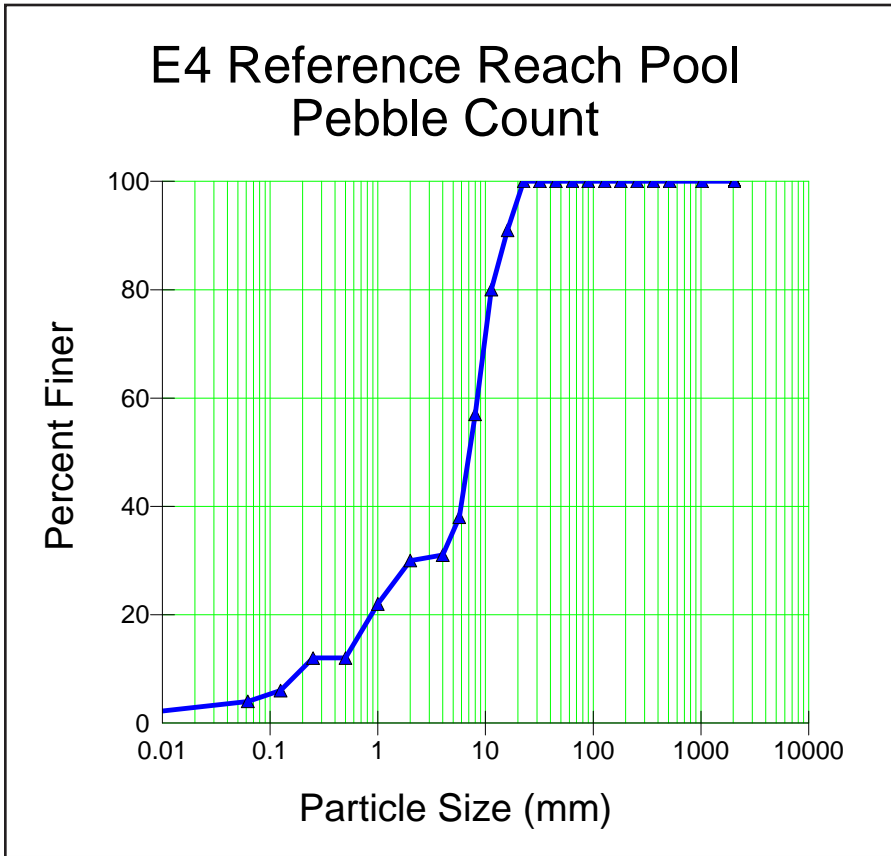
Run Cross-section 0+14 (graph generated from RIVERMorph™)



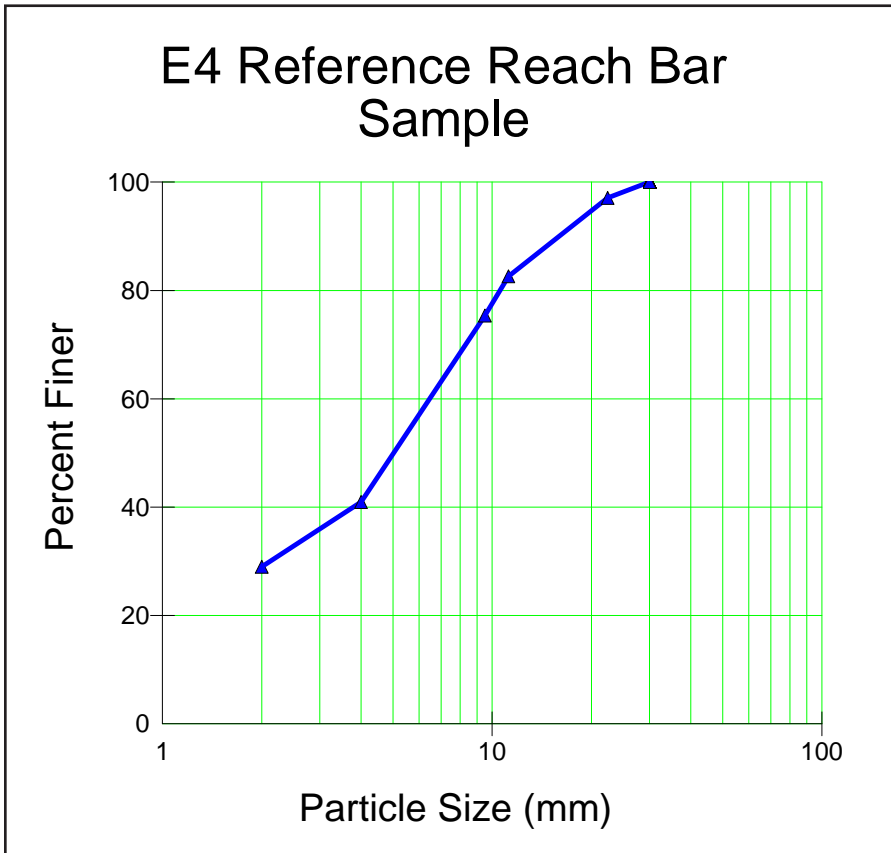
Composite Pebble Count (graph generated from RIVERMorph™)



Active Bed Riffle Pebble Count (graph generated from RIVERMorph™)



Pool Pebble Count (graph generated from RIVERMorph™)



Bar Sample (graph generated from RIVERMorph™)

# WARSSS Worksheets

## Velocity, Classification & Morphological Relations

Worksheet 5-2. Computations of velocity and bankfull discharge.

Bankfull VELOCITY & DISCHARGE Estimates					
Stream:	Trail Creek, E4 Reference Reach		Location:	Riffle XS 2+42.5, Pike N.F., CO	
Date:	8/22/2010	Stream Type:	E4	Valley Type:	X
Observers:	K. Wright & B. Kasun		HUC:	-- -- -- -- -- -- -- -- -- --	
INPUT VARIABLES			OUTPUT VARIABLES		
Bankfull Riffle Cross-Sectional AREA	4.17	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	0.73	$d_{bkf}$ (ft)
Bankfull Riffle WIDTH	5.73	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim (2 * d_{bkf}) + W_{bkf}$	7.19	$W_p$ (ft)
$D_{84}$ at Riffle	11.3	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.04	$D_{84}$ (ft)
Bankfull SLOPE	0.0101	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	0.58	R (ft)
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness $R(ft) / D_{84}(ft)$	15.64	$R / D_{84}$
Drainage Area	7.9	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.435	$u^*$ (ft/sec)
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$			4.27	ft / sec	17.81 cfs
2. Roughness Coefficient: a) Manning's n from Friction Factor / Relative Roughness (Figs. 5-7, 5-8) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.028$			3.72	ft / sec	15.52 cfs
2. Roughness Coefficient: b) Manning's n from Stream Type (Fig. 5-9) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.048$			3.42	ft / sec	14.26 cfs
2. Roughness Coefficient: c) Manning's n from Jarrett (USGS): $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ <small>Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for Stream Types A1, A2, A3, B1, B2, B3, C2 &amp; E3</small> $n = 0.074$			1.40	ft / sec	5.85 cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Limerinos			4.47	ft / sec	18.6 cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Darcy-Weisbach			4.32	ft / sec	18.0 cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q = \text{[ ]}$ year $u = Q / A$				ft / sec	cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$				ft / sec	cfs
Protrusion Height Options for the $D_{84}$ Term in the Relative Roughness Relation ( $R/D_{84}$ ) – Estimation Method 1					
Option 1. For sand-bed channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.					
Option 2. For boulder-dominated channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.					
Option 3. For bedrock-dominated channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.					
Option 4. For log-influenced channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.					

**Worksheet 5-3.** Level II stream classification.

<b>Stream:</b> Trail Creek, E4 Reference Reach	
<b>Basin:</b>	Drainage Area: <b>5056</b> acres <b>7.9</b> mi <sup>2</sup>
<b>Location:</b> Pike National Forest, Colorado	
<b>Twp.&amp;Rge:</b>	Sec.&Qtr.:
<b>Cross-Section Monuments (Lat./Long.):</b> Riffle XS 2+42.5	Date: <b>8/22/2010</b>
<b>Observers:</b> K. Wright & B. Kasun	Valley Type: <b>X</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>5.73</b> ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A_{bkf} / W_{bkf}$ ).	<b>0.73</b> ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>4.17</b> ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>7.8</b> ft/ft
<b>Maximum DEPTH (<math>d_{max}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>0.95</b> ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mkt}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>35.78</b> ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>6.24</b> ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the median or dominant diameter of channel materials, as sampled proportionately from the channel surface, between the bankfull stage and Thalweg elevations.	<b>3</b> mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.0101</b> ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope ( $S_{val} / S$ ).	<b>1.23</b>

<div style="border: 1px solid black; padding: 5px; display: inline-block;">Stream Type</div>	<div style="border: 1px solid black; padding: 10px; display: inline-block; background-color: #e0f0ff;">E4</div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;">See Classification Key (Figure 2-14)</div>
--	---	---

**Worksheet 5-4a.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, E4 Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>							
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/23/2010</b>		Valley Type: <b>X</b>		Stream Type: <b>E4</b>			
<b>River Reach Dimension Summary Data.....1</b>									
<b>Riffle Dimensions* ** *</b>	<b>Riffle Dimensions* ** *</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Riffle Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Riffle Width ( $W_{bkt}$ )	5.8	3.9	7.8	ft	Riffle Cross-Sectional Area ( $A_{bkt}$ ) (ft <sup>2</sup> )	3.8	2.9	4.7
	Mean Riffle Depth ( $d_{bkt}$ )	0.67	0.60	0.75	ft	Riffle Width/Depth Ratio ( $W_{bkt} / d_{bkt}$ )	8.9	5.2	13.0
	Maximum Riffle Depth ( $d_{max}$ )	1.03	0.83	1.34	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	1.526	1.301	1.787
	Width of Flood-Prone Area ( $W_{fpa}$ )	41.2	29.6	56.6	ft	Entrenchment Ratio ( $W_{fpa} / W_{bkt}$ )	7.8	5.2	14.4
	Riffle Inner Berm Width ( $W_{ib}$ )	2.8	2.0	3.7	ft	Riffle Inner Berm Width to Riffle Width ( $W_{ib} / W_{bkt}$ )	0.500	0.348	0.642
	Riffle Inner Berm Depth ( $d_{ib}$ )	0.15	0.14	0.17	ft	Riffle Inner Berm Depth to Mean Depth ( $d_{ib} / d_{bkt}$ )	0.231	0.227	0.233
	Riffle Inner Berm Area ( $A_{ib}$ )	0.4	0.4	0.5	ft <sup>2</sup>	Riffle Inner Berm Area to Riffle Area ( $A_{ib} / A_{bkt}$ )	0.116	0.081	0.147
	Riffle Inner Berm W/D Ratio ( $W_{ib} / d_{ib}$ )	19.1	11.8	26.2					
<b>Pool Dimensions* ** *</b>	<b>Pool Dimensions* ** *</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Pool Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Pool Width ( $W_{bkfp}$ )	8.8	8.3	9.3	ft	Pool Width to Riffle Width ( $W_{bkfp} / W_{bkt}$ )	1.520	1.437	1.603
	Mean Pool Depth ( $d_{bkfp}$ )	0.82	0.80	0.83	ft	Mean Pool Depth to Mean Riffle Depth ( $d_{bkfp} / d_{bkt}$ )	1.216	1.194	1.239
	Pool Cross-Sectional Area ( $A_{bkfp}$ )	7.2	6.7	7.7	ft	Pool Area to Riffle Area ( $A_{bkfp} / A_{bkt}$ )	1.884	1.751	2.017
	Maximum Pool Depth ( $d_{maxp}$ )	1.59	1.44	1.73	ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	2.366	2.149	2.582
	Pool Inner Berm Width ( $W_{ibp}$ )	4.4	3.7	5.1	ft	Pool Inner Berm Width to Pool Width ( $W_{ibp} / W_{bkfp}$ )	0.496	0.442	0.550
	Pool Inner Berm Depth ( $d_{ibp}$ )	0.38	0.24	0.51	ft	Pool Inner Berm Depth to Pool Depth ( $d_{ibp} / d_{bkfp}$ )	0.457	0.300	0.614
	Pool Inner Berm Area ( $A_{ibp}$ )	1.7	0.9	2.6	ft <sup>2</sup>	Pool Inner Berm Area to Pool Area ( $A_{ibp} / A_{bkfp}$ )	0.234	0.131	0.337
	Point Bar Slope ( $S_{pb}$ )	0.322	0.276	0.368	ft/ft	Pool Inner Berm Width/Depth Ratio ( $W_{ibp} / d_{ibp}$ )	12.7	10.0	15.3
<b>Run Dimensions*</b>	<b>Run Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Run Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Run Width ( $W_{bktr}$ )	5.7			ft	Run Width to Riffle Width ( $W_{bktr} / W_{bkt}$ )	0.988		
	Mean Run Depth ( $d_{bktr}$ )	0.83			ft	Mean Run Depth to Mean Riffle Depth ( $d_{bktr} / d_{bkt}$ )	1.239		
	Run Cross-Sectional Area ( $A_{bktr}$ )	4.8			ft	Run Area to Riffle Area ( $A_{bktr} / A_{bkt}$ )	1.256		
	Maximum Run Depth ( $d_{maxr}$ )	1.08			ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )	1.612		
	Run Width/Depth Ratio ( $W_{bktr} / d_{bktr}$ )	6.9			ft				
<b>Glide Dimensions*</b>	<b>Glide Dimensions*</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Glide Dimensions &amp; Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Glide Width ( $W_{bkfg}$ )	5.7			ft	Glide Width to Riffle Width ( $W_{bkfg} / W_{bkt}$ )	0.991		
	Mean Glide Depth ( $d_{bkfg}$ )	0.55			ft	Mean Glide Depth to Mean Riffle Depth ( $d_{bkfg} / d_{bkt}$ )	0.821		
	Glide Cross-Sectional Area ( $A_{bkfg}$ )	10.4			ft	Glide Area to Riffle Area ( $A_{bkfg} / A_{bkt}$ )	2.749		
	Maximum Glide Depth ( $d_{maxg}$ )	0.90			ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )	1.343		
	Glide Width/Depth Ratio ( $W_{bkfg} / d_{bkfg}$ )	10.4			ft/ft	Glide Inner Berm Width/Depth Ratio ( $W_{ibg} / d_{ibg}$ )	14.08		
	Glide Inner Berm Width ( $W_{ibg}$ )	3.7			ft	Glide Inner Berm Width to Glide Width ( $W_{ibg} / W_{bkfg}$ )	0.638		
	Glide Inner Berm Depth ( $d_{ibg}$ )	0.26			ft	Glide Inner Berm Depth to Glide Depth ( $d_{ibg} / d_{bkfg}$ )	0.260		
Glide Inner Berm Area ( $A_{ibg}$ )	1.0			ft <sup>2</sup>	Glide Inner Berm Area to Glide Area ( $A_{ibg} / A_{bkfg}$ )	0.309			
<b>Step**</b>	<b>Step Dimensions**</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>		<b>Step Dimensionless Ratios****</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>
	Step Width ( $W_{bkfs}$ )				ft	Step Width to Riffle Width ( $W_{bkfs} / W_{bkt}$ )			
	Mean Step Depth ( $d_{bkfs}$ )				ft	Mean Step Depth to Riffle Depth ( $d_{bkfs} / d_{bkt}$ )			
	Step Cross-Sectional Area ( $A_{bkfs}$ )				ft	Step Area to Riffle Area ( $A_{bkfs} / A_{bkt}$ )			
	Maximum Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )			
	Step Width/Depth Ratio ( $W_{bkfs} / d_{bkfs}$ )								



**Worksheet 5-4b.** Morphological relations (modified from Rosgen, 2006/2009).

Stream: <b>Trail Creek, E4 Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>							
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/23/2010</b>	Valley Type: <b>X</b>						
		Stream Type: <b>E4</b>							
<b>River Reach Summary Data.....2</b>									
<b>Hydraulics</b>	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $U_{bkt}$ )	<b>4.3</b>	ft/sec	Estimation Method	<b>Darcy-Weisbach</b>				
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )	<b>18.0</b>	cfs	Drainage Area	<b>7.9</b> mi <sup>2</sup>				
<b>Channel Pattern</b>	<b>Geometry</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Dimensionless Geometry Ratios</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	
	Linear Wavelength ( $\lambda$ )	<b>31.3</b>	<b>28.9</b>	<b>36.3</b>	ft	Linear Wavelength to Riffle Width ( $\lambda / W_{bkt}$ )	<b>5.40</b>	<b>4.99</b>	<b>6.27</b>
	Stream Meander Length ( $L_m$ )	<b>35.2</b>	<b>29.5</b>	<b>42.1</b>	ft	Stream Meander Length Ratio ( $L_m / W_{bkt}$ )	<b>6.08</b>	<b>5.09</b>	<b>7.27</b>
	Radius of Curvature ( $R_c$ )	<b>17.9</b>	<b>10.2</b>	<b>27.8</b>	ft	Radius of Curvature to Riffle Width ( $R_c / W_{bkt}$ )	<b>3.09</b>	<b>1.76</b>	<b>4.80</b>
	Belt Width ( $W_{bit}$ )	<b>19.3</b>	<b>16.0</b>	<b>22.0</b>	ft	Meander Width Ratio ( $W_{bit} / W_{bkt}$ )	<b>3.33</b>	<b>2.76</b>	<b>3.80</b>
	Arc Length ( $L_a$ )	<b>15.6</b>	<b>7.0</b>	<b>25.7</b>	ft	Arc Length to Riffle Width ( $L_a / W_{bkt}$ )	<b>2.69</b>	<b>1.21</b>	<b>4.44</b>
	Riffle Length ( $L_r$ )	<b>13.9</b>	<b>12.3</b>	<b>16.9</b>	ft	Riffle Length to Riffle Width ( $L_r / W_{bkt}$ )	<b>2.40</b>	<b>2.12</b>	<b>2.92</b>
	Individual Pool Length ( $L_p$ )	<b>8.3</b>	<b>5.4</b>	<b>14.6</b>	ft	Individual Pool Length to Riffle Width ( $L_p / W_{bkt}$ )	<b>1.42</b>	<b>0.94</b>	<b>2.52</b>
Pool to Pool Spacing ( $P_s$ )	<b>31.6</b>	<b>12.3</b>	<b>48.4</b>	ft	Pool to Pool Spacing to Riffle Width ( $P_s / W_{bkt}$ )	<b>5.46</b>	<b>2.12</b>	<b>8.36</b>	
<b>Channel Profile</b>	Valley Slope ( $S_{val}$ )	<b>0.0124</b>	ft/ft	Average Water Surface Slope (S)	<b>0.0101</b>	ft/ft	Sinuosity ( $S_{val} / S$ )	<b>1.23</b>	
	Stream Length (SL)	<b>261.5</b>	ft	Valley Length (VL)	<b>212.7</b>	ft	Sinuosity (SL / VL)	<b>1.23</b>	
	Low Bank Height (LBH)	start: <b>0.83</b> ft end: <b>1.71</b> ft		Max Bankfull Depth ( $d_{max}$ )	start: <b>0.83</b> ft end: <b>1.71</b> ft		Bank-Height Ratio (BHR) (LBH / $d_{max}$ )	start: <b>1.0</b> end: <b>1.0</b>	
	<b>Facet Slopes</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Dimensionless Facet Slope Ratios</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	
	Riffle Slope ( $S_{rit}$ )	<b>0.0230</b>	<b>0.0140</b>	<b>0.0300</b>	ft/ft	Riffle Slope to Average Water Surface Slope ( $S_{rit} / S$ )	<b>2.2727</b>	<b>1.3834</b>	<b>2.9644</b>
	Run Slope ( $S_{run}$ )	<b>0.0550</b>	<b>0.0340</b>	<b>0.0720</b>	ft/ft	Run Slope to Average Water Surface Slope ( $S_{run} / S$ )	<b>5.4348</b>	<b>3.3597</b>	<b>7.1146</b>
	Pool Slope ( $S_p$ )	<b>0.0018</b>	<b>0.0010</b>	<b>0.0070</b>	ft/ft	Pool Slope to Average Water Surface Slope ( $S_p / S$ )	<b>0.1729</b>	<b>0.0988</b>	<b>0.6917</b>
	Glide Slope ( $S_g$ )	<b>0.0050</b>	<b>0.0010</b>	<b>0.0080</b>	ft/ft	Glide Slope to Average Water Surface Slope ( $S_g / S$ )	<b>0.4941</b>	<b>0.0988</b>	<b>0.7905</b>
	Step Slope ( $S_s$ )				ft/ft	Step Slope to Average Water Surface Slope ( $S_s / S$ )			
	<b>Max Depths<sup>a</sup></b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Dimensionless Depth Ratios</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	
	Max Riffle Depth ( $d_{max}$ )	<b>1.02</b>	<b>0.95</b>	<b>1.19</b>	ft	Max Riffle Depth to Mean Riffle Depth ( $d_{max} / d_{bkt}$ )	<b>1.522</b>	<b>1.418</b>	<b>1.776</b>
	Max Run Depth ( $d_{maxr}$ )	<b>1.08</b>			ft	Max Run Depth to Mean Riffle Depth ( $d_{maxr} / d_{bkt}$ )	<b>1.612</b>		
	Max Pool Depth ( $d_{maxp}$ )	<b>1.74</b>	<b>1.44</b>	<b>2.94</b>	ft	Max Pool Depth to Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )	<b>2.597</b>	<b>2.149</b>	<b>4.388</b>
	Max Glide Depth ( $d_{maxg}$ )	<b>0.97</b>			ft	Max Glide Depth to Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )	<b>1.448</b>		
Max Step Depth ( $d_{maxs}$ )				ft	Max Step Depth to Mean Riffle Depth ( $d_{maxs} / d_{bkt}$ )				
<b>Channel Materials</b>		<b>Reach<sup>b</sup></b>	<b>Riffle<sup>c</sup></b>	<b>Bar</b>	<b>Reach<sup>b</sup></b>	<b>Riffle<sup>c</sup></b>	<b>Bar</b>	<b>Protrusion Height<sup>d</sup></b>	
	% Silt/Clay	<b>11</b>	<b>1</b>	<b>0</b>	$D_{16}$	<b>0.1</b>	<b>0.8</b>	<b>0.0</b>	mm
	% Sand	<b>28</b>	<b>29</b>	<b>29</b>	$D_{35}$	<b>1.4</b>	<b>2.6</b>	<b>3.0</b>	mm
	% Gravel	<b>61</b>	<b>70</b>	<b>71</b>	$D_{50}$	<b>3.2</b>	<b>4.3</b>	<b>5.5</b>	mm
	% Cobble				$D_{84}$	<b>7.8</b>	<b>11.3</b>	<b>12.3</b>	mm
	% Boulder				$D_{95}$	<b>11.3</b>	<b>17.1</b>	<b>20.8</b>	mm
	% Bedrock				$D_{100}$	<b>22.6</b>	<b>22.6</b>	<b>30.0</b>	mm

<sup>a</sup> Min, max & mean depths are measured from Thalweg to bankfull at mid-point of feature for riffles and runs, the deepest part of pools, & at the tail-out of glides.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

## Stability Indices


**Worksheet 5-6.** Riparian vegetation.

Riparian Vegetation								
Stream: <b>Trail Creek, E4 Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>						
Observers: <b>K. Wright &amp; B. Kasun</b>		Reference reach <input checked="" type="checkbox"/>	Disturbed (impacted reach) <input type="checkbox"/>	Date: <b>8/22/10</b>				
Existing species composition: <b>Willow, Carex, Ponderosa Pine, Spruce, Grasses</b>		Potential species composition: <b>Same as Existing Composition but without Invasives</b>						
	Riparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition			
<b>1. Overstory</b>	Canopy layer	<b>85%</b>	<b>60%</b>	<b>Willow</b>	<b>50%</b>			
				<b>Carex</b>	<b>40%</b>			
				<b>Conifers</b>	<b>10%</b>			
				<b>100%</b>				
<b>2. Understory</b>	Shrub layer	<b>25%</b>	<b>25%</b>	<b>Willow</b>	<b>95%</b>			
				<b>Grasses</b>	<b>5%</b>			
				<b>100%</b>				
<b>3. Ground level</b>	Herbaceous	<b>12%</b>	<b>12%</b>	<b>Carex</b>	<b>50%</b>			
				<b>Juncus</b>	<b>25%</b>			
				<b>Annuals</b>	<b>20%</b>			
				<b>Thistle</b>	<b>5%</b>			
				<b>100%</b>				
<b>3. Ground level</b>	Leaf or needle litter	<b>2%</b>	<b>2%</b>	<b>Remarks:</b> Condition, vigor and/or usage of existing reach: <b>Excellent riparian vegetative protection; needs some eradication of invasives.</b>				
	Bare ground	<b>1%</b>	<b>1%</b>					
						<b>100%</b>		
*Based on crown closure.		**Based on basal area to surface area.		<b>Column total = 100%</b>				

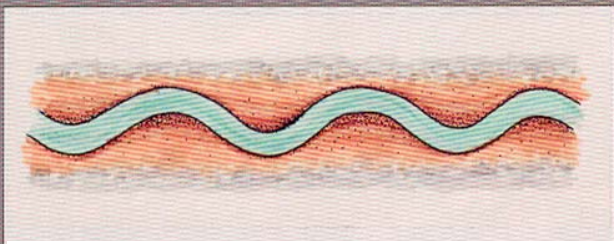

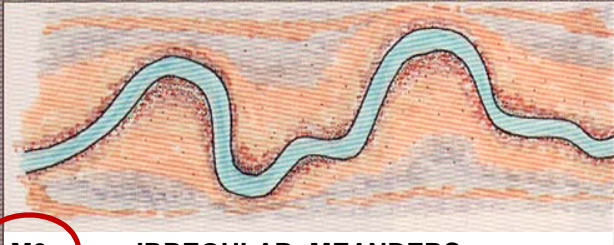
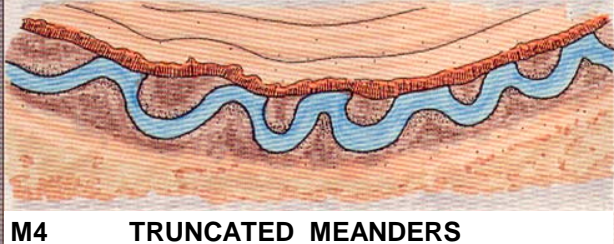

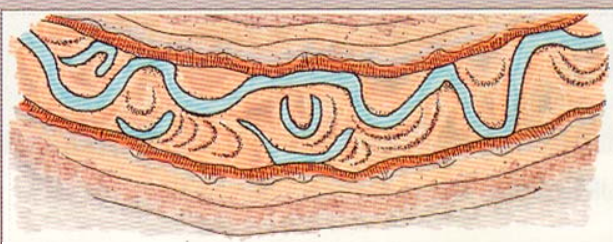
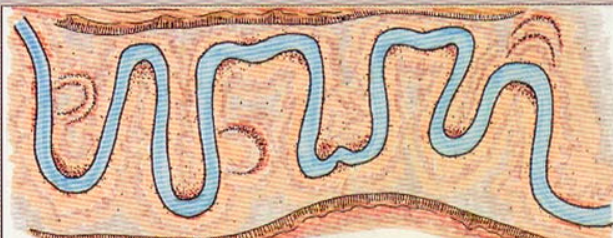

**Worksheet 5-7.** Flow regime.

<b>FLOW REGIME</b>								
Stream: <b>Trail Creek, E4 Reference</b>			Location: <b>Pike National Forest, Colorado</b>					
Observers: <b>K. Wright &amp; B. Kasun</b>						Date: <b>8/22/2010</b>		
List ALL COMBINATIONS that APPLY.....☞			P1	P2	P8			
<b>General Category</b>								
<b>E</b>	Ephemeral stream channels: Flows only in response to precipitation							
<b>S</b>	Subterranean stream channel: Flows parallel to and near the surface for various seasons - a sub-surface flow that follows the stream bed.							
<b>I</b>	Intermittent stream channel: Surface water flows discontinuously along its length. Often associated with sporadic and/or seasonal flows and also with Karst (limestone) geology where losing/gaining reaches create flows that disappear then reappear farther downstream.							
<b>P</b>	Perennial stream channels: Surface water persists yearlong.							
<b>Specific Category</b>								
<b>1</b>	Seasonal variation in streamflow dominated primarily by snowmelt runoff.							
<b>2</b>	Seasonal variation in streamflow dominated primarily by stormflow runoff.							
<b>3</b>	Uniform stage and associated streamflow due to spring-fed condition, backwater, etc.							
<b>4</b>	Streamflow regulated by glacial melt.							
<b>5</b>	Ice flows/ice torrents from ice dam breaches.							
<b>6</b>	Alternating flow/backwater due to tidal influence.							
<b>7</b>	Regulated streamflow due to diversions, dam release, dewatering, etc.							
<b>8</b>	Altered due to development, such as urban streams, cut-over watersheds or vegetation conversions (forested to grassland) that change flow response to precipitation events.							
<b>9</b>	Rain-on-snow generated runoff.							

**Worksheet 5-8.** Stream order & stream size.

<b>Stream Size and Order</b>			
Stream:	<b>Trail Creek, E4 Reference Reach</b>		
Location:	<b>Pike National Forest, Colorado</b>		
Observers:	<b>K. Wright &amp; B. Kasun</b>		
Date:	<b>8/22/2010</b>		
<b>Stream Size Category and Order</b> 			<b>S-3(3)</b>
Category	STREAM SIZE: Bankfull width		Check (✓) appropriate category
	meters	feet	
S-1	0.305	<1	<input type="checkbox"/>
S-2	0.3 – 1.5	1 – 5	<input type="checkbox"/>
<b>S-3</b>	<b>1.5 – 4.6</b>	<b>5 – 15</b>	<input checked="" type="checkbox"/>
S-4	4.6 – 9	15 – 30	<input type="checkbox"/>
S-5	9 – 15	30 – 50	<input type="checkbox"/>
S-6	15 – 22.8	50 – 75	<input type="checkbox"/>
S-7	22.8 – 30.5	75 – 100	<input type="checkbox"/>
S-8	30.5 – 46	100 – 150	<input type="checkbox"/>
S-9	46 – 76	150 – 250	<input type="checkbox"/>
S-10	76 – 107	250 – 350	<input type="checkbox"/>
S-11	107 – 150	350 – 500	<input type="checkbox"/>
S-12	150 – 305	500 – 1000	<input type="checkbox"/>
S-13	>305	>1000	<input type="checkbox"/>
<b>Stream Order</b>			
Add categories in parenthesis for specific stream order of reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).			

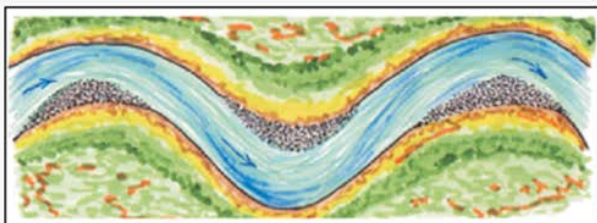

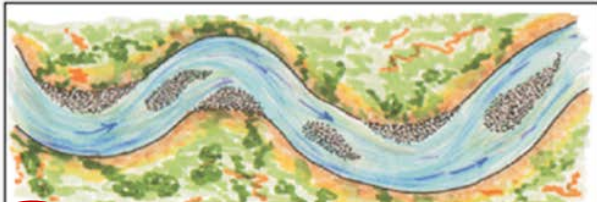
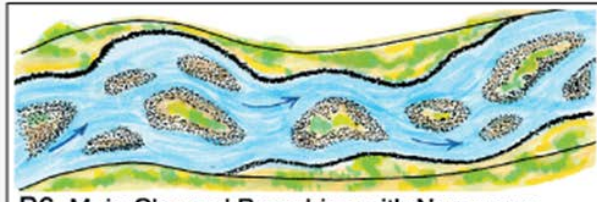
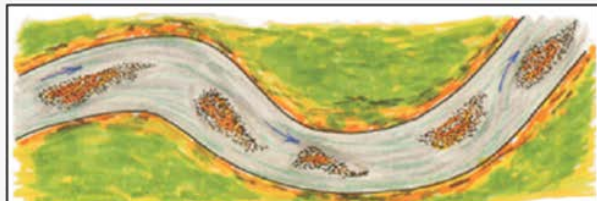
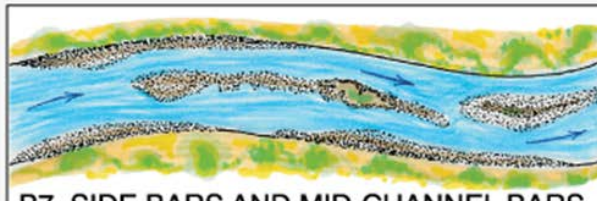

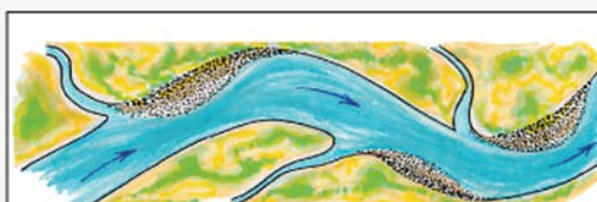
Worksheet 5-9. Meander patterns.

<b>Meander Patterns</b>					
Stream: <b>Trail Creek, E4 Reference Reach</b>			Location: <b>Pike National Forest, CO</b>		
Observers: <b>K. Wright &amp; B. Kasun</b>			Date: <b>8/22/2010</b>		
List ALL CATEGORIES that APPLY		<b>M3</b>			
<i>Various Meander Pattern variables modified from Galay et al. (1973)</i>					
					
<b>M1</b> <b>REGULAR MEANDERS</b>					
					
<b>M2</b> <b>TORTUOUS MEANDERS</b>					
					
<b>M3</b> <b>IRREGULAR MEANDERS</b>					
					
<b>M4</b> <b>TRUNCATED MEANDERS</b>					
					
			<b>M5</b> <b>UNCONFINED MEANDER SCROLLS</b>		
					
			<b>M6</b> <b>CONFINED MEANDER SCROLLS</b>		
					
			<b>M7</b> <b>DISTORTED MEANDER LOOPS</b>		
					
			<b>M8</b> <b>IRREGULAR MEANDERS with oxbows and</b>		

**Worksheet 5-10.** Depositional patterns.

<b>Depositional Patterns</b>					
Stream:	Trail Creek, E4 Reference Reach	Location:	Pike National Forest, Colorado		
Observers:	K. Wright & B. Kasun	Date:	8/22/2010		
List ALL CATEGORIES that APPLY		B2			

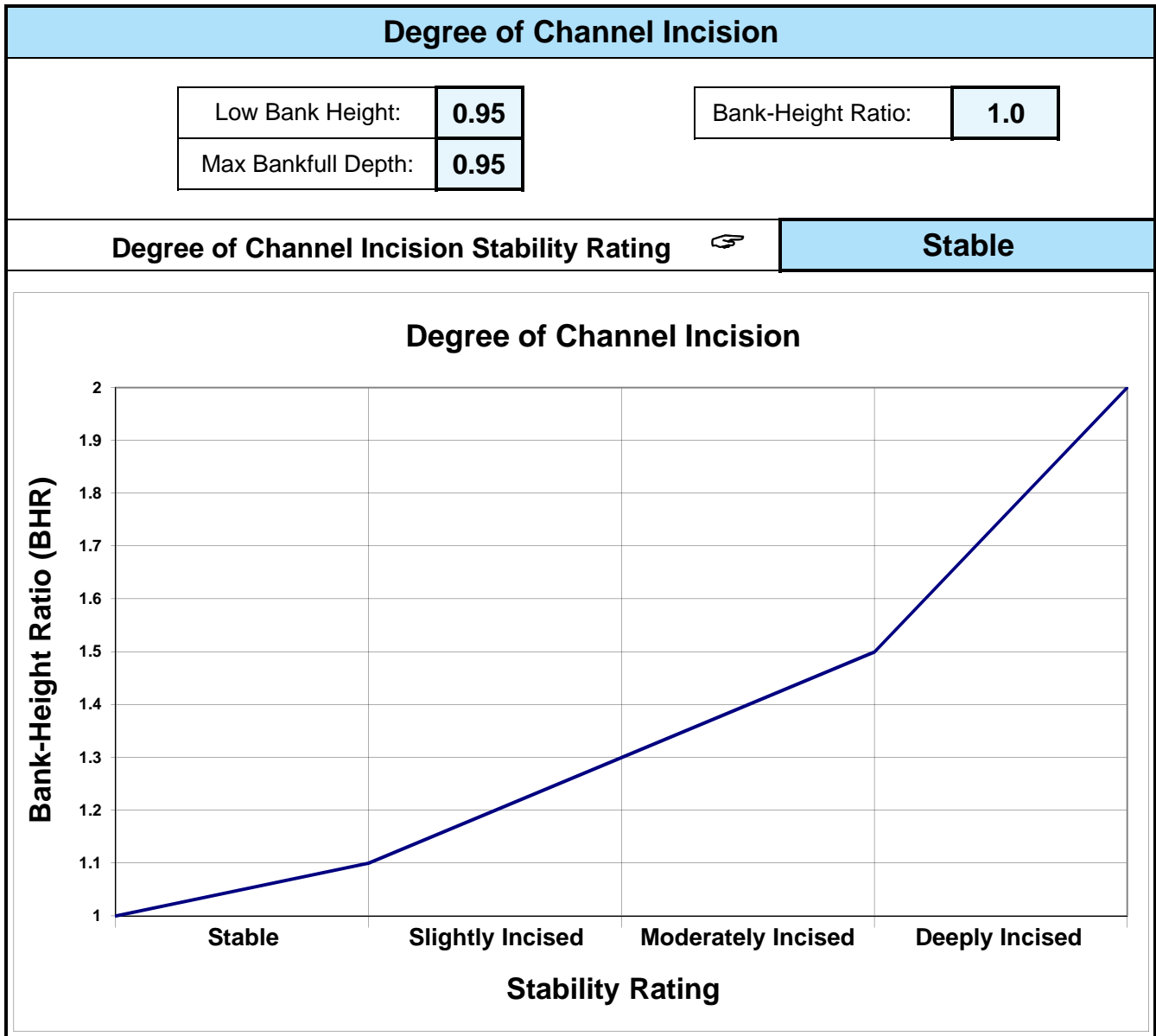
*Various Depositional Features modified from Galay et al. (1973)*

 <p><b>B1</b> POINT BARS</p>	 <p><b>B5</b> DIAGONAL BARS</p>
 <p><b>B2</b> POINT BARS with Few MID-CHANNEL BARS</p>	 <p><b>B6</b> Main Channel Branching with Numerous MID-CHANNEL BARS and Islands</p>
 <p><b>B3</b> NUMEROUS MID-CHANNEL BARS</p>	 <p><b>B7</b> SIDE BARS AND MID-CHANNEL BARS with Length Exceeding 2 to 3 Channel Widths</p>
 <p><b>B4</b> SIDE BARS</p>	 <p><b>B8</b> DELTA BARS</p>

## Worksheet 5-11. Channel blockages.

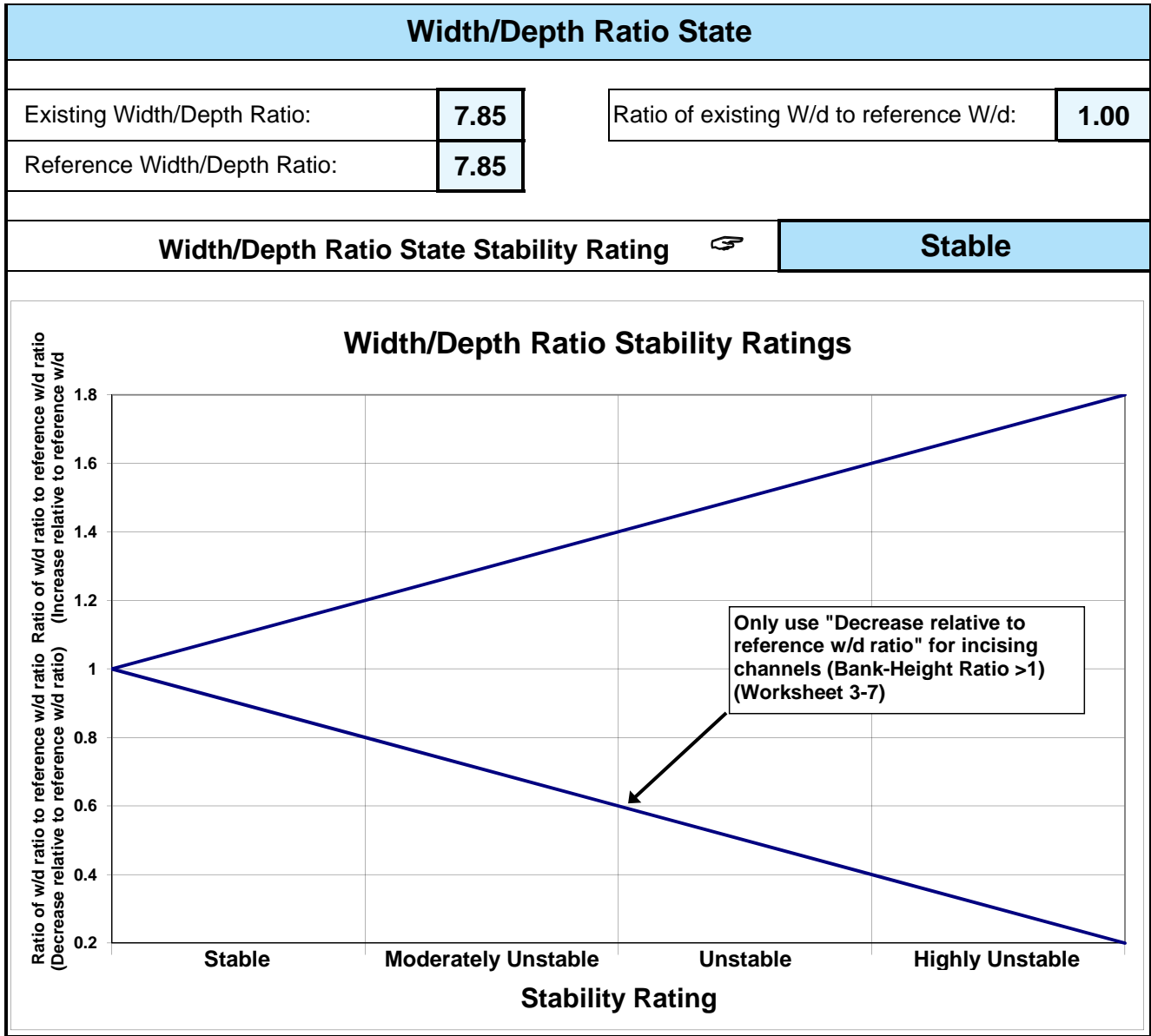
Channel Blockages		
Stream: <b>Trail Creek, E4 Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/22/2010</b>
Description/extent	Materials that upon placement into the active channel or flood-prone area may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (✓) all that apply
<b>D1</b> None	Minor amounts of small, floatable material.	<input checked="" type="checkbox"/>
<b>D2</b> Infrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	<input type="checkbox"/>
<b>D3</b> Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	<input type="checkbox"/>
<b>D4</b> Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	<input type="checkbox"/>
<b>D5</b> Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	<input type="checkbox"/>
<b>D6</b> Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	<input type="checkbox"/>
<b>D7</b> Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	<input type="checkbox"/>
<b>D8</b> Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	<input type="checkbox"/>
<b>D9</b> Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avulsion, aggradation and degradation.	<input type="checkbox"/>
<b>D10</b> Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	<input type="checkbox"/>

**Worksheet 5-12.** Degree of channel incision.

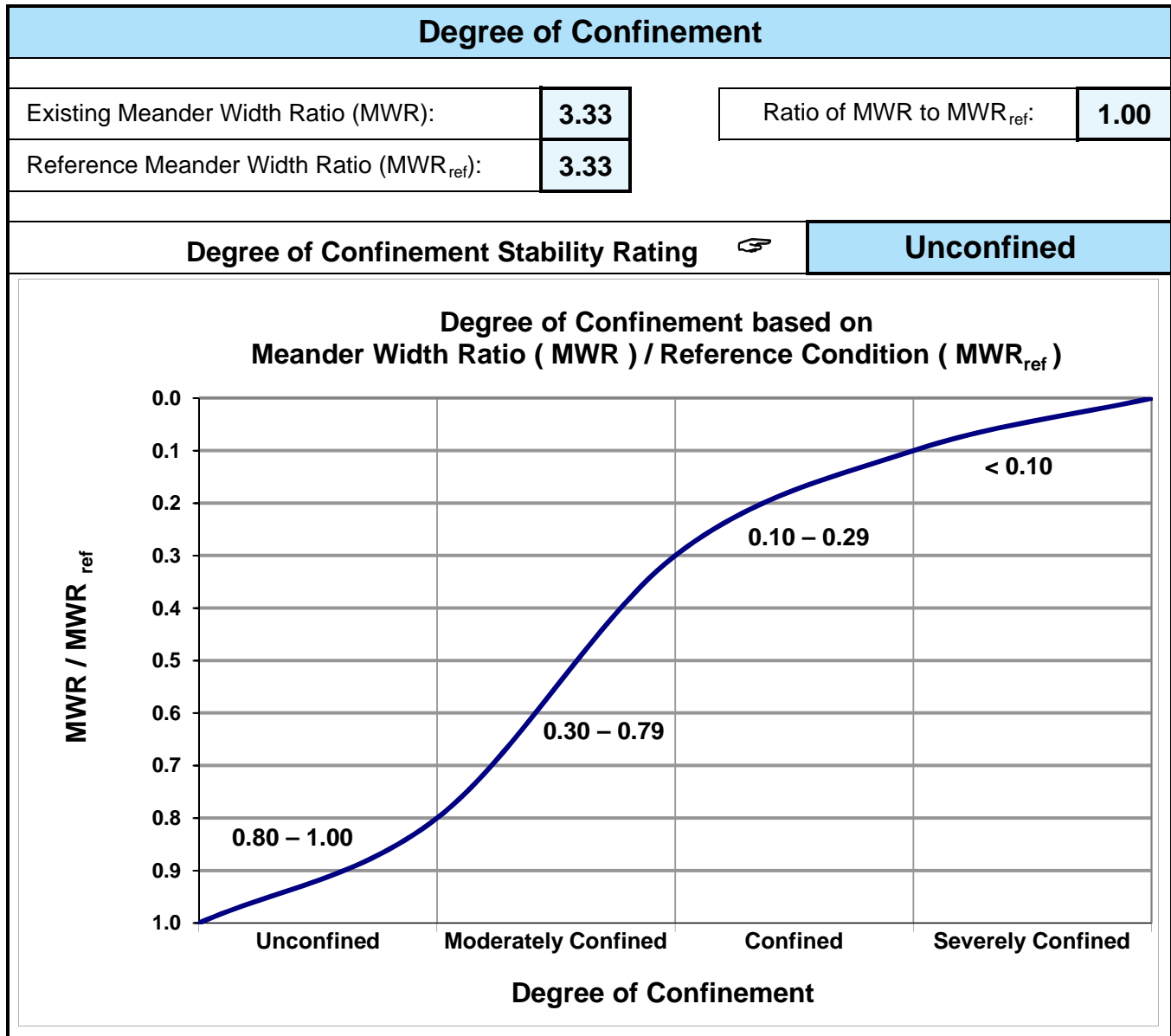




Worksheet 5-13. Width/depth ratio state.



**Worksheet 5-14.** Degree of channel confinement (lateral containment).



Worksheet 5-15. Pfankuch channel stability rating.

Stream: Trail Creek, E4 Reference Reach		Location: Pike National Forest, CO			Valley Type: X			Observers: K. Wright & B. Kasun			Date: 8/22/2010																										
Loca-tion	Key Category	Excellent Description	Rating	Good Description	Rating	Fair Description	Rating	Poor Description	Rating																												
Upper banks	1	Landform slope	Bank slope gradient <30%.	2	Bank slope gradient 30–40%.	4	Bank slope gradient 40–60%.	6	Bank slope gradient > 60%.	8																											
	2	Mass erosion	No evidence of past or future mass erosion.	3	Infrequent. Mostly healed over. Low future potential.	6	Frequent or large, causing sediment nearly yearlong.	9	Frequent or large, causing sediment nearly yearlong OR imminent danger of same.	12																											
	3	Debris jam potential	Essentially absent from immediate channel area.	2	Present, but mostly small twigs and limbs.	4	Moderate to heavy amounts, mostly larger sizes.	6	Moderate to heavy amounts, predominantly larger sizes.	8																											
	4	Vegetative bank protection	> 90% plant density. Vigor and variety suggest a deep, dense soil-binding root mass.	3	70–90% density. Fewer species or less vigor suggest less dense or deep root mass.	6	50–70% density. Lower vigor and fewer species from a shallow, discontinuous root mass.	9	<50% density plus fewer species and less vigor indicating poor, discontinuous and shallow root mass.	12																											
Lower banks	5	Channel capacity	Bank heights sufficient to contain the bankfull stage. Width/depth ratio departure from reference width/depth ratio = 1.0. Bank-Height Ratio (BHR) = 1.0.	1	Bankfull stage is contained within banks. Width/depth ratio departure from reference width/depth ratio = 1.0–1.2. Bank-Height Ratio (BHR) = 1.0–1.1.	2	Bankfull stage is not contained. Width/depth ratio departure from reference width/depth ratio = 1.2–1.4. Bank-Height Ratio (BHR) = 1.1–1.3.	3	Bankfull stage is not contained; over-bank flows are common with flows less than bankfull. Width/depth ratio departure from reference width/depth ratio > 1.4. Bank-Height Ratio (BHR) > 1.3.	4																											
	6	Bank rock content	> 65% with large angular boulders. 12"+ common.	2	40–65%. Mostly boulders and small cobbles 6–12".	4	20–40%. Most in the 3–6" diameter class.	6	<20% rock fragments of gravel sizes, 1–3" or less.	8																											
	7	Obstructions to flow	Rocks and logs firmly imbedded. Flow pattern w/o cutting or deposition. Stable bed.	3	Some present causing erosive cross currents and minor pool filling. Obstructions fewer and less firm.	4	Moderately frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	6	Frequent obstructions and deflectors cause bank erosion yearlong. Sediment traps full, channel migration occurring.	8																											
	8	Cutting	Little or none. Infrequent raw banks <6".	4	Some, intermittently at outcrops and constrictions. Raw banks may be up to 12".	5	Significant. Cuts 12–24" high. Root mat overhangs and sloughing evident.	12	Almost continuous cuts, some over 24" high. Failure of overhangs frequent.	16																											
	9	Deposition	Little or no enlargement of channel or point bars.	4	Some new bar increase, mostly from coarse gravel.	6	Moderate deposition of new gravel and coarse sand on old and some new bars.	12	Extensive deposit of predominantly fine particles. Accelerated bar development.	16																											
Bottom	10	Rock angularity	Sharp edges and corners. Plane surfaces rough.	1	Rounded corners and edges. Surfaces smooth and flat.	2	Corners and edges well rounded in 2 dimensions.	3	Well rounded in all dimensions, surfaces smooth.	4																											
	11	Brightness	Surfaces dull, dark or stained. Generally not bright.	1	Mostly dull, but may have <35% bright surfaces.	2	Mixture dull and bright, i.e., 35–65% mixture range.	3	Predominantly bright, > 65%, exposed or scoured surfaces.	4																											
	12	Consolidation of particles	Assorted sizes tightly packed or overlapping.	2	Moderately packed with some overlapping.	4	Mostly loose assortment with no apparent overlap.	5	No packing evident. Loose assortment, easily moved.	8																											
	13	Bottom size distribution	No size change evident. Stable material 80–100%.	4	Distribution shift light. Stable material 50–80%.	6	Moderate change in sizes. Stable materials 20–50%.	12	Marked distribution change. Stable materials 0–20%.	16																											
	14	Scouring and deposition	<5% of bottom affected by scour or deposition.	8	5–30% affected. Scour at constrictions and where grades steepen. Some deposition in pools.	12	30–50% affected. Deposits and scour at obstructions, constrictions and bends. Some filling of pools.	18	More than 50% of the bottom in a state of flux or change nearly yearlong.	24																											
	15	Aquatic vegetation	Abundant growth moss-like, dark green perennial. In swift water too.	1	Common. Algae forms in low velocity and pool areas. Moss here too.	2	Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick.	3	Perennial types scarce or absent. Yellow-green, short-term bloom may be present.	4																											
			<b>Excellent total = 22</b>				<b>Good total = 21</b>				<b>Fair total = 5</b>																										
												<b>Poor total = 12</b>																									
Stream type		A1	A2	A3	A4	A5	A6	B1	B2	B3	B4	B5	B6	C1	C2	C3	C4	C5	C6	D3	D4	D5	D6	Grand total = 60													
Good (Stable)		38-43	38-43	54-90	60-95	60-95	50-80	38-45	38-45	38-45	40-60	40-64	49-68	40-60	38-50	38-50	60-85	70-90	60-85	85-107	85-107	85-107	85-107	85-107	85-107	67-98											
Fair (Mod. unstable)		44-47	44-47	91-129	96-132	96-142	81-110	46-58	46-58	61-78	65-84	69-88	61-78	51-61	51-61	51-61	86-105	91-110	86-105	108-132	108-132	108-132	108-132	108-132	108-132	99-125											
Poor (Unstable)		48+	48+	130+	133+	143+	111+	59+	59+	79+	85+	89+	79+	62+	62+	106+	111+	111+	106+	133+	133+	133+	133+	133+	126+												
Stream type		DA3	DA4	DA5	DA6	E3	E4	E5	E6	F1	F2	F3	F4	F5	F6	G1	G2	G3	G4	G5	G6																
Good (Stable)		40-63	40-63	40-63	40-63	50-75	50-75	50-75	40-63	40-63	60-85	60-85	85-110	85-110	90-115	80-95	40-60	40-60	85-107	85-107	90-112	85-107															
Fair (Mod. unstable)		64-86	64-86	64-86	64-86	76-96	76-96	76-96	64-86	64-86	86-105	111-125	111-125	116-130	96-110	61-78	61-78	108-120	108-120	113-125	108-120																
Poor (Unstable)		87+	87+	87+	87+	97+	97+	97+	87+	106+	106+	126+	126+	131+	111+	79+	79+	121+	121+	126+	121+	126+	121+	126+													
																								<b>Excellent total = 22</b>				<b>Good total = 21</b>				<b>Fair total = 5</b>			<b>Poor total = 12</b>		
																								Grand total = 60		Existing stream type = E4		Potential stream type = E4		Modified channel stability rating = Good							

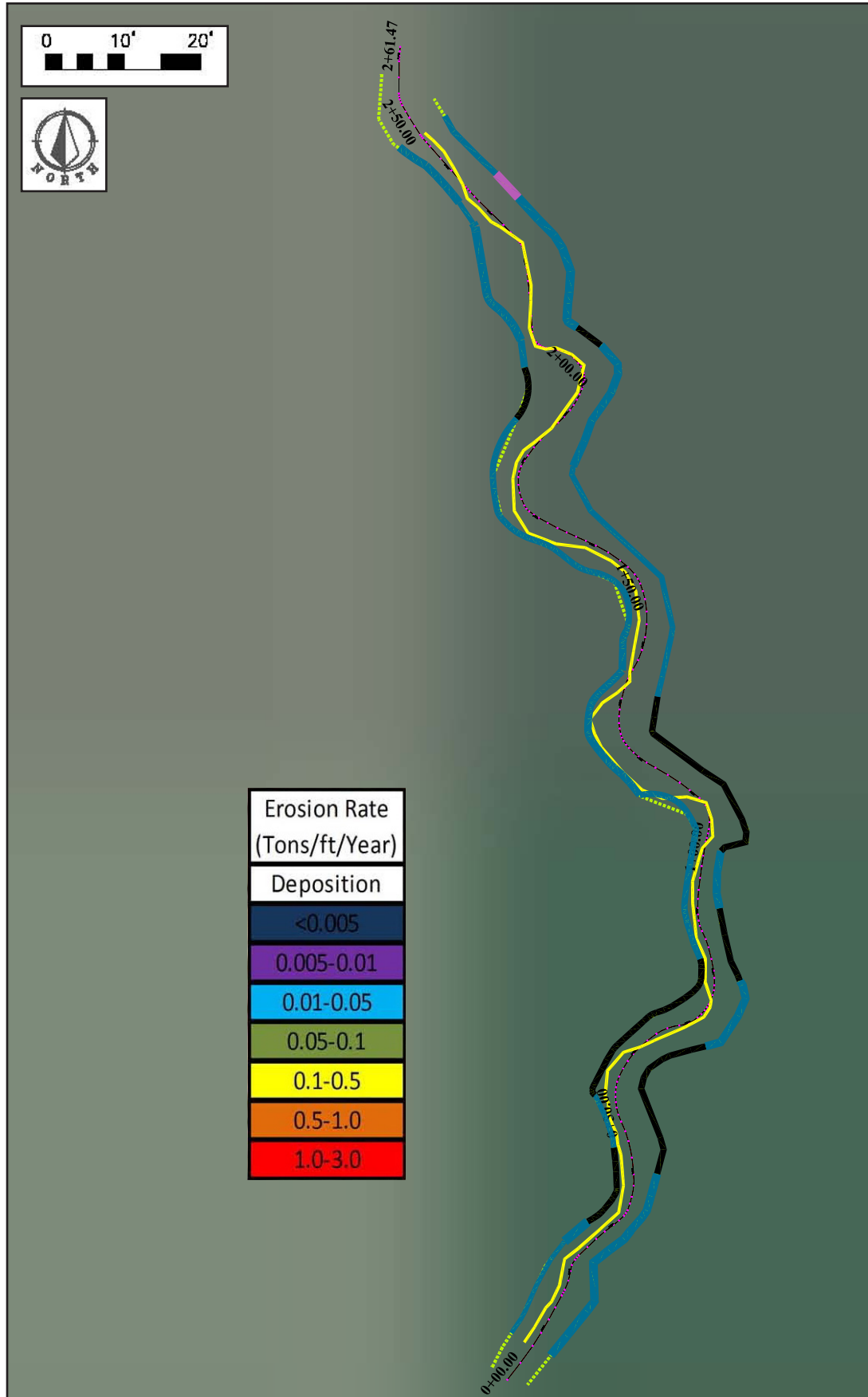
\*Rating is adjusted to potential stream type, not existing.

## BANCS Model – Streambank Erosion

**Worksheet 5-18.** Annual streambank erosion estimates.

Stream: <b>Trail Creek, E4 Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>					
Graph Used: <b>Colorado</b>		Total Stream Length (ft): <b>250</b>			Date: <b>8/22/2010</b>		
Observers: <b>K. Wright &amp; B. Kasun</b>		Valley Type: <b>X</b>			Stream Type: <b>E4</b>		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Station (ft)	BEHI rating (Worksheet 5-16) (adjective)	NBS rating (Worksheet 5-17) (adjective)	Bank erosion rate (Figure 5-34 or 5- 35) (ft/yr)	Length of bank (ft)	Study bank height (ft)	Erosion subtotal [(4)×(5)×(6)] (ft <sup>3</sup> /yr)	Erosion Rate {[(7)/27] × 1.3 / (5)}
0+00 to 0+18 1. Left Bank	Low	Low	0.03566	16.0	0.8	0.43	0.00129
0+00 to 0+27 2. Right Bank	Very Low	Very Low	0.00164	27.0	1.4	0.06	0.00011
0+18 to 0+23 3. Left Bank	Very Low	High	0.02130	5.0	1.5	0.16	0.00154
0+27 to 0+39 4. Right Bank	Very Low	High	0.02130	12.0	1.3	0.33	0.00133
0+41 to 0+52 5. Left Bank	Very Low	Low	0.00386	11.0	0.8	0.03	0.00015
0+56 to 0+71 6. Right Bank	Very Low	High	0.02130	15.0	1.3	0.42	0.00133
0+81 to 1+09 7. Right Bank	Low	Low	0.03566	28.0	1.0	1.00	0.00172
0+85 to 0+99 8. Right Bank	Low	Low	0.03566	14.0	1.3	0.65	0.00223
1+09 to 1+28 9. Left Bank	Very Low	Moderate	0.00907	18.0	1.2	0.20	0.00052
1+24 to 1+68 10. Right Bank	Very Low	Low	0.00386	44.0	0.9	0.15	0.00017
1+28 to 1+70 11. Left Bank	Very Low	Low	0.00386	42.0	1.0	0.16	0.00019
1+70 to 1+88 12. Left Bank	Very Low	Low	0.00386	18.0	0.9	0.06	0.00017
1+80 to 1+88 13. Right Bank	Low	Moderate	0.07435	8.0	1.3	0.77	0.00465
1+98 to 2+02 14. Right Bank	Low	Low	0.03566	4.0	0.7	0.10	0.00120
1+88 to 1+94 15. Left Bank	Low	Moderate	0.07435	6.0	1.1	0.49	0.00394
1+94 to 2+19 16. Left Bank	Very Low	Low	0.00386	23.0	1.4	0.12	0.00026
2+02 to 2+23 17. Right Bank	Low	Low	0.03566	21.0	1.1	0.82	0.00189
2+23 to 2+29 18. Right Bank	Low	High	0.15505	6.0	1.4	1.30	0.01045
2+29 to 2+50 19. Right Bank	Very Low	Low	0.00386	21.0	1.0	0.08	0.00019
2+19 to 2+28 20. Left Bank	Very Low	Very Low	0.00164	9.0	0.8	0.01	0.00006
2+28 to 2+41 21. Left Bank	Low	Moderate	0.07435	13.0	1.3	1.26	0.00465
2+41 to 2+50 22. Left Bank	Very Low	Low	0.00386	9.0	1.1	0.04	0.00020
Sum erosion subtotals in Column (7) for each BEHI/NBS combination					Total Erosion (ft <sup>3</sup> /yr)	<b>8.65</b>	
Convert erosion in ft <sup>3</sup> /yr to yds <sup>3</sup> /yr {divide Total Erosion (ft <sup>3</sup> /yr) by 27}					Total Erosion (yds <sup>3</sup> /yr)	<b>0.32</b>	
Convert erosion in yds <sup>3</sup> /yr to tons/yr {multiply Total Erosion (yds <sup>3</sup> /yr) by 1.3}					Total Erosion (tons/yr)	<b>0.42</b>	
Calculate erosion per unit length of channel {divide Total Erosion (tons/yr) by total length of stream (ft) surveyed}					Total Erosion (tons/yr/ft)	<b>0.0017</b>	

Streambank Erosion Map



## FLOWSED Model – Total Annual Sediment Yield

**Worksheet 19a.** Total annual sediment yield prediction for the pre-fire condition using the FLOWSED model.

Equation Type		Equation Source			Equation		Bankfull Discharge (cfs)			Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)		
1. Bedload Sediment		"Good/Fair" Pagosa			$Y = -0.0113 + 1.0139X^{2.1929}$		18			0.014898355		17.37654682		
2. Suspended Sediment		"Good/Fair" Pagosa			$Y = 0.06336 + 0.9326X^{2.4085}$									
From Dimensional Flow-Duration Curve														
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Percentage of Time	Daily Mean Discharge (cfs)	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Suspended Sediment Discharge	Suspended Sediment Discharge	Dimensionless Bedload Discharge	Bedload Sediment Discharge	Time Adjusted Streamflow [(5)×(6)]	Suspended Sediment [(5)×(9)]	Bedload Sediment [(5)×(11)]	Suspended + Bedload Sediment [(13)×(14)]
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>bed</sub> )	(S/S <sub>bed</sub> )	(tons/day)	(b <sub>y</sub> /b <sub>bed</sub> )	(tons/day)	(cfs)	(tons)	(tons)	(tons)
0%	45.8													
0.10%	39.3	0.05%	0.09%	0.34	42.5	2.363	7.461	14.89	6.670	9.47	14.6	5.11	3.25	8.36
0.25%	34.0	0.08%	0.15%	0.55	36.6	2.036	5.232	8.99	4.809	6.83	20.1	4.92	3.74	8.66
0.50%	29.4	0.13%	0.25%	0.91	31.7	1.761	3.706	5.51	3.494	4.96	28.9	5.03	4.53	9.55
0.75%	25.1	0.13%	0.25%	0.91	27.2	1.513	2.592	3.31	2.502	3.55	24.8	3.02	3.24	6.26
1%	21.7	0.13%	0.25%	0.91	23.4	1.300	1.817	1.99	1.790	2.54	21.3	1.82	2.32	4.14
1.5%	18.6	0.25%	0.50%	1.83	20.2	1.120	1.289	1.22	1.289	1.83	36.8	2.23	3.34	5.56
2%	15.5	0.25%	0.50%	1.83	17.1	0.949	0.886	0.71	0.893	1.27	31.2	1.30	2.31	3.61
3%	13.1	0.50%	1.00%	3.65	14.3	0.795	0.600	0.40	0.602	0.85	52.2	1.47	3.12	4.59
4%	11.2	0.50%	1.00%	3.65	12.1	0.674	0.424	0.24	0.415	0.59	44.3	0.88	2.15	3.03
5%	10.0	0.50%	1.00%	3.65	10.6	0.587	0.322	0.16	0.304	0.43	38.6	0.58	1.57	2.16
10%	6.3	2.50%	5.00%	18.25	8.1	0.450	0.200	0.08	0.165	0.23	147.9	1.39	4.27	5.66
20%	3.4	5.00%	10.00%	36.50	4.8	0.269	0.103	0.02	0.045	0.06	176.4	0.85	2.35	3.20
30%	2.3	5.00%	10.00%	36.50	2.8	0.158	0.075	0.01	0.006	0.01	103.8	0.36	0.33	0.70
40%	1.6	5.00%	10.00%	36.50	1.9	0.108	0.068	0.01	0.000	0.00	70.9	0.23	0.00	0.23
50%	1.2	5.00%	10.00%	36.50	1.4	0.079	0.066	0.00	0.000	0.00	51.9	0.16	0.00	0.16
60%	0.9	5.00%	10.00%	36.50	1.1	0.061	0.065	0.00	0.000	0.00	39.8	0.12	0.00	0.12
70%	0.8	5.00%	10.00%	36.50	0.9	0.047	0.064	0.00	0.000	0.00	31.1	0.09	0.00	0.09
80%	0.7	5.00%	10.00%	36.50	0.7	0.039	0.064	0.00	0.000	0.00	25.9	0.08	0.00	0.08
90%	0.5	5.00%	10.00%	36.50	0.6	0.032	0.064	0.00	0.000	0.00	20.8	0.06	0.00	0.06
100%	0.1	5.00%	10.00%	36.50	0.3	0.016	0.064	0.00	0.000	0.00	10.4	0.03	0.00	0.03
<b>Annual Totals:</b>							991.7 (cfs)		29.7 (tons/yr)		36.5 (tons/yr)		66.3 (tons/yr)	
							1,966.9 (acre-ft)							

**Worksheet 19b.** Total annual sediment yield prediction for the post-fire condition using the FLOWSED model.

Equation Type		Equation Source			Equation		Bankfull Discharge (cfs)			Bankfull Bedload Sediment (kg/s)		Bankfull Suspended Sediment (mg/l)		
1. Bedload Sediment		"Good/Fair" Pagosa			$y = -0.0113x + 1.0139x^{2.1929}$		18			0.014898355		17.37654682		
2. Suspended Sediment		"Good/Fair" Pagosa			$y = 0.06336 + 0.9326x^{2.4085}$									
From Dimensional Flow-Duration Curve														
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
Percentage of Time	Daily Mean Discharge	Mid-Ordinate	Time Increment (percent)	Time Increment (days)	Mid-Ordinate Streamflow	Dimensionless Streamflow	Dimensionless Suspended Sediment Discharge	Suspended Sediment Discharge	Dimensionless Bedload Discharge	Bedload Discharge	Time Adjusted Streamflow [(5)×(6)]	Suspended Sediment [(5)×(9)]	Bedload Sediment [(5)×(11)]	Suspended Sediment + Bedload Sediment [(13)+(14)]
(%)	(cfs)	(%)	(%)	(days)	(cfs)	(Q/Q <sub>bed</sub> )	(S/S <sub>bed</sub> )	(tons/day)	(b <sub>y</sub> /b <sub>bed</sub> )	(tons/day)	(cfs)	(tons)	(tons)	(tons)
0%	62.5													
0.10%	56.0	0.05%	0.09%	0.34	59.2	3.290	16.487	45.81	13.801	19.59	20.3	15.72	6.72	22.44
0.25%	50.7	0.08%	0.15%	0.55	53.3	2.963	12.829	32.11	10.969	15.57	29.2	17.58	8.52	26.10
0.50%	46.1	0.13%	0.25%	0.91	48.4	2.688	10.157	23.06	8.855	12.57	44.2	21.04	11.47	32.51
0.75%	41.8	0.13%	0.25%	0.91	43.9	2.440	8.061	16.61	7.162	10.16	40.1	15.16	9.28	24.44
1%	38.4	0.13%	0.25%	0.91	40.1	2.227	6.480	12.19	5.859	8.32	36.6	11.12	7.59	18.71
1.5%	35.1	0.25%	0.50%	1.83	36.7	2.041	5.264	9.07	4.836	6.86	67.1	16.56	12.53	29.09
2%	31.8	0.25%	0.50%	1.83	33.4	1.857	4.204	6.59	3.928	5.58	61.0	12.03	10.18	22.21
3%	29.3	0.50%	1.00%	3.65	30.5	1.696	3.394	4.86	3.219	4.57	111.5	17.75	16.68	34.43
4%	26.1	0.50%	1.00%	3.65	27.7	1.539	2.696	3.50	2.597	3.69	101.1	12.79	13.45	26.24
5%	23.1	0.50%	1.00%	3.65	24.6	1.365	2.038	2.35	1.995	2.83	89.7	8.57	10.34	18.91
10%	14.4	2.50%	5.00%	18.25	18.7	1.040	1.088	0.96	1.093	1.55	341.5	17.43	28.31	45.74
20%	4.8	5.00%	10.00%	36.50	9.6	0.533	0.269	0.12	0.244	0.35	350.3	4.41	12.64	17.05
30%	2.4	5.00%	10.00%	36.50	3.6	0.200	0.083	0.01	0.018	0.03	131.3	0.51	0.95	1.46
40%	1.6	5.00%	10.00%	36.50	2.0	0.111	0.068	0.01	0.000	0.00	72.6	0.23	0.00	0.23
50%	1.2	5.00%	10.00%	36.50	1.4	0.079	0.066	0.00	0.000	0.00	51.9	0.16	0.00	0.16
60%	0.9	5.00%	10.00%	36.50	1.1	0.061	0.065	0.00	0.000	0.00	39.8	0.12	0.00	0.12
70%	0.8	5.00%	10.00%	36.50	0.9	0.047	0.064	0.00	0.000	0.00	31.1	0.09	0.00	0.09
80%	0.7	5.00%	10.00%	36.50	0.7	0.039	0.064	0.00	0.000	0.00	25.9	0.08	0.00	0.08
90%	0.5	5.00%	10.00%	36.50	0.6	0.032	0.064	0.00	0.000	0.00	20.8	0.06	0.00	0.06
100%	0.1	5.00%	10.00%	36.50	0.3	0.016	0.064	0.00	0.000	0.00	10.4	0.03	0.00	0.03
<b>Annual Totals:</b>											1,676.3 (cfs)	171.5 (tons/yr)	148.7 (tons/yr)	320.1 (tons/yr)
											3,324.9 (acre-ft)			

## Sediment Competence/Entrainment

**Worksheet 5-22.** Sediment competence calculations.

Stream: <b>Trail Creek, E4 Reference Reach</b>		Stream Type: <b>E4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>X</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/22/2010</b>			
<b>Enter Required Information for Existing Condition</b>					
4.3	$D_{50}$	Riffle bed material $D_{50}$ (mm)			
5.5	$\hat{D}_{50}$	Bar sample $D_{50}$ (mm)			
0.10	$D_{max}$	Largest particle from bar sample (ft)	30	(mm)	304.8 mm/ft
0.01012	$S$	Existing bankfull water surface slope (ft/ft)			
0.73	$d$	Existing bankfull mean depth (ft)			
1.65	$\gamma_s - 1$	Immersed specific gravity of sediment			
<b>Select the Appropriate Equation and Calculate Critical Dimensionless Shear Stress</b>					
0.79	$D_{50}/\hat{D}_{50}$	Range: 3 – 7	Use EQUATION 1: $\tau^* = 0.0834 ( D_{50}/\hat{D}_{50} )^{-0.872}$		
6.96	$D_{max}/D_{50}$	Range: 1.3 – 3.0	Use EQUATION 2: $\tau^* = 0.0384 ( D_{max}/D_{50} )^{-0.887}$		
N/A	$\tau^*$	Bankfull Dimensionless Shear Stress	EQUATION USED:		
<b>Calculate Bankfull Mean Depth Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	$d$	Required bankfull mean depth (ft)	$d = \frac{\tau^*(\gamma_s - 1)D_{max}}{S}$ (use $D_{max}$ in ft)		
<b>Calculate Bankfull Water Surface Slope Required for Entrainment of Largest Particle in Bar Sample</b>					
N/A	$S$	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau^*(\gamma_s - 1)D_{max}}{d}$ (use $D_{max}$ in ft)		
Check: <input type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					
<b>Sediment Competence Using Dimensional Shear Stress</b>					
0.461	Bankfull shear stress $\tau = \gamma d S$ (lbs/ft <sup>2</sup> ) (substitute hydraulic radius, R, with mean depth, d ) $\gamma = 62.4$ , d = existing depth, S = existing slope				
Shields 32	CO 62	Predicted largest moveable particle size (mm) at bankfull shear stress $\tau$ (Figure 5-49)			
Shields 0.44	CO 0.12	Predicted shear stress required to initiate movement of measured $D_{max}$ (mm) (Figure 5-49)			
Shields 0.70	CO 0.19	Predicted mean depth required to initiate movement of measured $D_{max}$ (mm) $\tau =$ predicted shear stress, $\gamma = 62.4$ , S = existing slope	$d = \frac{\tau}{\gamma S}$		
Shields 0.0097	CO 0.0026	Predicted slope required to initiate movement of measured $D_{max}$ (mm) $\tau =$ predicted shear stress, $\gamma = 62.4$ , d = existing depth	$S = \frac{\tau}{\gamma d}$		
Check: <input checked="" type="checkbox"/> Stable <input type="checkbox"/> Aggrading <input type="checkbox"/> Degrading					



## Channel Stability Ratings

**Worksheet 5-24.** Successional stage shifts.

Stream: <b>Trail Creek, E4 Reference</b>		Stream Type: <b>E4</b>
Location: <b>Pike National Forest, CO</b>		Valley Type: <b>X</b>
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/22/2010</b>
<b>Stream Type Changes Due to Successional Stage Shifts (Figure 5-52)</b>	<b>Stability Rating (Check Appropriate Rating)</b>	
<b>Stream Type at potential, (C→E), (F<sub>b</sub>→B), (G→B), (F→B<sub>c</sub>), (F→C), (D→C)</b>	<input checked="" type="checkbox"/> Stable	
(E→C), (C→High W/d C)	<input type="checkbox"/> Moderately Unstable	
(G→F), (F→D), (C→F)	<input type="checkbox"/> Unstable	
(C→D), (B→G), (D→G), (C→G), (E→G)	<input type="checkbox"/> Highly Unstable	

**Worksheet 5-25.** Lateral stability.

Stream: <b>Trail Creek, E4 Reference Reach</b>		Stream Type: <b>E4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>X</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/22/2010</b>			
Lateral stability criteria (choose one stability category for each criterion 1-5)	Lateral Stability Categories				Selected Points (from each row)
	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	
1 <b>W/d Ratio State</b> (Worksheet 5-13)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	2
	1.0 (2)	(4)	(6)	(8)	
2 <b>Depositional Patterns</b> (Worksheet 5-10)	B1, B2	B4, B8	B3	B5, B6, B7	1
	B2 (1)	(2)	(3)	(4)	
3 <b>Meander Patterns</b> (Worksheet 5-9)	M1, M3, M4		M2, M5, M6, M7, M8		1
	M3 (1)		(3)		
4 <b>Dominant BEHI / NBS</b> (Worksheet 5-18)	L/VL, L/L, L/M, L/H, L/VH, M/VL	M/L, M/M, M/H, L/Ex, H/L	M/VH, M/Ex, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	2
	VL/L (2)	(4)	(6)	(8)	
5 <b>Degree of Confinement</b> (MWR / MWR <sub>ref</sub> ) (Worksheet 5-14)	0.8 – 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	1
	1.0 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>7</b>
<b>Lateral Stability Category Point Range</b>					
<b>Overall Lateral Stability Category</b> (use total points and check stability rating)	<i>Stable</i> 7 – 9 <input checked="" type="checkbox"/>	<i>Moderately Unstable</i> 10 – 12 <input type="checkbox"/>	<i>Unstable</i> 13 – 21 <input type="checkbox"/>	<i>Highly Unstable</i> > 21 <input type="checkbox"/>	

**Worksheet 5-26.** Vertical stability – aggradation.

Stream: <b>Trail Creek, E4 Reference Reach</b>		Stream Type: <b>E4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>X</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/22/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–6)	Vertical Stability Categories for Excess Deposition / Aggradation				Selected Points (from each row)
	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	
1 <b>Sediment Competence</b> (Worksheet 5-22)	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope—slightly incompetent	Cannot move D <sub>35</sub> of bed material and/or D <sub>100</sub> of bar material	Cannot move D <sub>16</sub> of bed material and/or D <sub>100</sub> of bar or sub-pavement size	2
	(2)	(4)	(6)	(8)	
2 <b>Sediment Capacity (POWERSED)</b> (Worksheet 5-20)	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended sand	Reduction over 25% of annual sediment yield for bedload and/or suspended sand	2
	Ref. Reach (2)	(4)	(6)	(8)	
3 <b>W/d Ratio State</b> (Worksheet 5-13)	1.0 – 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	2
	1.0 (2)	(4)	(6)	(8)	
4 <b>Stream Succession States</b> (Worksheet 5-24)	Current stream type at potential or does not indicate deposition/aggradation	(E→C)	(C→High W/d C), (B→High W/d B), (C→F)	(C→D), (F→D)	2
	at potential (2)	(4)	(6)	(8)	
5 <b>Depositional Patterns</b> (Worksheet 5-10)	B1	B2, B4	B3, B5	B6, B7, B8	2
	(1)	B2 (2)	(3)	(4)	
6 <b>Debris / Blockages</b> (Worksheet 5-11)	D1, D2, D3	D4, D7	D5, D8	D6, D9, D10	1
	D1 (1)	(2)	(3)	(4)	
<b>Total Points</b>					<b>11</b>
<b>Vertical Stability Category Point Range for Excess Deposition / Aggradation</b>					
<b>Vertical Stability for Excess Deposition / Aggradation</b> (use total points and check stability rating)	<i>No Deposition</i> 10 – 14 <input checked="" type="checkbox"/>	<i>Moderate Deposition</i> 15 – 20 <input type="checkbox"/>	<i>Excess Deposition</i> 21 – 30 <input type="checkbox"/>	<i>Aggradation</i> > 30 <input type="checkbox"/>	

**Worksheet 5-27.** Vertical stability – degradation.

Stream: <b>Trail Creek, E4 Reference Reach</b>		Stream Type: <b>E4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>X</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/22/2010</b>			
Vertical Stability Criteria (choose one stability category for each criterion 1–5)	Vertical Stability Categories for Channel Incision / Degradation				Selected Points (from each row)
	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	
<b>1 Sediment Competence (Worksheet 5-22)</b>	Does not indicate excess competence <b>(2)</b>	Trend to move larger sizes than $D_{100}$ of bar or $> D_{84}$ of bed <b>(4)</b>	$D_{100}$ of bed moved <b>(6)</b>	Particles much larger than $D_{100}$ of bed moved <b>(8)</b>	<b>2</b>
<b>2 Sediment Capacity (POWERSED) (Worksheet 5-20)</b>	Does not indicate excess capacity <b>Ref. Reach (2)</b>	Slight excess energy: up to 10% increase above reference <b>(4)</b>	Excess energy sufficient to increase load up to 50% of annual load <b>(6)</b>	Excess energy transporting more than 50% of annual load <b>(8)</b>	<b>2</b>
<b>3 Degree of Channel Incision (BHR) (Worksheet 5-12)</b>	1.00 – 1.10 <b>1.00 (2)</b>	1.11 – 1.30 <b>(4)</b>	1.31 – 1.50 <b>(6)</b>	$> 1.50$ <b>(8)</b>	<b>2</b>
<b>4 Stream Succession States (Worksheets 5-12 and 5-24)</b>	Does not indicate incision or degradation <b>at potential (2)</b>	If BHR $> 1.1$ and stream type has W/d between 5–10 <b>(4)</b>	If BHR $> 1.1$ and stream type has W/d less than 5 <b>(6)</b>	(B→G), (C→G), (E→G), (D→G) <b>(8)</b>	<b>2</b>
<b>5 Confinement (MWR / MWR<sub>ref</sub>) (Worksheet 5-14)</b>	0.80 – 1.00 <b>1.00 (1)</b>	0.30 – 0.79 <b>(2)</b>	0.10 – 0.29 <b>(3)</b>	$< 0.10$ <b>(4)</b>	<b>1</b>
<b>Total Points</b>					<b>9</b>
<b>Vertical Stability Category Point Range for Channel Incision / Degradation</b>					
<b>Vertical Stability for Channel Incision/ Degradation (use total points and check stability rating)</b>	<i>Not Incised</i> 9 – 11 <input checked="" type="checkbox"/>	<i>Slightly Incised</i> 12 – 18 <input type="checkbox"/>	<i>Moderately Incised</i> 19 – 27 <input type="checkbox"/>	<i>Degradation</i> $> 27$ <input type="checkbox"/>	

Worksheet 5-28. Channel enlargement.

Stream: <b>Trail Creek, E4 Reference Reach</b>		Stream Type: <b>E4</b>			
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>X</b>			
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/22/2010</b>			
Channel Enlargement Prediction Criteria (choose one stability category for each criterion 1-4)	Channel Enlargement Prediction Categories				Selected Points (from each row)
	<i>No Increase</i>	<i>Slight Increase</i>	<i>Moderate Increase</i>	<i>Extensive</i>	
1 <b>Successional Stage Shift (Worksheet 5-24)</b>	Stream Type at Potential, (C→E), (F <sub>b</sub> →B), (G→B), (F→B <sub>c</sub> ), (F→C), (D→C)	(C→High W/d C), (E→C)	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	2
	at potential (2)	(4)	(6)	(8)	
2 <b>Lateral Stability (Worksheet 5-25)</b>	<i>Stable</i>	<i>Moderately Unstable</i>	<i>Unstable</i>	<i>Highly Unstable</i>	2
	(2)	(4)	(6)	(8)	
3 <b>Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)</b>	<i>No Deposition</i>	<i>Moderate Deposition</i>	<i>Excess Deposition</i>	<i>Aggradation</i>	2
	(2)	3	(6)	(8)	
4 <b>Vertical Stability Channel Incision or Degradation (Worksheet 5-27)</b>	<i>Not Incised</i>	<i>Slightly Incised</i>	<i>Moderately Incised</i>	<i>Degradation</i>	2
	(2)	(4)	(6)	(8)	
<b>Total Points</b>					<b>8</b>
<b>Category Point Range</b>					
<b>Channel Enlargement Prediction (use total points and check stability rating)</b>	<i>No Increase</i> 8 – 10 <input checked="" type="checkbox"/>	<i>Slight Increase</i> 11 – 16 <input type="checkbox"/>	<i>Moderate Increase</i> 17 – 24 <input type="checkbox"/>	<i>Extensive</i> > 24 <input type="checkbox"/>	

Worksheet 5-29. Overall sediment supply.

Stream: <b>Trail Creek, E4 Reference Reach</b>		Stream Type: <b>E4</b>		
Location: <b>Pike National Forest, Colorado</b>		Valley Type: <b>X</b>		
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/22/2010</b>		
Overall Sediment Supply Prediction Criteria (choose corresponding points for each criterion 1-5)	Stability Rating	Points	Selected Points	
1 Lateral Stability (Worksheet 5-25)	<i>Stable</i>	1	1	
	<i>Mod. Unstable</i>	2		
	<i>Unstable</i>	3		
	<i>Highly Unstable</i>	4		
2 Vertical Stability Excess Deposition or Aggradation (Worksheet 5-26)	<i>No Deposition</i>	1	1	
	<i>Mod. Deposition</i>	2		
	<i>Excess Deposition</i>	3		
	<i>Aggradation</i>	4		
3 Vertical Stability Channel Incision or Degradation (Worksheet 5-27)	<i>Not Incised</i>	1	1	
	<i>Slightly Incised</i>	2		
	<i>Mod. Incised</i>	3		
	<i>Degradation</i>	4		
4 Channel Enlargement Prediction (Worksheet 5-28)	<i>No Increase</i>	1	1	
	<i>Slight Increase</i>	2		
	<i>Mod. Increase</i>	3		
	<i>Extensive</i>	4		
5 Pfankuch Channel Stability (Worksheet 5-15)	<i>Good: Stable</i>	1	1	
	<i>Fair: Mod. Unstable</i>	2		
	<i>Poor: Unstable</i>	4		
<b>Total Points</b>			<b>5</b>	
<b>Category Point Range</b>				
Overall Sediment Supply Rating (use total points and check stability rating)	<b>Low</b> 5 <input checked="" type="checkbox"/>	<b>Moderate</b> 6 – 10 <input type="checkbox"/>	<b>High</b> 11 – 15 <input type="checkbox"/>	<b>Very High</b> 16 – 20 <input type="checkbox"/>

Worksheet 5-32. Summary of stability condition categories.

Stream: <b>Trail Creek, E4 Reference Reach</b>		Location: <b>Pike National Forest, Colorado</b>		Stream Type: <b>E4</b>		Valley Type: <b>X</b>	
Observers: <b>K. Wright &amp; B. Kasun</b>		Date: <b>8/22/2010</b>		Stream Type: <b>E4</b>		Valley Type: <b>X</b>	
<b>Channel Dimension (Rifle XS 2+42.5)</b>	Mean Bankfull Depth (ft): <b>0.73</b>	Bankfull Width (ft): <b>5.73</b>	Cross-Sectional Area (ft <sup>2</sup> ): <b>4.17</b>	Width of Flood-Prone Area (ft): <b>35.78</b>	Entrenchment Ratio: <b>6.24</b>		
<b>Channel Pattern</b>	Mean: $\lambda/W_{b,sk}$ : <b>5.4</b> Range: <b>4.99-6.27</b>	$L_m/W_{b,sk}$ : <b>5.09-7.27</b>	$R_c/W_{b,sk}$ : <b>3.09</b>	MWR: <b>2.76-3.80</b>	Sinuosity: <b>1.23</b>		
<b>River Profile &amp; Bed Features</b>	Check: <input checked="" type="checkbox"/> Riffle/Pool <input type="checkbox"/> Step/Pool <input type="checkbox"/> Plane Bed <input type="checkbox"/> Convergence/Divergence <input type="checkbox"/> Dunes/Antidunes/Smooth Bed	Riffle	Pool	Pool-to-Pool Ratio	Slope		
	Max Bankfull Depth (ft): <b>1.02</b>   <b>1.74</b>	Depth Ratio (max to mean): <b>1.52</b>   <b>2.6</b>	Riffle	Pool	Slope		
	Bankfull Depth (ft): <b>0.95-1.19</b>   <b>1.44-2.94</b>	Depth Ratio (max to mean): <b>1.4-1.78</b>   <b>2.15-4.39</b>	Riffle	Pool	Valley: <b>0.0124</b>	Water Surface: <b>0.0101</b>	
<b>Level III Stream Stability Indices</b>	Riparian Vegetation: <b>Willow, Carex, Conifers</b>	Current Composition/Density: <b>Same as existing</b>	Potential Composition/Density: <b>Excellent coverage - some invasives need erad.</b>	Remarks: Condition, Vigor & Usage of Existing Reach:			
<b>Bank Erosion Summary</b>	Flow Regime: <b>P1, P2, P8 &amp; Order: S-3(3)</b>	Meander Patterns: <b>M3</b>	Depositional Patterns: <b>B2</b>	Debris/Channel Blockages: <b>D1</b>	Remarks: <b>60 (Good)</b>		
<b>Sediment Capacity (POWERSED)</b>	Degree of Incision (Bank-Height Ratio): <b>1.0</b>	Degree of Incision Stability Rating: <b>Stable</b>	Modified Pfankuch Stability Rating (Numeric & Adjective Rating): <b>60 (Good)</b>				
<b>Entrainment/Competence</b>	Width/depth Ratio (W/d): <b>7.85</b>	Reference W/d Ratio (W/d <sub>ref</sub> ): <b>7.85</b>	Width/Depth Ratio State (W/d) / (W/d <sub>ref</sub> ): <b>1.0</b>	W/d Ratio State Stability Rating: <b>Stable</b>			
<b>Successional Stage Shift</b>	Meander Width Ratio (MWR): <b>3.33</b>	Reference MWR <sub>ref</sub> : <b>3.33</b>	Degree of confinement (MWR / MWR <sub>ref</sub> ): <b>1.0</b>	MWR / MWR <sub>ref</sub> Stability Rating: <b>Unconfined</b>			
<b>Lateral Stability</b>	Length of Reach Studied (ft): <b>250</b>	Annual Streambank Erosion Rate: (tons/yr) <b>0.42</b>	Curve Used: <b>Colorado</b>	Remarks: <b>Great Vegetation (Used Yellowstone Curve for VL BEHI)</b>			
<b>Vertical Stability (Aggradation)</b>	<input checked="" type="checkbox"/> Sufficient Capacity <input type="checkbox"/> Insufficient Capacity <input type="checkbox"/> Excess Capacity	Remarks: <b>Functioning as a stable, E4 Stream</b>					
<b>Vertical Stability (Degradation)</b>	Largest Particle from Bar Sample (mm): <b>30</b>	$\tau =$ <b>0.461</b>	$\tau^* =$ <b>N/A</b>	Required Depth: <b>0.73</b>	Existing Slope: <b>0.7</b>	Required Slope: <b>0.010</b>	
<b>Channel Enlargement</b>	$E \rightarrow G \rightarrow F \rightarrow C \rightarrow E$	$C \rightarrow E$	$E \rightarrow$	Existing Stream State (Type): <b>E4</b>	Potential Stream State (Type): <b>E4</b>	Remarks/causes: <b>No Change</b>	
<b>Sediment Supply (Channel Source)</b>	<input checked="" type="checkbox"/> Stable <input type="checkbox"/> Mod. Unstable <input type="checkbox"/> Unstable	<input type="checkbox"/> Ex. Deposition <input type="checkbox"/> Aggradation	<input type="checkbox"/> Mod. Incised <input type="checkbox"/> Degradation	Remarks/causes: <b>No Change</b>			
	<input checked="" type="checkbox"/> No Deposition <input type="checkbox"/> Mod. Deposition <input type="checkbox"/> Ex. Deposition	<input type="checkbox"/> Mod. Incised <input type="checkbox"/> Degradation	<input type="checkbox"/> Mod. Increase <input type="checkbox"/> Extensive	Remarks/causes: <b>No Change</b>			
	<input checked="" type="checkbox"/> Not Incised <input type="checkbox"/> Slightly Incised <input type="checkbox"/> Mod. Incised	<input type="checkbox"/> Mod. Increase <input type="checkbox"/> Extensive	<input type="checkbox"/> Very High	Remarks/causes: <b>Great Vegetation</b>			
	<input checked="" type="checkbox"/> No Increase <input type="checkbox"/> Slight Increase <input type="checkbox"/> Mod. Increase	<input type="checkbox"/> Moderate <input type="checkbox"/> High	<input type="checkbox"/> Very High	Remarks/causes: <b>Stable, Reference Reach with great Veg</b>			

